

MCTrans++ Reference Manual

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I. INTRODUCTION

MCTrans++ is the scoping tool used by the CMFX project and others for designing centrifugal magnetic mirrors.

II. MCTrans++: A USER'S GUIDE

MCTrans++ is driven from a configuration file. This file is written in the TOML language. This language endeavours to be transparent and easy to use. The configuration file is broken up into blocks. ARRANGE THE BLOCKS (or finish writing this manual).

III. THE PHYSICS MODEL OF MCTrans++

MCTrans++ solves simplified transport equations for the centrifugally-confined plasma. The underlying models are all based on the assumption that the plasma is well-confined and that the thermal Mach number is large compared to one.

In many places we use formulae straight from the NRL Plasma Formulary.

A. Fundamental Equations

As with any transport solver, MCTrans++ solves equations for the fluid-like conserved quantities – particles, energy, and momentum. We work in the usual (R, ϕ, Z) cylindrical coordinate system. The magnetic field lies purely in the $R - Z$ plane,^[1] and is given by

$$\mathbf{B} = \nabla\psi \times \nabla\phi, \quad (1)$$

where ψ is the poloidal flux function (proportional to the toroidal component of the vector potential). The electric field is given by

$$\mathbf{E} = -\nabla\psi \frac{d\Phi}{d\psi} - \nabla\varphi, \quad (2)$$

where we have split off the dominant radial electric field into the first term (which gives rise to the sonic rotation) and put all other electric field variation into the second term. Estimating the size of the two terms, we see that

$$\Phi \sim \frac{aMT_e}{e\rho_i} \gg \varphi \sim \frac{T_e}{e}, \quad (3)$$

where a is a typical radial scale length, M the thermal Mach number, and ρ_i the thermal ion Larmor radius.

We assume that the flow velocity \mathbf{u} is the same for all species and given by

$$\mathbf{u} = \omega R^2 \nabla\phi, \quad (4)$$

where ω is the toroidal angular velocity. We also assume that the angular velocity is only a function of flux-surface-label ψ .

The underlying transport equations are thus:

$$\frac{dn_s}{dt} + \nabla \cdot \Gamma_s = S_{ns} \quad (5)$$

$$\frac{d}{dt} \left(\frac{3}{2} n_s T_s \right) + \nabla \cdot \mathbf{q}_s = (\nabla\psi \cdot \nabla \cdot \nabla\phi) R^2 \frac{d\omega}{d\psi} + Q_s + S_{Es} \quad (6)$$

$$\frac{d\omega}{dt} + \nabla \cdot (\nabla \cdot R^2 \nabla\phi) = \mathbf{j} \times \mathbf{B} \cdot R^2 \nabla\phi + S_\omega. \quad (7)$$

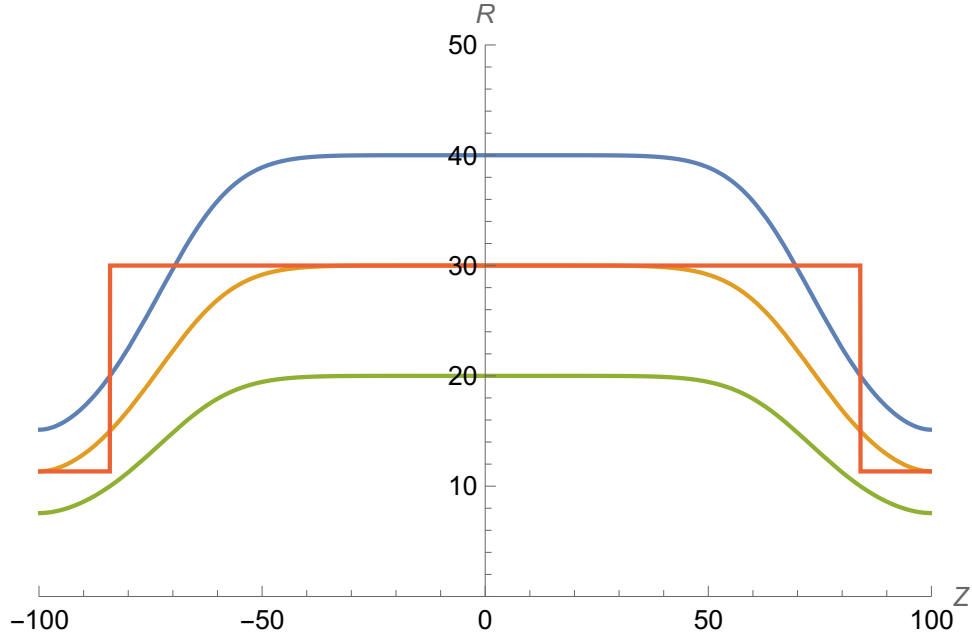


FIG. 1. An example plot of field lines and the square-well approximation to the central field line

In these equations the transport fluxes $\mathbf{\Gamma}_s$ and \mathbf{q}_s are the particle and heat fluxes of each species, and the species-summed momentum flux tensor is denoted by $\overleftrightarrow{\pi}$. We have also included arbitrary sources of particles S_{ns} , energy S_{Es} , and angular momentum $S_{\omega s}$; these source terms will be used to account for collisionless parallel losses and energy sources such as alpha-particle heating.

Currently, **MCTrans++** does not solve all these equations. In fact, we only solve for the transport of heat. The particle transport equation is assumed to contain a source that is feedback controlled to maintain the electron density at a fixed value. This restriction may be lifted at a later date.

The momentum transport equation is more interesting. We know that the angular velocity is driven by $\mathbf{E} \times \mathbf{B}$ rotation, and so is given by

$$\omega = -\frac{d\Phi}{d\psi}, \quad (8)$$

where the effect of φ in \mathbf{E} is small and can be neglected. Due to the electrical configuration of a centrifugal mirror (see figure) we often wish to consider the behaviour of a centrifugal plasma given a fixed input voltage. In this case, the momentum transport equation becomes an equation to determine the radial current drawn from the power supply in terms of other quantities. We never need to solve (7) for ω in this setup. If we instead held the input power or current fixed then (7) would be solved as normal.

In steady-state operation, **MCTrans++** sets the time derivatives to zero and solves the ensuing nonlinear algebraic equations to balance heat generation and heat losses. In the following subsections we will explain the approximations used to calculate those heat losses explicitly in terms of the system state.

B. Approximations to the Magnetic Geometry

The simplest, and most transparent, geometric approximation is the “square well” model. In this model we assume the field lines to be straight, directed in the Z direction, with a step-function shape and a step function in field strength. We demonstrate this in Fig. 1.

C. The Centrifugal Potential

Many results have been derived for confinement in mirror machines which possess an electrostatic potential that varies along the field line. We can make use of these results by noting the following fact: the potential energy of a

charged particle on a rotating field line at radius R with angular velocity ω is

$$\Xi_s = Z_s e \varphi - \frac{m_s}{2} \omega^2 R^2. \quad (9)$$

We can thus reuse results from existing papers simply by making the substitution $Z_s e \varphi \rightarrow \Xi_s$.

Physically, this electrostatic potential exists to keep the electrons (which are light and barely affected by the centrifugal force) next to the ions which are pushed to regions of large R by the centrifugal force. Hence, the potential φ has to be solved for by insisting that the plasma is quasineutral along field lines (and that the loss rate is ambipolar). If we assume that the plasma rotates at a large Mach number $M \gg 1$, then the plasma is well-confined and the confinement time is long compared to the collision time (this can be checked *a posteriori*). In such a situation the plasma is locally Maxwellian (equivalently it is in LTE) and we can write the density of species s as [2, 3]:

$$n_s = N_s(\psi) \exp\left(-\frac{\Xi_s}{T_s}\right). \quad (10)$$

If we now insist that the plasma is made up of ions (mass m_i and charge $Z_i e$) and electrons (mass m_e and charge $-e$) then quasineutrality reads

$$Z_i N_i \exp\left(-\frac{Z_i e \varphi}{T_i} + \frac{m_i}{2T_i} \omega^2 R^2\right) = N_e \exp\left(\frac{e \varphi}{T_e} + \frac{m_e}{2T_e} \omega^2 R^2\right). \quad (11)$$

Without loss of generality, we can pick a baseline for φ such that $Z_i N_i = N_e$ (to see this, average along a field line, use the fact that neither N_s nor T_s varies along the field line). Furthermore, by neglecting the term containing the electron mass, we can solve the resulting equation for φ :

$$\varphi = \left(\frac{Z_i e}{T_i} + \frac{e}{T_e}\right)^{-1} \frac{m_i}{2T_i} \omega^2 R^2, \quad (12)$$

up to a possible constant offset. It is clear that this potential is $\mathcal{O}(M^2 T_e / e)$ and is, in fact, the leading order term in an asymptotic series in M^{-1} . [4] To compute the next-order terms in this series we need to know about lost particles and hence parallel transport. This is tackled in the next section. We end with a convenient expression for the potential drop from the centre of a flux surface (at $R = R_{\max}$) in terms of suitably normalized variables:

$$\frac{e \varphi}{T_e} = \left(\frac{Z_i}{\tau} + 1\right)^{-1} \frac{M^2}{2} \left(\frac{R^2}{R_{\max}^2} - 1\right) + \mathcal{O}(1), \quad (13)$$

where we let $\tau = T_i / T_e$ be the temperature ratio, and we have defined the sonic Mach number $M = \omega R_{\max} / c_s$ in terms of the sound speed $c_s^2 = T_e / m_i$. [5] This is only the leading-order term in a $M \gg 1$ expansion, and so we collect all higher-order terms and denote them by φ_0 . Note that if $Z_i = \tau = 1$ then we get the usual $M^2/4$ scaling for the potential drop. It is also useful to note that, as a consequence of flux conservation

$$\frac{B_{\min}}{B_{\max}} = \left(\frac{R_{\max}}{R_{\min}}\right)^2, \quad (14)$$

and so we can relate the ratio of the radius of the flux surface at throat and in the central cell to the ‘‘Mirror Ratio’’ given by the ratio of magnetic field strengths.

For electrons, the only term in the potential energy is the electrostatic potential:

$$\Xi_e = \left(\frac{Z_i}{\tau} + 1\right)^{-1} \frac{M^2}{2} T_e \left(1 - \frac{R^2}{R_{\max}^2}\right) - e \phi_0, \quad (15)$$

but for ions we need to include the centrifugal potential to obtain

$$\Xi_i = \left(\frac{Z_i}{\tau} + 1\right)^{-1} \frac{M^2}{2} T_i \left(1 - \frac{R^2}{R_{\max}^2}\right) + Z_i e \phi_0, \quad (16)$$

where we have picked the constant offset of φ such that $\Xi_i = \Xi_e = 0$ at the midplane ($Z = 0$, $R = R_{\max}$). Again, φ_0 is the higher-order part of φ that must be determined by evaluating the parallel losses.

N.B. In contrast to a tandem mirror, where the only confining potential is electric, the addition of the centrifugal term allows the potential to be confining for *both* the species.

D. Parallel Transport

We assume that the plasma is hot enough to be in the collisionless regime where the particle bounce time (inside the potential well formed by the centrifugal force) is extremely short compared to the particle collision time. This is manifestly true in reactor-grade plasmas ($\nu_{ii}L_{\parallel}/v_{\text{th}_s} \sim 10^{-5}$ or smaller) but is even valid for warm plasmas above a few hundred electron Volts in temperature. The collisionality parameter is reported and if it is not much less than one the results of **MCTrans++** are not valid.

In this collisionless regime we use formulae that are derived in the manner originally used by Pastukhov [6] for the case of a tandem mirror with an electron-confining electrostatic potential. Pastukhov originally derived his results for electrons alone. We need the result for a multispecies plasma. We can find this result in Catto and Bernstein [7] by taking the square-well limit of (40) of that work to obtain the particle loss rate in our notation:

$$\left(\frac{\partial n_s}{\partial t}\right)_{\text{EndLosses}} = - \left(\frac{2n_s\Sigma}{\sqrt{\pi}}\right) \nu_s \frac{1}{\ln(R_{\text{mirror}}\Sigma)} \frac{\exp(-\Xi_s/T_s)}{\Xi_s/T_s}, \quad (17)$$

where $\Sigma = Z_i + 1$ for electrons and $\Sigma = 1$ for ions, and ν_s is the appropriate collision frequency for species s . For electrons this is the combination of electron-electron and electron-ion collisions. For ions this is just the ion-ion collision frequency.

Note that this equation only agrees with the results of Pastukhov [6] and Cohen et al. [8] in the limit of $R_{\text{mirror}} \rightarrow \infty$. The error induced by not knowing this prefactor accurately is much smaller than the approximation by a square well, and is comparable with the effect of several other approximations made in the analytic work.

We anticipate upgrading **MCTrans++** to use the full formulae of Catto and Bernstein [7] in the near future, thereby including some effect of the actual magnetic geometry.

This particle loss rate can be used to compute heat losses by multiplying by Ξ_s – the energy loss is dominated by energetic particles, nullifying the extra power of Ξ_s in the denominator of (17). Similarly, loss of toroidal angular momentum can be computed by multiplying the particle loss rate by the angular momentum lost per ion (electrons carrying negligible momentum).

1. Ambipolar Parallel Losses and Solving for φ

In the formula (17) for the losses we see that Ξ_s appears in the exponential. The leading order part of Ξ_s is $\mathcal{O}(M^2T_s)$, so this exponential is what strongly suppresses the collisional loss rate. Expanding this exponential schematically we have

$$\exp\left(-\frac{\Xi_s}{T_s}\right) \approx \exp[-(\dots)M^2] \exp(-Z_s e\varphi_0/T_s), \quad (18)$$

and we see that even though φ_0 is small compared to the leading-order part of the potential it has an $\mathcal{O}(1)$ effect on the loss rate and must be accounted for.

We find φ_0 by equating the electron and ion loss rates along the field line to enforce zero net charge loss along the field line. **N.B. This part of the code can be a little temperamental, and if you find a case that doesn't work it may be because you're starting to search for an equilibrium from a starting point that is so poorly confined that quasineutrality cannot be satisfied within the bounds that the code is searching.**

E. Perpendicular Transport

To completely evaluate the heat transport equations we need expressions for \mathbf{q}_s and $\nabla \cdot \mathbf{q}_s$. We consider only the classical collisional contribution to these transport fluxes. Turbulent transport should be fully suppressed by the flow shear.

We handle the heat flux first. From (2.14) of Braginskii [9] the collisional ion heat flux in a strongly-magnetized plasma is

$$\mathbf{q}_i = -\chi_{i\parallel} \mathbf{b}\mathbf{b} \cdot \nabla T_i - \chi_{i\perp} \nabla_{\perp} T_i + \frac{5}{2} \frac{n_i T_i}{m_i \Omega_i} \mathbf{b} \times \nabla T_i. \quad (19)$$

Now, in the collisionless limit, $T_i = T_i(\psi)$ and so the first term vanishes, and the third term is purely toroidal. Thus, when we evaluate the divergence of the heat flux, we obtain (using axisymmetry)

$$\nabla \cdot \mathbf{q}_i = \nabla \cdot (\chi_{i\perp} \nabla_{\perp} T_i). \quad (20)$$

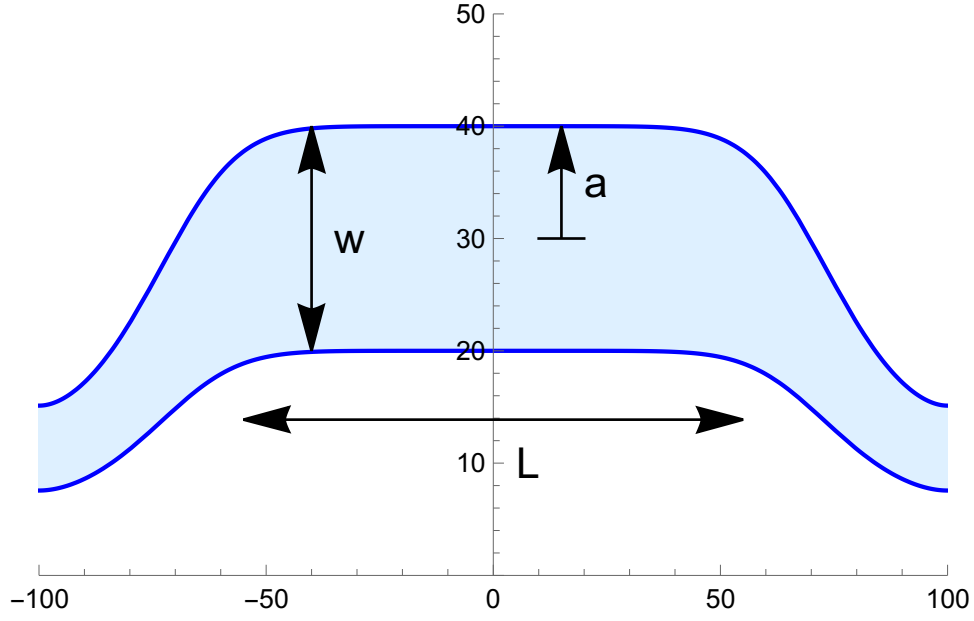


FIG. 2. Plasma column showing its width w , length L , and scale length a

To estimate this term, we assume that all the plasma profiles vary on a scale a that is related to the width of the plasma column w by $a = w/2$, see Fig. 2 for more details. Thus, we have that

$$\nabla \cdot \mathbf{q}_i \approx \frac{1}{a^2} \chi_{i\perp} T_i = \frac{2n_i T_i^2}{m_i \Omega_i^2 \tau_i a^2}, \quad (21)$$

where we have used (2.16) of Braginskii [9] for $\chi_{i\perp}$ and τ_i is the ion-ion collision time.

For electrons, the same geometric algebra applies and we have

$$\nabla \cdot \mathbf{q}_e \approx \frac{1}{a^2} \chi_{e\perp} T_e = \frac{4.66 n_e T_e^2}{m_e \Omega_e^2 \tau_e a^2}, \quad (22)$$

which is approximately $\sqrt{m_e/m_i}$ smaller than the ion heat loss, and usually negligible.

We only compute the stress tensor for the ions, electron perpendicular viscosity is at least m_e/m_i smaller than the ion viscosity and always negligible. To compute the Braginskii viscous stress tensor, we need to know the rate of strain tensor $\vec{\dot{W}}$:

$$\vec{\dot{W}} = (\nabla \mathbf{u}) + (\nabla \mathbf{u})^T - \frac{2}{3} (\nabla \cdot \mathbf{u}) \vec{I}, \quad (23)$$

which, upon using $\mathbf{u} = \omega R^2 \nabla \phi$, becomes

$$\vec{\dot{W}} = R^2 \frac{d\omega}{d\psi} (\nabla \psi \nabla \phi + \nabla \phi \nabla \psi) \approx \frac{R}{a} \omega \quad (24)$$

Evaluating this on the midplane, we see that in Braginskii's cartesian coordinates (with z along \mathbf{b}) the only nonzero component of $\vec{\dot{W}}$ is W_{xy} (equivalently W_{yx}). Thus, using (2.21) of Braginskii, we can compute the nonzero components of the stress tensor. The quantities we need are

$$\nabla \cdot (\vec{\pi} \cdot R^2 \nabla \phi) \approx \frac{1}{a} \pi_{xy} R = -\frac{R}{a} \frac{3}{10} \frac{n_i T_i}{\Omega_i^2 \tau_i} W_{xy} = -\frac{R}{a} \frac{3}{10} \frac{n_i T_i}{\Omega_i^2 \tau_i} \frac{R}{a} \omega, \quad (25)$$

and

$$\vec{\pi} : \nabla \mathbf{u} = \frac{1}{2} \pi_{xy} W_{xy} \approx -\frac{3}{10} \frac{n_i T_i}{\Omega_i^2 \tau_i} \frac{R^2 \omega^2}{a^2}. \quad (26)$$

Note that, because we are using Braginskii's formulae, we also have to use his formula for the collision times (see Braginskii [9]) which differ by $\sqrt{2}$ from some other definitions of τ_i .

F. Alpha Particles and Nuclear Physics

Our fundamental model for alpha particles is that they are all born with a delta-function distribution at the birth energy of $E_\alpha = 3.52$ MeV:

$$\left(\frac{\partial f_\alpha}{\partial t}\right)_{\text{Source}} = \frac{S_\alpha \delta(v - v_*)}{4\pi v_*^2} \quad (27)$$

where v_* is the birth velocity corresponding to E_α and S_α is the birth rate of alphas per unit time per unit volume.

1. Prompt Alpha Losses

Alpha particles are born isotropically. Thus, a fraction of them are born directly into the unconfined region of velocity space. The birth energy of alphas E_α is much greater than the centrifugal potential which is roughly $M^2 T_e / 4$ (at fusion temperatures and parameters this remains less than 0.5 MeV). We thus model the loss region for energetic alphas as a cone, and only classical mirror confinement applies, thus an alpha is lost if

$$\mu_\alpha B_{\text{max}} > E_\alpha. \quad (28)$$

Integrating this over all velocity space, we see that the fraction of alphas that is lost is

$$f_{\text{lost}} = 1 - \sqrt{1 - \frac{1}{R_{\text{mirror}}}}. \quad (29)$$

This fraction of alpha particles is removed from **MCTrans++** and hurled against the end plates. This prompt loss of alpha particles is taken into account in assessing quasineutrality.

2. Collisional Alpha Losses

Currently, we do not have any explicit collisional losses of alpha particles. However, the approximate lifetime of alpha particles in the machine is (under the twin assumptions that of $R_{\text{mirror}} \gg 1$ and that we can treat alphas like main ions, see e.g. Ryutov [10])

$$\tau_\alpha \approx 0.4 \tau_{\alpha i} \ln R_{\text{mirror}}, \quad (30)$$

where $\tau_{\alpha e}$ is the alpha-ion collision time (alpha-electron collisions do not change the pitch-angle of the alpha particles), which is marginally longer than the time it takes the alphas to deposit a reasonably large amount of their energy into electrons and ions. Really we should solve the Fokker-Planck kinetic equation for alpha particles with a source and a loss cone as is done in Santarius and Callen [11].

3. Alpha Heating

Currently, all the energy in the retained alpha particles is deposited into the electron species as heating through collisions. This is a pessimistic assumption as electron heating leads to a lower Mach number, faster electron losses, an increasingly electron-confining φ , and hence increased ion losses.

G. Neutral Transport

We currently have no model of transport due to neutral particles. A first step towards this will be implementing a diagnostic for the neutral mean free path in our plasma. In the limit of either very small or very long mean free path, we may be able to make further approximations to evaluate the losses from charge exchange.

N.B. Until more neutral physics is implemented, we have no way to handle self-consistent fuelling scenarios. The only reasonable assumption is that losses due to neutrals are small and feedback control is used to target a fixed electron density.

H. Radiative Processes and Impurities

There are two ways to model impurities in `MCTrans++`. Firstly is a “lumped impurity” that only changes the effective charge state Z_{eff} and provides *only* bremsstrahlung radiation. It does not dilute the main ion species, so quasineutrality is enforced by only considering the main ions and electrons.

1. Bremsstrahlung and Synchrotron Radiation

Taking the formulae for bremsstrahlung from the NRL formulary [12] and writing it in convenient units we have

$$P_{\text{rad}} = 5.34 \times 10^3 Z_{\text{eff}} \left(\frac{n_e}{10^{20} \text{m}^{-3}} \right)^2 \left(\frac{T_e}{1 \text{keV}} \right)^{1/2} \text{W/m}^3, \quad (31)$$

where we have used the definition

$$Z_{\text{eff}} = \frac{1}{n_e} \sum_s Z_s^2 n_s, \quad (32)$$

of the effective charge state of the plasma (summation taken over all positively charged species). Similarly, we can take the synchrotron radiation formula from the formulary [12] and write it as

$$P_{\text{rad}} = 6.21 \times 10^3 \left(\frac{B}{1 \text{T}} \right)^2 \left(\frac{n_e}{10^{20} \text{m}^{-3}} \right) \left(\frac{T_e}{1 \text{keV}} \right) \text{W/m}^3. \quad (33)$$

The plasma is assumed to be optically thin, and so all radiation is lost onto the first wall.

2. Line Radiation

Without a better model for the impurity species that are present (including multiple charge states) we cannot reliably predict the amount of line radiation lost from the plasma.

N.B. Because of the lack of ionization and radiative cooling, one should view low-temperature outputs from `MCTrans++` extremely sceptically!

Appendix A: Full Syntax for `MCTrans++` configuration files

Appendix B: Non-Physical Implementation

The use of “fudge-factors” has been included to simulate arbitrarily better or worse confinement. The default value is 1, and values less than or greater than 1 result in better or worse confinement, respectively. The fudge factors are applied to loss rates (either particle or heat). There are separate fudge factors for perpendicular and parallel, and viscous and thermal transport.

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- [1] Note1, estimates of ripple / mis-alignment induced transport can be computed, but it is currently out of scope for `MCTrans++`.
 - [2] P. J. Catto, I. B. Bernstein, and M. Tessarotto, *Phys. Fluids* **30**, 2784 (1987).
 - [3] I. G. Abel, G. G. Plunk, E. Wang, M. A. Barnes, S. C. Cowley, W. Dorland, and A. A. Schekochihin, *Rep. Prog. Phys* **76**, 116201 (2013).
 - [4] Note2, in computing the densities in (10), we have integrated over a full Maxwellian distribution, neglecting the fact that some small number of high-energy particles are in fact lost along the field line. This is a consistent approximation as we have determined that the potential barrier is $\mathcal{O}(M^2 T_e)$, which to leading order is effectively infinite.
 - [5] Note3, this is not the speed at which sound waves propagate in a warm plasma, but provides a very convenient normalization. It is the cold-ion limit of the sound speed, and we will continue to call it the sound speed despite this abuse of terminology.

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