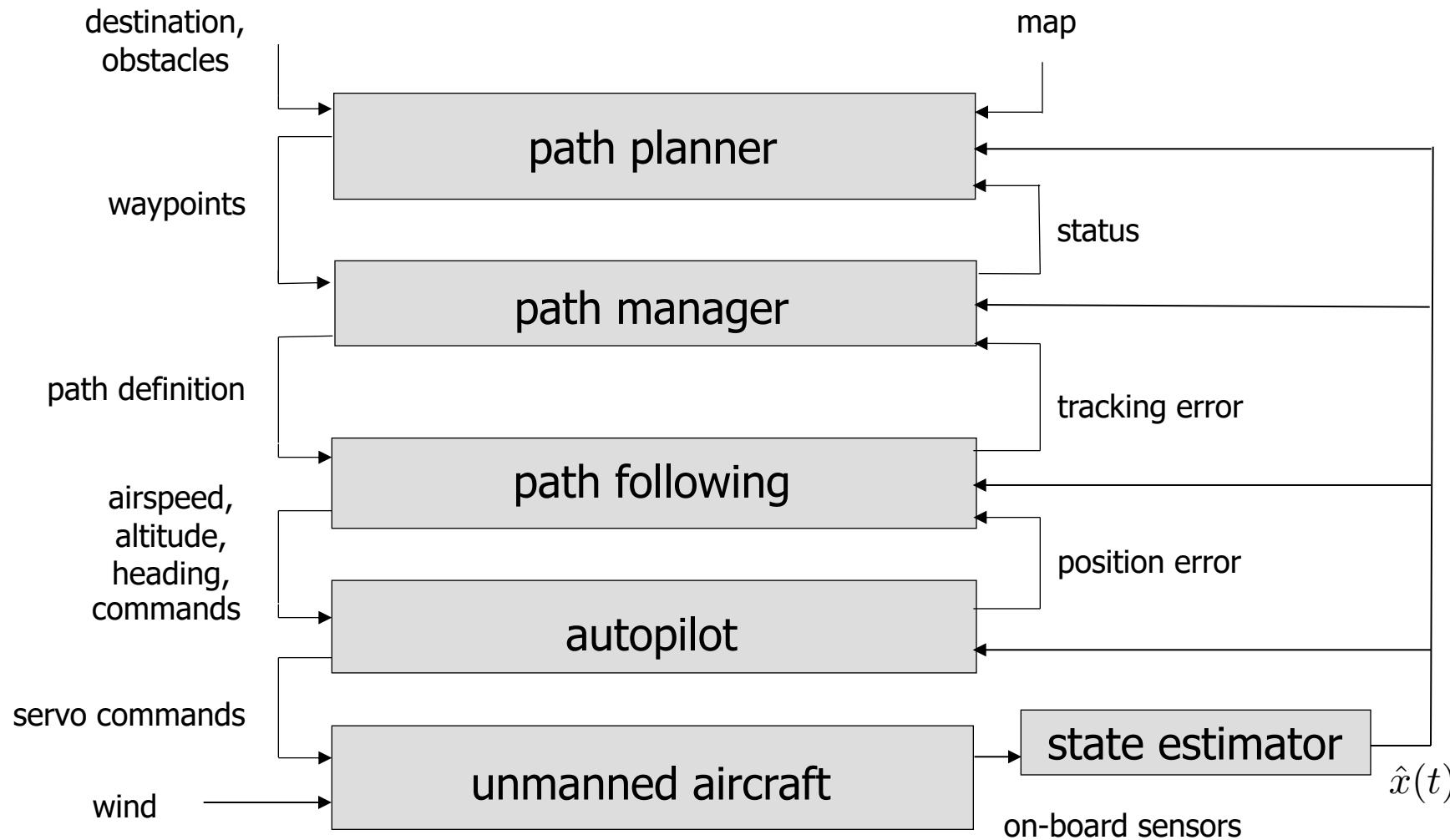
A photograph of a yellow and black glider plane flying from left to right across a vast, open landscape. The sky is filled with large, white, billowing clouds against a blue background. In the foreground, there's a field of tall grass or crops. In the distance, a small farm with several buildings and a windmill is visible.

# Chapter 11

Path Manager

# Control Architecture

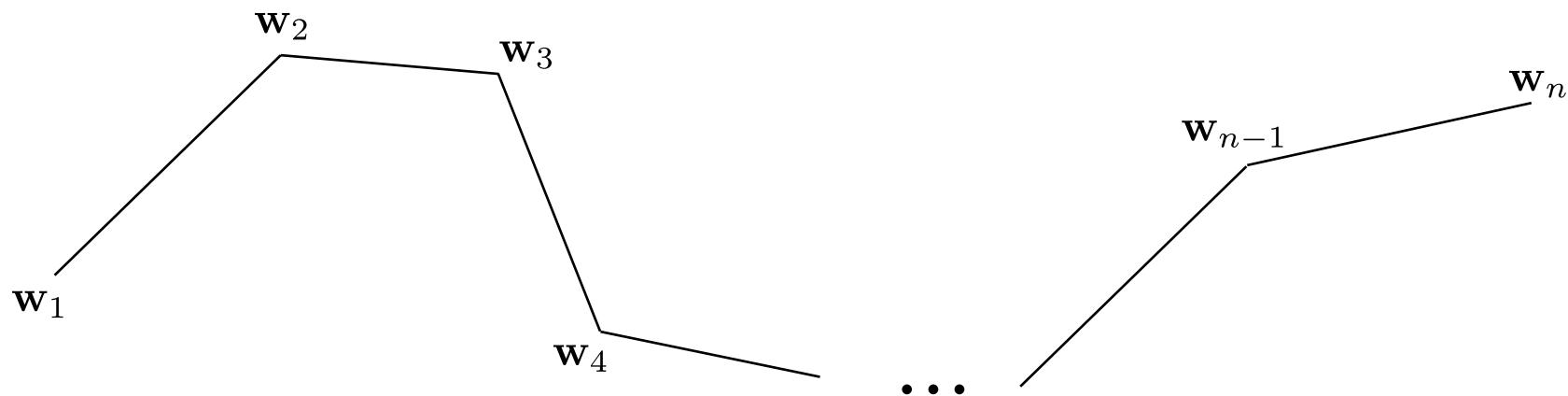


# Path Definition

Waypoint path defined as ordered sequence of waypoints

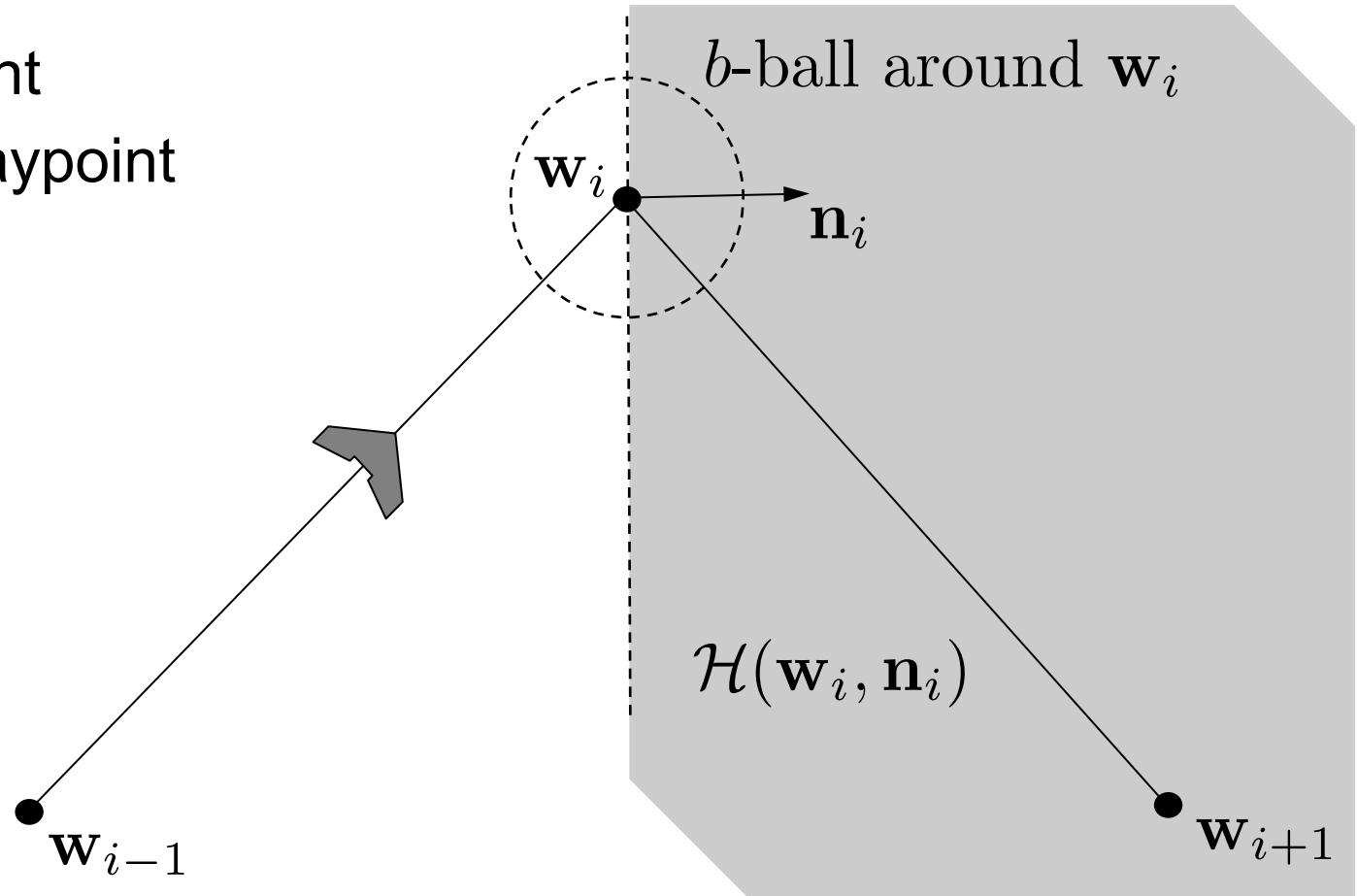
$$\mathcal{W} = \{\mathbf{w}_1, \mathbf{w}_2, \dots, \mathbf{w}_N\}$$

where  $\mathbf{w}_i = (w_{n,i}, w_{e,i}, w_{d,i})^\top \in \mathbb{R}^3$ .



# Waypoint Switching

- Two methods
  - $b$ -ball around waypoint
  - half plane through waypoint



# Waypoint Switching

Given point  $\mathbf{r} \in \mathbb{R}^3$  and normal vector  $\mathbf{n} \in \mathbb{R}^3$ , define half plane

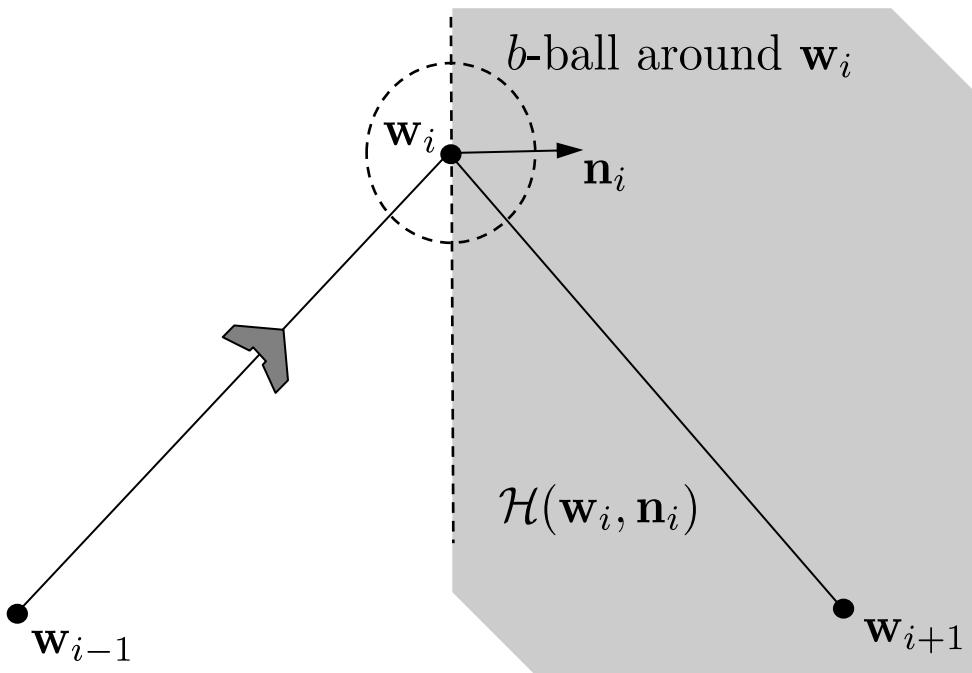
$$\mathcal{H}(\mathbf{r}, \mathbf{n}) \triangleq \{\mathbf{p} \in \mathbb{R}^3 : (\mathbf{p} - \mathbf{r})^\top \mathbf{n} \geq 0\}$$

Define unit vector pointing in direction of line  $\overline{\mathbf{w}_i \mathbf{w}_{i+1}}$  as

$$\mathbf{q}_i \triangleq \frac{\mathbf{w}_{i+1} - \mathbf{w}_i}{\|\mathbf{w}_{i+1} - \mathbf{w}_i\|}$$

Unit normal to the 3-D half plane that separates the line  $\overline{\mathbf{w}_{i-1} \mathbf{w}_i}$  from the line  $\overline{\mathbf{w}_i \mathbf{w}_{i+1}}$  is given by

$$\mathbf{n}_i \triangleq \frac{\mathbf{q}_{i-1} + \mathbf{q}_i}{\|\mathbf{q}_{i-1} + \mathbf{q}_i\|}$$



MAV tracks straight-line path from  $\mathbf{w}_{i-1}$  to  $\mathbf{w}_i$  until it enters  $\mathcal{H}(\mathbf{w}_i, \mathbf{n}_i)$ , at which point it will track straight-line path from  $\mathbf{w}_i$  to  $\mathbf{w}_{i+1}$

# Waypoint Following

---

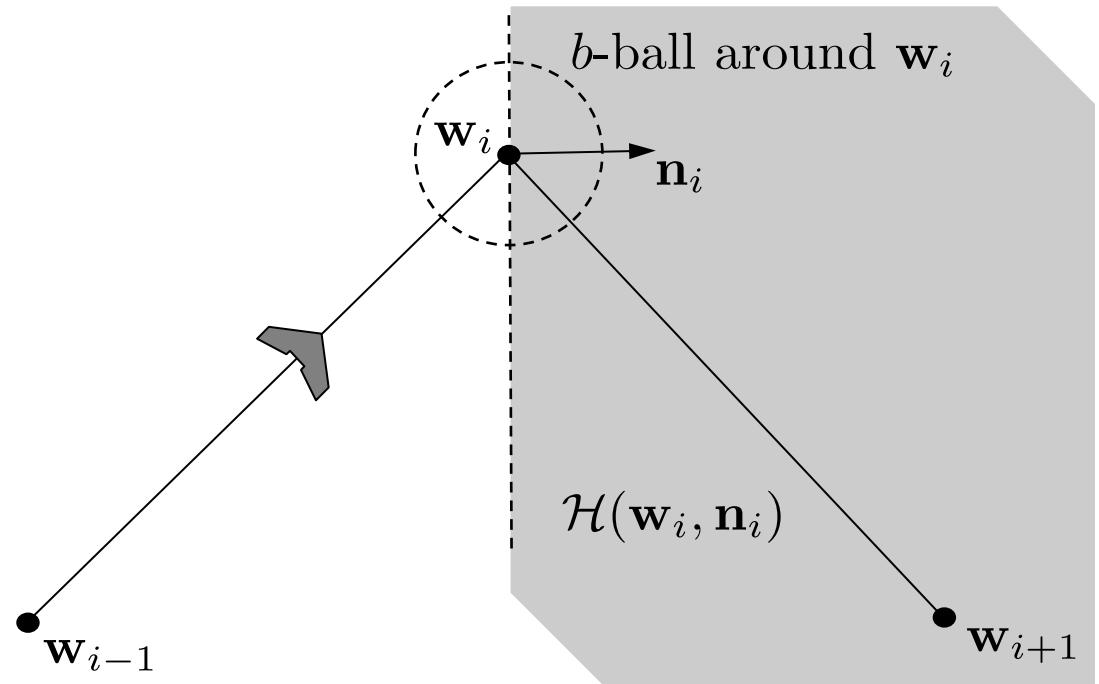
**Algorithm 5** Follow Waypoints:  $(\mathbf{r}, \mathbf{q}) = \text{followWpp}(\mathcal{W}, \mathbf{p})$

---

**Input:** Waypoint path  $\mathcal{W} = \{\mathbf{w}_1, \dots, \mathbf{w}_N\}$ , MAV position  
 $\mathbf{p} = (p_n, p_e, p_d)^\top$ .

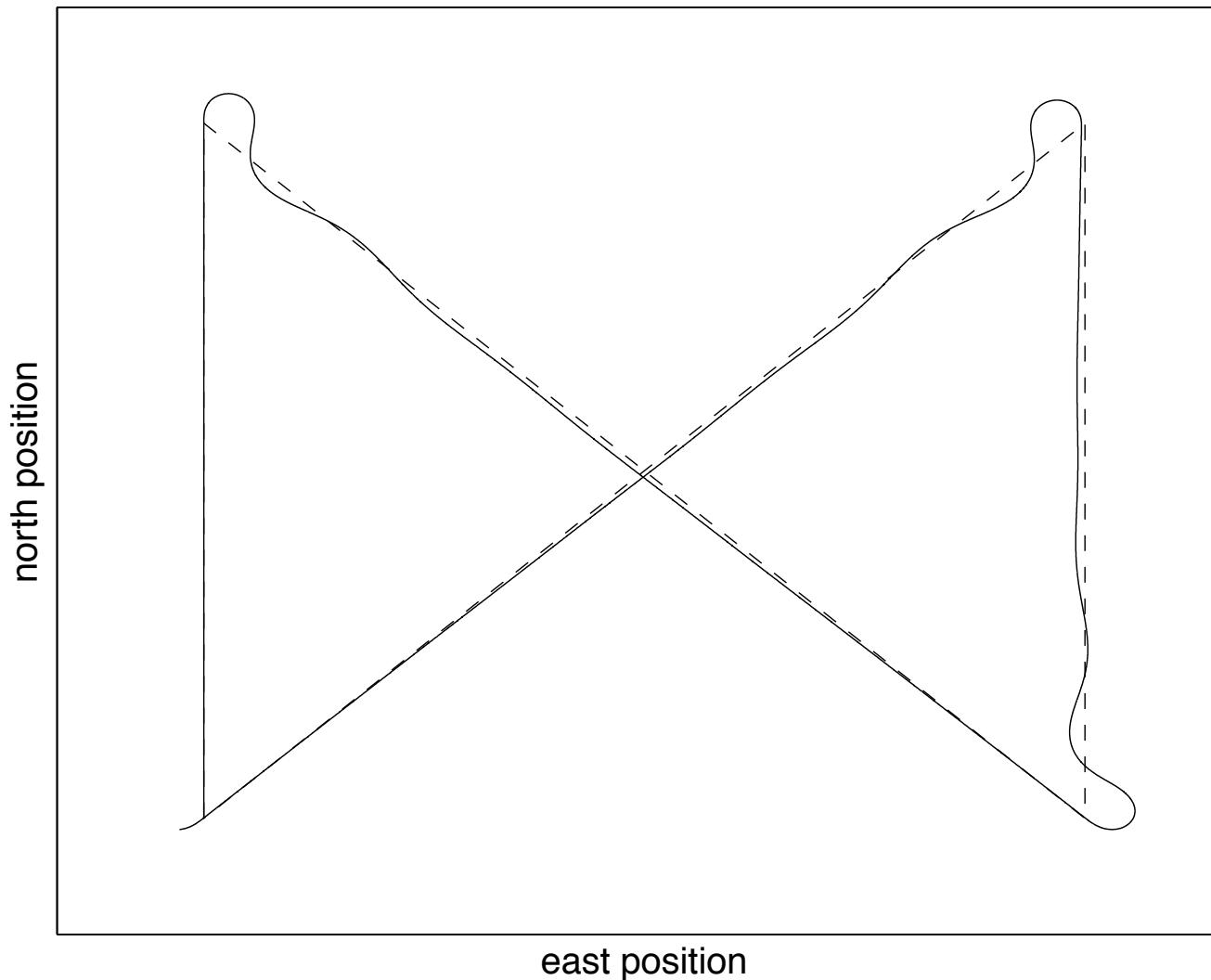
**Require:**  $N \geq 3$

- 1: **if** New waypoint path  $\mathcal{W}$  is received **then**
  - 2:   Initialize waypoint index:  $i \leftarrow 2$
  - 3: **end if**
  - 4:  $\mathbf{r} \leftarrow \mathbf{w}_{i-1}$
  - 5:  $\mathbf{q}_{i-1} \leftarrow \frac{\mathbf{w}_i - \mathbf{w}_{i-1}}{\|\mathbf{w}_i - \mathbf{w}_{i-1}\|}$
  - 6:  $\mathbf{q}_i \leftarrow \frac{\mathbf{w}_{i+1} - \mathbf{w}_i}{\|\mathbf{w}_{i+1} - \mathbf{w}_i\|}$
  - 7:  $\mathbf{n}_i \leftarrow \frac{\mathbf{q}_{i-1} + \mathbf{q}_i}{\|\mathbf{q}_{i-1} + \mathbf{q}_i\|}$
  - 8: **if**  $\mathbf{p} \in \mathcal{H}(\mathbf{w}_i, \mathbf{n}_i)$  **then**
  - 9:   Increment  $i \leftarrow (i + 1)$  until  $i = N - 1$
  - 10: **end if**
  - 11: **return**  $\mathbf{r}, \mathbf{q} = \mathbf{q}_{i-1}$  at each time step
- 



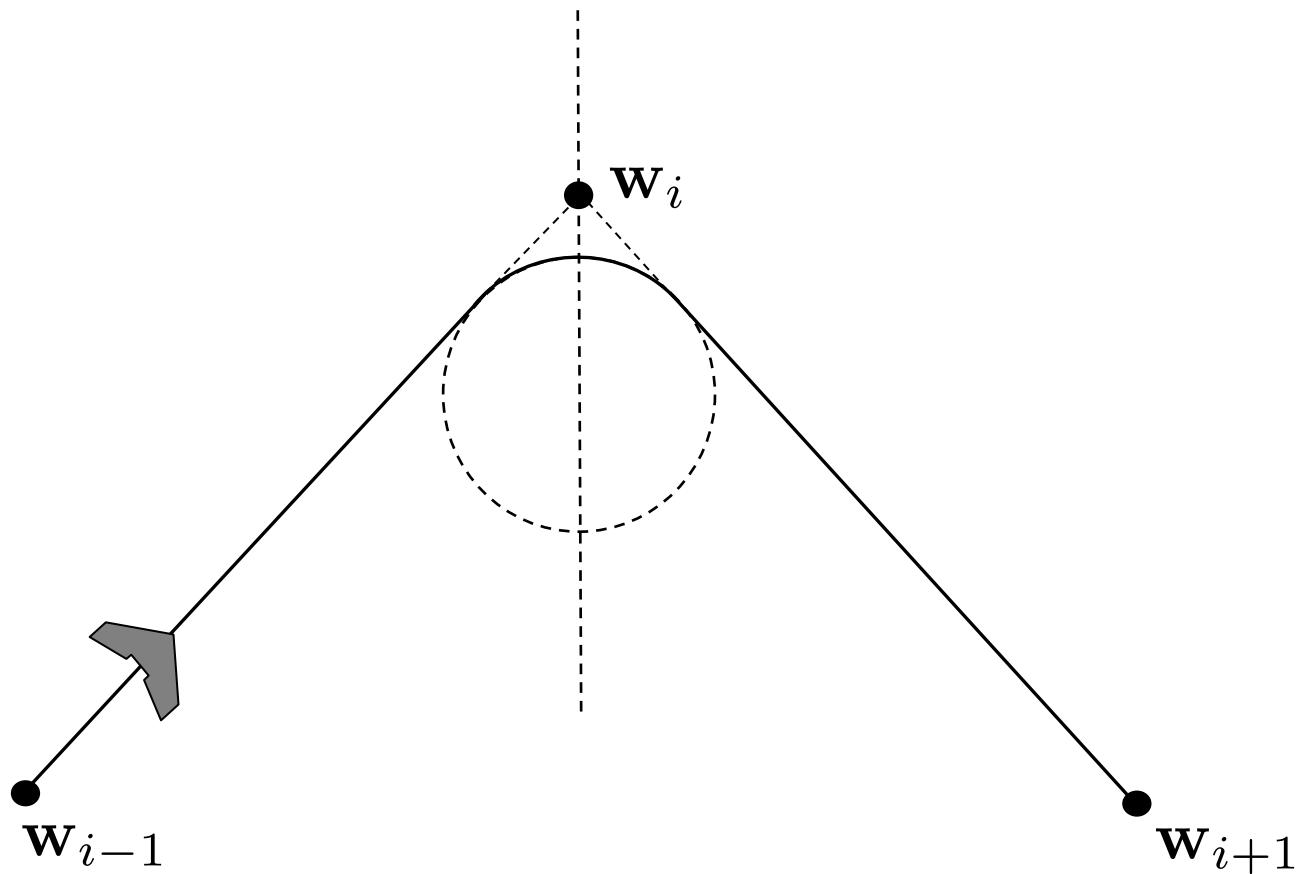
# Waypoint Following Results

Path Manager – Straight Line

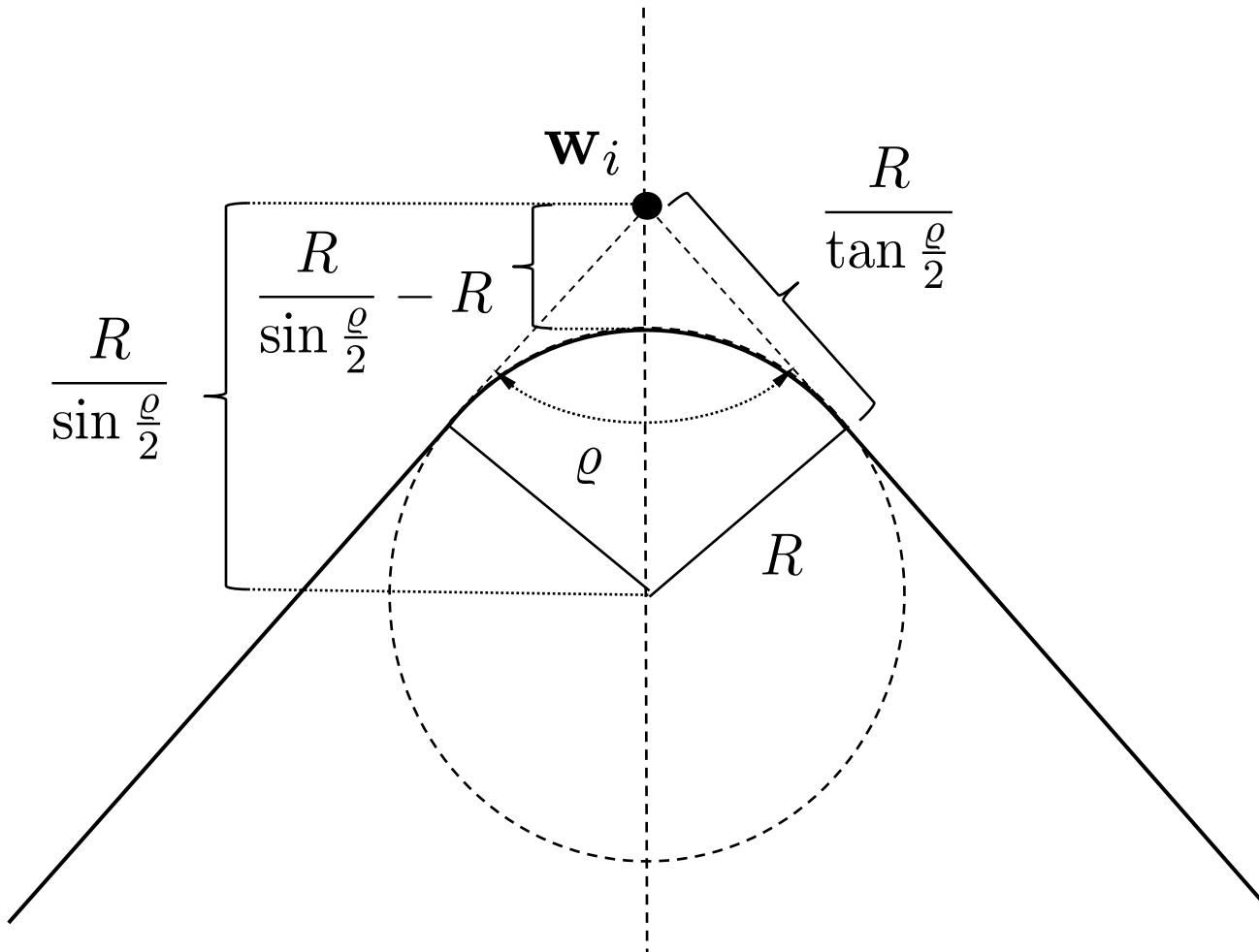


# Fillet Transition

Transition between path segments can be smoothed by adding a fillet



# Fillet Geometry



# Fillet Smoothing Half Planes

Fillet center defined as

$$\mathbf{c} = \mathbf{w}_i - \left( \frac{R}{\sin \frac{\varrho}{2}} \right) \frac{\mathbf{q}_{i-1} - \mathbf{q}_i}{\|\mathbf{q}_{i-1} - \mathbf{q}_i\|}$$

Half plane  $\mathcal{H}_1$  is defined by location

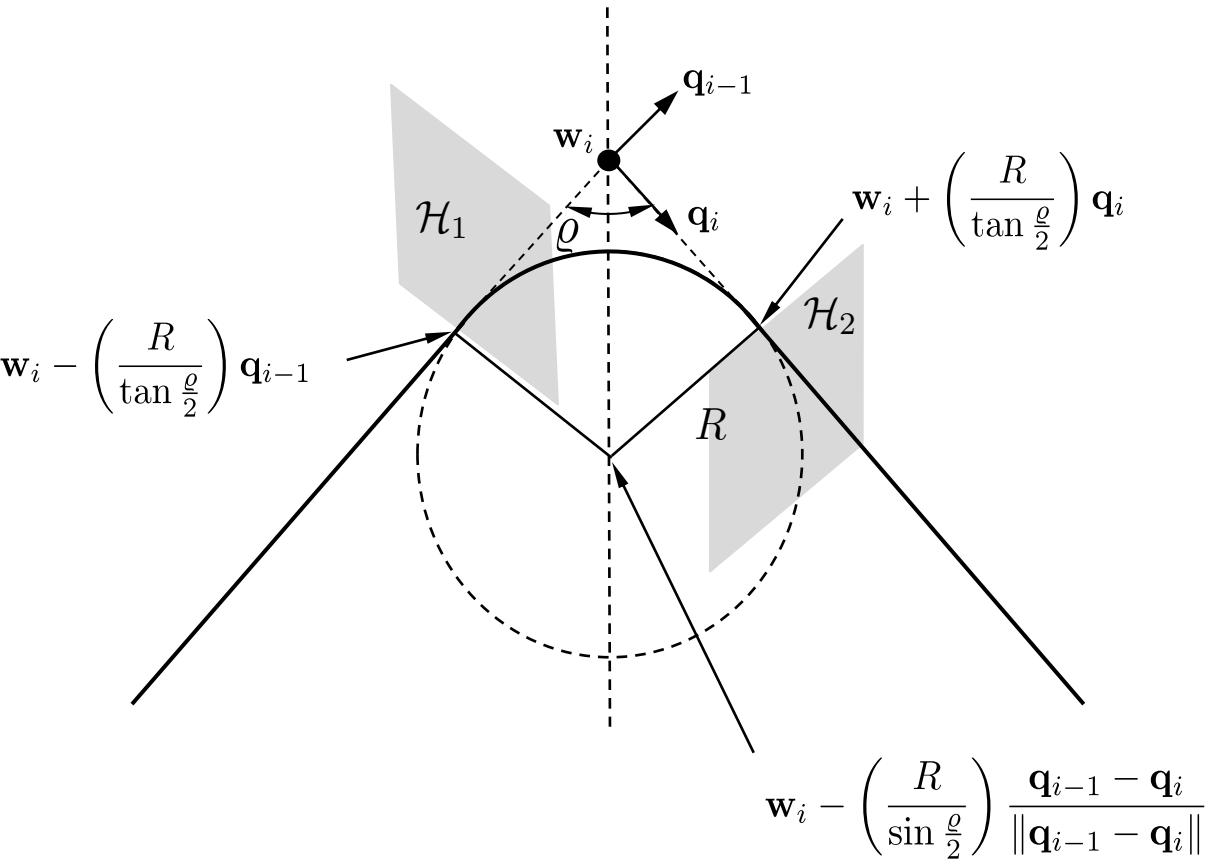
$$\mathbf{r}_1 = \mathbf{w}_i - \left( \frac{R}{\tan \frac{\varrho}{2}} \right) \mathbf{q}_{i-1}$$

and normal vector  $\mathbf{q}_{i-1}$

Half plane  $\mathcal{H}_2$  is defined by location

$$\mathbf{r}_2 = \mathbf{w}_i + \left( \frac{R}{\tan \frac{\varrho}{2}} \right) \mathbf{q}_i$$

and normal vector  $\mathbf{q}_i$



# Waypoint Following with Fillets

---

**Algorithm 1** Follow Waypoints with Fillets:  $(\text{flag}, \mathbf{r}, \mathbf{q}, \mathbf{c}, \rho, \lambda) = \text{followWppFillet}(\mathcal{W}, \mathbf{p}, R)$

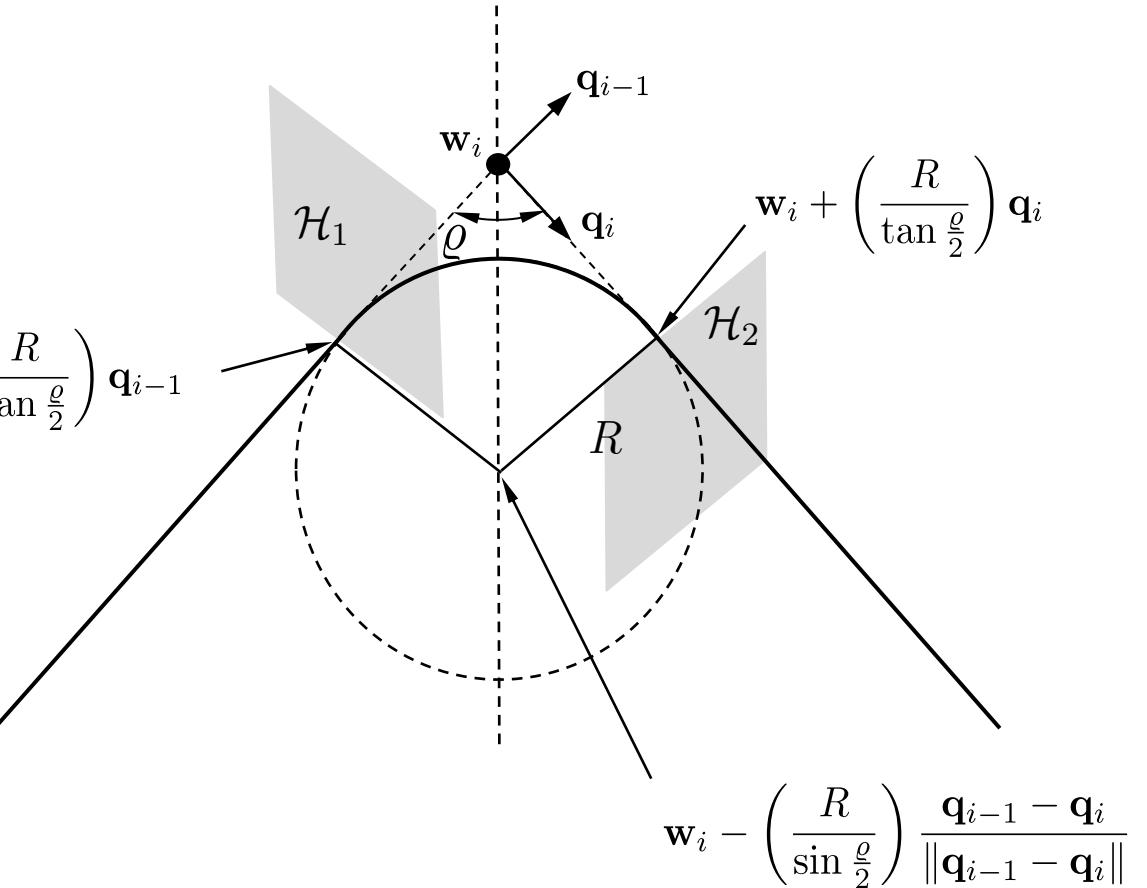
**Ensure:** Waypoint path  $\mathcal{W} = \{\mathbf{w}_1, \dots, \mathbf{w}_N\}$ , MAV position  $\mathbf{p} = (p_n, p_e, p_d)^\top$ , fillet radius  $R$ .

**Require:**  $N \geq 3$ .

```

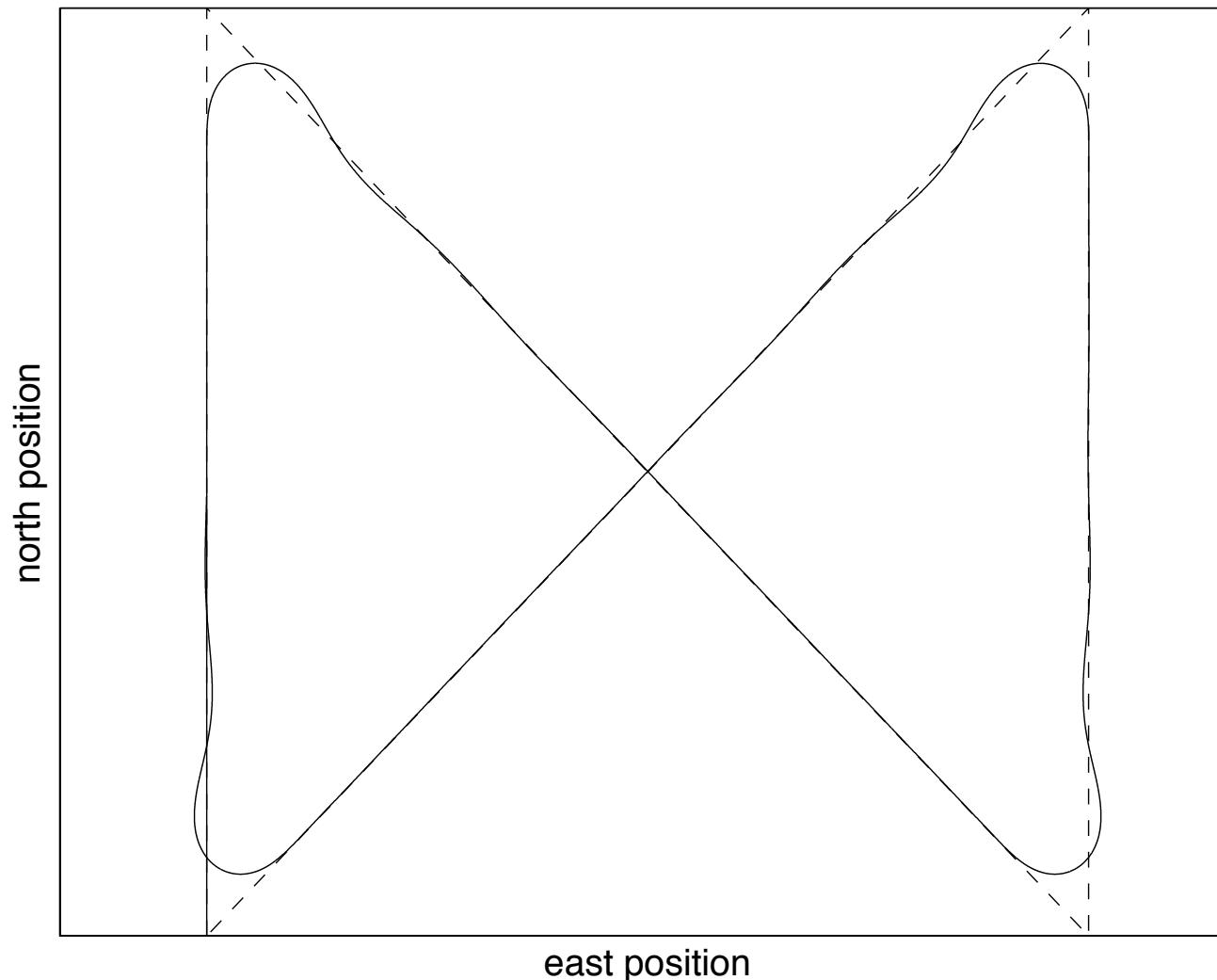
1: if New waypoint path  $\mathcal{W}$  is received then
2:   Initialize waypoint index:  $i \leftarrow 2$ , and state machine: state  $\leftarrow 1$ .
3: end if
4:  $\mathbf{q}_{i-1} \leftarrow \frac{\mathbf{w}_i - \mathbf{w}_{i-1}}{\|\mathbf{w}_i - \mathbf{w}_{i-1}\|}$ .
5:  $\mathbf{q}_i \leftarrow \frac{\mathbf{w}_{i+1} - \mathbf{w}_i}{\|\mathbf{w}_{i+1} - \mathbf{w}_i\|}$ .
6:  $\varrho \leftarrow \cos^{-1}(-\mathbf{q}_{i-1}^\top \mathbf{q}_i)$ .
7: if state = 1 then
8:   flag  $\leftarrow 1$ 
9:    $\mathbf{r} \leftarrow \mathbf{w}_{i-1}$ 
10:   $\mathbf{q} \leftarrow \mathbf{q}_{i-1}$ 
11:   $\mathbf{z} \leftarrow \mathbf{w}_i - \left(\frac{R}{\tan(\varrho/2)}\right) \mathbf{q}_{i-1}$ 
12:  if  $\mathbf{p} \in \mathcal{H}(\mathbf{z}, \mathbf{q}_{i-1})$  then
13:    state  $\leftarrow 2$ 
14:  end if
15: else if state = 2 then
16:   flag  $\leftarrow 2$ 
17:    $\mathbf{c} \leftarrow \mathbf{w}_i - \left(\frac{R}{\sin(\varrho/2)}\right) \frac{\mathbf{q}_{i-1} - \mathbf{q}_i}{\|\mathbf{q}_{i-1} - \mathbf{q}_i\|}$ 
18:    $\rho \leftarrow R$ 
19:    $\lambda \leftarrow \text{sign}(q_{i-1,n} q_{i,e} - q_{i-1,e} q_{i,n})$ .
20:    $\mathbf{z} \leftarrow \mathbf{w}_i + \left(\frac{R}{\tan(\varrho/2)}\right) \mathbf{q}_i$ 
21:   if  $\mathbf{p} \in \mathcal{H}(\mathbf{z}, \mathbf{q}_i)$  then
22:      $i \leftarrow (i+1)$  until  $i = N-1$ .
23:     state  $\leftarrow 1$ 
24:   end if
25: end if
26: return flag,  $\mathbf{r}$ ,  $\mathbf{q}$ ,  $\mathbf{c}$ ,  $\rho$ ,  $\lambda$ .

```



# Waypoint Following with Fillets

Path Manager – Fillets



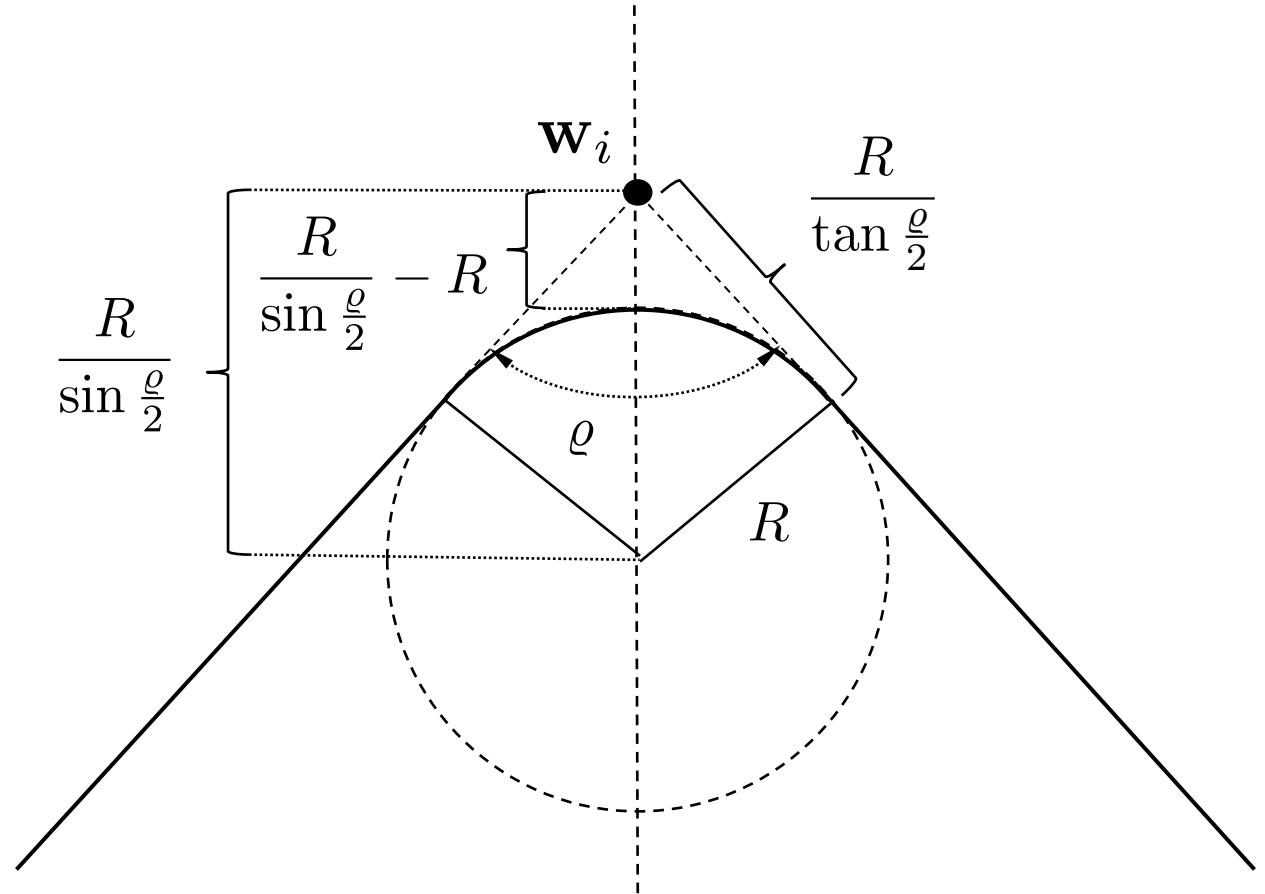
# Fillet Path Length

Straight-line path length (no fillets):

$$|\mathcal{W}| \triangleq \sum_{i=2}^N \|\mathbf{w}_i - \mathbf{w}_{i-1}\|.$$

Path length with fillets:

$$|\mathcal{W}|_F = |\mathcal{W}| + \sum_{i=2}^N \left( R\varrho_i - \frac{2R}{\tan \frac{\varrho_i}{2}} \right).$$



# Dubins Paths

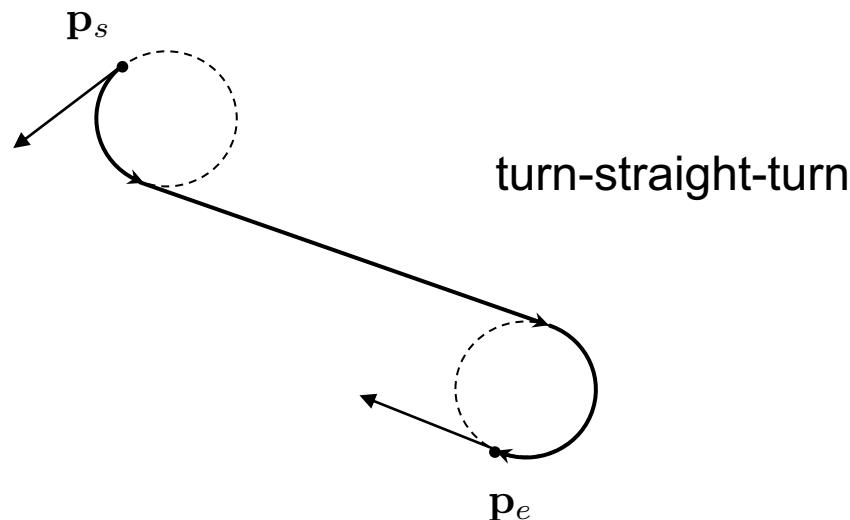
For vehicle with kinematics given by

$$\dot{p}_n = V \cos \vartheta$$

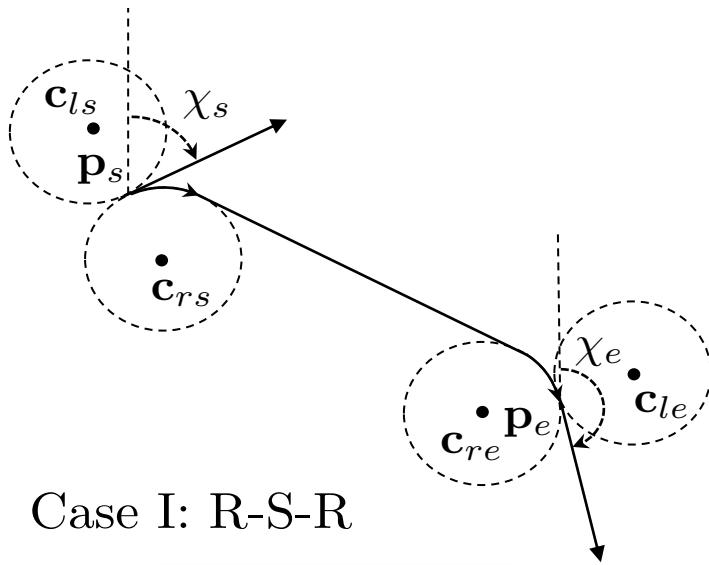
$$\dot{p}_e = V \sin \vartheta$$

$$\dot{\vartheta} = u,$$

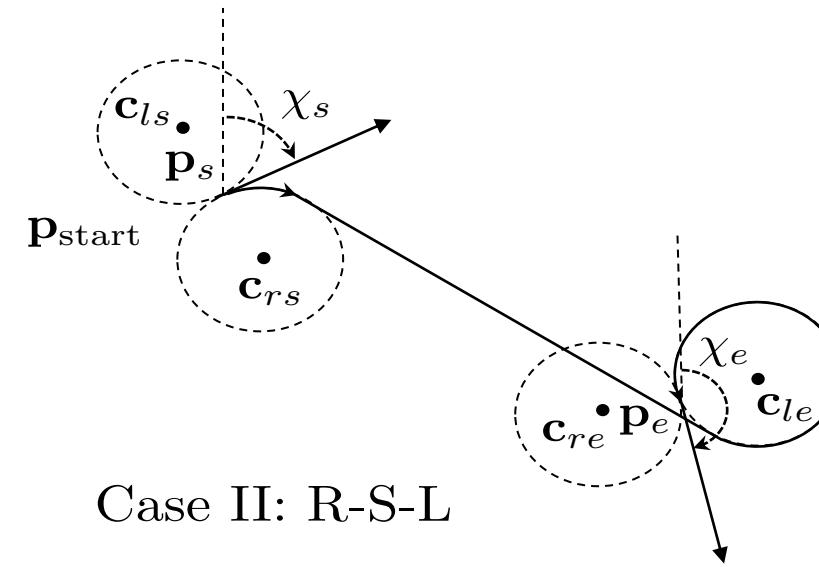
where  $V$  is constant and  $u \in [-\bar{u}, \bar{u}]$ , time-optimal path between two different configurations consists of circular arc, followed by straight line, and concluding with another circular arc to the final configuration, where the radius of the circular arcs is  $V/\bar{u}$ .



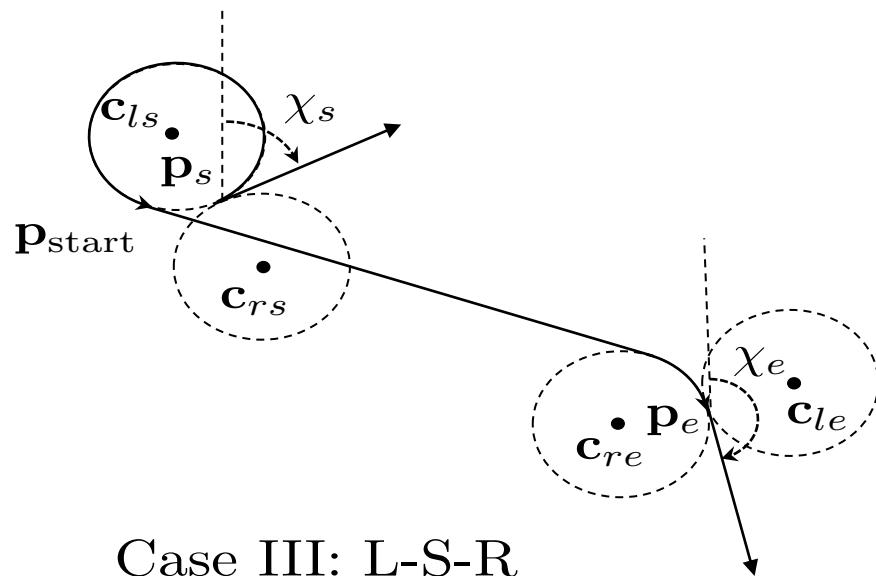
# Dubins path is defined as shortest of four cases



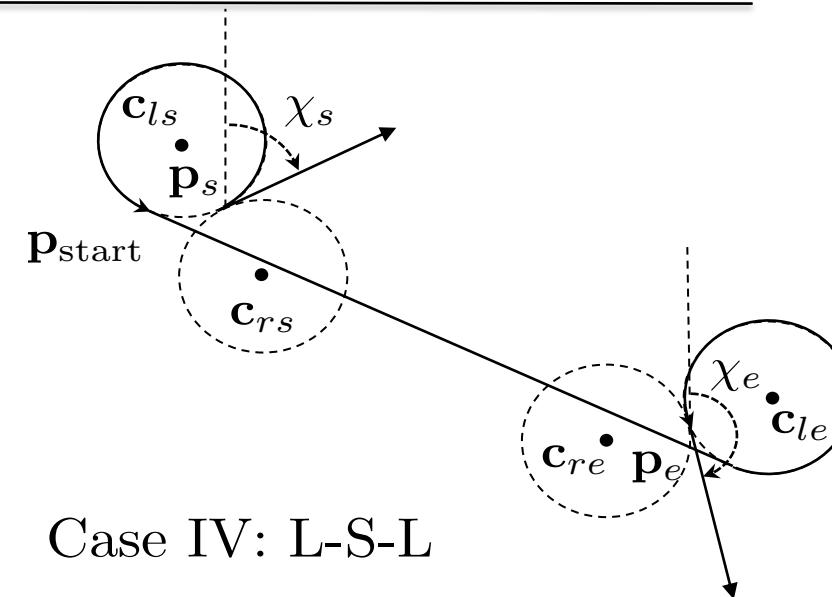
Case I: R-S-R



Case II: R-S-L



Case III: L-S-R



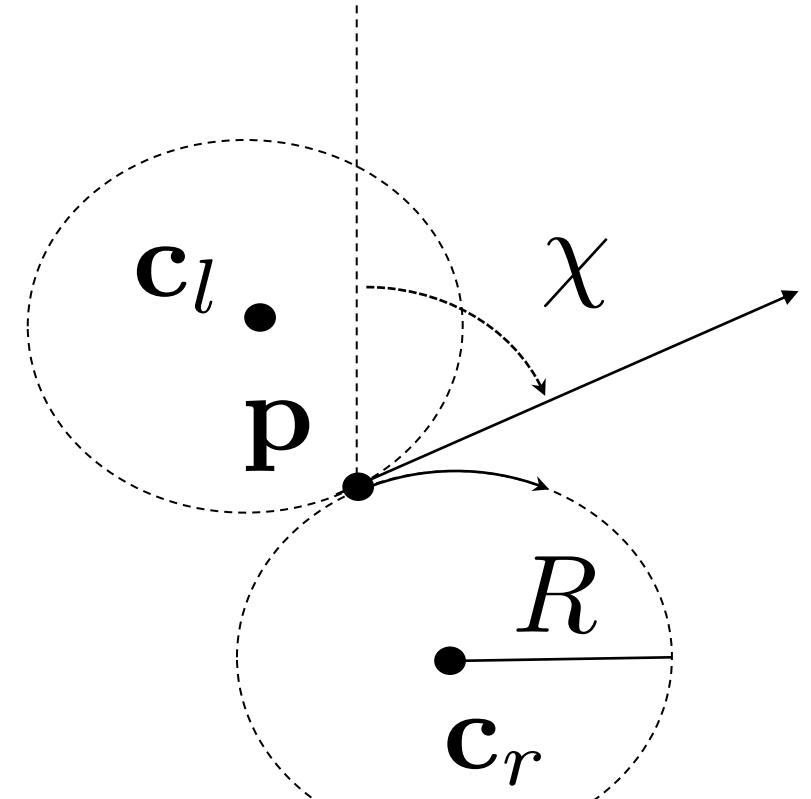
Case IV: L-S-L

# Path Length Preliminaries

Given position  $\mathbf{p}$ , course  $\chi$ , and radius  $R$ , centers of right and left turning circles are given by

$$\mathbf{c}_r = \mathbf{p} + R \left( \cos\left(\chi + \frac{\pi}{2}\right), \sin\left(\chi + \frac{\pi}{2}\right), 0 \right)^\top$$

$$\mathbf{c}_l = \mathbf{p} + R \left( \cos\left(\chi - \frac{\pi}{2}\right), \sin\left(\chi - \frac{\pi}{2}\right), 0 \right)^\top$$



# Path Length Preliminaries

$$\langle 2\pi + \vartheta_2 - \vartheta_1 \rangle$$

For clockwise circles, angular distance between  $\vartheta_1$  and  $\vartheta_2$  given by

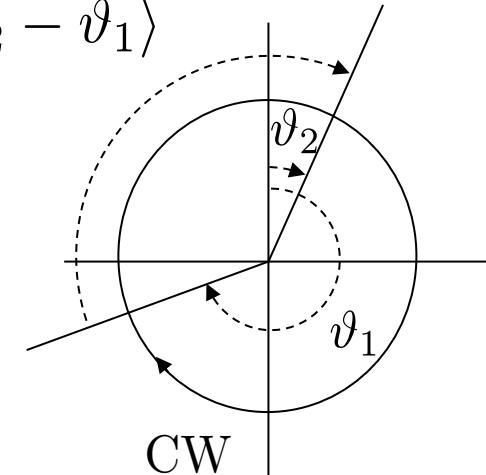
$$|\vartheta_2 - \vartheta_1|_{CW} \triangleq \langle 2\pi + \vartheta_2 - \vartheta_1 \rangle,$$

where

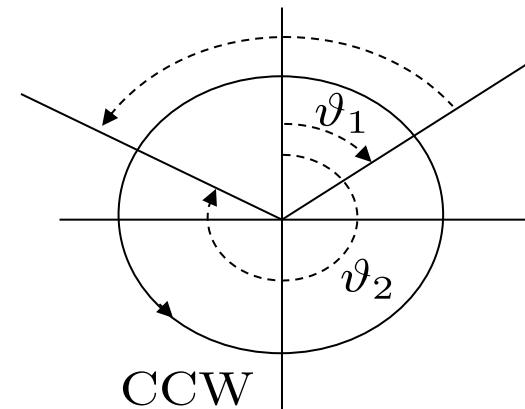
$$\langle \varphi \rangle \triangleq \varphi \mod 2\pi$$

For counter clockwise circles,

$$|\vartheta_2 - \vartheta_1|_{CCW} \triangleq \langle 2\pi - \vartheta_2 + \vartheta_1 \rangle$$



$$\langle 2\pi - \vartheta_2 + \vartheta_1 \rangle$$



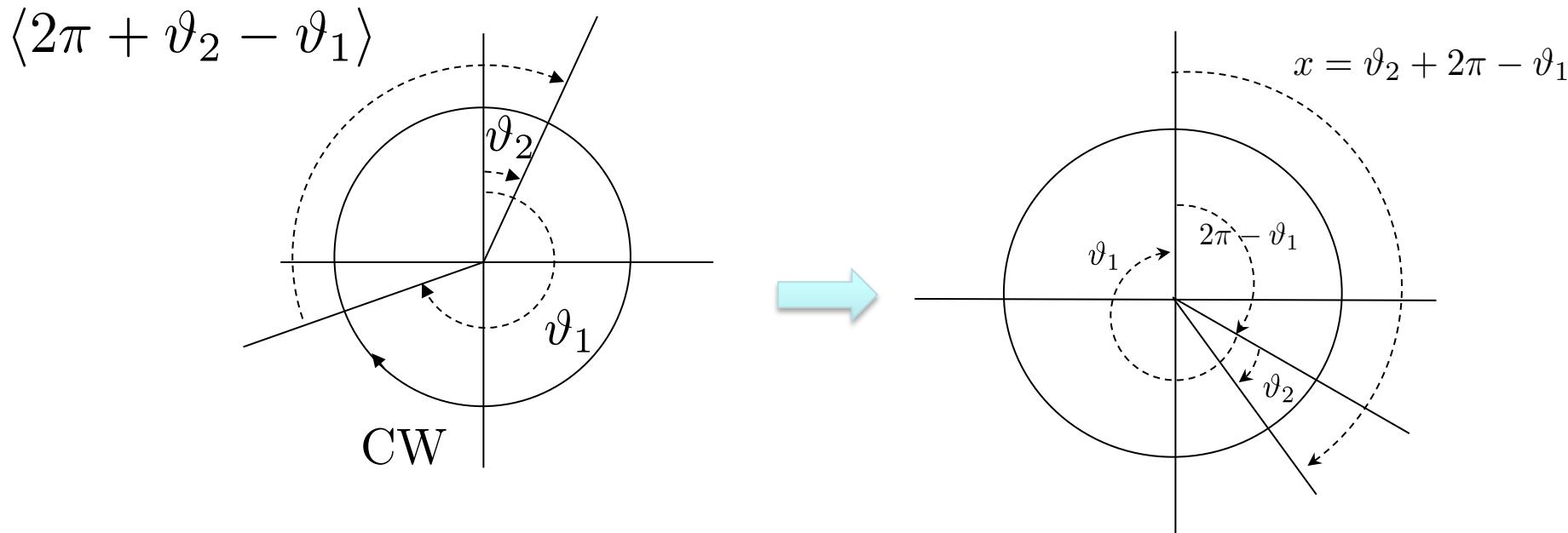
# Alternative Viewpoint

For clockwise circles, angular distance between  $\vartheta_1$  and  $\vartheta_2$  given by

$$|\vartheta_2 - \vartheta_1|_{CW} \triangleq \langle 2\pi + \vartheta_2 - \vartheta_1 \rangle,$$

where

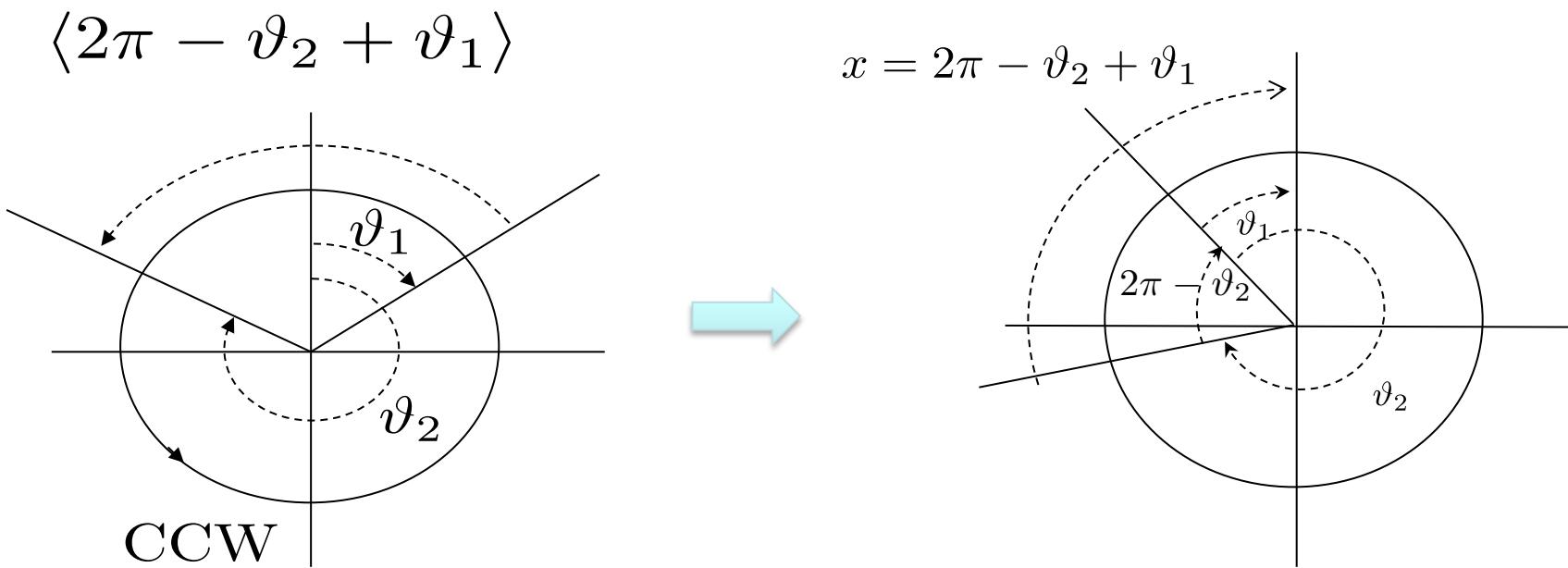
$$\langle \varphi \rangle \triangleq \varphi \mod 2\pi$$



# Alternative Viewpoint

For counter clockwise circles,

$$|\vartheta_2 - \vartheta_1|_{CCW} \stackrel{\triangle}{=} \langle 2\pi - \vartheta_2 + \vartheta_1 \rangle$$



# Dubins Case I: R-S-R

Distance traveled along  $\mathbf{c}_{rs}$

$$R\left\langle 2\pi + \left\langle \vartheta - \frac{\pi}{2} \right\rangle - \left\langle \chi_s - \frac{\pi}{2} \right\rangle \right\rangle$$

Distance traveled along  $\mathbf{c}_{re}$

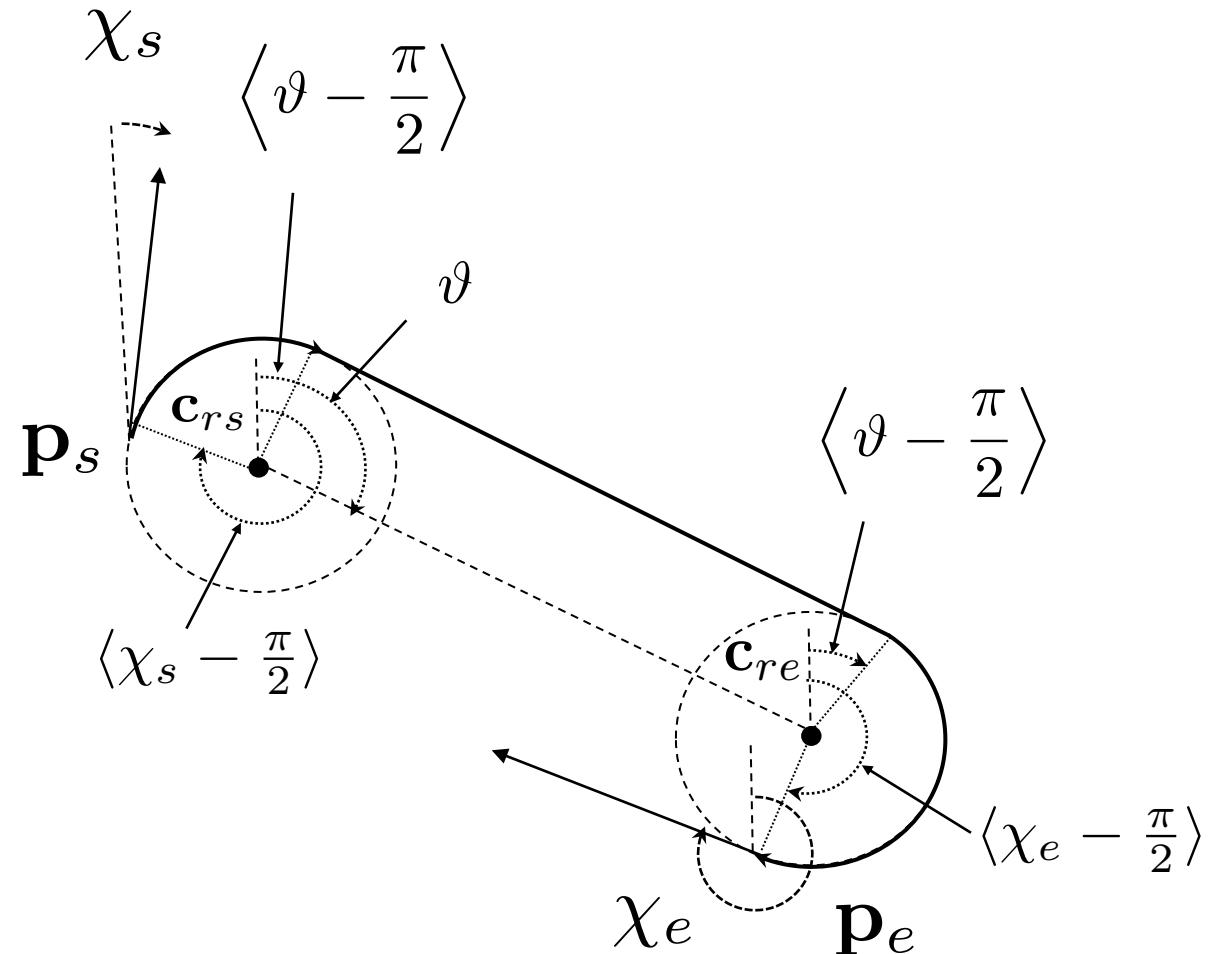
$$R\left\langle 2\pi + \left\langle \chi_e - \frac{\pi}{2} \right\rangle - \left\langle \vartheta - \frac{\pi}{2} \right\rangle \right\rangle$$

where

$$\vartheta = \text{atan2}(c_{ree} - c_{rse}, c_{ren} - c_{rsn})$$

Total path length:

$$L_1 = \|\mathbf{c}_{rs} - \mathbf{c}_{re}\| + R\left\langle 2\pi + \left\langle \vartheta - \frac{\pi}{2} \right\rangle - \left\langle \chi_s - \frac{\pi}{2} \right\rangle \right\rangle + R\left\langle 2\pi + \left\langle \chi_e - \frac{\pi}{2} \right\rangle - \left\langle \vartheta - \frac{\pi}{2} \right\rangle \right\rangle$$



# Dubins Case II: R-S-L

Distance traveled along  $\mathbf{c}_{rs}$

$$R\left\langle 2\pi + \left\langle \vartheta_2 \right\rangle - \left\langle \chi_s - \frac{\pi}{2} \right\rangle \right\rangle$$

Distance traveled along  $\mathbf{c}_{le}$

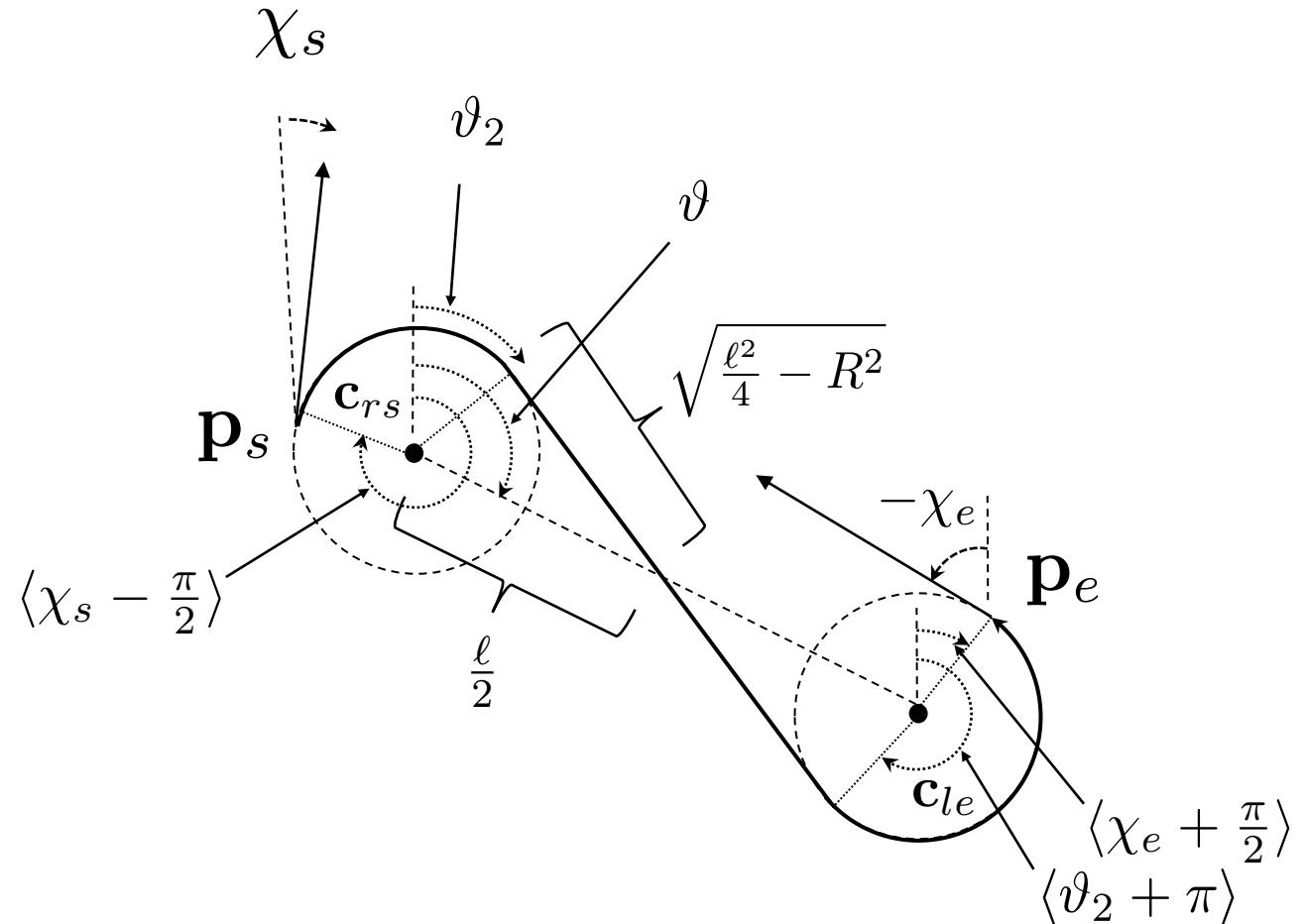
$$R\left\langle 2\pi + \left\langle \vartheta_2 + \pi \right\rangle - \left\langle \chi_e + \frac{\pi}{2} \right\rangle \right\rangle$$

where

$$\vartheta_2 = \vartheta - \frac{\pi}{2} + \sin^{-1} \left( \frac{2R}{\ell} \right)$$

Total path length:

$$L_2 = \sqrt{\ell^2 - 4R^2} + R\left\langle 2\pi + \left\langle \vartheta_2 \right\rangle - \left\langle \chi_s - \frac{\pi}{2} \right\rangle \right\rangle + R\left\langle 2\pi + \left\langle \vartheta_2 + \pi \right\rangle - \left\langle \chi_e + \frac{\pi}{2} \right\rangle \right\rangle$$



# Dubins Case III: L-S-R

Distance traveled along  $\mathbf{c}_{ls}$

$$R\left\langle 2\pi + \left\langle \chi_s + \frac{\pi}{2} \right\rangle - \langle \vartheta + \vartheta_2 \rangle \right\rangle$$

Distance traveled along  $\mathbf{c}_{re}$

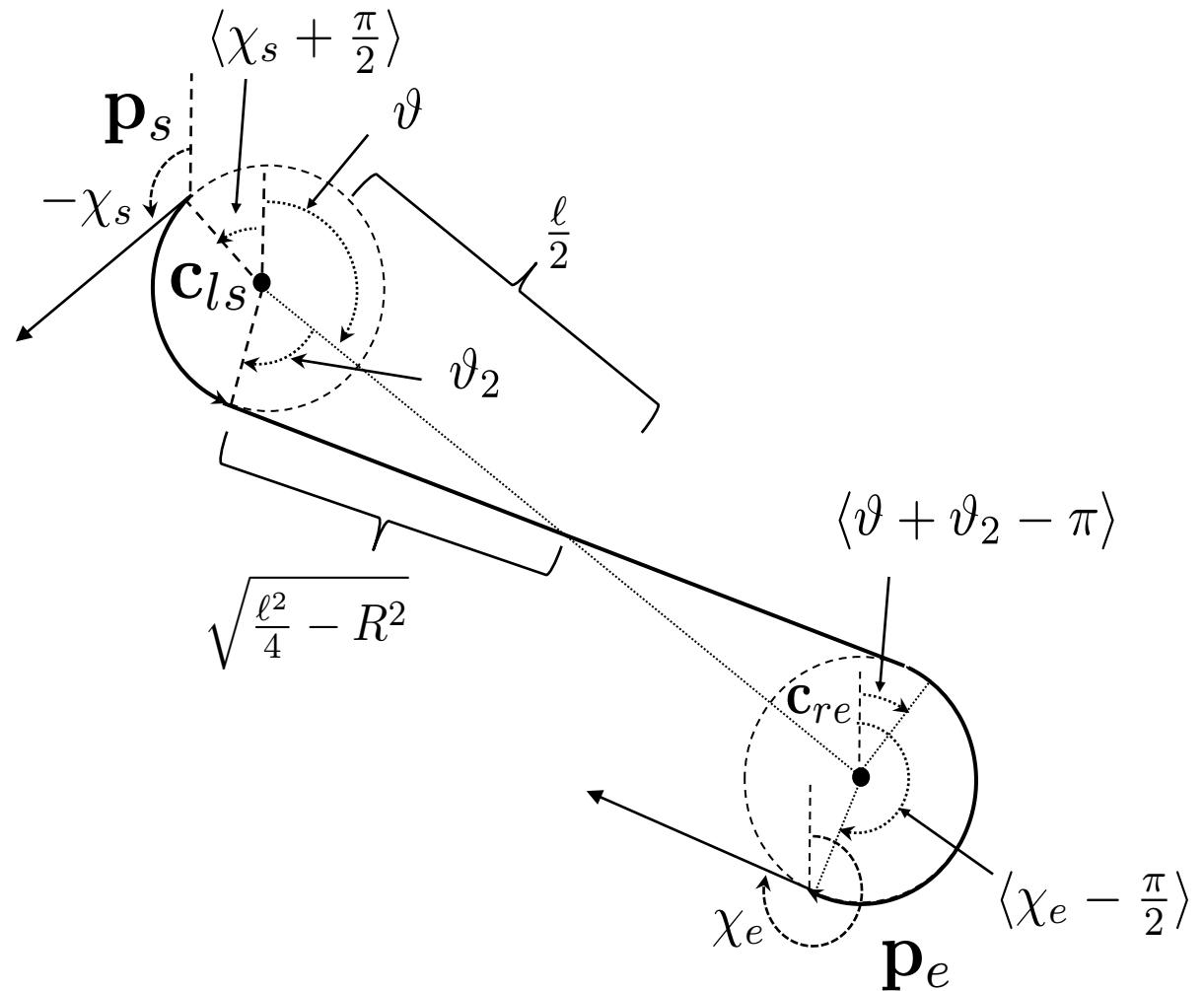
$$R\left\langle 2\pi + \left\langle \chi_e - \frac{\pi}{2} \right\rangle - \langle \vartheta + \vartheta_2 - \pi \rangle \right\rangle$$

where

$$\vartheta_2 = \cos^{-1} \left( \frac{2R}{\ell} \right)$$

Total path length:

$$L_3 = \sqrt{\ell^2 - 4R^2} + R\left\langle 2\pi + \left\langle \chi_s + \frac{\pi}{2} \right\rangle - \langle \vartheta + \vartheta_2 \rangle \right\rangle + R\left\langle 2\pi + \left\langle \chi_e - \frac{\pi}{2} \right\rangle - \langle \vartheta + \vartheta_2 - \pi \rangle \right\rangle$$



# Dubins Case IV: L-S-L

Distance traveled along  $\mathbf{c}_{ls}$

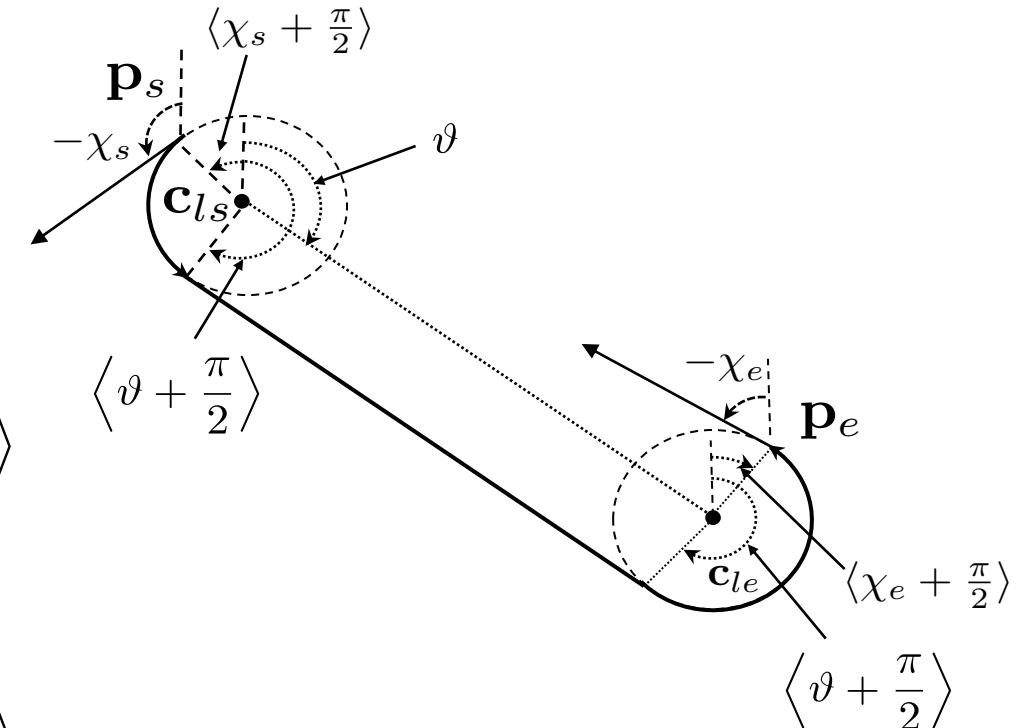
$$R\left\langle 2\pi + \left\langle \chi_s + \frac{\pi}{2} \right\rangle - \left\langle \vartheta + \frac{\pi}{2} \right\rangle \right\rangle$$

Distance traveled along  $\mathbf{c}_{le}$

$$R\left\langle 2\pi + \left\langle \vartheta + \frac{\pi}{2} \right\rangle - \left\langle \chi_e + \frac{\pi}{2} \right\rangle \right\rangle$$

Total path length:

$$L_4 = \|\mathbf{c}_{ls} - \mathbf{c}_{le}\| + R\left\langle 2\pi + \left\langle \chi_s + \frac{\pi}{2} \right\rangle - \left\langle \vartheta + \frac{\pi}{2} \right\rangle \right\rangle + R\left\langle 2\pi + \left\langle \vartheta + \frac{\pi}{2} \right\rangle - \left\langle \chi_e + \frac{\pi}{2} \right\rangle \right\rangle$$



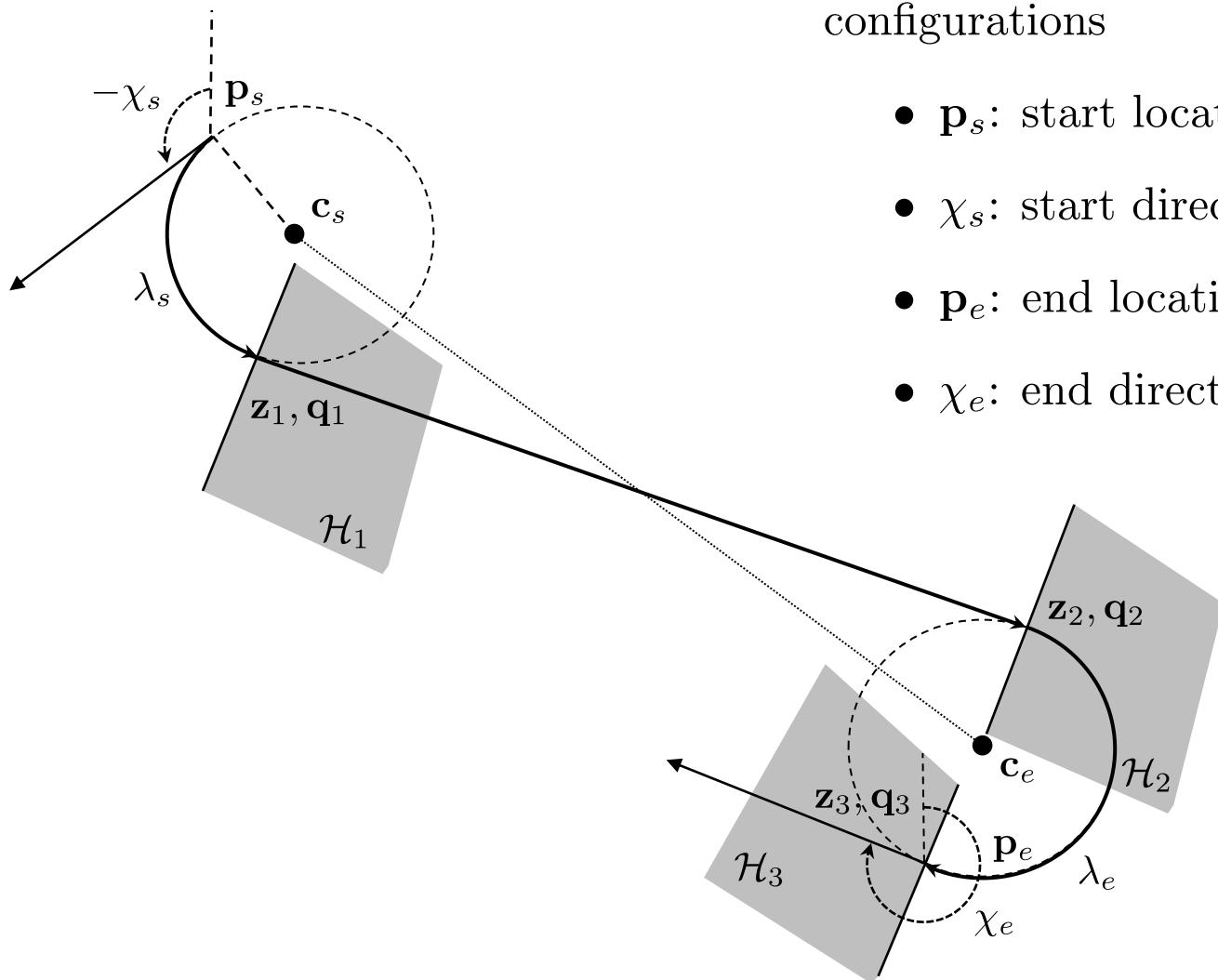
# Dubins Path Half-plane Switching

Given desired start and end configurations

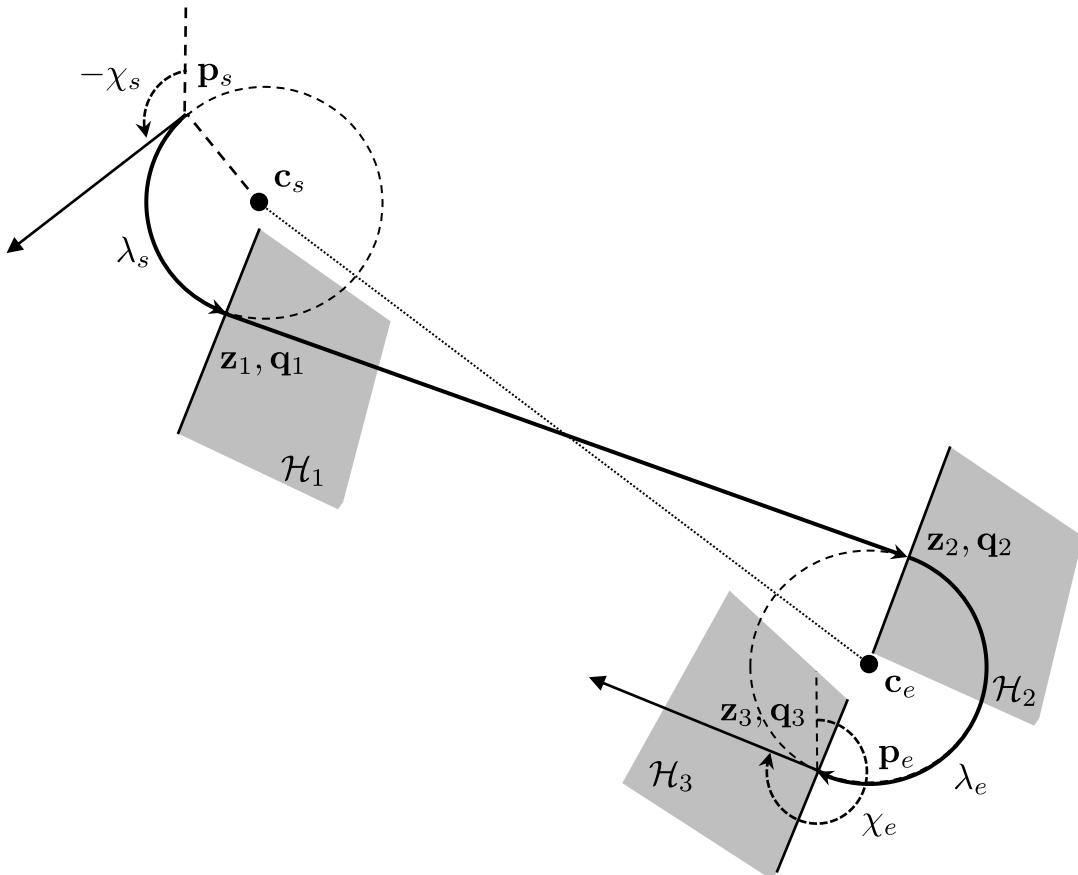
- $\mathbf{p}_s$ : start location
- $\chi_s$ : start direction
- $\mathbf{p}_e$ : end location
- $\chi_e$ : end direction

Calculate Dubins path parameters

- $\mathbf{c}_s$ : start circle location
- $\lambda_s$ : start circle direction
- $\mathbf{c}_e$ : end circle location
- $\lambda_e$ : end circle direction
- $\mathbf{z}_1, \mathbf{q}_1$ : half-plane  $\mathcal{H}_1$  parameters
- $\mathbf{z}_2, \mathbf{q}_2$ : half-plane  $\mathcal{H}_2$  parameters
- $\mathbf{z}_3, \mathbf{q}_3$ : half-plane  $\mathcal{H}_3$  parameters



# Dubins Path Parameters Algorithm



**Algorithm 7** Find Dubins Parameters:

$(L, \mathbf{c}_s, \lambda_s, \mathbf{c}_e, \lambda_e, \mathbf{z}_1, \mathbf{q}_1, \mathbf{z}_2, \mathbf{z}_3, \mathbf{q}_3) =$   
findDubinsParameters( $\mathbf{p}_s, \chi_s, \mathbf{p}_e, \chi_e, R$ )

**Input:** Start configuration  $(\mathbf{p}_s, \chi_s)$ , End configuration  $(\mathbf{p}_e, \chi_e)$ , Radius  $R$ .

**Require:**  $\|\mathbf{p}_s - \mathbf{p}_e\| \geq 3R$

**Require:**  $R$  is larger than minimum turn radius of MAV

- 1:  $\mathbf{c}_{rs} \leftarrow \mathbf{p}_s + R\mathcal{R}_z\left(\frac{\pi}{2}\right)(\cos \chi_s, \sin \chi_s, 0)^T$
- 2:  $\mathbf{c}_{ls} \leftarrow \mathbf{p}_s + R\mathcal{R}_z\left(-\frac{\pi}{2}\right)(\cos \chi_s, \sin \chi_s, 0)^T$
- 3:  $\mathbf{c}_{re} \leftarrow \mathbf{p}_e + R\mathcal{R}_z\left(\frac{\pi}{2}\right)(\cos \chi_e, \sin \chi_e, 0)^T$
- 4:  $\mathbf{c}_{le} \leftarrow \mathbf{p}_e + R\mathcal{R}_z\left(-\frac{\pi}{2}\right)(\cos \chi_e, \sin \chi_e, 0)^T$
- 5: Compute  $L_1, L_2, L_3$ , and  $L_4$  using equations (11.9) through (11.12).

- 6:  $L \leftarrow \min\{L_1, L_2, L_3, L_4\}$

- 7: if  $\arg \min\{L_1, L_2, L_3, L_4\} = 1$  then

- 8:    $\mathbf{c}_s \leftarrow \mathbf{c}_{rs}, \quad \lambda_s \leftarrow +1, \quad \mathbf{c}_e \leftarrow \mathbf{c}_{re}, \quad \lambda_e \leftarrow +1$
- 9:    $\mathbf{q}_1 \leftarrow \frac{\mathbf{c}_e - \mathbf{c}_s}{\|\mathbf{c}_e - \mathbf{c}_s\|}$
- 10:    $\mathbf{z}_1 \leftarrow \mathbf{c}_s + R\mathcal{R}_z\left(-\frac{\pi}{2}\right)\mathbf{q}_1$
- 11:    $\mathbf{z}_2 \leftarrow \mathbf{c}_e + R\mathcal{R}_z\left(-\frac{\pi}{2}\right)\mathbf{q}_1$

- 12: else if  $\arg \min\{L_1, L_2, L_3, L_4\} = 2$  then

- 13:    $\mathbf{c}_s \leftarrow \mathbf{c}_{rs}, \quad \lambda_s \leftarrow +1, \quad \mathbf{c}_e \leftarrow \mathbf{c}_{le}, \quad \lambda_e \leftarrow -1$
- 14:    $\ell \leftarrow \|\mathbf{c}_e - \mathbf{c}_s\|$
- 15:    $\vartheta \leftarrow \text{angle}(\mathbf{c}_e - \mathbf{c}_s)$
- 16:    $\vartheta_2 \leftarrow \vartheta - \frac{\pi}{2} + \sin^{-1} \frac{2R}{\ell}$
- 17:    $\mathbf{q}_1 \leftarrow \mathcal{R}_z\left(\vartheta_2 + \frac{\pi}{2}\right)\mathbf{e}_1$
- 18:    $\mathbf{z}_1 \leftarrow \mathbf{c}_s + R\mathcal{R}_z(\vartheta_2)\mathbf{e}_1$
- 19:    $\mathbf{z}_2 \leftarrow \mathbf{c}_e + R\mathcal{R}_z(\vartheta_2 + \pi)\mathbf{e}_1$

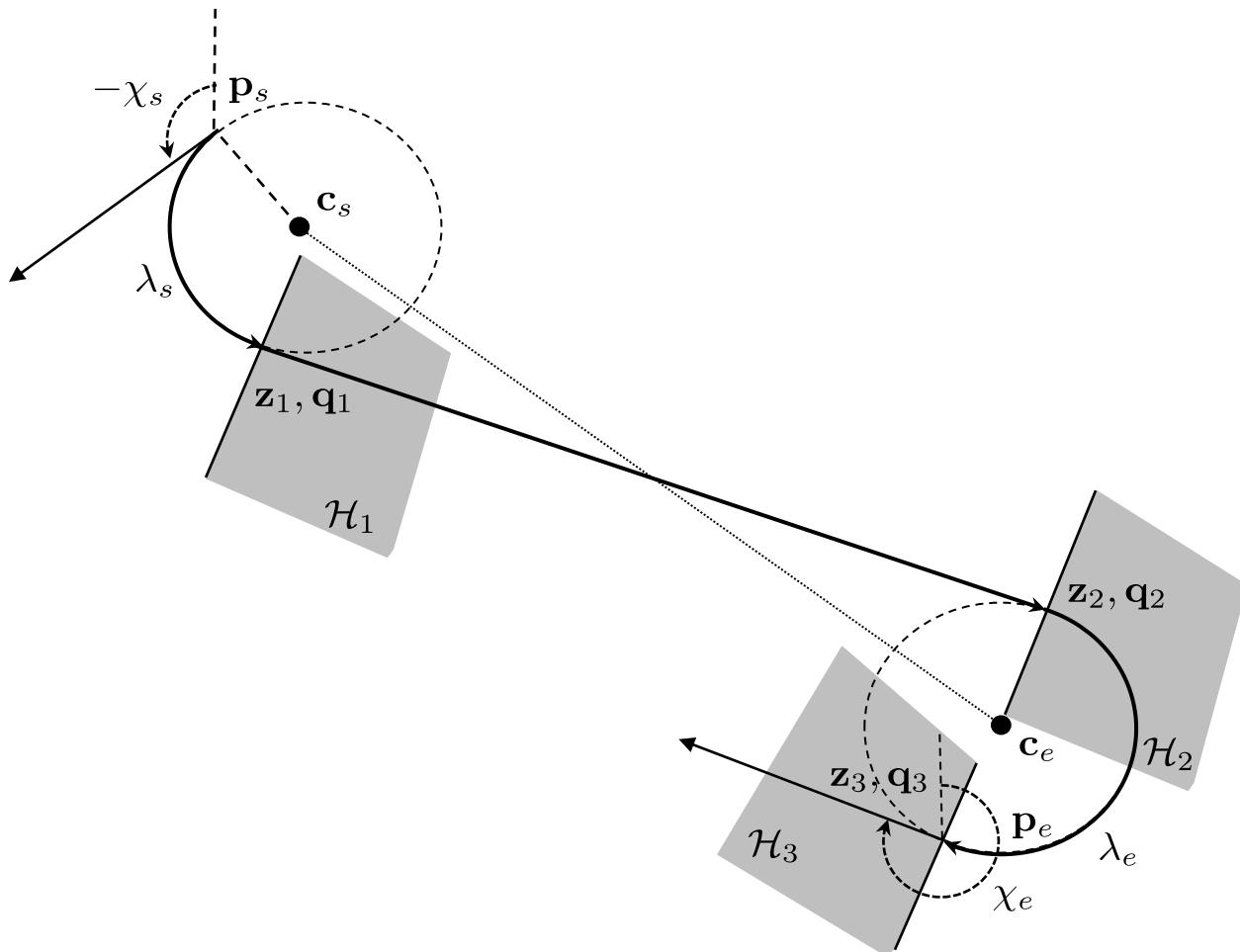
- 20: else if  $\arg \min\{L_1, L_2, L_3, L_4\} = 3$  then

- 21:    $\mathbf{c}_s \leftarrow \mathbf{c}_{ls}, \quad \lambda_s \leftarrow -1, \quad \mathbf{c}_e \leftarrow \mathbf{c}_{re}, \quad \lambda_e \leftarrow +1$
- 22:    $\ell \leftarrow \|\mathbf{c}_e - \mathbf{c}_s\|$
- 23:    $\vartheta \leftarrow \text{angle}(\mathbf{c}_e - \mathbf{c}_s)$ ,
- 24:    $\vartheta_2 \leftarrow \cos^{-1} \frac{2R}{\ell}$
- 25:    $\mathbf{q}_1 \leftarrow \mathcal{R}_z\left(\vartheta + \vartheta_2 - \frac{\pi}{2}\right)\mathbf{e}_1$ ,
- 26:    $\mathbf{z}_1 \leftarrow \mathbf{c}_s + R\mathcal{R}_z(\vartheta + \vartheta_2)\mathbf{e}_1$ ,
- 27:    $\mathbf{z}_2 \leftarrow \mathbf{c}_e + R\mathcal{R}_z(\vartheta + \vartheta_2 - \pi)\mathbf{e}_1$

- 28: else if  $\arg \min\{L_1, L_2, L_3, L_4\} = 4$  then

- 29:    $\mathbf{c}_s \leftarrow \mathbf{c}_{ls}, \quad \lambda_s \leftarrow -1, \quad \mathbf{c}_e \leftarrow \mathbf{c}_{le}, \quad \lambda_e \leftarrow -1$
- 30:    $\mathbf{q}_1 \leftarrow \frac{\mathbf{c}_e - \mathbf{c}_s}{\|\mathbf{c}_e - \mathbf{c}_s\|}$ ,
- 31:    $\mathbf{z}_1 \leftarrow \mathbf{c}_s + R\mathcal{R}_z\left(\frac{\pi}{2}\right)\mathbf{q}_1$ ,
- 32:    $\mathbf{z}_2 \leftarrow \mathbf{c}_e + R\mathcal{R}_z\left(\frac{\pi}{2}\right)\mathbf{q}_2$
- 33: end if
- 34:  $\mathbf{z}_3 \leftarrow \mathbf{p}_e$
- 35:  $\mathbf{q}_3 \leftarrow \mathcal{R}_z(\chi_e)\mathbf{e}_1$

# Dubins Path Following Algorithm




---

**Algorithm 8** Follow Waypoints with Dubins:  $(\text{flag}, \mathbf{r}, \mathbf{q}, \mathbf{c}, \rho, \lambda) = \text{followWppDubins}(\mathcal{P}, \mathbf{p}, R)$

---

**Input:** Configuration path  $\mathcal{P} = \{(\mathbf{w}_1, \chi_1), \dots, (\mathbf{w}_N, \chi_N)\}$ , MAV position  $\mathbf{p} = (p_n, p_e, p_d)^\top$ , fillet radius  $R$ .

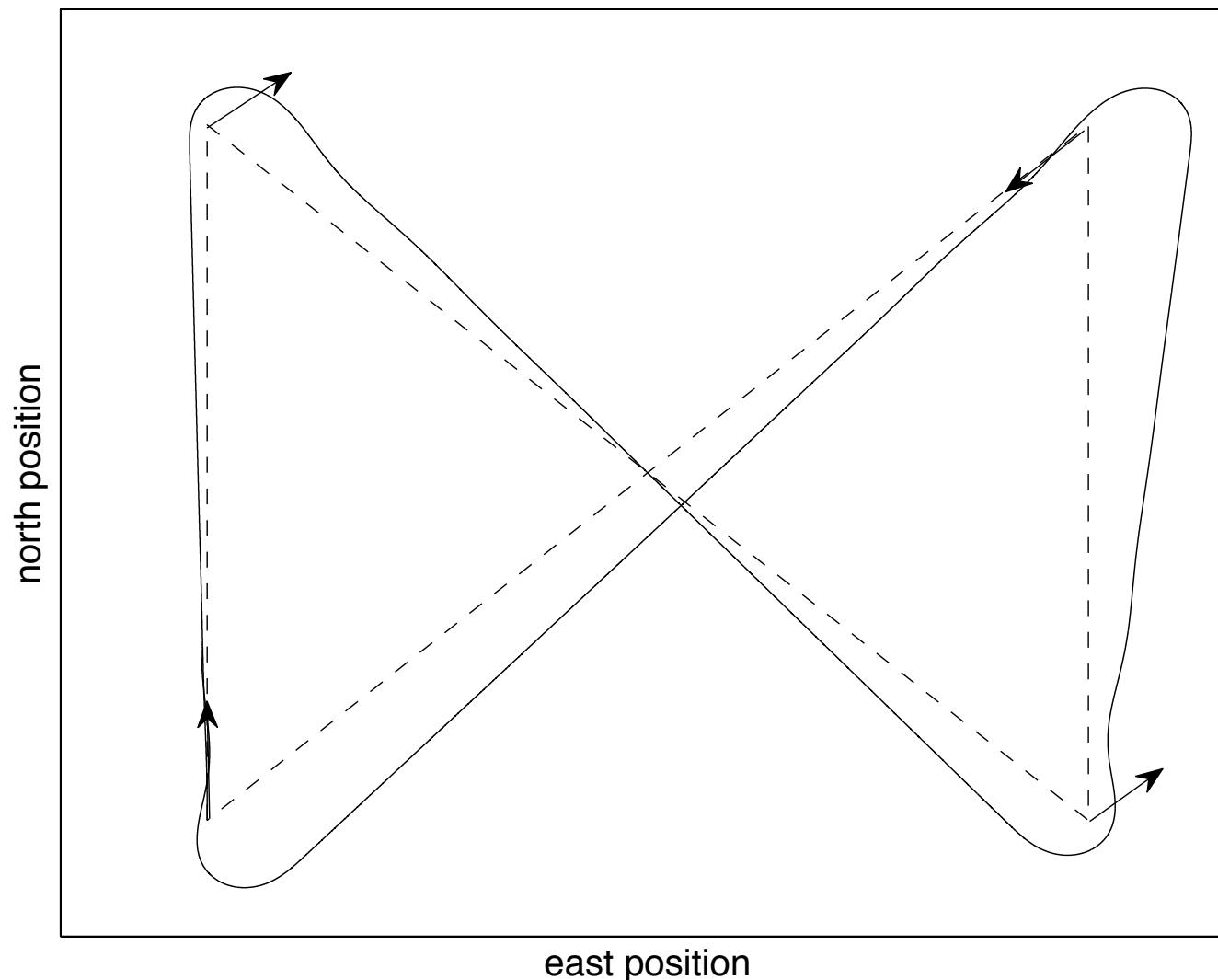
**Require:**  $N \geq 3$

- 1: **if** New configuration path  $\mathcal{P}$  is received **then**
- 2:   Initialize waypoint pointer:  $i \leftarrow 2$ , and state machine: state  $\leftarrow 1$ .
- 3: **end if**
- 4:  $(L, \mathbf{c}_s, \lambda_s, \mathbf{c}_e, \lambda_e, \mathbf{z}_1, \mathbf{q}_1, \mathbf{z}_2, \mathbf{z}_3, \mathbf{q}_3) \leftarrow \text{findDubinsParameters}(\mathbf{w}_{i-1}, \chi_{i-1}, \mathbf{w}_i, \chi_i, R)$
- 5: **if** state = 1 **then**
- 6:   flag  $\leftarrow 2$ ,  $\mathbf{c} \leftarrow \mathbf{c}_s$ ,  $\rho \leftarrow R$ ,  $\lambda \leftarrow \lambda_s$
- 7:   **if**  $\mathbf{p} \in \mathcal{H}(\mathbf{z}_1, -\mathbf{q}_1)$  **then**
- 8:     state  $\leftarrow 2$
- 9:   **end if**
- 10: **else if** state = 2 **then**
- 11:   **if**  $\mathbf{p} \in \mathcal{H}(\mathbf{z}_1, \mathbf{q}_1)$  **then**
- 12:     state  $\leftarrow 3$
- 13:   **end if**
- 14: **else if** state = 3 **then**
- 15:   flag  $\leftarrow 1$ ,  $\mathbf{r} \leftarrow \mathbf{z}_1$ ,  $\mathbf{q} \leftarrow \mathbf{q}_1$
- 16:   **if**  $\mathbf{p} \in \mathcal{H}(\mathbf{z}_2, \mathbf{q}_1)$  **then**
- 17:     state  $\leftarrow 4$
- 18:   **end if**
- 19: **else if** state = 4 **then**
- 20:   flag  $\leftarrow 2$ ,  $\mathbf{c} \leftarrow \mathbf{c}_e$ ,  $\rho \leftarrow R$ ,  $\lambda \leftarrow \lambda_e$
- 21:   **if**  $\mathbf{p} \in \mathcal{H}(\mathbf{z}_3, -\mathbf{q}_3)$  **then**
- 22:     state  $\leftarrow 5$
- 23:   **end if**
- 24: **else if** state = 5 **then**
- 25:   **if**  $\mathbf{p} \in \mathcal{H}(\mathbf{z}_3, \mathbf{q}_3)$  **then**
- 26:     state  $\leftarrow 1$
- 27:     *i*  $\leftarrow (i + 1)$  until  $i = N$ .
- 28:      $(L, \mathbf{c}_s, \lambda_s, \mathbf{c}_e, \lambda_e, \mathbf{z}_1, \mathbf{q}_1, \mathbf{z}_2, \mathbf{z}_3, \mathbf{q}_3) \leftarrow \text{findDubinsParameters}(\mathbf{w}_{i-1}, \chi_{i-1}, \mathbf{w}_i, \chi_i, R)$
- 29:   **end if**
- 30: **end if**
- 31: **return** flag,  $\mathbf{r}$ ,  $\mathbf{q}$ ,  $\mathbf{c}$ ,  $\rho$ ,  $\lambda$ .

---

# Dubins Path Following Results

Path Manager – Dubins



Need to incorporate in this next set of slides into book, and also slide deck.

# C-C-C DUBINS PATHS

- Dubins RRT in dense obstacle fields works better with short segment lengths
- While methods exist to determine optimality without calculating paths [6], an exhaustive search was implemented as in the textbook with help from [7]
- An additional state is needed in the path manager (state 3.5)

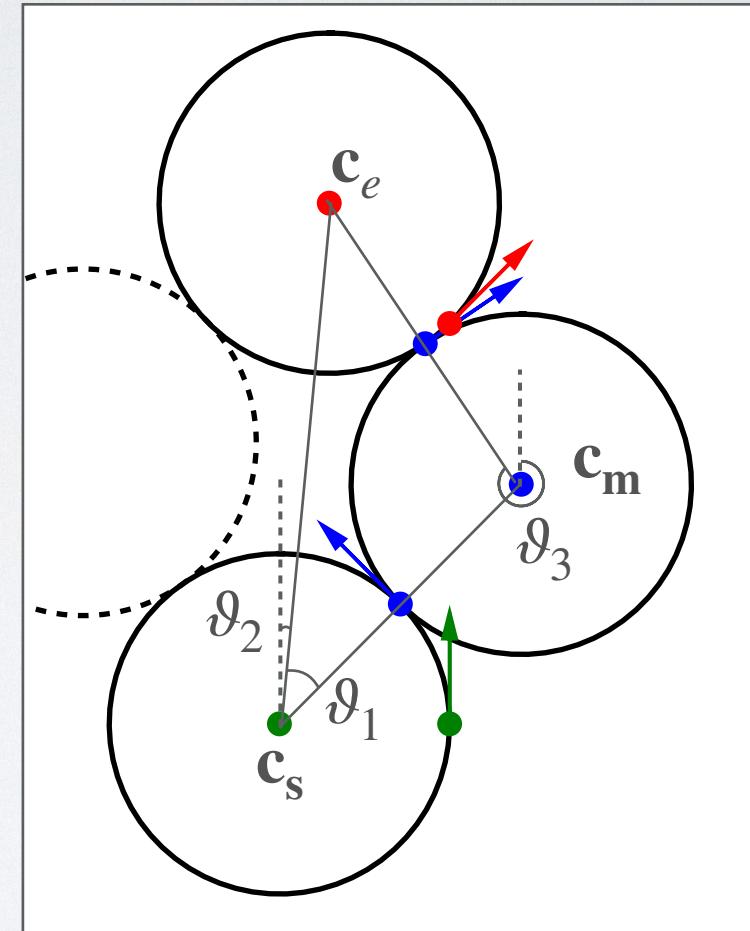
Case	Conditions for Validity
Case I: R-S-R	Always
Case II: R-S-L	$\ \mathbf{p}_e - \mathbf{p}_s\  \geq 4R$ and $\ \mathbf{c}_{le} - \mathbf{c}_{rs}\  \geq 4R$
Case III: L-S-R	$\ \mathbf{p}_e - \mathbf{p}_s\  \geq 4R$ and $\ \mathbf{c}_{re} - \mathbf{c}_{ls}\  \geq 4R$
Case IV: L-S-L	Always
Case V: R-L-R	$\ \mathbf{p}_e - \mathbf{p}_s\  \leq 4R$ and $\ \mathbf{c}_{re} - \mathbf{c}_{rs}\  \geq 4R$
Case VI: L-R-L	$\ \mathbf{p}_e - \mathbf{p}_s\  \leq 4R$ and $\ \mathbf{c}_{le} - \mathbf{c}_{ls}\  \geq 4R$

# C-C-C DUBINS PATHS

- The angle between  $\mathbf{c}_e - \mathbf{c}_s$  and the middle circle center  $\mathbf{c}_m$  is given by

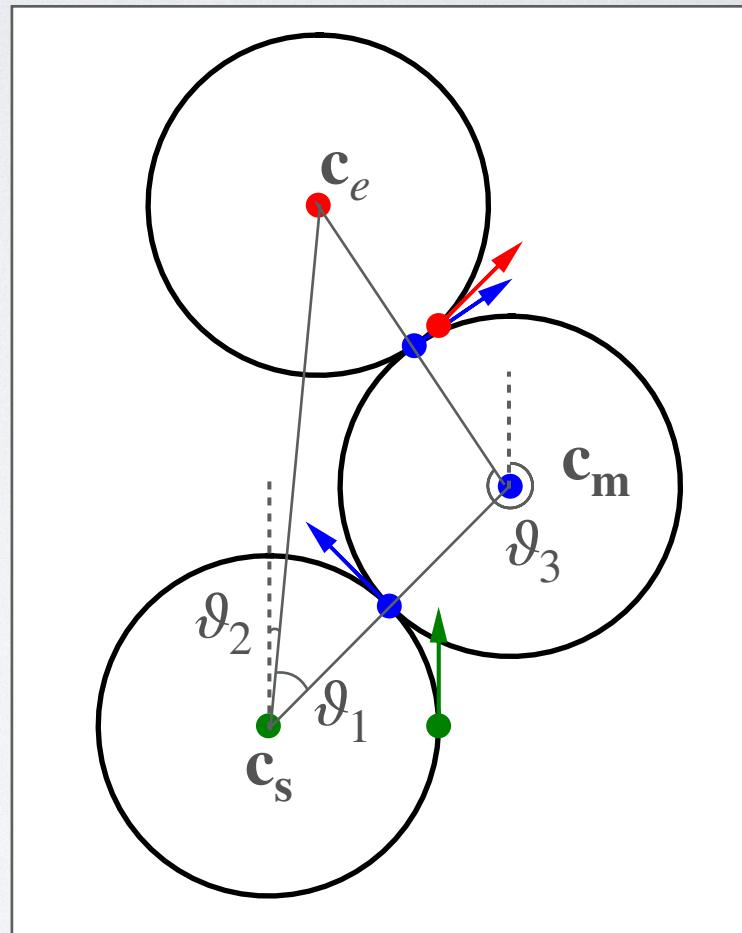
$$\vartheta_1 = \left\langle \pm \cos^{-1} \left( \frac{\ell}{4R} \right) \right\rangle$$

- The  $\pm$  in the equation for  $\vartheta_1$  indicates that there are two cases for both R-L-R and L-R-L: one where the circle is to the right of  $\mathbf{c}_e - \mathbf{c}_s$  (+) and one where it is to the left (-)



# C-C-C DUBINS PATHS

- The center of the middle circle is given by  $\mathbf{c}_m = \mathbf{c}_{rs} + 2R\mathcal{R}_z(\vartheta_1)\frac{\mathbf{c}_{re} - \mathbf{c}_{rs}}{\ell}$ , where  $\ell = \|\mathbf{c}_{re} - \mathbf{c}_{rs}\|$  for R-L-R and  $\ell = \|\mathbf{c}_{le} - \mathbf{c}_{ls}\|$  for L-R-L
- $\vartheta_2$  and  $\vartheta_1$  are defined as the angles of the vectors  $\mathbf{c}_m - \mathbf{c}_s$  and  $\mathbf{c}_e - \mathbf{c}_m$  respectively



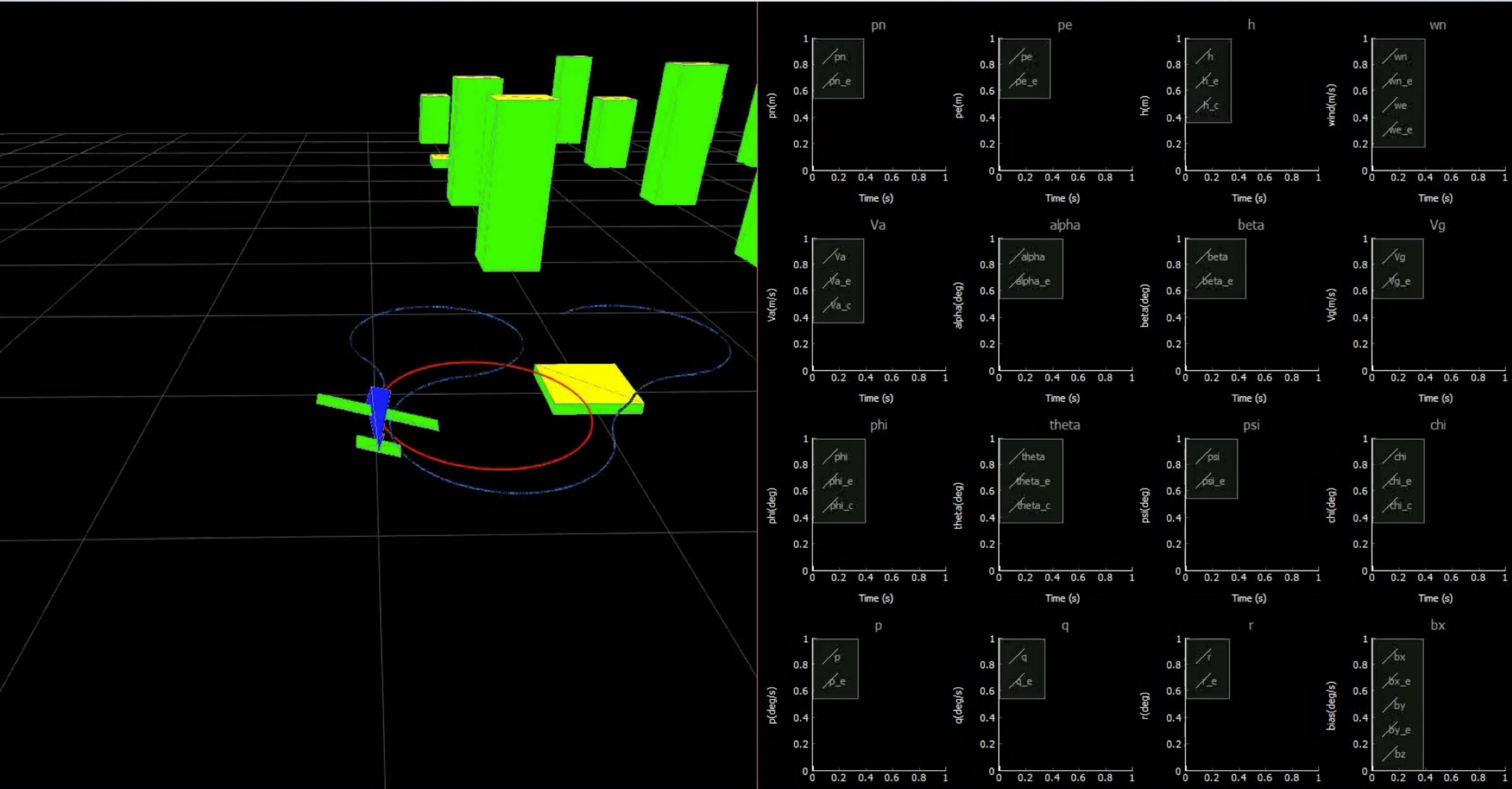
# C-C-C DUBINS PATHS

- R-L-R Length:

$$L_5 = R \left\langle 2\pi + \left\langle \frac{\pi}{2} - \vartheta_2 \right\rangle - \left\langle \chi_s - \frac{\pi}{2} \right\rangle \right\rangle \\ + R \left\langle 2\pi - \left\langle \frac{\pi}{2} - \vartheta_3 \right\rangle + \left\langle \frac{3\pi}{2} - \vartheta_2 \right\rangle \right\rangle \\ + R \left\langle 2\pi + \left\langle \chi_e - \frac{\pi}{2} \right\rangle - \left\langle \frac{3\pi}{2} - \vartheta_3 \right\rangle \right\rangle$$

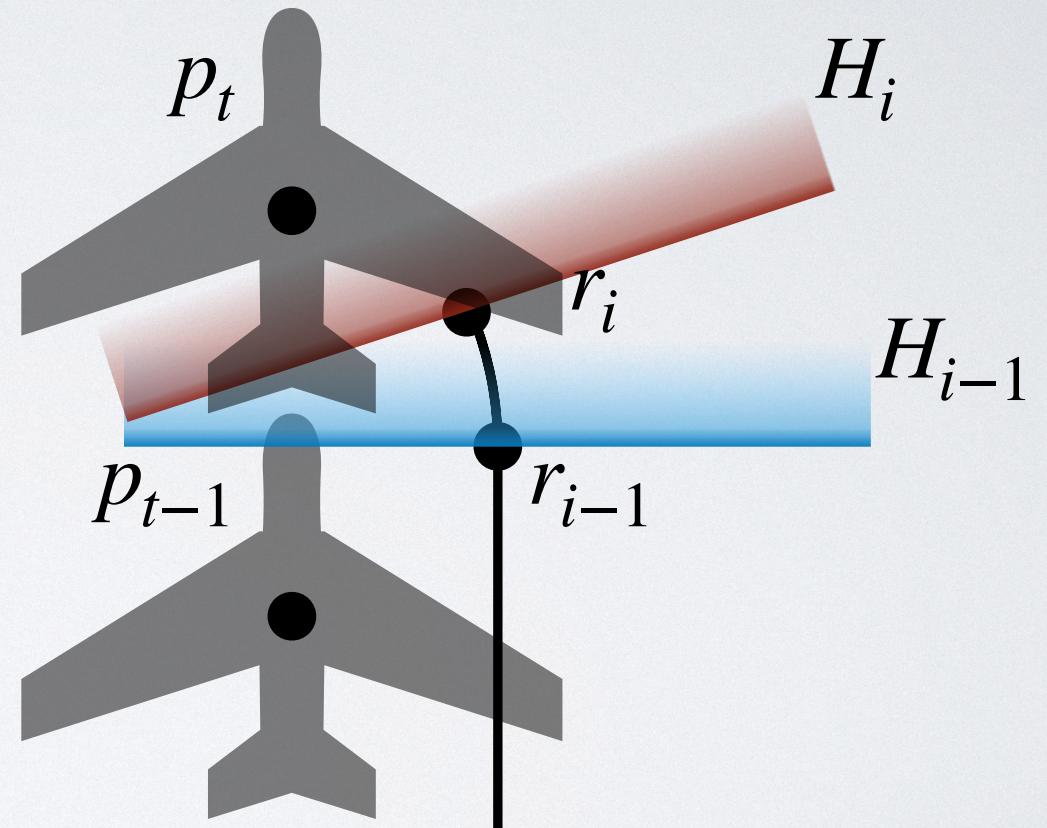
- L-R-L Length:

$$L_6 = R \left\langle 2\pi - \left\langle \frac{\pi}{2} - \vartheta_2 \right\rangle + \left\langle \chi_s - \frac{\pi}{2} \right\rangle \right\rangle \\ + R \left\langle 2\pi + \left\langle \frac{\pi}{2} - \vartheta_3 \right\rangle - \left\langle \frac{3\pi}{2} - \vartheta_2 \right\rangle \right\rangle \\ + R \left\langle 2\pi - \left\langle \chi_e - \frac{\pi}{2} \right\rangle + \left\langle \frac{3\pi}{2} - \vartheta_3 \right\rangle \right\rangle$$



# ROBUST PATH MANAGEMENT

- The dual half-plane path manager occasionally flew a full orbit when paths included short arcs
- The negative half plane check should be skipped when points are close
  - $r_{i-1} \in -H_i$
  - $s < R\pi$
  - $\theta < \pi$



The best way to do this is check distance along circles and straight lines. If it is small, then just transition to the next segment.

# REFERENCES

- [1] T.Wallace, D.Watkins, and J. Schwartz, “A Map of Every Building in America,” *The New York Times*, Oct 2018. Data available: <https://github.com/microsoft/USBuildingFootprints>.
- [2] J. O'Rourke *et al.*, *Computational Geometry in C*. Cambridge University Press, 2 ed., 1998.
- [3] S. Gillies *et al.*, “Shapely: Manipulation and Analysis of Geometric Objects,” 2007.
- [4] P. Virtanen *et al.*, “SciPy 1.0: Fundamental Algorithms for Scientific Computing in Python,” *Nature Methods*, vol. 17, pp. 261–272, 2020.
- [5] A. Hagberg, P. Swart, and D. S Chult, “Exploring Network Structure, Dynamics, and Function using NetworkX,” Tech. Rep. LA-UR-08-05495, Los Alamos National Laboratory, I 2008.
- [6] A. M. Shkel and V. Lumelsky, “Classification of the Dubins set,” *Robotics and Autonomous Systems*, vol. 34, no. 4, pp. 179–202, 2001.
- [7] A. Giese, “A Comprehensive, Step-by-Step Tutorial on Computing Dubins Curves,” 2014.

# Dubins Airplane Model

Adapted from: Mark Owen, Randal W. Beard, Timothy W. McLain, "Implementing Dubins Airplane Paths on Fixed-wing UAVs," *Handbook of Unmanned Aerial Vehicles*, ed. Kimon P. Valavanis, George J. Vachtsevanos, Springer Verlag, Section XII, Chapter 68, p. 1677-1702, 2014.

**Dubins Airplane model:**

$$\dot{r}_n = V \cos \psi \cos \gamma^c$$

$$\dot{r}_e = V \sin \psi \cos \gamma^c$$

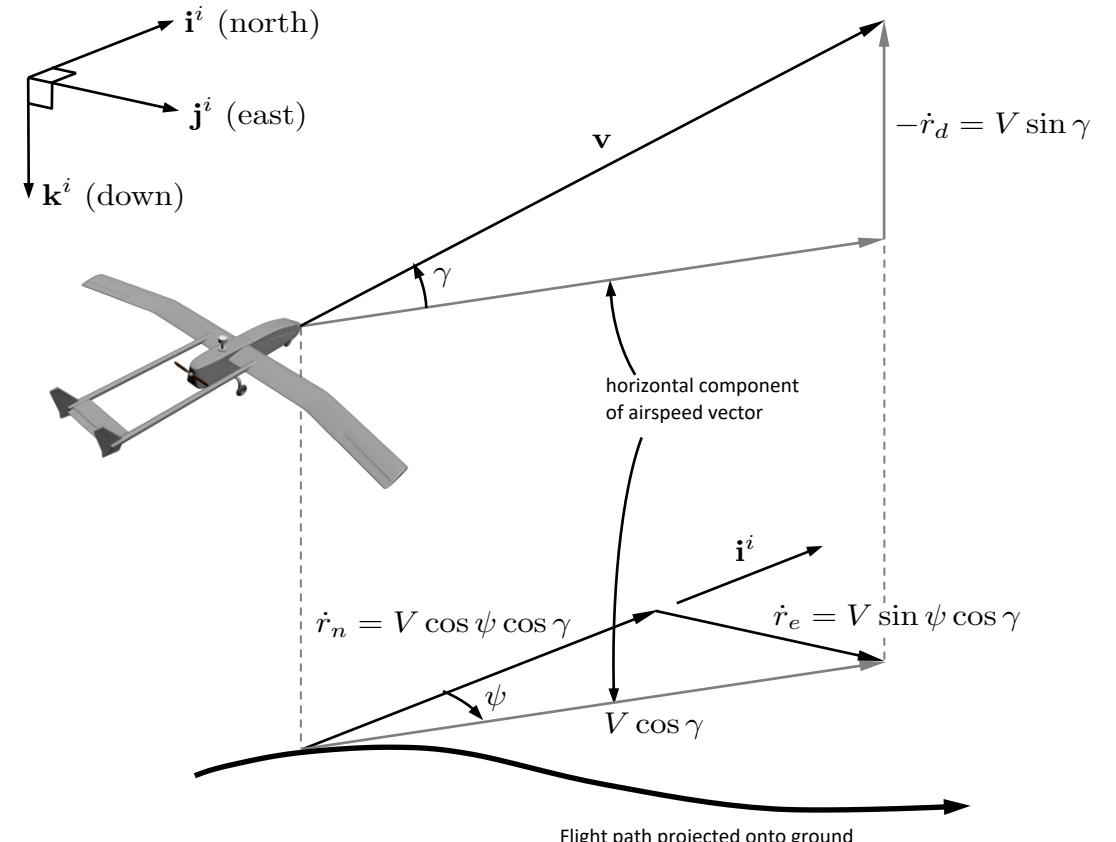
$$\dot{r}_d = -V \sin \gamma^c$$

$$\dot{\psi} = \frac{g}{V} \tan \phi^c$$

Where the commanded flight path angle  $\gamma^c$  and the commanded roll angle  $\phi^c$  are constrained by

$$|\phi^c| \leq \bar{\phi}$$

$$|\gamma^c| \leq \bar{\gamma}.$$



# 3D Vector Field Path Following

Adapted from: V. M. Goncalves, L. C. A. Pimenta, C. A. Maia, B. C. O. Durtra, G. A. S. Pereira, B. C. O. Dutra, and G. A. S. Pereira, "Vector Fields for Robot Navigation Along Time-Varying Curves in n-Dimensions," IEEE Transactions on Robotics, vol. 26, pp. 647–659, Aug 2010.

The path is specified as the intersection of two 2D manifolds given by

$$\alpha_1(\mathbf{r}) = 0$$

$$\alpha_2(\mathbf{r}) = 0$$

$\mathbf{r} \in \mathbb{R}^3$ . Define the composite function

$$W(\mathbf{r}) = \frac{1}{2}\alpha_1^2(\mathbf{r}) + \frac{1}{2}\alpha_2^2(\mathbf{r}),$$

Note that the gradient

$$\frac{\partial W}{\partial \mathbf{r}} = \alpha_1(\mathbf{r}) \frac{\partial \alpha_1}{\partial \mathbf{r}}(\mathbf{r}) + \alpha_2(\mathbf{r}) \frac{\partial \alpha_2}{\partial \mathbf{r}}(\mathbf{r}).$$

points away from the path.

# 3D Vector Field Path Following

The desired velocity vector can be chosen as

$$\mathbf{u}' = \underbrace{-K_1 \frac{\partial W}{\partial \mathbf{r}}}_{\text{velocity directed toward the path}} + \underbrace{K_2 \frac{\partial \alpha_1}{\partial \mathbf{r}} \times \frac{\partial \alpha_2}{\partial \mathbf{r}}}_{\text{velocity directed along the path}}$$

where  $K_1 > 0$  and  $K_2$  are symmetric tuning matrices, and the definiteness of  $K_2$  determines the direction of travel along the path.

Since  $\mathbf{u}'$  may not equal  $V_a$ , normalize to get

$$\mathbf{u} = V_a \frac{\mathbf{u}'}{\|\mathbf{u}'\|}.$$

# 3D Vector Field Path Following

Setting the NED components of the velocity of the Dubins airplane model to  $\mathbf{u} = (u_1, u_2, u_3)^\top$  gives

$$\begin{aligned} V \cos \psi^d \cos \gamma^c &= u_1 \\ V \sin \psi^d \cos \gamma^c &= u_2 \\ -V \sin \gamma^c &= u_3. \end{aligned}$$

Solving for  $\gamma^c$ , and  $\psi^d$  results in

$$\begin{aligned} \gamma^c &= -\text{sat}_{\bar{\gamma}} \left[ \sin^{-1} \left( \frac{u_3}{V} \right) \right] \\ \psi^d &= \text{atan2}(u_2, u_1). \end{aligned}$$

Assuming the inner-loop lateral-directional dynamics are accurately modeled by the coordinated-turn equation, the commanded roll angle is

$$\phi^c = \text{sat}_{\bar{\phi}} \left[ k_\phi (\psi^d - \psi) \right],$$

where  $k_\phi$  is a positive constant.

# 3D Vector Field – Straight Line path

The straight line path is given by

$$\mathcal{P}_{\text{line}}(\mathbf{c}_\ell, \psi_\ell, \gamma_\ell) = \left\{ \mathbf{r} \in \mathbb{R}^3 : \mathbf{r} = \mathbf{c}_\ell + \sigma \mathbf{q}_\ell, \sigma \in \mathbb{R} \right\},$$

where

$$\mathbf{q}_\ell = \begin{pmatrix} q_n \\ q_e \\ q_d \end{pmatrix} = \begin{pmatrix} \cos \psi_\ell \cos \gamma_\ell \\ \sin \psi_\ell \cos \gamma_\ell \\ -\sin \gamma_\ell \end{pmatrix}.$$

Define

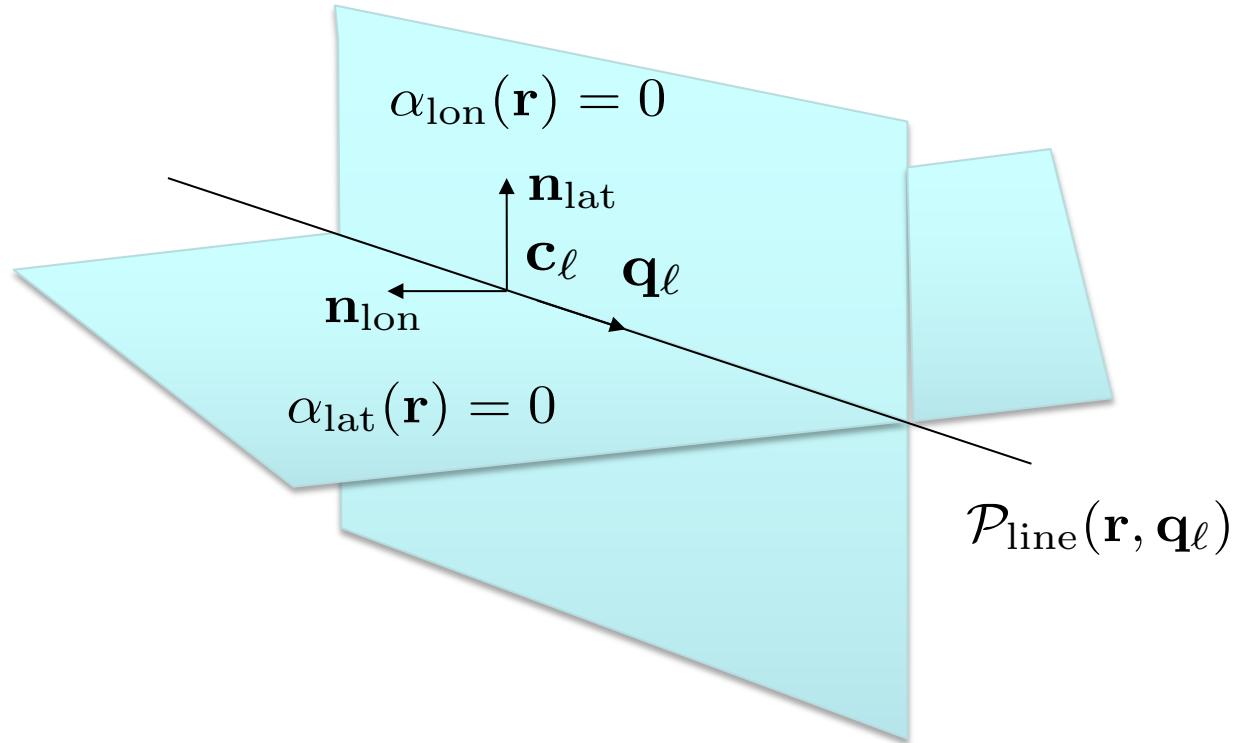
$$\mathbf{n}_{\text{lon}} = \begin{pmatrix} -\sin \psi_\ell \\ \cos \psi_\ell \\ 0 \end{pmatrix}$$

$$\mathbf{n}_{\text{lat}} = \mathbf{n}_{\text{lon}} \times \mathbf{q}_\ell = \begin{pmatrix} -\cos \psi_\ell \sin \gamma_\ell \\ -\sin \psi_\ell \sin \gamma_\ell \\ -\cos \gamma_\ell \end{pmatrix},$$

to get

$$\alpha_{\text{lon}}(\mathbf{r}) = \mathbf{n}_{\text{lon}}^\top (\mathbf{r} - \mathbf{c}_\ell) = 0$$

$$\alpha_{\text{lat}}(\mathbf{r}) = \mathbf{n}_{\text{lat}}^\top (\mathbf{r} - \mathbf{c}_\ell) = 0.$$



# 3D Vector Field – Helical Path

A helical path is then defined as

$$\mathcal{P}_{\text{helix}}(\mathbf{c}_h, \psi_h, \lambda_h, R_h, \gamma_h) = \{\mathbf{r} \in \mathbb{R}^3 : \alpha_{\text{cyl}}(\mathbf{r}) = 0 \text{ and } \alpha_{\text{pl}}(\mathbf{r}) = 0\}.$$

where

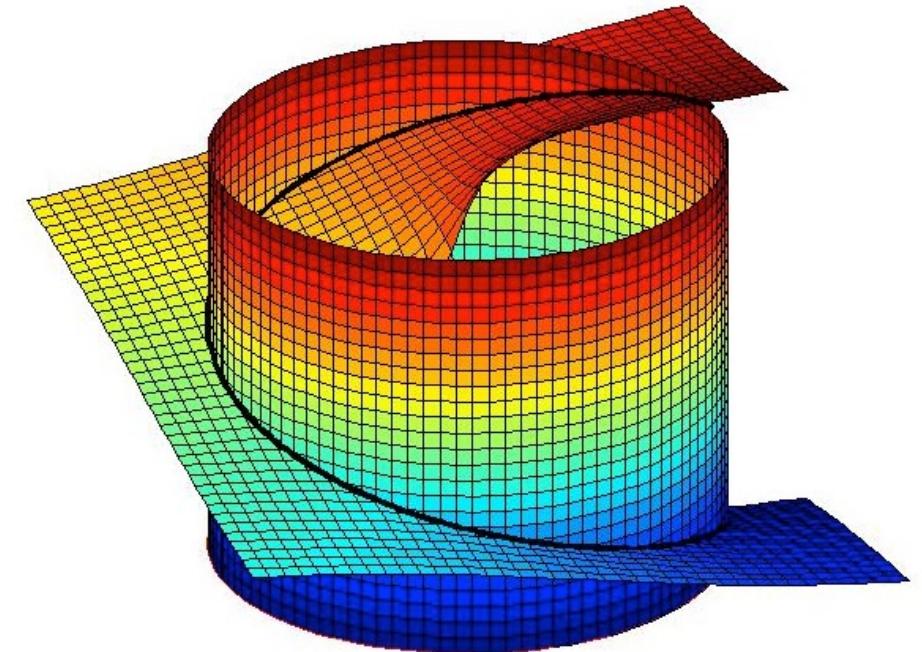
$$\alpha_{\text{cyl}}(\mathbf{r}) = \left( \frac{r_n - c_n}{R_h} \right)^2 + \left( \frac{r_e - c_e}{R_h} \right)^2 - 1$$

$$\alpha_{\text{pl}}(\mathbf{r}) = \left( \frac{r_d - c_d}{R_h} \right) + \frac{\tan \gamma_h}{\lambda_h} \left( \tan^{-1} \left( \frac{r_e - c_e}{r_n - c_n} \right) - \psi_h \right)$$

where the initial position along the helix is

$$\mathbf{r}(0) = \mathbf{c}_h + \begin{pmatrix} R_h \cos \psi_h \\ R_h \sin \psi_h \\ 0 \end{pmatrix}.$$

$\mathbf{c}_h$  is the center of the helix,  $R_h$  is the radius,  $\gamma_h$  is the climb angle.



# Dubins Airplane Paths

Given the start configuration  $\mathbf{z}_s = (z_{ns}, z_{es}, z_{ds}, \psi_s)^\top$  and the end configuration  $\mathbf{z}_e = (z_{ne}, z_{ee}, z_{de}, \psi_e)^\top$  and the turn radius  $R$ , let  $L_{\text{car}}(R, \mathbf{z}_s, \mathbf{z}_e)$  be the length of the Dubins car path.

Recall that  $\bar{\gamma}$  is the limit of the flight path angle. There are three possible cases for the commanded altitude gain:

**Low Altitude:**

$$|z_{de} - z_{ds}| \leq L_{\text{car}}(R_{\min}) \tan \bar{\gamma},$$

i.e., the altitude gain can be achieved by following the Dubins car path with a flight path angle  $|\gamma^c| \leq \bar{\gamma}$ .

**High Altitude:**

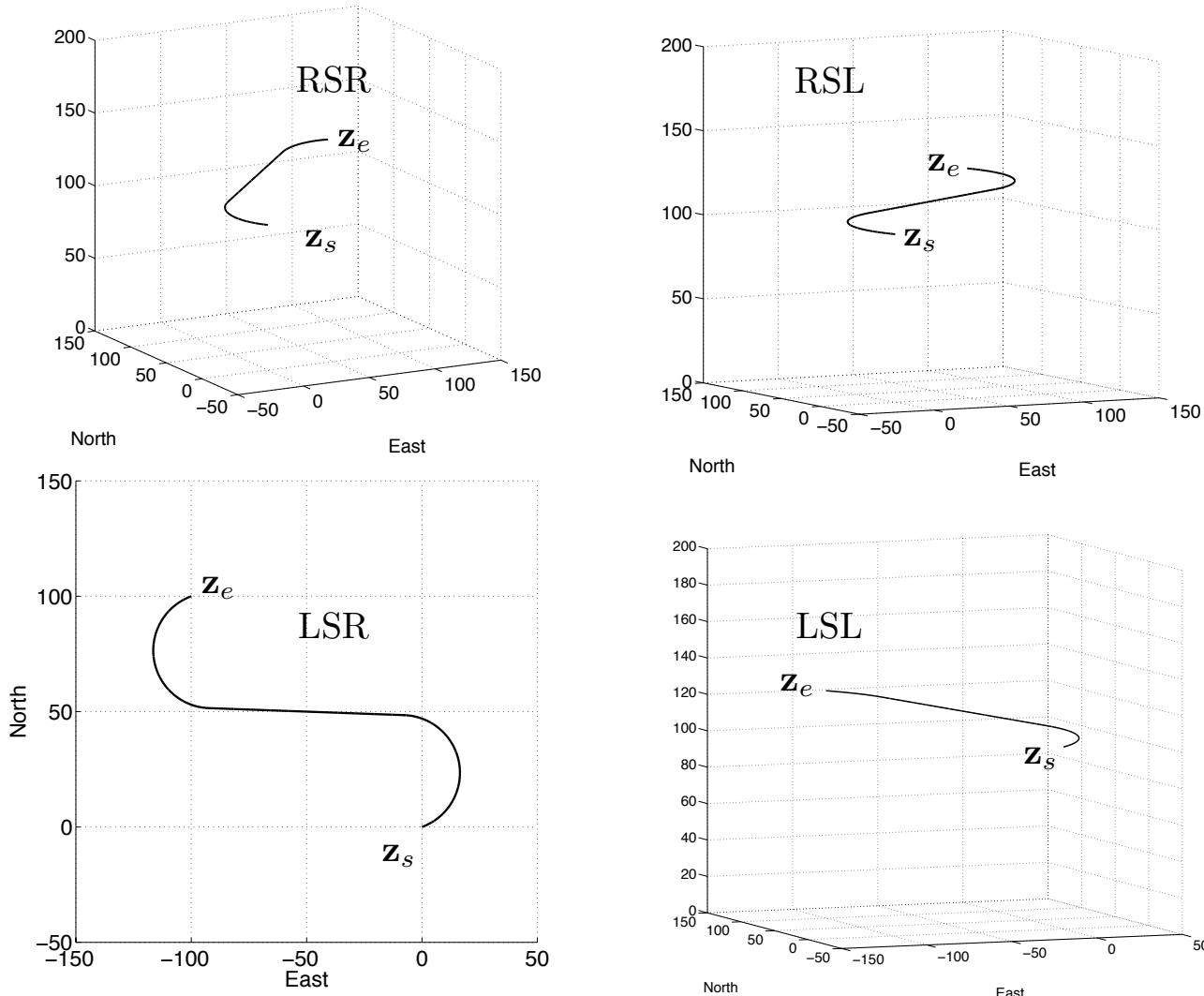
$$|z_{de} - z_{ds}| > [L_{\text{car}}(R_{\min}) + 2\pi R_{\min}] \tan \bar{\gamma}.$$

i.e., the altitude gain is larger than following the Dubins car path plus one orbit, at flight path angle  $\bar{\gamma}$ .

**Medium Altitude:**

$$L_{\text{car}}(R_{\min}) \tan \bar{\gamma} < |z_{de} - z_{ds}| \leq [L_{\text{car}}(R_{\min}) + 2\pi R_{\min}] \tan \bar{\gamma}.$$

# Low Altitude Dubins Airplane Paths

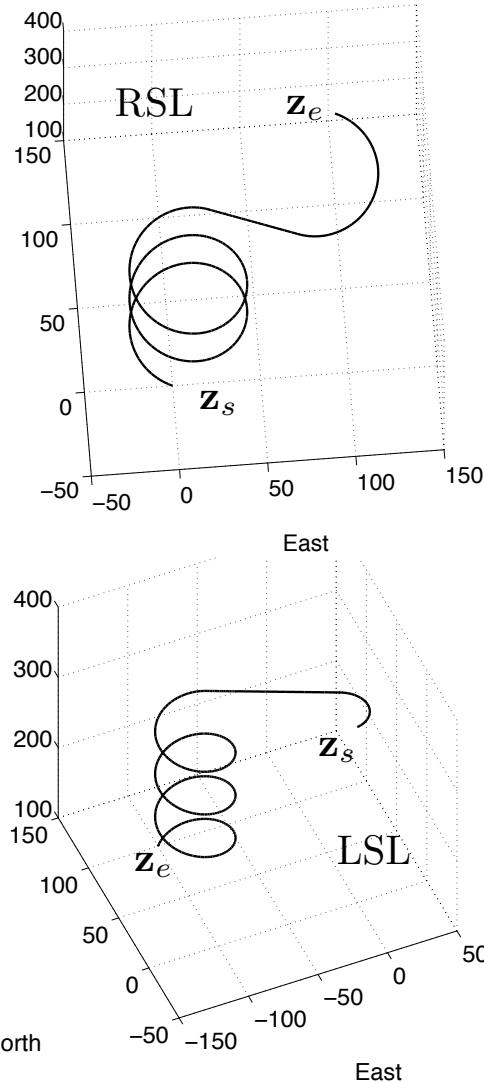
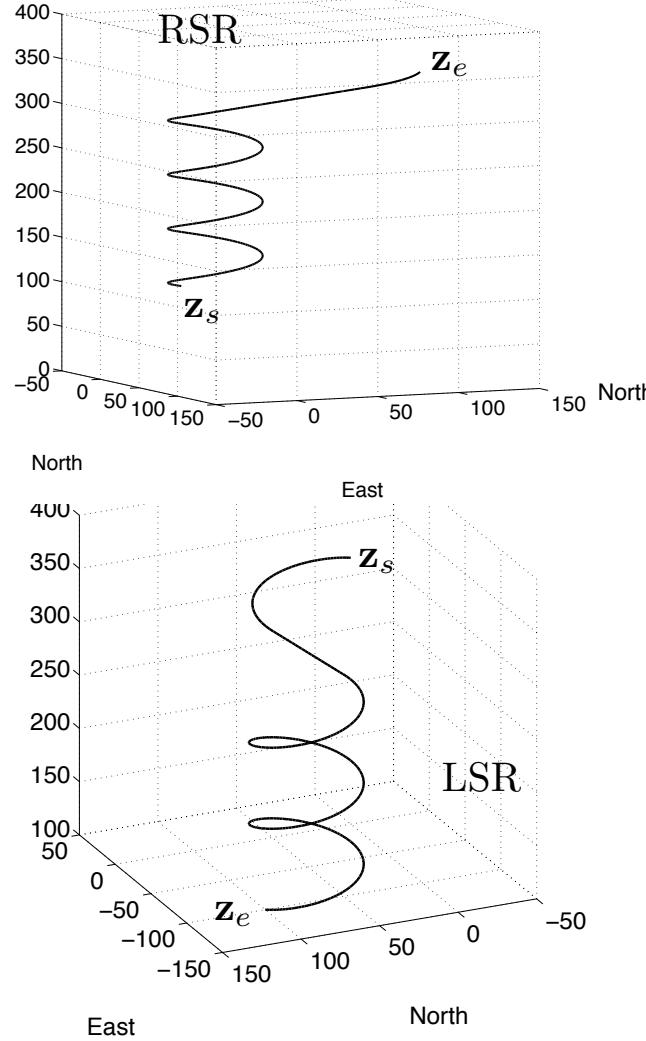


$$\gamma^* = \tan^{-1} \left( \frac{|z_{de} - z_{ds}|}{L_{\text{car}}(R_{\min})} \right)$$

$$R^* = R_{\min}$$

$$L_{\text{air}}(R_{\min}, \gamma^*) = \frac{L_{\text{car}}(R_{\min})}{\cos \gamma^*}.$$

# High Altitude Dubins Airplane Paths



Find smallest integer  $k$  such that

$$(L_{\text{car}}(R_{\min}) + 2\pi k R_{\min}) \tan \bar{\gamma} \leq |z_{de} - z_{ds}| < (L_{\text{car}}(R_{\min}) + 2\pi(k+1)R_{\min}) \tan \bar{\gamma}.$$

Increase the radius  $R^*$  so that

$$(L_{\text{car}}(R^*) + 2\pi k R^*) \tan \bar{\gamma} = |z_{de} - z_{ds}|.$$

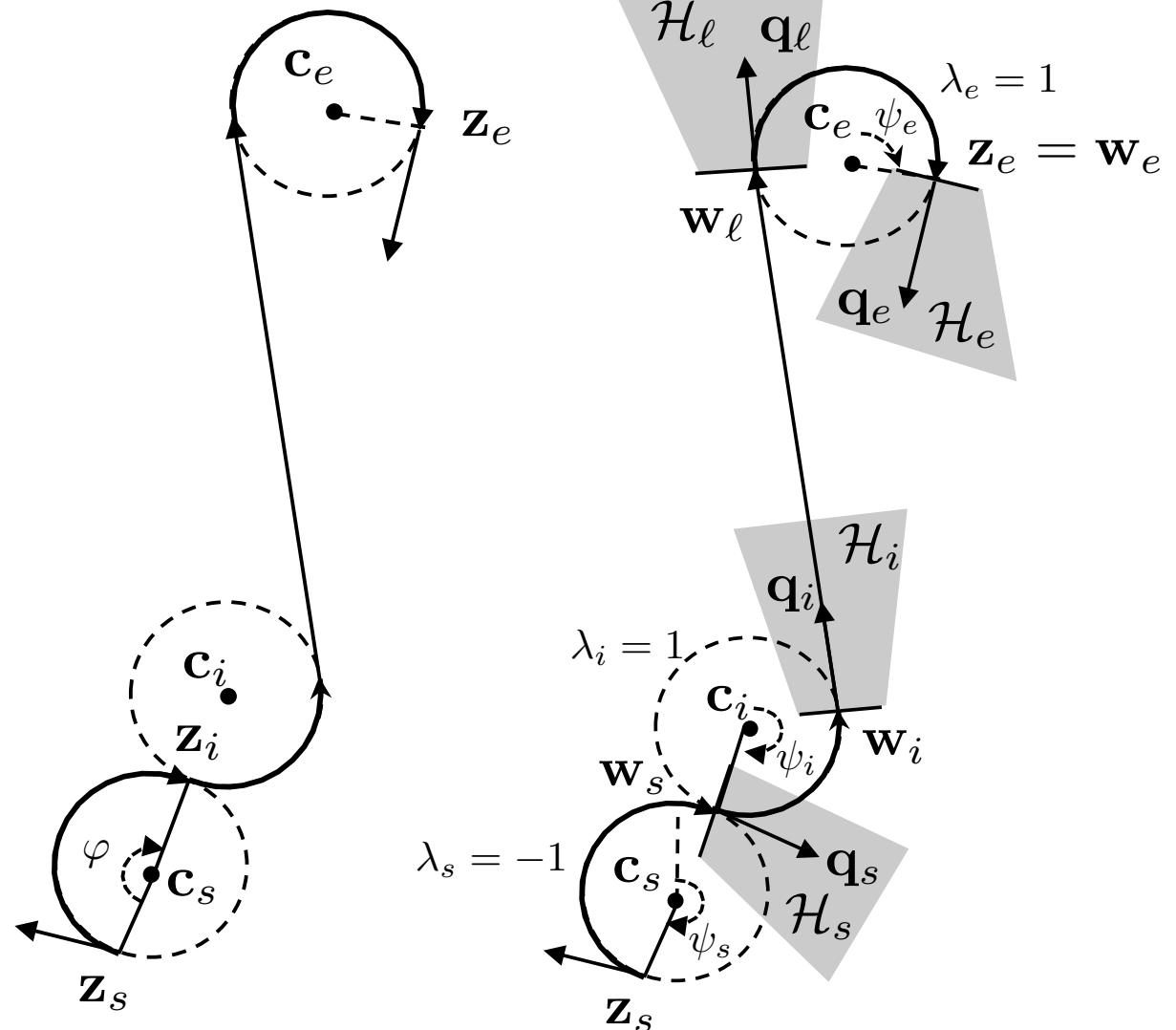
The resulting path is

$$L_{\text{air}}(R^*, \bar{\gamma}) = \frac{L_{\text{car}}(R^*)}{\cos \bar{\gamma}}.$$

# Medium Altitude Dubins Airplane Paths

Key idea: Add an intermediate helix along the path.

Could add intermediate helix at start, end, or in the middle of path.



# Medium Altitude Dubins Airplane Paths

