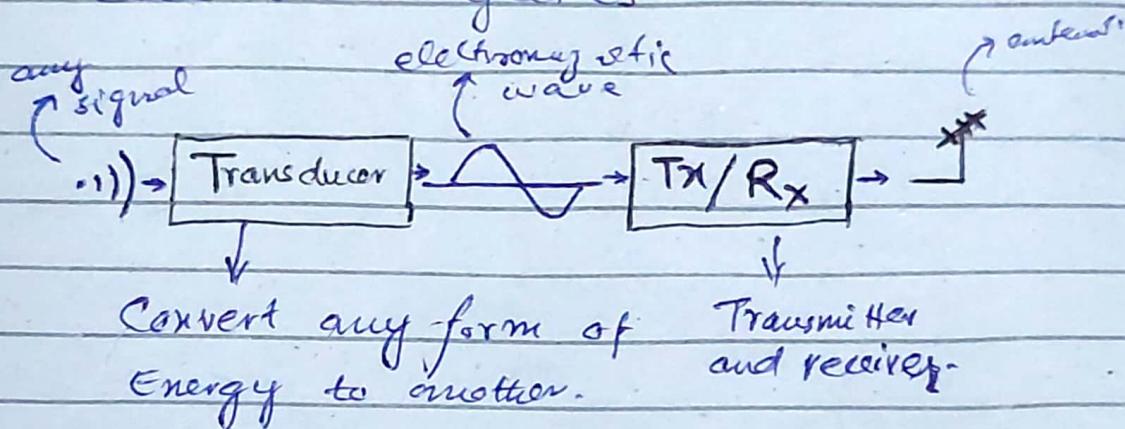


Communication System Lecture

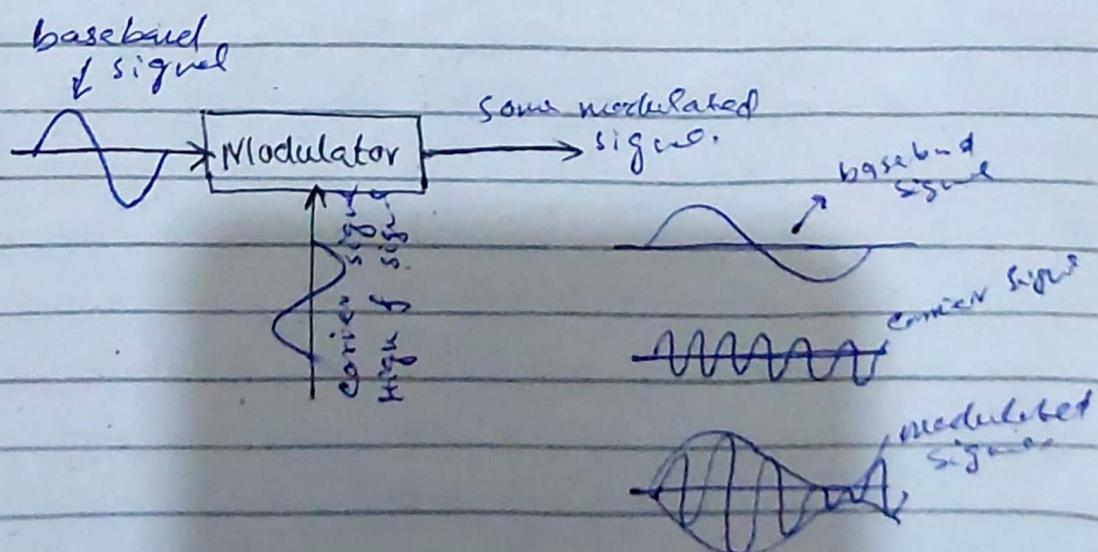
* Communication System:

Exchange of messages over a long distances (Tele-Communication) by using some electro gates.



* Modulation:

If we vary any amplitude upto carrier signal in accordance with the instantaneous value of the baseband signals, the process is called modulation.



Modulation
channels
Noise



8.

8.

8.

فیل (پاکستان)

27-9-23

8.

$$y(t) = m(t) * h(t) + n(t)$$

↓
AWGN

additive white Gaussian Noise

→ Internal Noise is additive in nature.

* SNR: Signal to Noise Ratio

$$\text{SNR} \leftarrow \frac{P_{\text{Signal}}}{P_{\text{Noise}}} \quad \begin{matrix} \uparrow \\ \downarrow \end{matrix} \quad \rightarrow \text{unit less but represented in db's.}$$

$$\text{db} = 10 \log()$$

Multiplexing:

Sending many channels signals through one channel.

- ? * FDM (Frequency division multiplexing)
- * FDMA (Frequency division access).
- * CDMA (Code division multiple access).
- * SDMA (Space division multiple access).

* ALOHA & Slotted Aloha

* Throughput: number of successful packets received per unit time

* Data rate:

$$\rightarrow \text{Bels (B)}: \log \frac{a}{b}$$

$$\rightarrow \text{decibels (DB)}: 10 \log \frac{a}{b}$$

eq:

$P = 10 \text{ mW}$	$= 10^{-2} \text{ W}$
$P = 10 \log_{10}$	$= 10 \log 10^2$
$= 10 \text{ dBm}$	$= 20 \text{ dBW}$

$$\rightarrow 20 \text{ dBm} - 10 \text{ dBm} = 10 \text{ dB} \quad \times$$

$$\therefore \frac{20 \text{ dBm}}{10 \text{ dBm}} = 20 \text{ dB} - 10 \text{ dB} = 10 \text{ dB.}$$

$$\rightarrow 20 \text{ dBW} + 10 = 30 \text{ dBW.}$$

Shannon Capacity:

$$C = B \log_2 (1 + SNR).$$

Hamming Code:

k - redundant bits

m - info bits

$$2^k \geq m+k+1.$$

Let if we have $m=8$

then $k=4$ for which

the expression is true.

Ch no 3

* Signal transmission through LTI System.

$$* g(t) \xrightarrow{H(t)} y(t), = g(t) * h(t)$$
$$Y(\omega) = G(\omega) H(\omega)$$

$$* y(t) = \delta(t) * h(t)$$
$$= h(t) \rightarrow \text{impulse response}$$

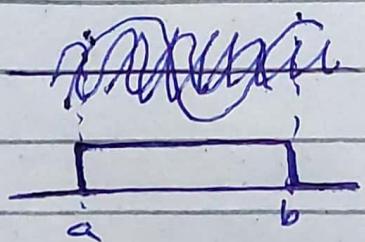
$$* |Y(\omega)| e^{j\Theta_y(\omega)} = |G(\omega)| e^{j\Theta_g(\omega)} \cdot |H(\omega)| e^{j\Theta_h(\omega)}$$

$$* |Y(\omega)| = |G(\omega)| \cdot |H(\omega)| \rightarrow \text{amplitude response}$$

$$* \Theta_y(\omega) = \Theta_g(\omega) + \Theta_h(\omega) \rightarrow \text{phase response}$$

$$* H(\omega) = |H(\omega)| e^{j\Theta_h(\omega)} \rightarrow \text{frequency response of LTI system}$$

* Marvelous Balancing Act:



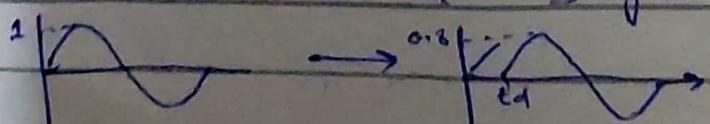
added envelope such that
between $a & b \neq 0$ while
outside $a & b = 0$.

* Distortion Less Signal:

$$* y(t) = K g(t - t_d)$$

→ delaying a signal doesn't
distort a signal

→ changing amplitude does
distort a signal



$$g(t-t_d) = G(\omega)e^{j\omega t}$$

$$Y(\omega) = K G(\omega) e^{j\omega t}$$

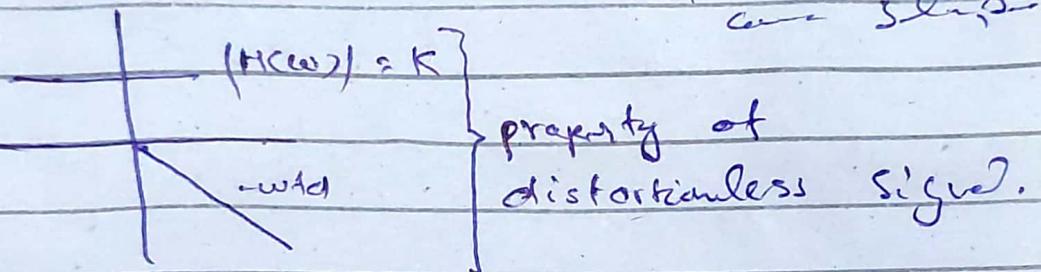
$$H(\omega) = K e^{j\omega t_d}$$

$$\therefore |H(\omega)| = K, \theta_H(\omega) = \omega t_d$$

Should be constant
for all frequency

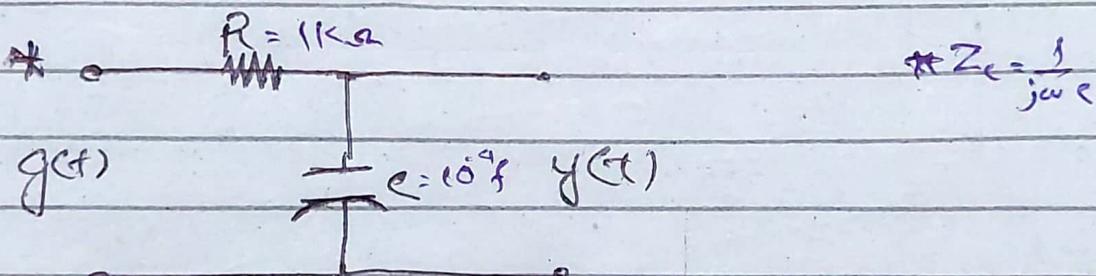
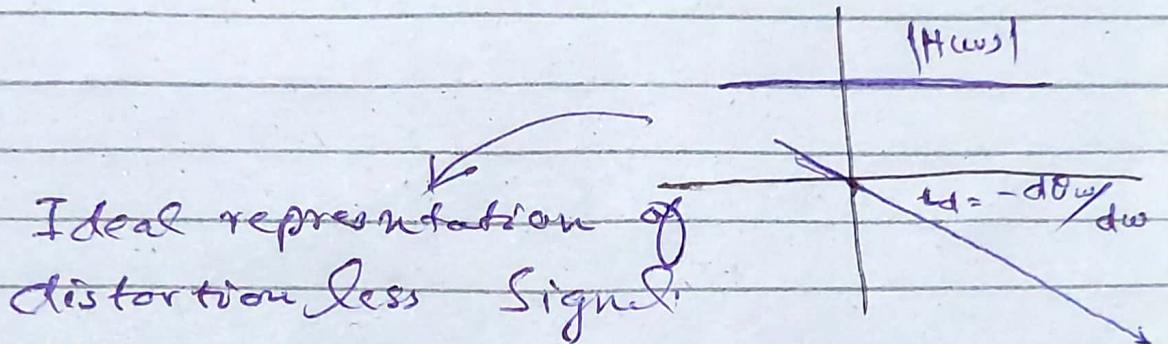
$$\frac{d\theta_H(\omega)}{d\omega} = t_d$$

Should be
constant



$$g(t) \xrightarrow{\text{channel}} K g(t-t_d)$$

$$G(\omega) \longrightarrow K G(\omega) e^{-j\omega t_d}$$



→ It is a low-pass filter

$$\rightarrow Y(\omega) = \frac{1/j\omega c}{R + 1/j\omega c} G(\omega)$$

$$\frac{Y(\omega)}{G(\omega)} = H(\omega) = \frac{1/j\omega c}{R + 1/j\omega c}$$

$$|H(\omega)| = \frac{a}{\sqrt{a^2 + \omega^2}}$$

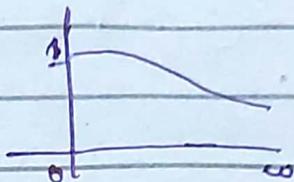
$$\Theta_H(\omega) = -\tan^{-1} \frac{\omega}{a}$$

$$t_d = -\frac{\Theta_H(\omega)}{\omega} = \frac{a}{\omega^2 + a^2}$$

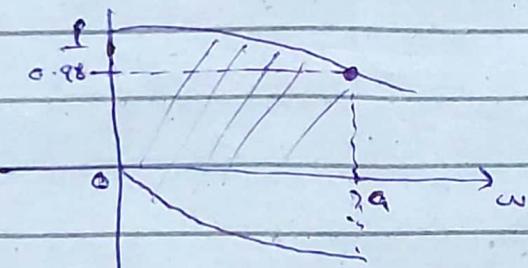
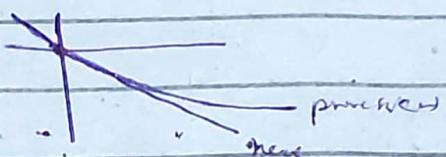
If $\omega \ll \alpha$:

$$|H(\omega)| \approx 1$$

If $\omega \approx 1/\alpha$



$$\Theta_H(\omega) = -\tan \omega / \alpha$$



$$|H(\omega)| = \frac{\alpha}{\sqrt{\alpha^2 + \omega^2}} \rightarrow 0.98$$

$$\alpha \geq 0.96\alpha^2 + 0.96\omega^2$$

$$\omega_0 \approx \sqrt{\frac{0.04\omega^2}{0.96}}$$

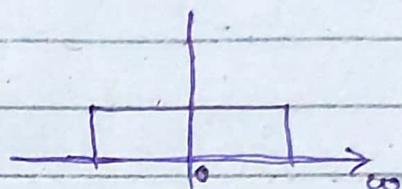
$$\omega_0 \gtrsim 20300 \text{ rad/sec}$$

follow same procedure for Ed.

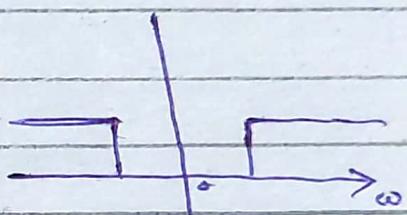
- * Amplitude response is remain constant for some band of frequency.
- * Phase response should be linear function.

Ideal vs Practical filter:

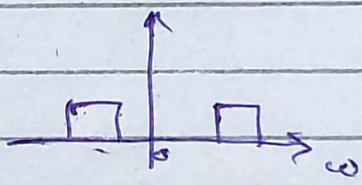
→ Low-pass filter.



→ High-pass filter

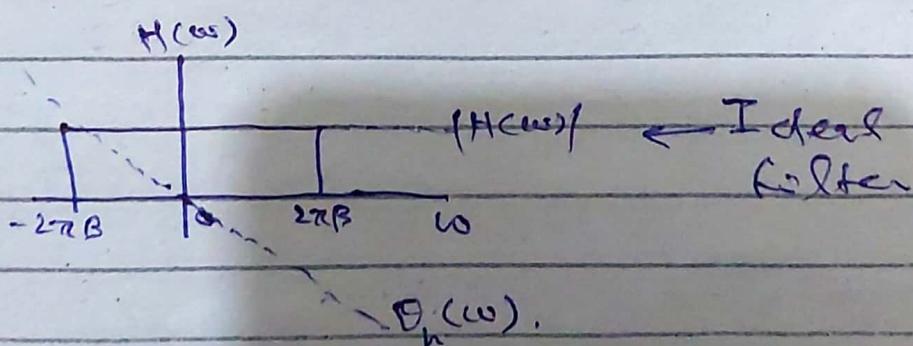


→ Band-pass filter

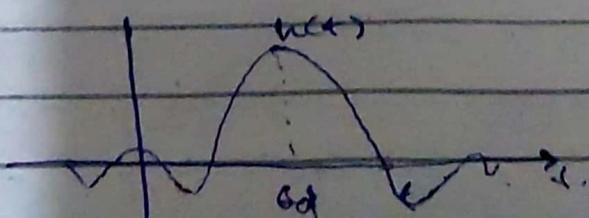


$$\begin{array}{c}
 g(t) \\
 \xrightarrow{\quad} \\
 G(\omega)
 \end{array}
 \xrightarrow{\text{Ideal filter}}
 \begin{array}{c}
 y(t) = 1 \cdot g(t-t_0) \\
 Y(\omega) = G(\omega) e^{-j\omega t_0}
 \end{array}$$

$\Rightarrow H(\omega) = e^{j\omega t_0}$

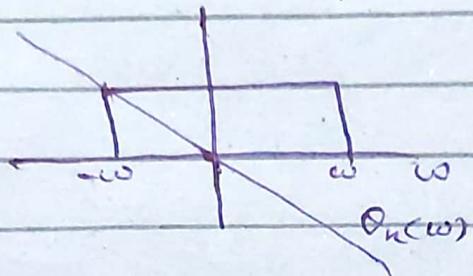


→ In time



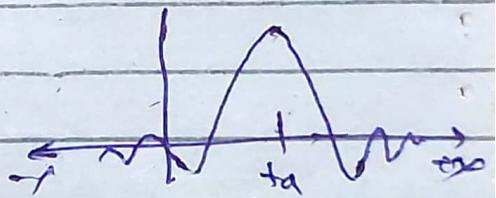
$$h(t) = h(t) \cdot u(t),$$

practical
 only records
 for $t > 0$



$$H(\omega) = \operatorname{rect} \frac{\omega}{2\omega} e^{-j\omega t_d}$$

$$\mathcal{F}\left\{ \operatorname{rect} \frac{\omega}{2\omega} e^{-j\omega t_d} \right\} = \frac{\omega}{\pi} \sin \omega(t - t_d)$$



passes zero when $\omega t_d = n\pi$
 so $\omega(t - t_d) = n\pi$

→ It should be delayed only
 3 or 4 times of π/ω .

* Paley-Wiener Criteria:

→ Shows us when a signal
 is ideal or practical.

$$\int_{-\infty}^{\infty} \frac{|H(\omega)|}{1+\omega^2} d\omega < \infty$$

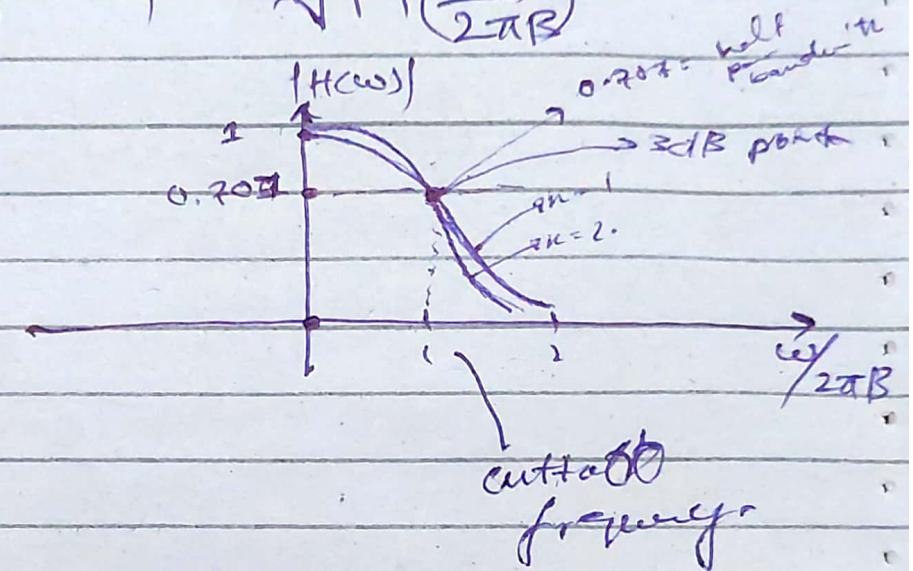
finite.

$$*\frac{W}{\pi} \sin \omega t \Leftrightarrow \text{rect} \frac{\omega}{2\pi}$$

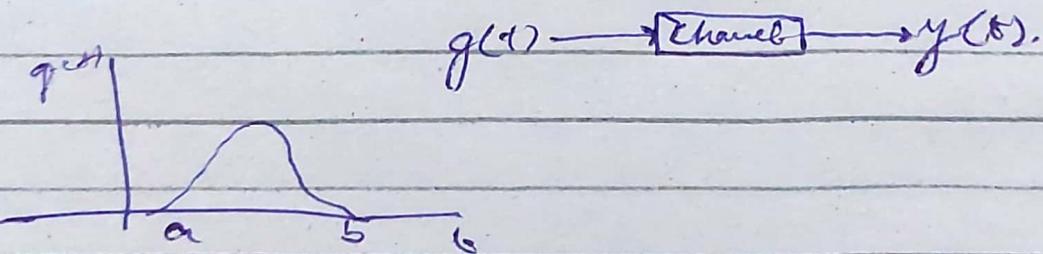
$$*\frac{\omega}{2\pi} \sin^2 \frac{\omega t}{2} \Leftrightarrow \Delta \left(\frac{\omega}{2\pi} \right)$$

* Butterworth filter:

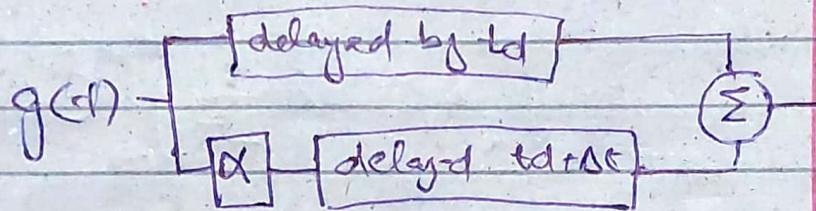
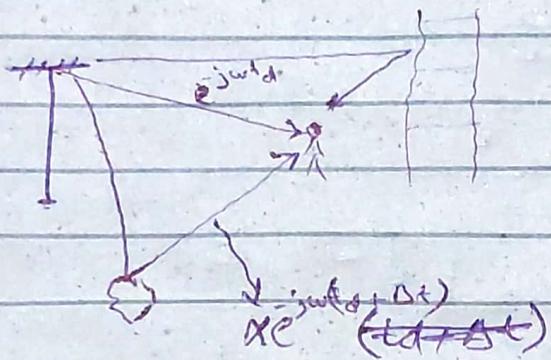
$$|H(\omega)| = \sqrt{1 + \left(\frac{\omega}{2\pi B} \right)^2}$$



* Linear Distortion:



Multipaths:



$$\bar{e}^{-j\omega t d} + \alpha \bar{e}^{-j\omega(t_d + \Delta t)} = (1 + \alpha \bar{e}^{-j\omega \Delta t}) \bar{e}^{-j\omega t d}$$

$$= (1 + \alpha \cos \omega \Delta t - j \alpha \sin \omega \Delta t) \bar{e}^{-j\omega t d}$$

amplitude and phase

$$= \sqrt{(1 + \alpha \cos \omega \Delta t)^2 + (\alpha^2 \sin^2 \omega \Delta t)}$$

$$\cdot e^{j \tan^{-1} \frac{\alpha \sin \omega \Delta t}{1 + \alpha \cos \omega \Delta t} + \omega t d}$$

$$= \sqrt{1 + \alpha^2 + 2 \alpha \cos \omega \Delta t}$$

* frequency Selective fading

$$g(t) \xrightarrow{\text{gate' dt}} G(\omega)$$

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} G(\omega) e^{j\omega t} d\omega$$

* $G(\omega) = g(\omega)$

Energy of Signal.

$$E_g = \int_{-\infty}^{\infty} |g(t)|^2 dt$$

\leftarrow sign $E_g = \int_{-\infty}^{\infty} |g^2(t)| dt$

$$(a+bi)(a-bi) \leftarrow = \int_{-\infty}^{\infty} g(t) g^*(t) dt$$

from w.r.t. ω .

$$= \int_{-\infty}^{\infty} g(t) \left\{ \frac{1}{2\pi} \int_{-\infty}^{\infty} G(\omega) e^{-j\omega t} d\omega \right\} d\omega$$

$$= \frac{1}{2\pi} \left\{ \int_{-\infty}^{\infty} g(t) e^{-j\omega t} dt \right\} \int_{-\infty}^{\infty} G(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} G(\omega) \cdot G^*(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} |G(\omega)|^2 d\omega$$

Parseval's Theorem in which
energy is represented in frequency
domain.

Example: $g(t) = e^{-at} u(t) \quad a > 0$

$$E_g = \frac{1}{2a}$$

$$G(\omega) = \frac{1}{a+j\omega}$$

$$|G(\omega)| = \frac{1}{\sqrt{a^2 + \omega^2}}$$

$$|G(\omega)|^2 = \frac{1}{a^2 + \omega^2}$$

$$E_g = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{1}{a^2 + \omega^2} d\omega$$

$$= \frac{1}{2\pi a} \cdot \left(\text{arctan} \frac{\omega}{a} \right) \Big|_{-\infty}^{\infty}$$

$$= \frac{1}{2\pi a} \left(\text{atan}(0) - \text{atan}(-\infty) \right)$$

$$= \frac{1}{2\pi a} \times \pi = \frac{1}{2a}$$

* Energy Spectral Density:

$$\frac{E_y(\omega)}{dt} = |G(\omega)|^2$$

Amplitude modulation:

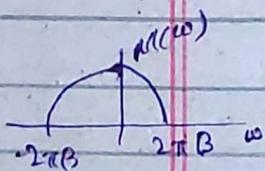
- Without doing modulation is called baseband communication.
- Signal has frequency, amplif., please - $\frac{\text{amp}}{\text{freq}}$ - $\frac{\text{phase}}$.
- Let $m(t)$ be a baseband signal, multiply it with a carrier signal.

$$m(t) \times \cos \omega_c t$$

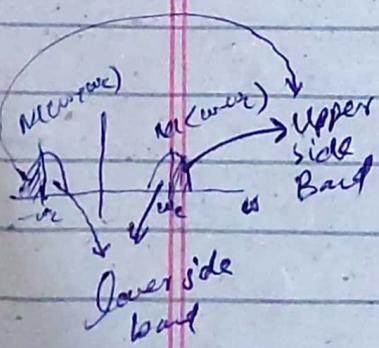
$$= \phi_{AM}(t) = m(t) \cos \omega_c t.$$

$$= m(t) \left[\frac{e^{j\omega_c t} + e^{-j\omega_c t}}{2} \right]$$

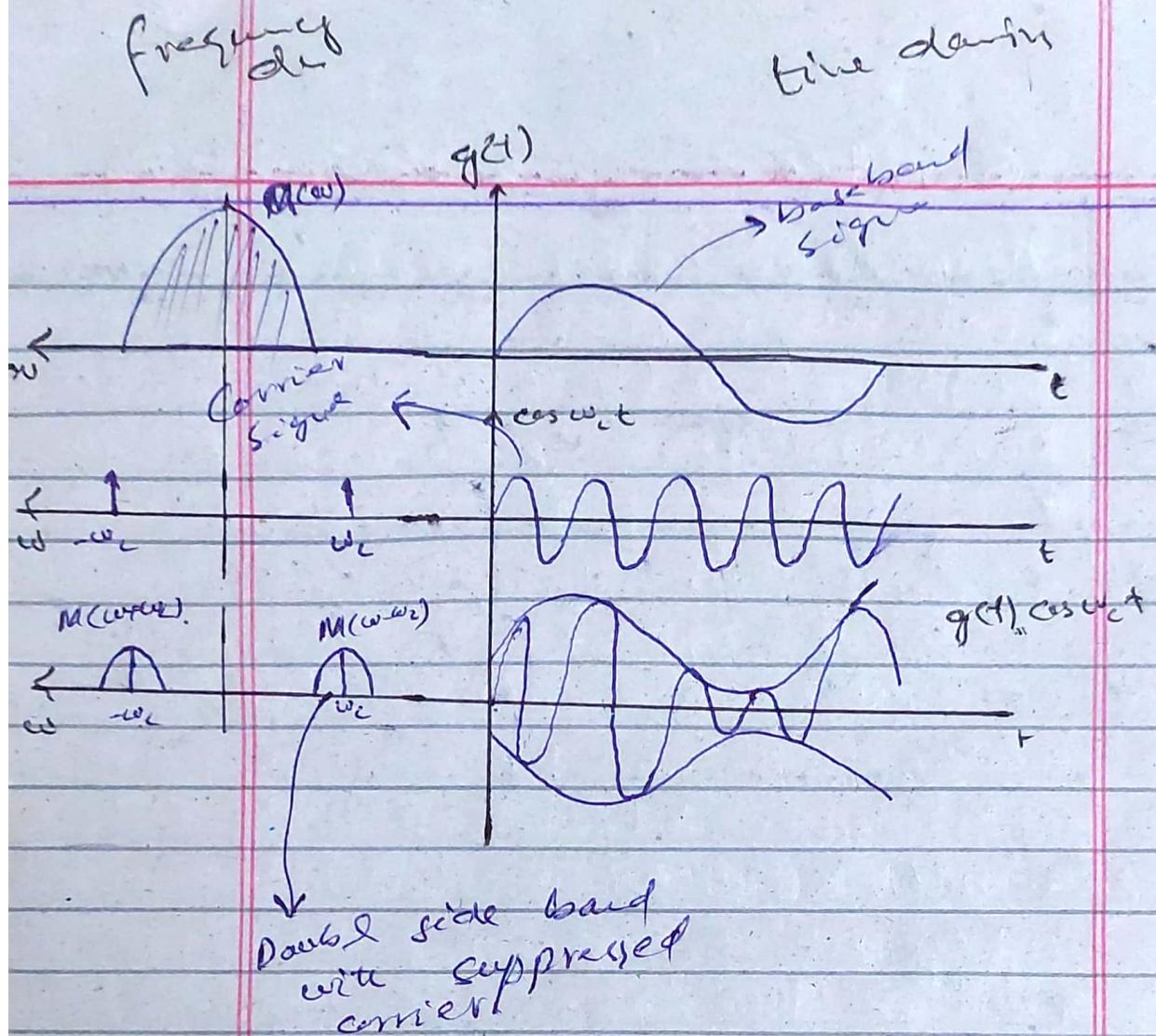
$$= \frac{m(t)e^{j\omega_c t}}{2} + \frac{m(t)\bar{e}^{-j\omega_c t}}{2}$$



$$\therefore g(t)e^{j\omega t} = G(\omega + \omega_0), \quad g(t)\bar{e}^{-j\omega t} = G(\omega - \omega_0)$$



$$= \frac{M(\omega + \omega_c) + M(\omega - \omega_c)}{2}$$



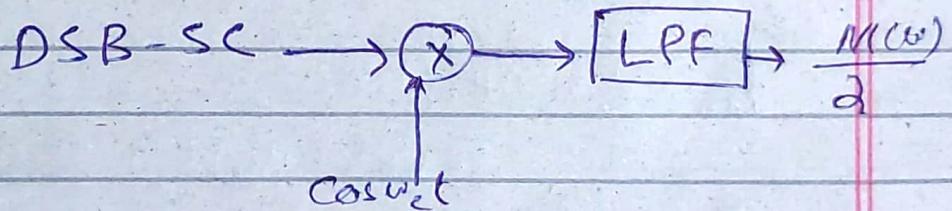
* ω_c should be greater or equal to $2\pi B$, so that the components should not interfere with each other.

$$\omega_c \geq 2\pi B.$$

* Now performing demodulation.

$$\begin{aligned}
 & \{m(t) \cos \omega_c t\} \cos \omega_c t \\
 &= m(t) \cos^2 \omega_c t \\
 &= m(t) \left(\frac{1 + \cos 2\omega_c t}{2} \right)
 \end{aligned}$$

$$\begin{aligned}
 &= \frac{m(t)}{2} + \frac{m(t)\cos 2\omega_c t}{2} \\
 &= \frac{m(t)}{2} + \frac{m(t)e^{j2\omega_c t}}{4} + \frac{m(t)e^{-j2\omega_c t}}{4} \\
 &= \frac{M(\omega)}{2} + \frac{M(\omega+2\omega_c)}{4} + \frac{M(\omega-2\omega_c)}{4}
 \end{aligned}$$



Synchronous or coherent detection.

- In above communication we are not transmitting carrier signal but we are just using it.
- If we transmit a carrier signal too with baseband signal it will consume 66.67% of total power.

Assignment:

$$* m(t) = \cos \omega_c t$$

modulate it add even
de modulate it

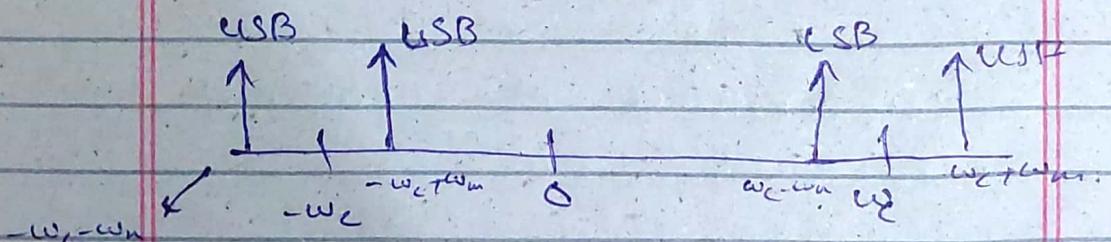
CS - Lecture

25 Oct 2023 / We

$$m(t) = \cos \omega_m t$$

$$M(\omega) = M(\omega + \omega_m) + M(\omega - \omega_m)$$

$$\begin{aligned}\phi_{AM}(\omega) &= m(t) \cos \omega_m t = \cos \omega_m t \cdot \cos \omega_c t \\ &= \cos(\omega_c + \omega_m)t + \cos(\omega_c - \omega_m)t\end{aligned}$$



Modulators:

→ Electronic devices to perform modulation

① → Multiplier

② Non-Linear Modulator:

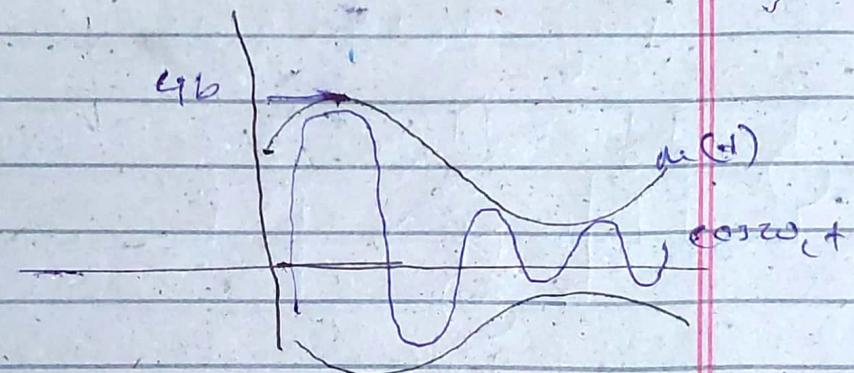
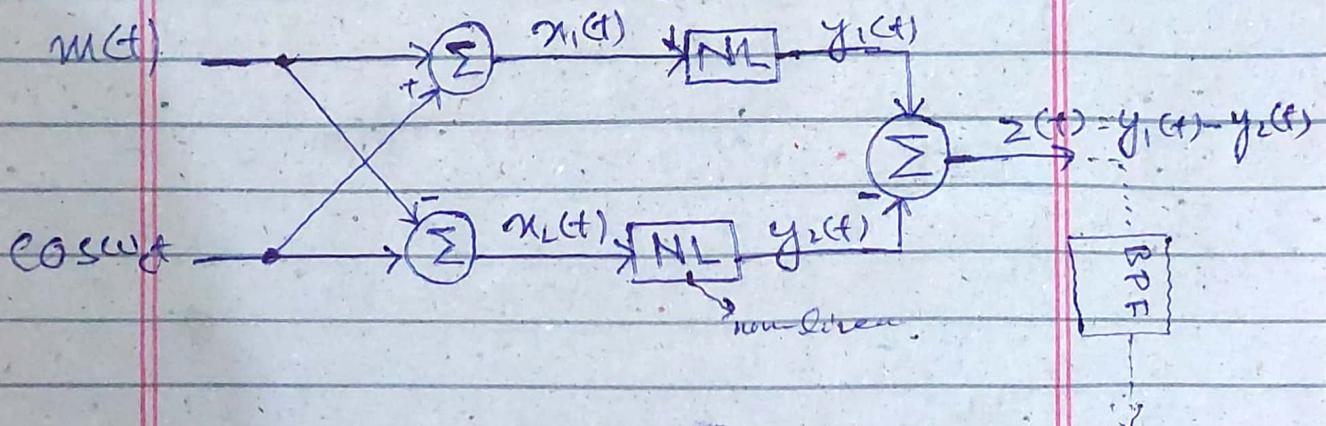
having higher order inputs

$$y(t) = a_0(t) + b_1 x^2(t)$$

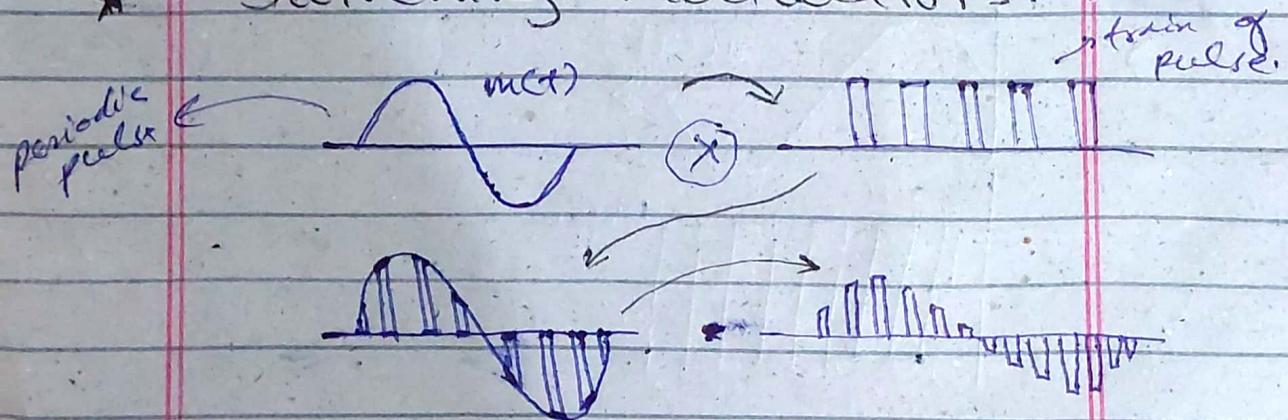
$$\Sigma(t) = y_1(t) - y_2(t)$$

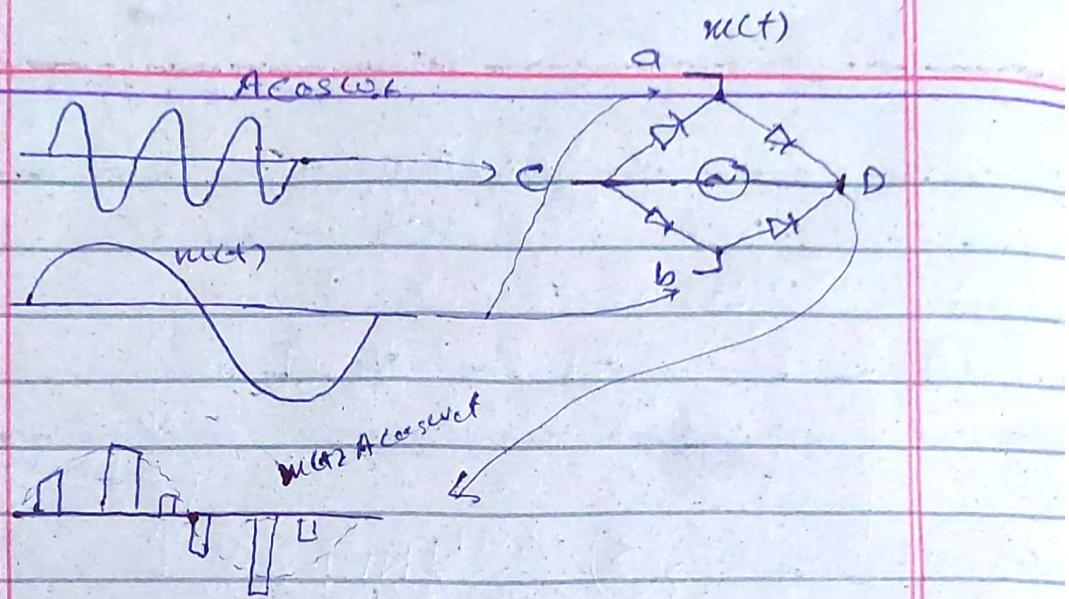
$$y_1(t) = \cos \omega_c t + m(t)$$

$$y_2(t) = \cos \omega_c t - m(t)$$

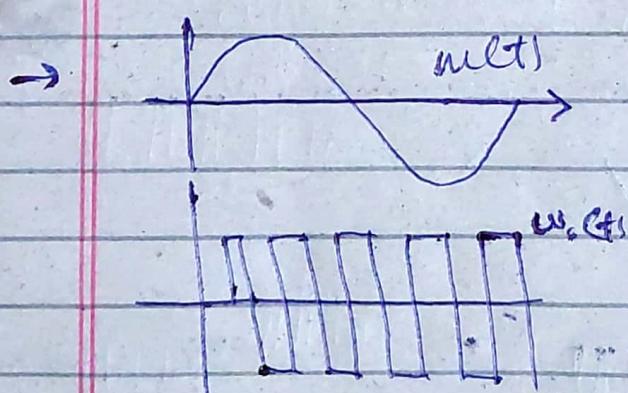
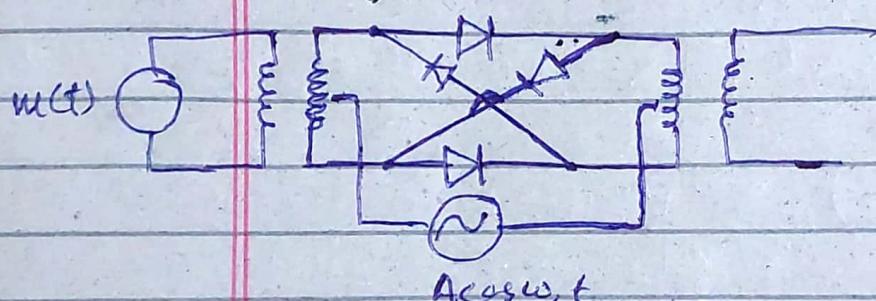


* Switching Modulators:





Ring Modulator:



$$\phi_{Am}(t) = A \cos \omega c t + m(t) \cos \omega c t$$

$$\phi_{Am}(\omega) = \pi \{ \delta(\omega - \omega_c) + \delta(\omega + \omega_c) \}$$

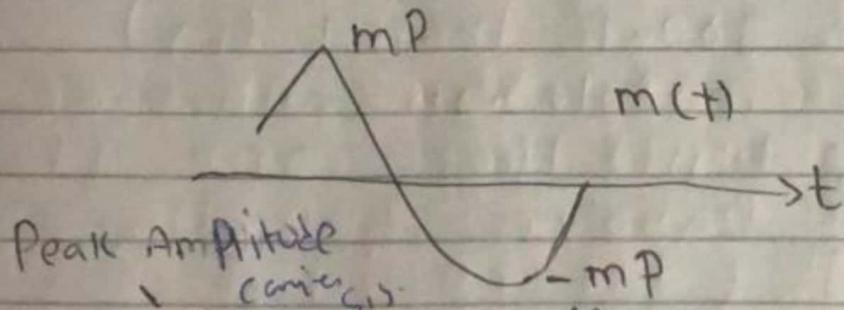
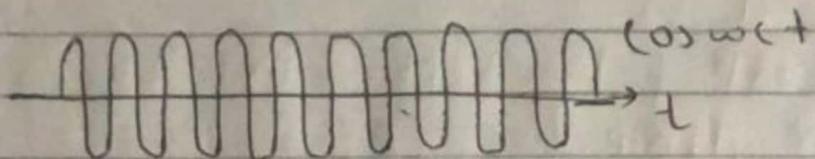
$$+ \frac{m(\omega + \omega_c) + m(\omega - \omega_c)}{2}$$

So impulse will also be transformed.

$$e^{j\omega t} \rightarrow 2\pi S(\omega - \omega_c)$$

$$\tilde{e} = 2\pi S(\omega + \omega_c)$$

$$\begin{aligned}\phi_{Am}(t) &= A \cos \omega c t + m(t) (\omega_c \omega c t) \\ &= (A + m(t)) \cos \omega c t\end{aligned}$$

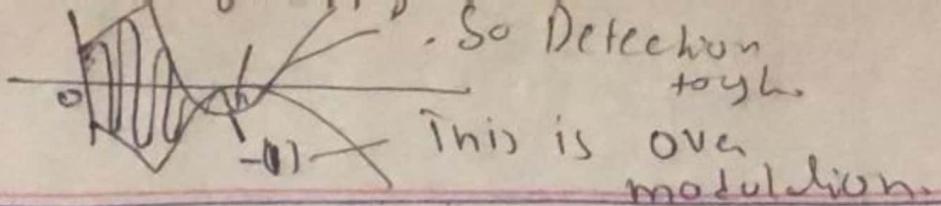


$A + m(t) > 0$ "for all error detection."

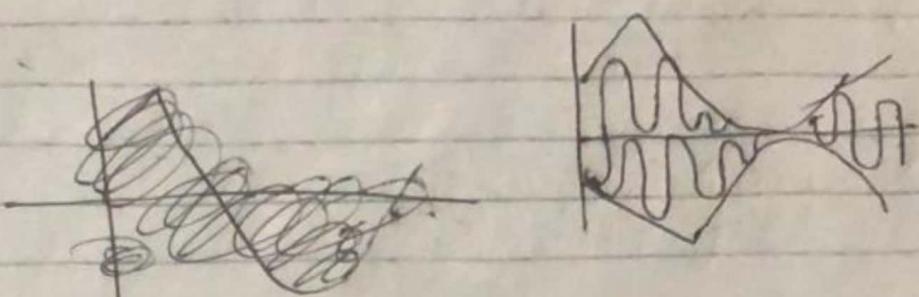
$A - mP \geq 0$ Peak Amplitude modulates signal

if $-mP$ is greater than A
then some of Envelope
will come to $-v_c$

e.g. $A = 5, mP = 7.6, \zeta + j(0.6) = -1$



- So this is the case of over modulation. (Some part in -ve Side.)



- MODULATION INDEX-

$$u = \frac{mP}{A} \quad 0 \leq u \leq 1$$

if $\frac{u}{mP} = 1$ it is touching zero line

if $\frac{u}{mP} >$ greater than 1 (1.5)

So over modulation will come

. if $u = 1$ less than one it will be above zero line,

$$m(t) = B \cos \omega_m t$$

$$u = 0.5$$

$$u = 1$$

we know that:

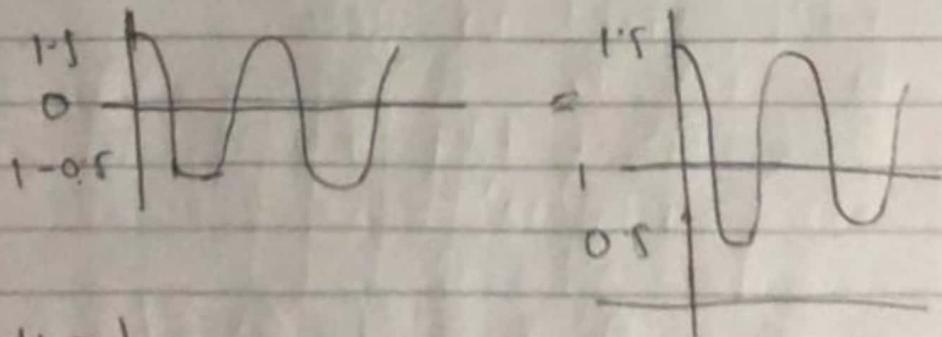
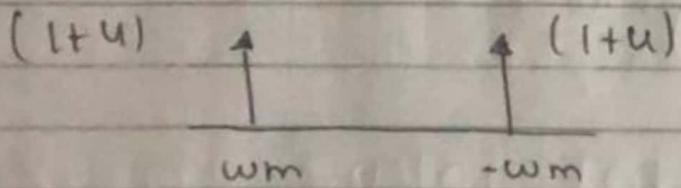
$$\varphi_{AM} = \{ A + m(t) \} \cos \omega_c t$$

$$= \{ A + B \cos \omega_m t \} \cos \omega_c t$$

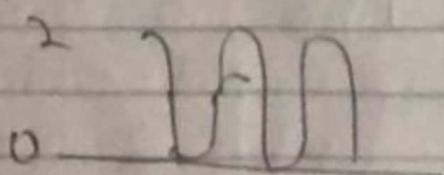
$$= \{ A + uA \cos \omega_m t \} \cos \omega_c t$$

$$= A \{ 1 + u \cos \omega_m t \} \cos \omega_c t$$

$$1 + u \cos \omega_m t \quad \text{Down}$$



$$f_0 \quad u = 1$$



$$(1+u) = 1+1=2$$

$$(1-u) = (1-1)=0$$

• if carrier is going to transmit
so excessive power is used.

• Carrier Power & Side Bands

Power A Coswt

To find Power = $\frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} |A \cos \omega t|^2 dt$

$$P(t) = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} A^2 \cos^2 \omega t dt$$

$$= \frac{A^2}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} \int \frac{1}{2} (1 + \cos 2\omega t) dt$$

• we will not integrate because
it will give us zero.

$$= \frac{A^2}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} 1 dt + 0$$

$$= \frac{A^2 \times T}{2T} = \boxed{\frac{A^2}{2}}$$

$$\text{So } m(t) \cos \omega_c t + A \cos \omega_c t \xrightarrow{\text{mean (because variable)}}$$

$$P_m = \frac{\tilde{m}^2(t)}{2} \xrightarrow{\text{mean}} P_m = \frac{A^2}{2}$$

So

$$m(t) = B \cos \omega_m t \quad (\text{tone signal}).$$

$$\therefore B = uA$$

$$B \cos \omega_m t$$

$$m(t) = \boxed{\frac{B^2}{2}}$$

$$m(t) = \boxed{B^2 = \frac{u^2 A^2}{2}} \quad (\text{Power of tone signal}).$$

• Power Efficiency

$$\frac{P_m}{P_c + P_m} = \frac{\tilde{m}^2(t)/2}{A^2/2 + \tilde{m}^2(t)/2} \times 100$$

(consider also transmission),

$$= \frac{\tilde{m}^2(t) \times 100}{A^2 + \tilde{m}^2(t)} = \frac{u^2 A^2 / 2 \times 100}{A^2 + u^2 A^2 / 2}$$

$$= \frac{u^2 A^2 / 2 \times 100}{2A^2 + u^2 A^2} = \frac{u^2 A^2 \times 100}{(2 + u^2) A^2}$$

X

$$\% \eta = \frac{u^2}{2 + u^2} \times 100$$

$$u = B \quad \text{if } u = 1$$

then

$$\boxed{B - A}$$

$$\therefore \eta = \frac{u^2}{2+u^2} \times 100$$

if $u = 1$

$$= \frac{1 \times 100}{2+1} = \frac{1 \times 100}{3} = 33.33\%$$

66% Power consumed

if $u = 0.5$

Consumed by current

$$= \frac{(0.5)^2}{2+(0.5)^2} \times 100 = 11.11\%$$

more
Degraded.

$u = 1.5$

$$= \frac{(1.5)^2}{2+(1.5)^2} \times 100 =$$

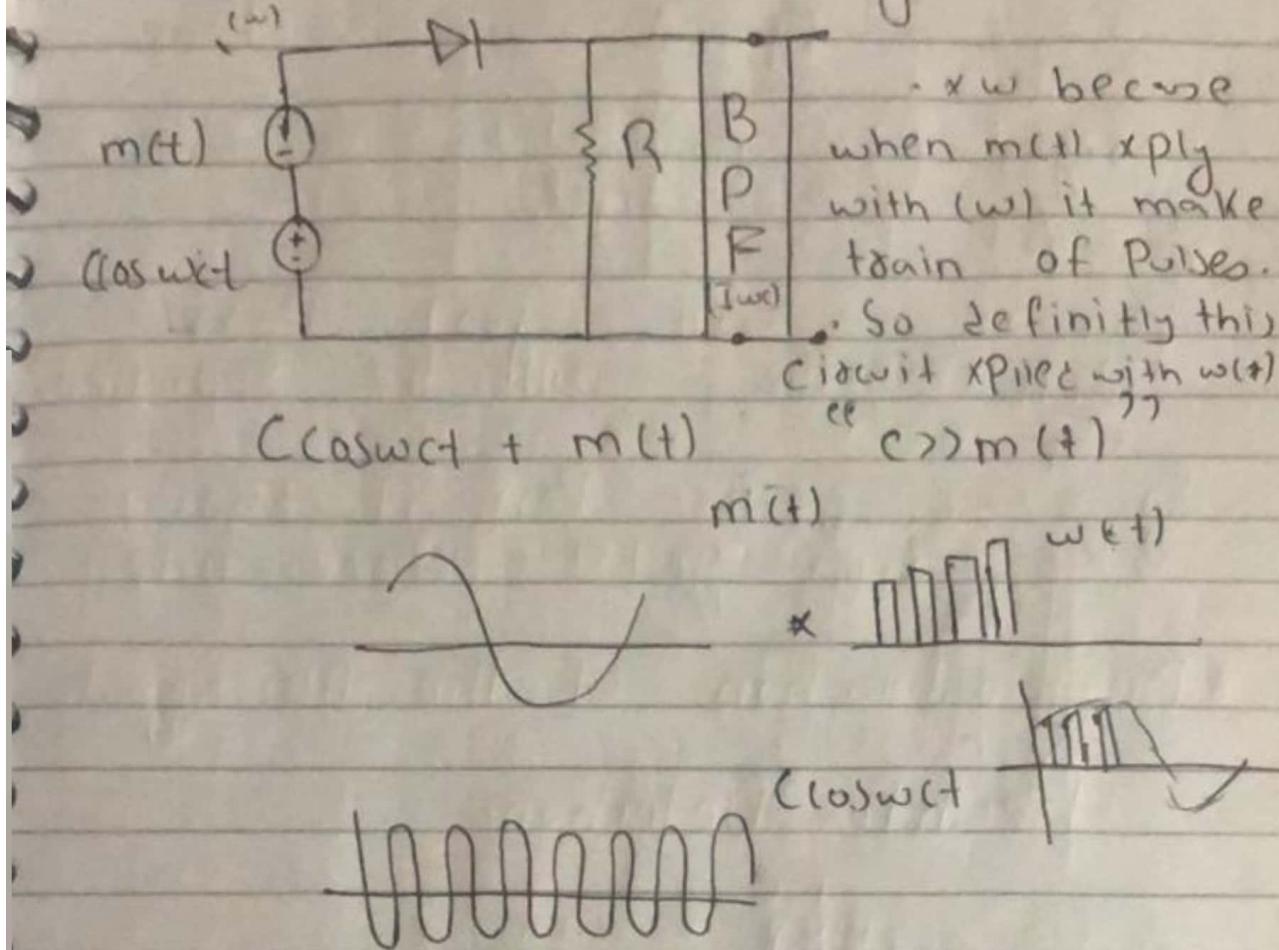
• Six by inc u value less value of power is consumed

by common signal

• and more only signal is transferring

But we have limited Power in a more optimization info is lost

• Generation of A.M Signals

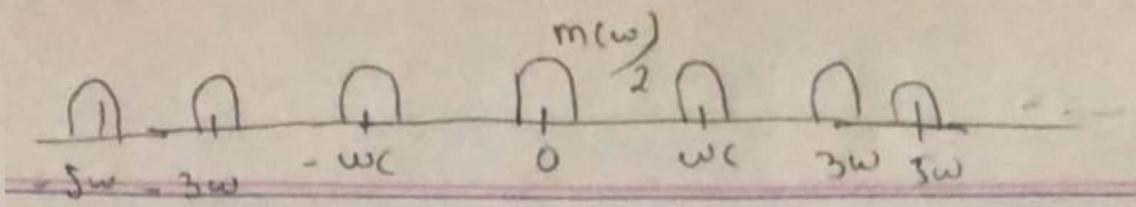


- if $\cos \omega t$ So Diode will conduct F.B. value is transmitted.
- if $\cos \omega t$ is -ve Diode will not conduct R.B.

$$\{(\cos \omega t + m(t))\} w(t)^- \text{ impulse periodic train pulse}$$

$$\{(\cos \omega t + m(t))\} \left\{ \frac{1}{2} + \frac{2}{\pi} \right\} \left\{ \cos \omega t - \frac{1}{3} \cos 3\omega t + \frac{1}{7} \cos 7\omega t \dots \right\}$$

carily

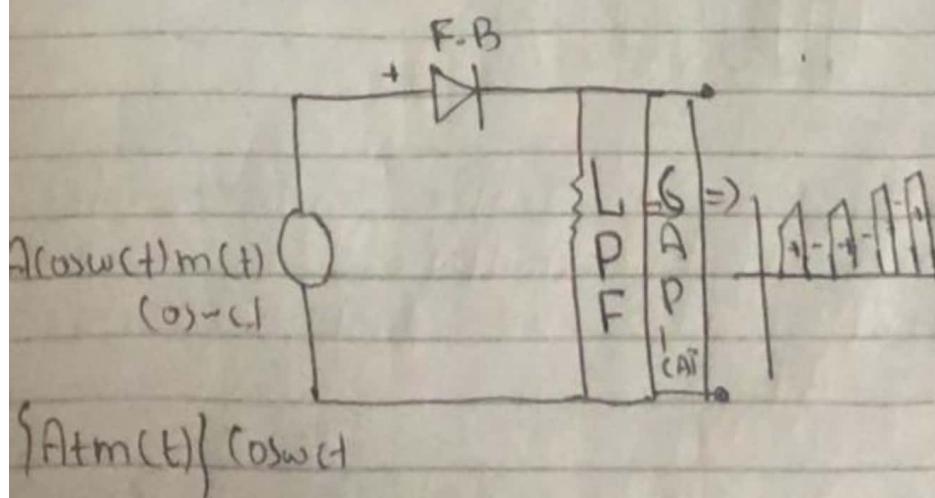


$= 1 \cos(\omega t + 2m(t)) \cos(\omega t + \text{other terms})$
 $\stackrel{2}{\cancel{1}} / \stackrel{\pi}{\cancel{1}}$
 carrier modulated signal generated.

- So we will just pass $m(t)$ other will be suppressed.
- So we will pass it through B.P.F so get desired output.

* Demodulation of the Am Signal.

* Rectifier Detection



$$\left\{ A + m(t) \right\} \cos(\omega t) \times w(t)$$

• we apply with the 2nd because it will give us the sum of cos.

$$\{A + m(t) \cos \omega_c t\} \left\{ \frac{1}{2} + \frac{2}{\pi} \left(\cos \omega_c t - \frac{1}{3} \cos 3\omega_c t \right) \right. \\ \left. + \dots \text{etc terms} \right\}$$

$$\{A + m(t) \cos \omega_c t\} \left\{ \frac{2}{\pi} (\cos \omega_c t) \right\}$$

$$\frac{2}{\pi} \{ A + m(t) \cos \omega_c t \}$$

$$\frac{2}{\pi} \{ A + m(t) \left\{ \frac{1 + \cos 2\omega_c t}{2} \right\} \}$$

(1)

(2)

$$\frac{2}{\pi} \left\{ \frac{A + m(t)}{2} + \frac{1}{2} A + \frac{m(t)}{2} \cos 2\omega_c t \right\}$$

Pass it throgh L.P.T 2 will be removed

$$\frac{2}{\pi} \left\{ \frac{A + m(t)}{2} \right\}$$

$$= \frac{A}{\pi} + \frac{1}{\pi} m(t)$$

DC

Now add capacitor to remove

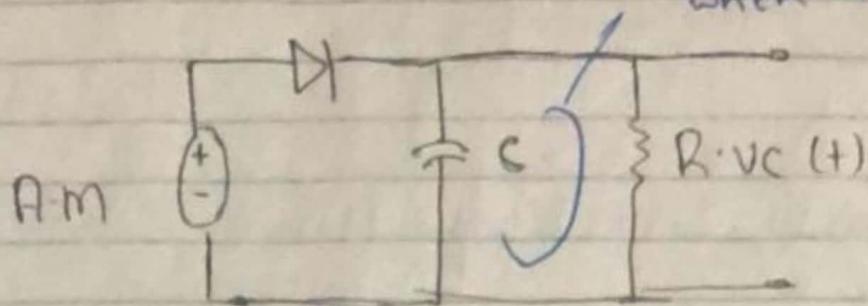
$$- \frac{1}{\pi} m(t)$$

DC

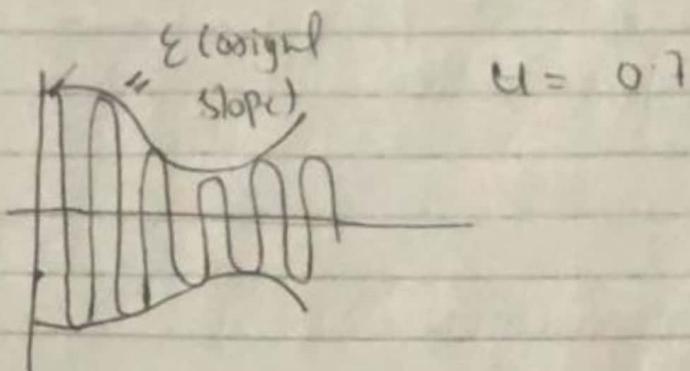
De modulated

- Envelope Detection -

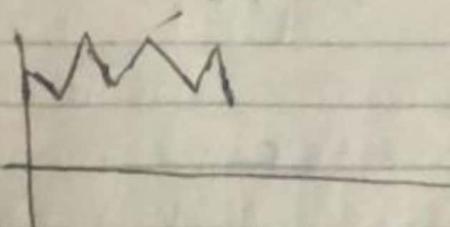
Discharge when -ve cycle



For Envelope detection it
is must $A \gg 1$



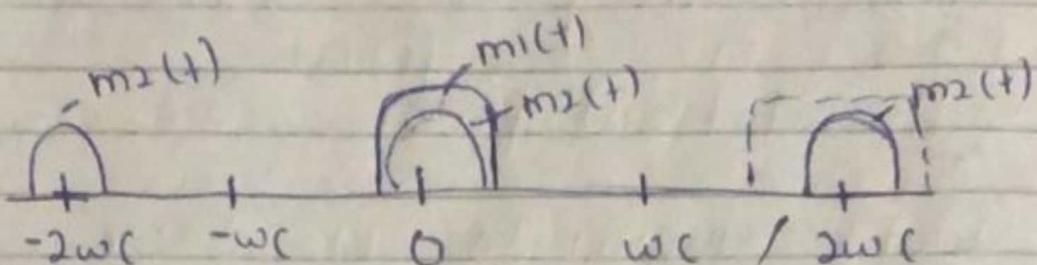
capacitive slope.



- when +ve will occur so F.B is capacitor will charge
- when -ve will occur so R.B is capacitor will discharge still give value.
- So Both the +ve & -ve Envelope will be made so Envelope detection will occur.

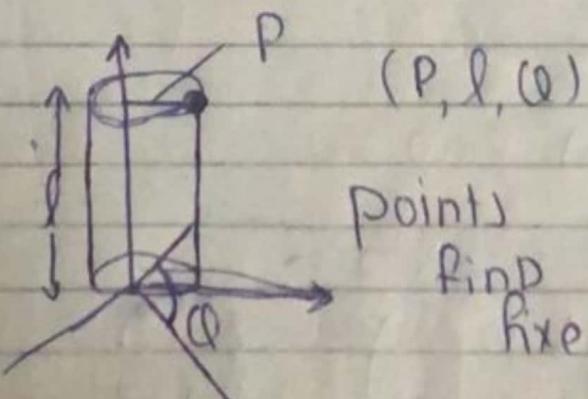
Now to get $m_2(t)$ we will apply it with $\sin(wt)$.

$$\text{Param } \sin wct = m_1(t) \cos wct \sin wct + m_2(t) \sin^2 wct$$



Pass it through LPF we will obtain $m_2(t)$.

- Cylindrical co-ordinate System



By these points we can find the fixed point.

- 3. Coordinate System.
- Cartesian
- Cylindrical

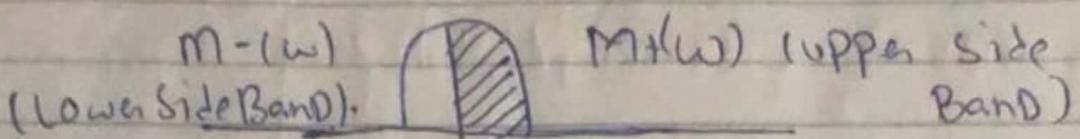
- with carrier transmission two loads
- Power
- Band.

Assignment

$$\Phi_{\text{am}}(t) = \{ m_1(t) \cos \omega_c t + m_2(t) \sin \omega_c t \} / x(\cos \omega_c t + \phi)$$

- Single Side Band A.M.

$$m(t) \Rightarrow m(\omega) \text{ F.T}$$

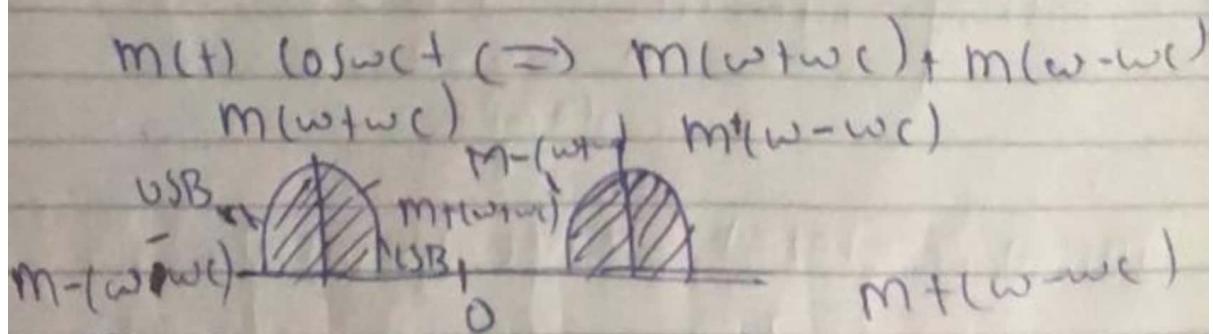


To send half of the Band.

$$m(\omega) = m_+(\omega) + m_-(\omega)$$

$$\begin{aligned} M_+(t) &\Rightarrow m_+(\omega) && (\text{Upper Side}) \\ M_-(t) &\Rightarrow m_-(\omega) && (\text{Lower Side}). \end{aligned}$$

lets say.



To find Upper side one

$$\Phi_B(\omega) = M_+(\omega - \omega_c) + M_-(\omega + \omega_c)$$

$$\Phi_{LSB}(\omega) = m_-(\omega - \omega_c) + m_+(\omega + \omega_c)$$

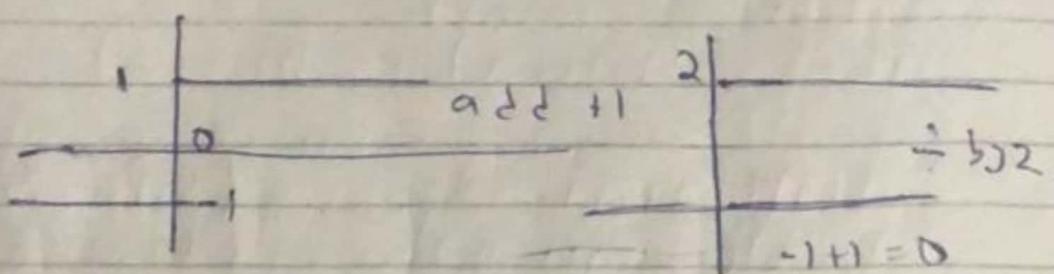
$$* m_+(t) = \frac{1}{2} \left\{ m(t) + j m_h(t) \right\} \quad \text{--(ii)}$$

$$* m_-(t) = \frac{1}{2} \left\{ m(t) - j m_h(t) \right\} \quad \text{--(iii)}$$

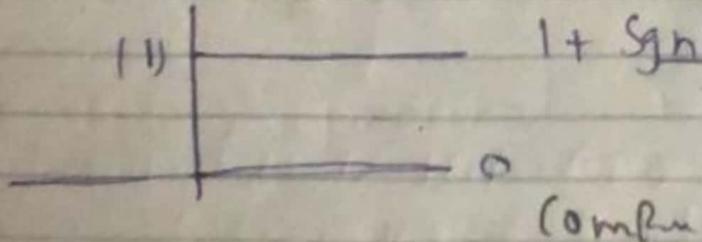
Pre Jao

$$m_+(\omega) = m(\omega) u(\omega)$$

$$m_+(\omega) = m(\omega) \left\{ \frac{1 + \text{sgn}(\omega)}{2} \right\}$$



$$1 + \frac{\text{sgn}(\omega)}{2} = u(\omega)$$



$$m_+(\omega) = \frac{m(\omega)}{2} + \frac{m(\omega) \text{sgn}(\omega)}{2} \quad \text{--(iii)}$$

So $m_+(\omega) = \frac{m(\omega)}{2} + \frac{m(\omega) \text{sgn}(\omega)}{2}$ (from (ii) & (iii))

$$j m_h(t) \iff m(\omega) \text{sgn}(\omega)$$

$$q_{\text{USB}}(\omega) = m_+(\omega - \omega_c) + m_-(\omega + \omega_c)$$

in TP.

$$= \frac{m_+(t)e^{j\omega ct}}{2} + \frac{m_-(t)e^{-j\omega ct}}{2} \quad \text{--- (i)}$$

We know that

$$m_+(t) = \frac{1}{2} \{ m(t) + j m_h(t) \}$$

$$m_+(t) e^{j\omega ct} \Rightarrow$$

$$m(\omega - \omega_c)$$

$$m_-(t) = \frac{1}{2} \{ m(t) - j m_h(t) \} \quad \begin{matrix} \text{Put in eq} \\ \text{(i)} \end{matrix}$$

$$= \frac{1}{2} \{ m(t) + j m_h(t) \} e^{j\omega ct} + \frac{1}{2} \{ m(t) - j m_h(t) \} e^{-j\omega ct}$$

$$= \frac{m(t)e^{j\omega ct}}{2} + \frac{j m_h(t)e^{j\omega ct}}{2} + \frac{m(t)e^{-j\omega ct}}{2} - \frac{j m_h(t)e^{-j\omega ct}}{2} \quad \text{Simplify}$$

$$= m(t) \left\{ \frac{e^{j\omega ct} + e^{-j\omega ct}}{2} \right\} - j m_h(t) \left\{ \frac{e^{j\omega ct} - e^{-j\omega ct}}{2} \right\}$$

$$q_{\text{USB}}(t) = m(t) \cos(\omega_c t) - m_h(t) \sin(\omega_c t)$$

$$\begin{array}{c} m(\omega) + m(-\omega) \\ \hline -m(-\omega) \end{array}$$

So we write j .

j because it is not even after flip.

$$mh(t) \Rightarrow -j(m(\omega)) \operatorname{Sign}(\omega)$$

$$m(\omega) \rightarrow \boxed{H(\omega)} \quad r(\omega) = m(\omega) H(\omega)$$

So $H(\omega) = -j \operatorname{Sign}(\omega)$

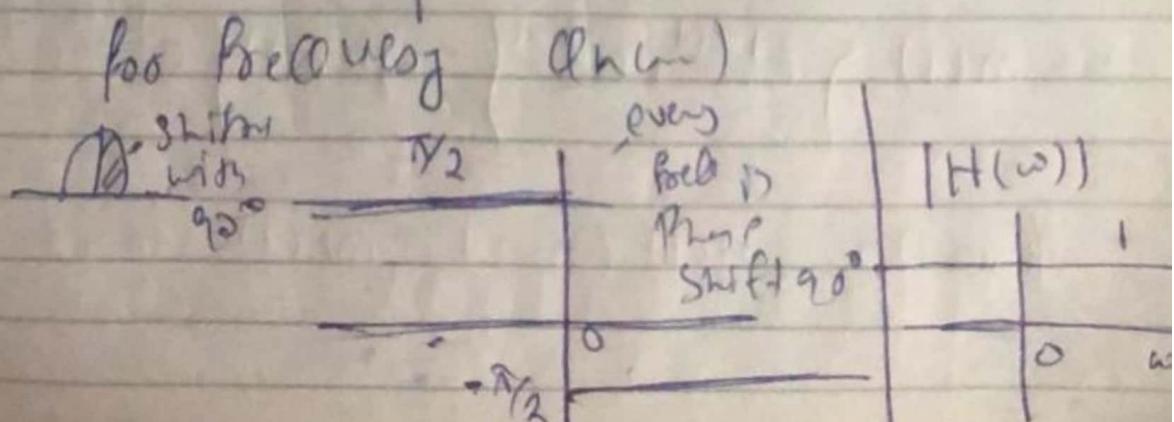
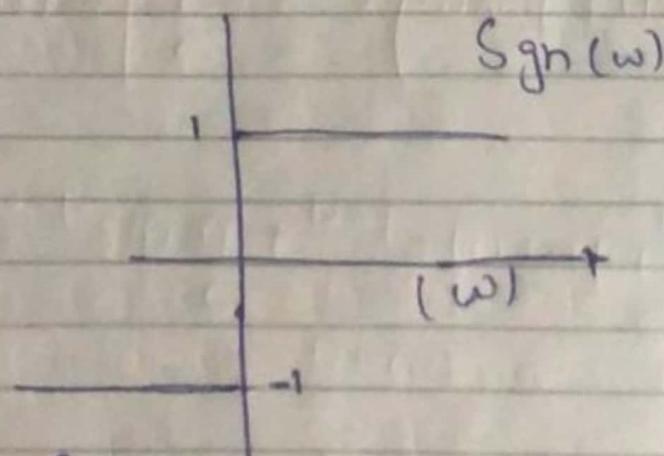
constant
amplitude

$H(\omega) = |H(\omega)| e^{j\phi_{\omega}}$

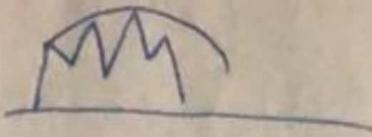
$$H(\omega) = |e^{-j\pi/2}| \quad \omega > 0$$

Phase shift with 90°

$$H(\omega) = |e^{j\pi/2}| \quad \omega < 0$$



$$\sum_{RC}$$



$$V_C = \epsilon e^{-t/RC} \rightarrow \text{exponential decay.}$$

$$RC \gg \frac{1}{\omega_C}$$

$$\left| \frac{dV_C(t)}{dt} \right| \geq \left| \frac{d\epsilon(t)}{dt} \right| \quad (\text{slope should be more, more step so it could be detected}).$$

Let

$$V_C(t) = \epsilon e^{-t/RC} \text{ in p.v.c}$$

Let in Taylor Seri:

$$V_C(t) \approx \epsilon \left(1 - \frac{t}{RC} \right)$$

$$\left| \frac{dV_C(t)}{dt} \right| = \frac{\epsilon}{RC}$$

Find Value of RC condition.

$$m(t) = B \cos \omega t$$

$$\epsilon(t) = u A \cos \omega m t$$

$$\begin{aligned} \epsilon(t) &= A + m(t) \\ &= A + u A \cos \omega m t \end{aligned}$$

$$\frac{d\epsilon(t)}{dt} = u A \omega m \sin \omega m t$$

$$\frac{\epsilon(1+u \cos \omega m t)}{RC} > u A \omega m \sin \omega m t$$