

Electronic Devices and Circuits

Assignment-3(CEP)

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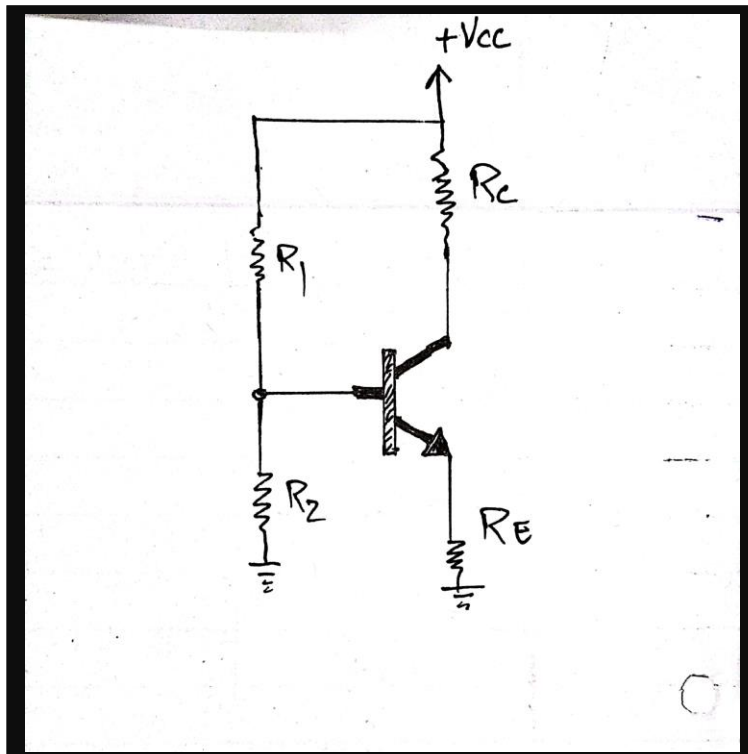
Roll number: 23L-6006 (3B)

Design and Analysis of Single-Stage BJT Amplifier.

- Open circuit voltage gain
 $A_{vo} = 5 \times (6 + 0 + 0 + 6) = 60$
- Input resistance must be greater than $40k\Omega$
 $R_{in} = (1 + \beta)(r_e + R_E) > 40k\Omega$
- The output impedance should be less than 500Ω
 $Z_{out} \approx R_C \parallel R_L < 500\Omega$

So first we do **DC Analysis**

- As a starting point, take DC operating current $I_C = 1\text{mA}$ at room temperature.
- Assume $\beta = 100$



$$R_E = \frac{V_T}{I_E} \quad (I_C \approx I_E)$$

$$R_E = \frac{26m}{1mA} = 26$$

$$V_{CC} = +15V$$

We use Assumptions

$$V_B = \frac{V_{CC}}{3} = \frac{15}{3} = 5V$$

$$I_{C(RC)} = \frac{V_{CC}}{3}$$

$$R_C = 5k\Omega$$

$$V_{BE} = V_B - V_E$$

$$V_E = 5 - 0.7 = 4.3V$$

$$V_E = I_E R_E$$

$$R_E = \frac{V_E}{I_E} = 4.3k\Omega$$

Take I_B 10% of I_E

$$I_B = 0.1mA$$

$$R_1 + R_2 = \frac{V_{CC}}{I_B} = \frac{15}{0.1mA}$$

$$R_1 + R_2 = 150k$$

Applying VDR

$$V_B = V_{CC} \times \frac{R_2}{R_1 + R_2}$$

$$(150) \frac{5}{15} = R_2$$

$$R_2 = 50k\Omega$$

$$R_1 + R_2 = 150k$$

$$R_1 = 100k\Omega$$

$$R1 \parallel R2 = 33.3k\Omega$$

$$R_{in} = (1 + \beta) (r_e + R_e) = 101 \times (26 + 4.3k) = 436.92k > 40k$$

If we take R_B parallel, then R_{in} is

$$R_{in} = R_B \parallel (1 + \beta) (r_e + R_e) = 33.3k \parallel 436.92k = 30.94k < 40k \text{ (false)}$$

- Cheak the Open circuit voltage gain

$$\begin{aligned} A_{vo} &= \frac{R_C}{r_e + R_e} \\ &= \frac{5k}{26 + 4.3k} = 1.13, \text{ Our requirements are not fulfilled} \end{aligned}$$

So, we put $A_{vo} = 60$

$$R_E = \frac{R_C}{A_{vo}} - r_e = \frac{5k}{60} - 26 = 57.33 \Omega \text{ (Take standard } 56\Omega)$$

$$\begin{aligned} A_{vo} &= \frac{R_C}{r_e + R_e} \\ &= \frac{5k}{26 + 56} = 60.97 \end{aligned}$$

Cheak R_{in}

$$R_{in} = (1 + \beta) (r_e + R_e) = 101 \times (26 + 56) = 8282$$

$$R_{in} = R_B \parallel (1 + \beta) (r_e + R_e) = 33.3k \parallel 8282 = 6232.45\Omega$$

$$g_m = \frac{I_C}{V_T} = \frac{1m}{26m} = 0.0384$$

$$r_{\pi} = \frac{\beta}{g_m} = 2.6k\Omega$$

Output Impedance, take $R_L = 450\Omega$

$$R_C \parallel R_L = \frac{R_C \times R_L}{R_C + R_L} = 5k \parallel 450 = 395.94 < 500\Omega \text{ (Condition true)}$$

$$A_v = \frac{-g_m (R_c || R_L)}{1 + g_m R_e} = 95.26 \text{ m V/V.}$$

➤ **Take $I_s = 10^{-14}$ and $V_B = 0.7\text{V}$ at room temperature**

$$I_C = I_s \times e^{V_{be}/V_t} \quad \rightarrow V_t = 26\text{m}$$

$$I_C = 4.92\text{mA}$$

$$I_{CRC} = V_{CC}/3$$

$$R_C = 345.78\Omega$$

$$\text{We take } R_C = 360\Omega$$

$$I_E \approx I_C$$

$$R_E = V_E / I_E$$

$$= \frac{4.3}{4.92\text{mA}} = 873.9\Omega$$

$$\text{We take } 810\Omega \text{ standard}$$

$$r_e = V_t / I_E = 5.284\Omega$$

$$R_{in} = (1 + \beta) (r_e + R_E) = 101 \times (5.284 + 810) = 82.3\text{k}\Omega > 40\text{k}\Omega$$

$$I_B \text{ 10\% of } I_E$$

$$I_B = 0.492\text{mA}$$

$$R_1 + R_2 = 15 / 0.492\text{mA}$$

$$R_1 + R_2 = 30.48\text{k}$$

Apply VDR

$$R_1 = 20.32\text{k}\Omega$$

$$R_2 = 10.16\text{k}\Omega$$

$$R_B = R_1 || R_2 = 6.77\text{k}\Omega$$

➔ Take RB in parallel

$$R_{in} = R_B \parallel (1 + \beta) (r_e + R_E) = 6.27k\Omega \text{ (False)}$$

➔ Take RB in the Series

$$R_{in} = \frac{R_B}{1 + \beta} + (1 + \beta) (r_e + R_E) = 82.367k\Omega > 40k\Omega$$

Consider a biasing scheme that provides thermal bias stability.

$$V_E = 2V$$

$$\text{Then } R_E = \frac{V_E}{I_E} = 406\Omega$$

->Take standard 390Ω

$$R_{in} = (1 + \beta) (r_e + R_E) = 101 \times (5.284 + 390) = 39.9k\Omega < 40k\Omega$$

->So, we improve it take 430Ω

$$R_{in} = (1 + \beta) (r_e + R_E) = 101 \times (5.284 + 430) = 43.9k\Omega > 40k\Omega$$

$$A_{vo} = \frac{R_C}{r_e + R_E}$$

$$60 = \frac{360}{5.284 + R_E}, R_E = 0.716\Omega$$

So, we adjusted Re so that our open circuit gain was equal to our requirement.

$$A_{vo} = \frac{R_C}{r_e + R_E}$$

$$= \frac{390}{5.284 + 0.716}$$

$$= \frac{390}{5.284 + 1} \quad \text{take } R_E \text{ standard } 1.0\Omega, \text{ and adjust the } R_C = 390\Omega$$

$$= 62.06$$

Check Output Impedance

$$Z_{out} = R_C \parallel R_L$$

Take $R_L = 2.2k\Omega$, $R_C = 390\Omega$

$$Z_o = \frac{R_C \times R_L}{R_C + R_L} = \frac{390 \times 2.2k}{390 + 2.2k} = 331.27 < 500\Omega$$

$$g_m = \frac{I_c}{V_t} = \frac{4.96m}{26m} = 0.1907$$

$$A_v = \frac{-g_m (R_c || R_L)}{1 + g_m R_e} = -53.055 \text{ V/V}$$

Temperature Analysis

The performance of the amplifier changes with temperature due to variations in the parameters of the BJT:

Effect on DC Parameters

1. V_{BE} :

- V_{BE} decreases at $-2\text{mV}/^\circ\text{C}$.
- At room temperature (25°C), $V_{BE} = 0.7\text{V}$.
- At 60°C : $V_{BE} = 0.7\text{V} - 2\text{mV}/^\circ\text{C} \cdot (60 - 25) = 0.63\text{V}$
- At -10°C : $V_{BE} = 0.7\text{V} + 2\text{mV}/^\circ\text{C} \cdot (25 - (-10)) = 0.76\text{V}$

2. I_C :

- $I_C = I_s \times e^{V_{be}/V_t}$
- As V_{BE} decreases, I_C increases exponentially.
- I_C approximately doubles for every 10°C rise in temperature.

3. V_{CE} :

- $V_{CE} = V_{CC} - I_C R_C$
- As I_C increases, V_{CE} decreases, reducing the available signal swing.

Effect on AC Parameters

1. r_e :

- $r_e = V_T / I_E$
- With V_T increasing linearly and I_C increasing exponentially, r_e decreases:

$$r_e \propto \frac{1}{I_c}$$

- At 25°C , $r_e = 5.284\Omega$

- At 60°C, assuming IC doubles (IC ≈ 9.84mA): $r_e = 26\text{m} / 9.84 = 2.64\Omega$

2. Open-Circuit Voltage Gain (Avo):

- $A_{vo} = \frac{R_c}{r_e + R_e}$
- At 25°C: $r_e = 5.284$, $A_{vo} = \frac{390}{5.284 + 1} = 62.06$
- At 60°C, $r_e = 2.64\Omega$, $A_{vo} = \frac{390}{2.64 + 1} = 110.57$
- The gain increases with temperature, which may lead to distortion.

3. Input Resistance (Rin):

- $R_{in} = (1 + \beta)(r_e + R_E)$
- At 25°C, $R_{in} = 43.9\text{k}\Omega$
- At 60°C, $r_e = 2.64\Omega$, $R_{in} = 101 \times (2.64\Omega + 1\Omega) = 26.56\text{k}\Omega$
- R_{in} decreases, which could cause input signal distortion.

4. Output Resistance (Rout):

- R_{out} is determined primarily by $R_C \parallel R_L$ and is less affected by temperature.

➤ Signal Swing

The signal swing is determined by the maximum VCE variation. For proper operation, VCE must remain above the saturation voltage (VCE (sat)) and below VCC.

1. Maximum VCE:

$$V_{CE}(\text{max}) = V_{CC} - I_C(\text{min}) R_C$$

- At 25°C, $I_C = 4.92\text{mA}$, $V_{CE}(\text{max}) = 15\text{V} - (4.92\text{mA} \cdot 390\Omega) = 13.08\text{V}$

2. Minimum VCE:

$$V_{CE}(\text{min}) = V_E$$

- $V_{CE}(\text{min}) = 2\text{V}$

3. Signal Swing:

$$\Delta V_{CE} = V_{CE}(\text{max}) - V_{CE}(\text{min}) = 13.08\text{V} - 2\text{V} = 11.08\text{V}$$

Using the open-circuit voltage gain $A_v = 62.06$

$V_P = 11.08 / 62.06 = 178.5\text{mV}$ this is too low, we take 300mV to achieve our requirements

➤ Conflicting Requirements and Tradeoffs

1. Voltage Gain vs. Thermal Stability:

- To achieve a gain of 60, R_E was minimized, reducing thermal stability.
- This tradeoff can be mitigated by adding a bypass capacitor across R_E , maintaining A_{vo} while improving thermal stability.

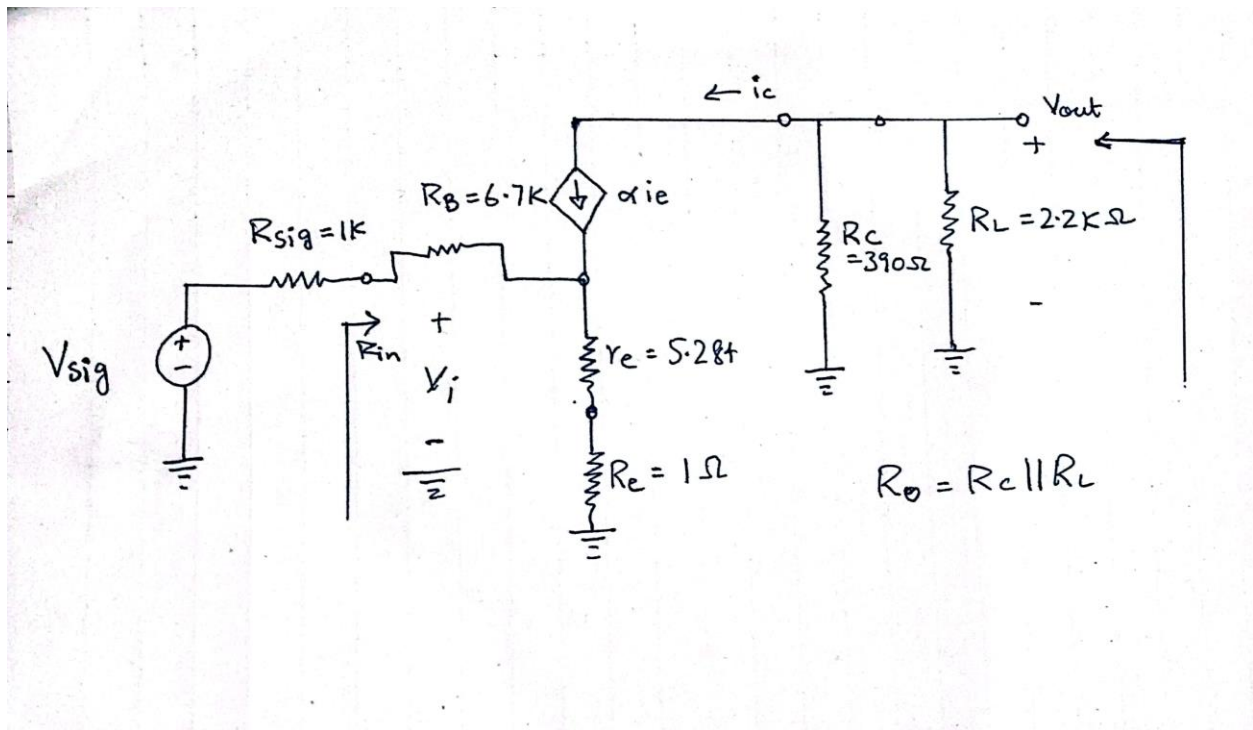
2. Input Resistance vs. Voltage Gain:

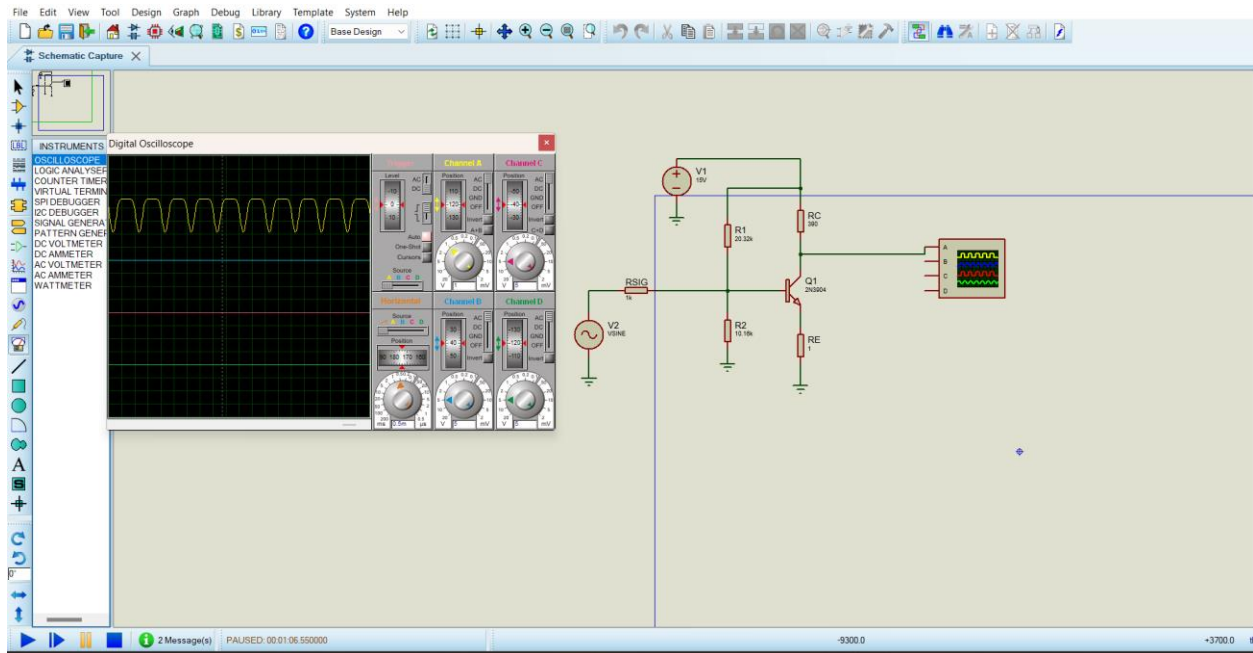
- Increasing R_E improves R_{in} but reduces A_{vo} . The chosen R_E balances both requirements.

3. Output Resistance vs. Signal Swing:

- A lower R_C reduces R_{out} but also limits signal swing. The chosen R_C provides an acceptable balance.

T – Model

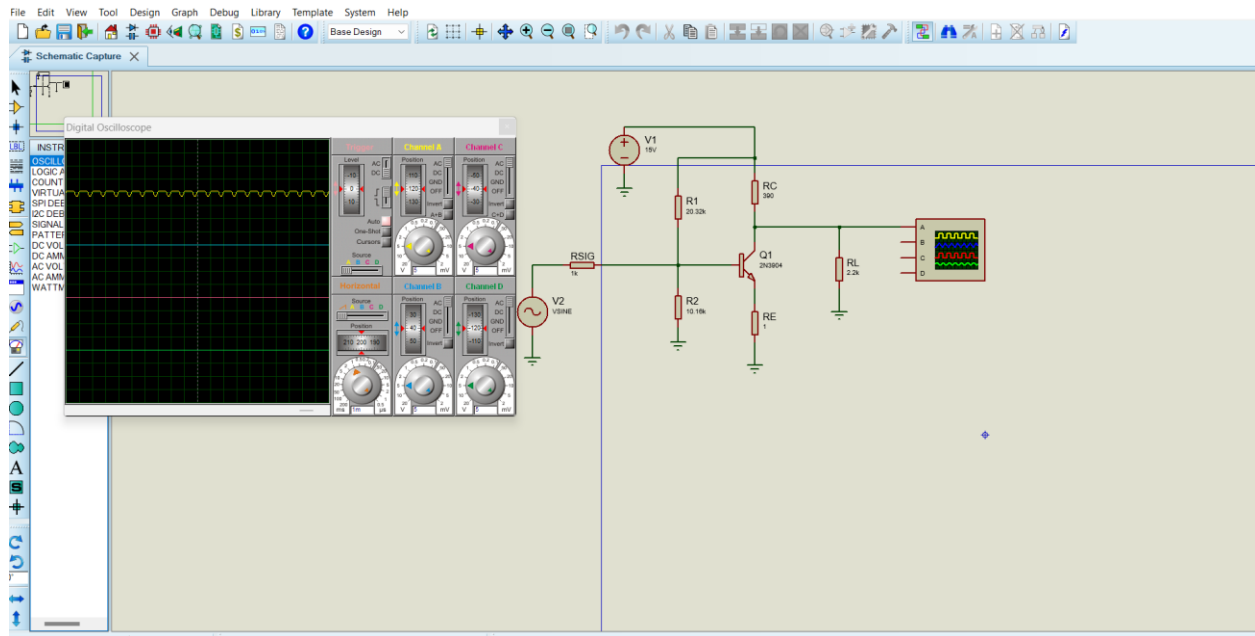




$$R_{in} = \frac{V_{in}}{V_{sig} - V_{in}} \times R_x$$

R_x is R_{SIG} we take it $1k\Omega$

$$R_{in} = \frac{300m}{306.2m - 300m} \times 1k = 48.3k > 40k\Omega$$



$$V_L = \frac{R_L}{R_o + R_L} \times V_{OUT}$$

$$R_o = \frac{V_{out} - V_L}{V_L} \times R_L$$

$$= \frac{260.3m - 300m}{260.3m} \times 2.2k$$

$$= 335.5\Omega$$

Output Impedance

$$Z_{out} \approx R_C \parallel R_L < 500\Omega$$

