**Reviewer: 1**

**Comment 1:**

It is important for authors to show how eq. (6) was derived (linearised) from the LLG equation, and what are the contributions taken for the effective field (applied, anisotropy, exchange, magnetostatics, eddy current etc.?).  The authors also need to clarify what Gamma is in this equation (in the LLG equation it should be the gyromagnetic ratio, not a damping factor).  The authors also need to clarify how they obtained the susceptibility tensor in (7) from (6).

**Answer 1:**

I have made these corrections in Section II.

1. I have explained the derivation of linearized Landau Lifshitz Gilbert equation (Equation (8) in the revised paper) from LLG equation (Equation (6) in the revised paper). It was assumed that magnetization has a large static term parallel to the DC bias and a small perturbation term. I have explained that only applied field contributions were considered for the effective magnetic field. Non-local effects like eddy currents, long-range dipole-dipole interactions and exchange interactions between non-neighboring dipoles were not considered.
2. I have explained that Gamma symbol is the gyromagnetic ratio in the LLG equation (Equation (6) in the revised paper). Gamma symbol was used as a loss factor in MEEP documentation and it caused confusion with gyromagnetic ratio, so I have replaced it with the complete form.
3. I have explained how the susceptibility tensor was derived from the linearized Landau Lifshitz Gilbert equation (Equation (8) in the revised paper) by assuming time harmonic dependence for magnetization and magnetic field intensity.

**Comment 2:**

It is not clear in Section II what material is assumed and what parameters values were used to determine the susceptibility (e.g. how did the authors work out wo - resonance frequency in (7) and Fig. 3? what was the assumed resonance mechanism and effective field contributions?). Did the authors use micromagnetic boundary conditions for the ferrite structure?

**Answer 2:**

I have made these corrections in Section II:

1. I have explained that permalloy ferromagnet sample was used for the simulation. I have also stated the following electromagnetic parameters: angular frequency of precession, saturation magnetization, Gilbert damping constant and relative permittivity. I assumed that the resonance frequency was 30-GHz based on gyromagnetic ratio 3.8MHz/T and applied bias field strength 1000A/m. Nickel: (493000/797700)\*(3.81e6)/(2\*pi\*1e9).
2. I have explained that only applied field contributions were considered for the effective magnetic field. Non-local effects like eddy currents, long-range dipole-dipole interactions and exchange interactions between non-neighboring dipoles were not considered.
3. I have explained that resonance occurred due to ferromagnetic resonance of the Larmor precession. Ferromagnetic resonance arises from the precessional motion of the magnetization of a ferromagnetic material in an external magnetic field. The magnetic field exerts a torque on the sample magnetization which causes the magnetic moments in the sample to precess.

I have made these corrections in Section III:

1. I have explained that the tangential components and normal components of the magnetic field were continuous on the boundaries of the magnetic structure.

**Comment 3:**

The authors also need to make it clear in Section II that the form of the permeability/susceptibility is enforced (preset) and not an outcome of the simulations (for example in contrast to rigorous combined simulations of micromagnetics and electromagnetics in Aziz PIER B, Vol. 15, 1–29, 2009 where the magnetisation is actually computed).  In this case, the calculated impedance and transmission characteristics of the transmission line/waveguide are pre-determined since the resonance frequency and permeability are set!

**Answer 3:**

I have made these corrections in Section II and III:

1. I have explained that permeability/ susceptibility was enforced and not an outcome of the simulations. Hence, the calculated impedance and transmission characteristics of the transmission line were pre-determined since the resonance frequency and permeability were preset.

**Comment 4:**

In Section III, the authors need to clearly define the geometry and dimensions of the simulated structure, the ferrite material used and material parameters (e.g. magnetic and electromagnetic).  The authors also need to specify the numerical parameters (grid cell size, time step, location of transmission line from PML, number of cells in PML .. etc.).  The source is not clear: is it a z-directed electrical current in the transmission line or is it a z-directed plane wave?  Also, what is the justification for using a 60 GHz pulse for the source (why not 10 GHz or 100 GHz)?  The authors also need to specify the magnitude and direction of the bias (DC) field.

**Answer 4:**

I have made these corrections in Section III:

1. I have explained that the grid was divided into a 3-D array of cubic cells with the dimensions 100nm × 100 nm × 100nm. The magnetized ferromagnetic sample had the dimensions 400nm × 400nm × 230um. The time step was chosen as ∆t=(1/6)fs. A perfectly matched boundary layer with 1600 cells was added on both ends of the transmission line. The perfectly matched boundary layer had a width of 10um. The perfectly matched boundary layer had a width of 10um. The z-axis bias magnetic field had a magnitude of 10^4 A/m.
2. I have explained that the sample permalloy ferromagnet used for the simulation had the following parameters: angular frequency of precession ω\_0 = 2π×30-GHz, saturation magnetization M\_s = 1.1×10^6 A/m , Gilbert damping constant α = 10^(-5)-10^(-2) and relative permittivity ε\_r = 1.5.
3. I have explained that a Gaussian soft magnetic current source (oscillating magnetic dipole) was placed in the magnetized ferrite. The Fourier transform of the source is plotted in Figure 5 for the frequency range 0-60 GHz. The oscillating magnetic dipole launched a z-directed wave which was linearly polarized in x-direction.

**Comment 5:**

The authors in page 5 make the statements "The phase constant and attenuation constant were calculated for the resultant magnetic spin wave" and "The nano-magnetic exchange interactions and dipole-dipole interactions dictated the excitation of spin wave modes".  There was no indication in Sections II or III in the article that the exchange contribution was taken into account (or how it was taken into account) - I assume since the material is saturated here, so how are spin-waves produced?  (even if the authors refer to magnetostatic waves, then the authors don't actually calculate the magnetostatic fields as they don't compute M directly)?  The authors need to clarify these statements.

**Answer 5:**

Ferromagnet is saturated but the 30-GHz ferromagnetic resonance causes the non-diagonal entries in the susceptibility matrix to become very large. This makes it skew symmetric. This gives rise to gyromagnetic resonance/ spin wave resonance. The propagation of spin waves is dictated by the Landau Lifshitz Gilbert equation. The linewidths of absorption peaks can be greatly affected by dipolar-narrowing and exchange-broadening (quantum) effects.

**Comment 6:**

The authors need to indicate (in the figure captions) the frequencies at which the quantities in Figures 4, 5, 6 and 7 were calculated.

**Answer 6:**

I have edited the captions for Figures 4, 5, 6 and 7. The quantities were calculated at the ferromagnetic resonance frequency of 30 GHz.

**Comment 7:**

The authors also need to comment on or indicate the purpose of the equivalent circuit model they introduced in Section I with the FDTD simulations.

**Answer 7:**

I have made the following corrections in Section IV:

1. I have explained the purpose of equivalent magnetic circuit model introduced in Section I. From the results of micromagnetic finite difference time domain simulations, the longitudinal magnetic admittance and transverse magnetic impedance were calculated using (4) - (5). In Figure 2, the per unit length transverse magnetic inductance represents a magnetic energy storage element storing magnetic flux; the per unit length longitudinal capacitance represents an electric energy storage element; and the per unit length magnetic conductance dissipates energy.
2. As seen in Figure 8, the longitudinal magnetic admittance dropped during ferromagnetic resonance hence it provided a low reluctance path for magnetic flux. From Figure 9, it was derived that the magnetic flux leakage was reduced because the transverse magnetic impedance increased.
3. When the Gilbert damping constant was increased, the effective magnetic susceptibility decreased, the magnetic reluctance increased and the absorption of magnetic flux dropped. As seen in Figure 8, this resulted in an increase in the longitudinal magnetic admittance. Meanwhile, the magnetic flux leakage increased which resulted in the drop of transverse magnetic impedance in Figure 9.

**Comment 8:**

Minor typing errors:  
 - Abbreviations must be defined in the text (e.g. EHF, TEM, .. etc.).  
 - Page 2, paragraph 2, "FDTD simulations .. "

**Answer 8:**

I have defined the abbreviations EHF, TEM, FDTD, FDFD, MEEP at the point they are first used.

**Reviewer: 2**

**Comment 1:**

The acronyms EHF, FDFD, FDTD, MEEP are used without prior description and must be defined at the point they are first used.

**Answer 1:**

I have defined the abbreviations EHF, TEM, FDTD, FDFD, MEEP at the point they are first used.

**Comment 2:**

The use of adjectives such as the word "huge" in the second paragraph of the Simulation Results section must be removed.

**Answer 2:**

I have removed the adjective “huge” in the second paragraph of the Simulation Results section.