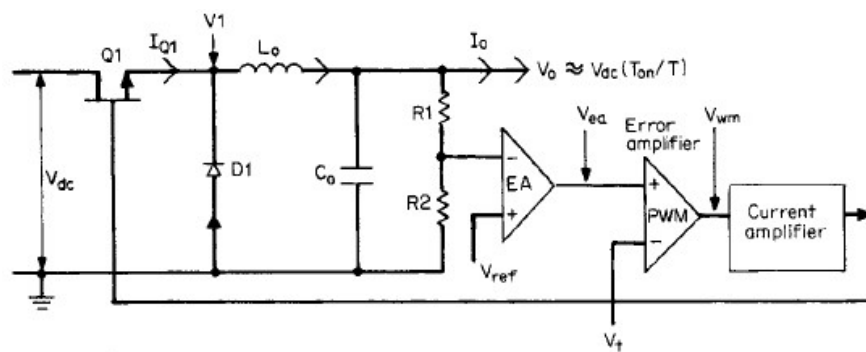


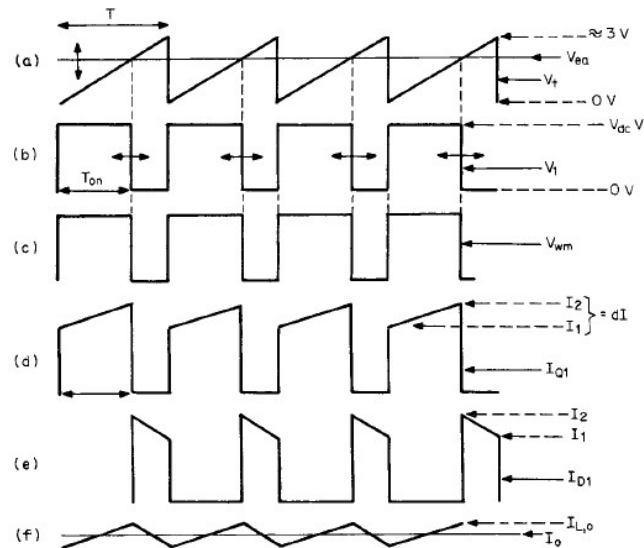
Switching Regulator Topologies

Dr. Tahir Izhar

The Buck Switching Regulator



Waveforms



Switching PS advantages

- 20 W/in³ compared to 0.3 W/in³ for linear PS.
- Multiple isolated output voltages from a single input.
- Low freq. Isolation Transformer not required.
- Efficiencies from 70% up to 95%.
- Some DC/DC converter designers are claiming load power densities of up to 50 W/in³ for the actual switching elements.

Conduction Loss and Efficiency

The average currents in $Q1$ and $D1$ is I_o .

These currents flow at a forward voltage of about 1 V over a wide range of currents.

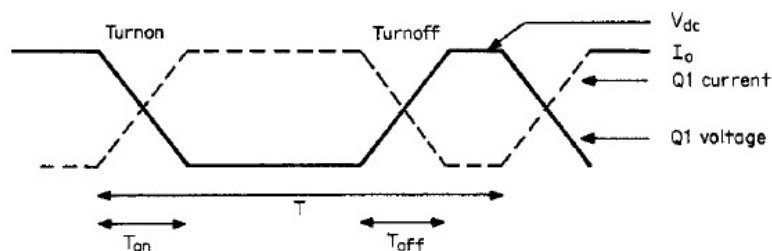
Thus conduction losses will be approximately

$$P_{dc} = L(Q1) + L(D1) = 1I_o \frac{T_{on}}{T} + 1I_o \frac{T_{off}}{T} = 1I_o$$

$$\text{Conduction Efficiency} = \frac{P_o}{P_o + \text{losses}} = \frac{V_o I_o}{V_o I_o + 1I_o} = \frac{V_o}{V_o + 1}$$

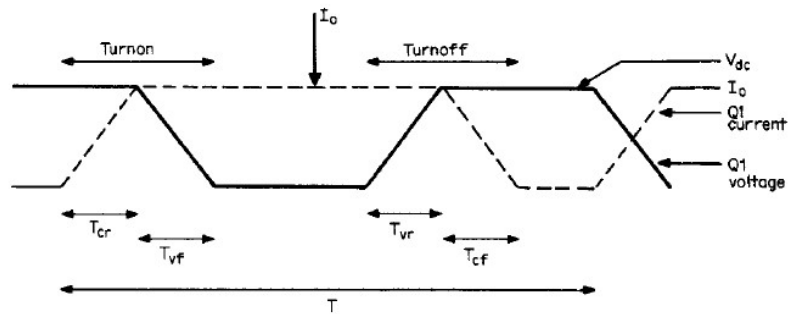
AC Switching Losses

Waveforms show the Best-case scenario



AC Switching Losses

Waveforms show the worst-case scenario



AC Switching Losses

For best-case scenario

$$P(T_{\text{on}}) = \int_0^{T_{\text{on}}} IV dt = I_o \bar{V}_{\text{dc}}/6$$

The power averaged over one complete period is

$$(I_o V_{\text{dc}}/6)(T_{\text{on}}/T)$$

$$P(T_{\text{off}}) = \int_0^{T_{\text{off}}} IV dt = I_o V_{\text{dc}}/6$$

AC Switching Losses

For best-case scenario

$$P(T_{\text{off}}) = \int_0^{T_{\text{off}}} IV \, dt = I_o V_{\text{dc}}/6$$

The power averaged over one complete period is

$$(I_o V_{\text{dc}}/6)(T_{\text{off}}/T)$$

Assuming

$$T_{\text{on}} = T_{\text{off}} = T_s$$

$$P_{\text{ac}} = (V_{\text{dc}} I_o T_s)/3T,$$

Efficiency

For Best-Case Scenario

$$\begin{aligned} \text{Efficiency} &= \frac{P_o}{P_o + \text{DC losses} + \text{AC losses}} \\ &= \frac{V_o I_o}{V_o I_o + I_o + V_{\text{dc}} I_o T_s/3T} \\ &= \frac{V_o}{V_o + 1 + V_{\text{dc}} T_s/3T} \end{aligned}$$

Efficiency

Assume the buck regulator provides 5 V from a 48-V DC input at 50-kHz switching frequency ($T = 20\mu\text{s}$) for $T_s = 0.3\mu\text{s}$ and $T = 20\mu\text{s}$

The switching-related efficiency is

$$\begin{aligned}\text{Efficiency} &= \frac{5}{5 + 1 + 48 \times 0.3/3 \times 20} \\ &= \frac{5}{5 + 1 + 0.24} = \frac{5}{5 + 1.24} \\ &= 80.1\%\end{aligned}$$

AC Switching Losses

For Worst-Case Scenario

$$P(T_{\text{on}}) = \frac{V_{\text{de}} I_o}{2} \frac{T_{\text{cr}}}{T} + \frac{I_o V_{\text{dc}}}{2} \frac{T_{\text{vf}}}{T}$$

The power averaged over one complete period is

Assuming

$$T_{\text{cr}} = T_{\text{vf}} = T_s, P(T_{\text{on}}) = V_{\text{dc}} I_o (T_s / T)$$

$$P_{\text{ac}} = 2V_{\text{dc}} I_o \frac{T_s}{T}$$

AC Switching Losses

For Worst-case scenario

The power averaged over one complete period is

Assuming

$$T_{cr} = T_{vf} = T_s, P(T_{on}) = V_{dc} I_o (T_s / T)$$

$$P_{ac} = 2 V_{dc} I_o \frac{T_s}{T}$$

AC Switching Losses

For Worst-case scenario

and the total losses (the sum of DC plus AC losses) will be

$$P_t = P_{dc} + P_{ac} = I_o + 2 V_{dc} I_o \frac{T_s}{T}$$

Efficiency

For Worst-case scenario

$$\begin{aligned}
 \text{Efficiency} &= \frac{P_o}{P_o + P_t} = \frac{V_o I_o}{V_o I_o + 1 I_o + 2 V_{dc} I_o T_s / T} \\
 &= \frac{V_o}{V_o + 1 + 2 V_{dc} T_s / T} \\
 \text{Efficiency} &= \frac{5}{5 + 1 + 2 \times 48 \times 0.3 / 20} = \frac{5}{5 + 1 + 1.44} \\
 &= \frac{5}{5 + 1 + 2.44} \\
 &= 67.2\%
 \end{aligned}$$

Conclusion

Comparing this with a linear regulator doing the same job (bringing 48 V down to 5 V), its efficiency would be $V_o/V_{dc}(\text{max})$, or 5/48; this is only 10.4% and is clearly unacceptable.