



EE-230 - 2025  
Mid - Sem Solutions

(1) Checking individual opamp of TL082.

By Making Voltage Buffer. ( $2+2 = 4M$ )

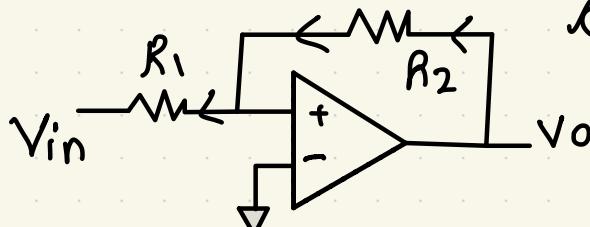
(2) (1) Analysis of Sub-circuit 1 (5M)

(i) +ve feedback (0.5M)

(ii) Non-Inverting Schmitt trigger (1M)

(iii) No Virtual ground concept is Not Applicable due to +ve feedback (0.5M)

(iv)



considering  $V_o = +V_{sat}$   
 $V_o$  for LTP calculation

$$V^+ = \frac{R_1}{R_1 + R_2} V_o + \frac{V_{in} \times R_2}{R_1 + R_2} \quad \left. \begin{array}{l} \text{for opamp to} \\ \text{Saturate to } -V_{sat} \end{array} \right\} V^+ < V^-$$

i.e.  $R_1 V_o + R_2 V_{in} < 0$

$$\boxed{V_{in} < -\frac{R_1}{R_2} V_{sat}} \quad \text{LTP}$$

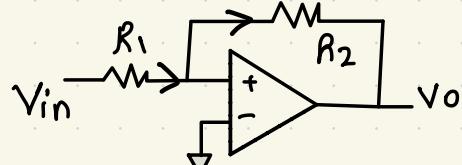
(0.5M)

For deviation  
+ correct Exp.

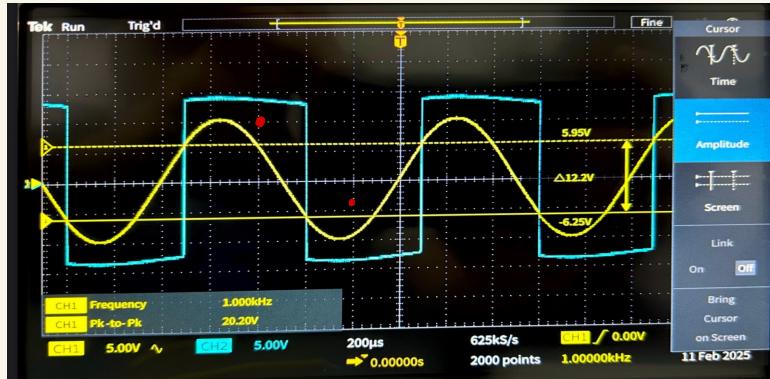
Similarly fix UTP

$$\boxed{UTP = \frac{R_1}{R_2} V_{sat}}$$

(0.5M)



(V) They Need to Show The  $V_{O1}$  &  $V_{IN}$  waveforms Simultaneously on DSO. & UTP & LTP using cursors & Verify The Theoretical & practical values.  
 $UTP \rightarrow (5.7V \text{ to } 6.8V)$

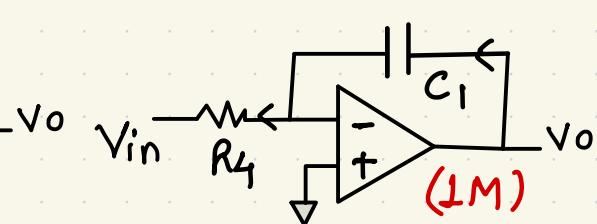
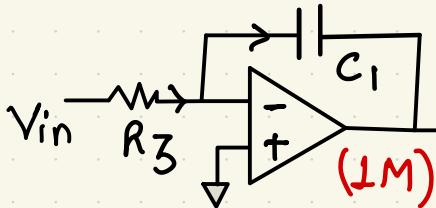


(3M)

## ② Analysis of Sub circuit 02 (5M)

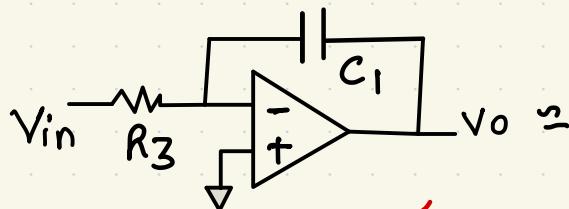
- (i) -ve feedback circuit. (0.5M)
- (ii) Integrator circuit (1M)
- (iii) Yes, As long as opamp doesn't Saturate Virtual ground concept is Applicable. (0.5M)

(IV) (i) (ii)



(iii) V<sub>out</sub> in terms of V<sub>in</sub>.

When diode D<sub>1</sub> is ON.



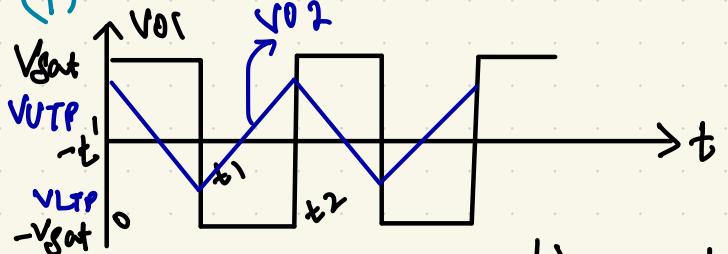
$$V_o \approx -\frac{1}{R_3 C_1} \int V_{in}(t) dt \quad \frac{1}{2} M$$

Similarly, when diode D<sub>2</sub> is ON

$$V_o = -\frac{1}{R_4 C_1} \int V_{in}(t) dt \quad \frac{1}{2} M$$

3) Analysis of overall circuit (8M)

(i)



} 2M

$$V_{o2} = -\frac{R_1}{R_2} V_{sat} + \frac{1}{R_4 C_1} \int_0^t V_{sat} dt \quad b)$$

at  $t = t$

$$\frac{R_1}{R_2} V_{sat} = -\frac{R_1}{R_2} V_{sat} + \frac{V_{sat} t_1}{R_4 C_1}$$

$$\frac{2R_1}{R_2} = \frac{t_1}{R_4 C_1} \quad \textcircled{1}$$

$\hookrightarrow (1.5M)$

Similarly

$$\frac{2R_1}{R_2} = \frac{t_2 - t_1}{R_3 C_1} \quad \textcircled{2} \quad \nearrow 1.5M$$

$t_2 = \text{Time period}$   
Solving \textcircled{1} & \textcircled{2}

$$\frac{2R_1}{R_2} (R_3 + R_4) C_1 = t_2 \quad \nearrow (1M)$$

$$f = \frac{1}{T_2} = \frac{1}{2(R_3 + R_4) C_1} \times \frac{R_2}{R_1}$$

- (iii) When  $R_3 = R_4$  then O/p will be Triangular Wave. (1M)
- (iv) The diodes  $D_1$  &  $D_2$  will change the duty cycle of Square Wave when connected in closed loop fashion. (0.5M)
- No, we can't get Sawtooth without diodes (0.5M).

Second Part: Determining component values (2M)

$$R_3 + R_4 \approx 7.33k$$

They can choose any value of  $R_3$  &  $R_4$  But

The  $R_3 + R_4 \approx 7.33k \Omega$ .

2M

Hardware Implementation (5M)

Circuit Building on Breadboard (2 M)

They will show the Sawtooth waveform & Triangular waveform ( $R_3 = R_4$ )

$$\text{Freq range: } 1.3 \text{ kHz} - 2.5 \text{ kHz}$$

Tabulation of frequency &  $V_{pp}$ . - (1M)

# Reference o/p



They will show the Sawtooth & Triangular wave on ISO. (2M)

\* Note:- Frequency expression in terms of V<sub>RP</sub> & V<sub>LTP</sub> is also considered.