

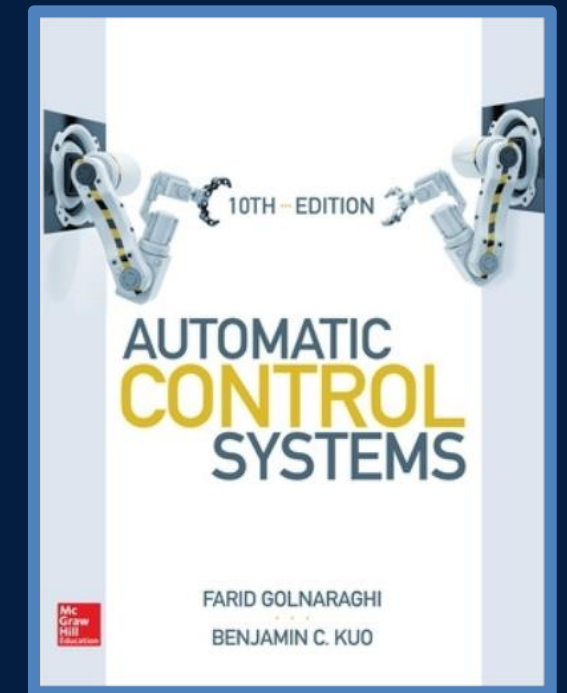
# HUMBER ENGINEERING

MENG 3510 – Control Systems  
LECTURE 4

# LECTURE 4

## Stability of Linear Control Systems

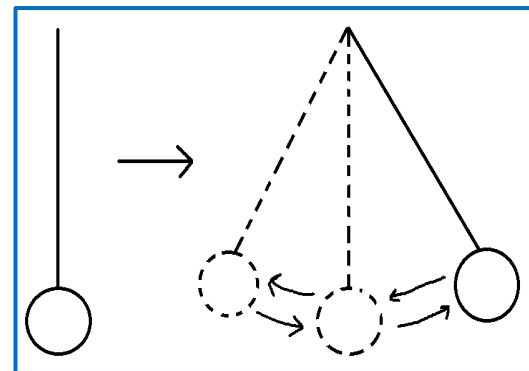
- Introduction to Stability
- Methods of Determining Stability
- Routh-Hurwitz Criterion
  - Special Cases
- Control Systems Stability Analysis
- Case Study: Antenna Control System
- Stability Analysis in LTI State-Space Models



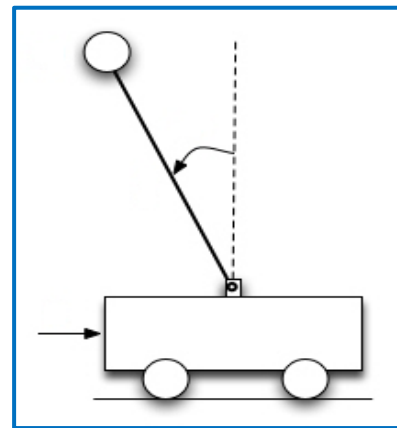
## Chapter 5

# Introduction to Stability

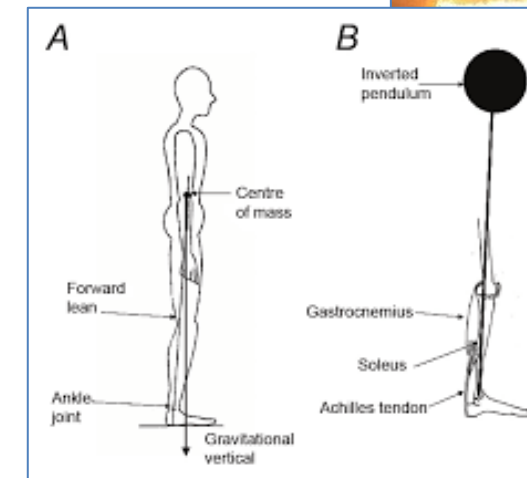
- In general, a **stable** system is the one that will
  - **Remain at rest** unless excited by an external source
  - **Return to rest** if all excitations are removed
- **Stability** is the most important specification of a control system.
- An **unstable** control system is generally useless.
- **Simple pendulum** hanging from the ceiling is a **stable** system, but an **inverted pendulum** is an **unstable** system.



**Simple Pendulum**



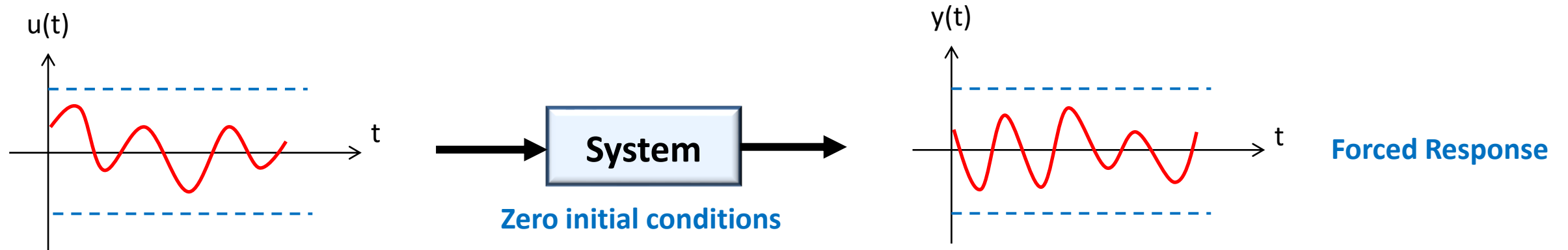
**Inverted Pendulum**



# Introduction to Stability

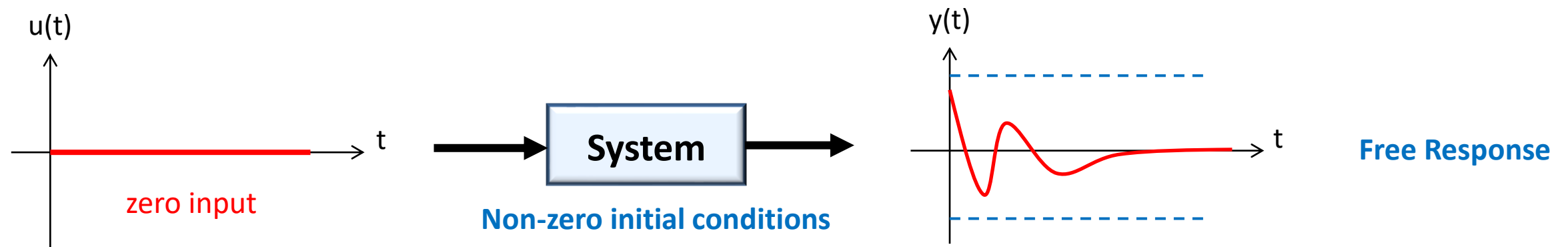
## □ Bounded-Input, Bounded-Output Stability (BIBO Stability)

- A system with **zero initial conditions** is **BIBO stable** if every bounded-input results in a bounded-output.



## □ Asymptotic Stability (Zero-Input Stability)

- A system with **zero input** is **asymptotically stable** if following conditions are satisfied:

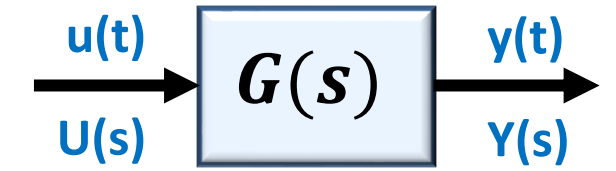


- In **LTI systems** the **asymptotic stability** is equivalent to **BIBO stability**, but in general they are different.

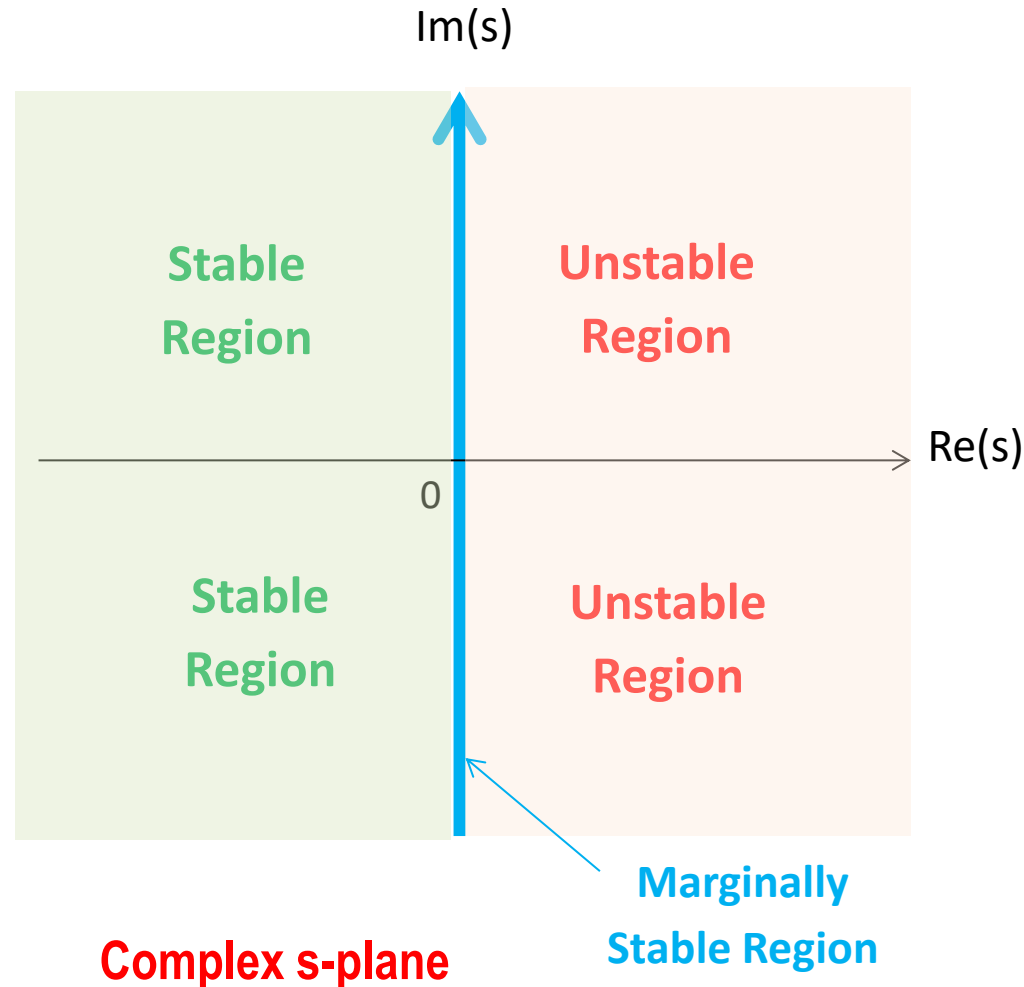
# Introduction to Stability

## □ Stability of Linear Dynamic Systems

- Consider the a LTI dynamic system with input  $u(t)$ , output  $y(t)$  and transfer function model of  $G(s)$



A linear dynamic system is **stable** if and only if all poles of  $G(s)$  are in the **left-half s-plane**



### Example 1

$$G_1(s) = \frac{10(s-1)}{(s+2)(s^2+5)}$$

$$\text{poles} \rightarrow \begin{cases} s_1 = -2 \\ s_{2,3} = \pm j\sqrt{5} \end{cases} \quad \text{Marginally Stable}$$

$$G_2(s) = \frac{2(s+2)}{(s+10)(s+3)}$$

$$\text{poles} \rightarrow \begin{cases} s_1 = -10 \\ s_2 = -3 \end{cases} \quad \text{Stable}$$

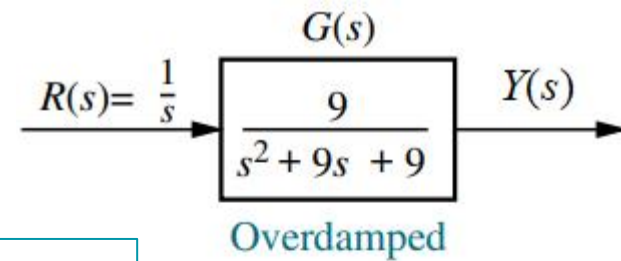
$$G_3(s) = \frac{10}{(s-10)(s^2+4)}$$

$$\text{poles} \rightarrow \begin{cases} s_1 = 10 \\ s_2 = \pm j2 \end{cases} \quad \text{Unstable}$$

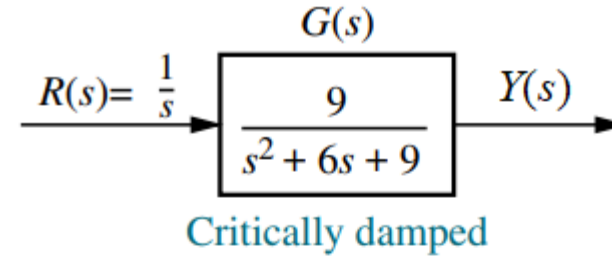
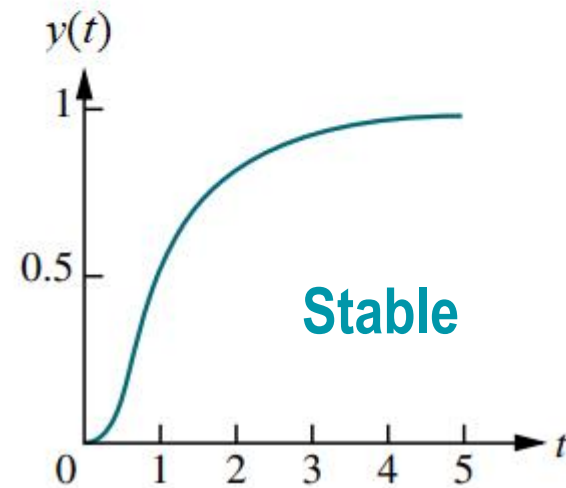
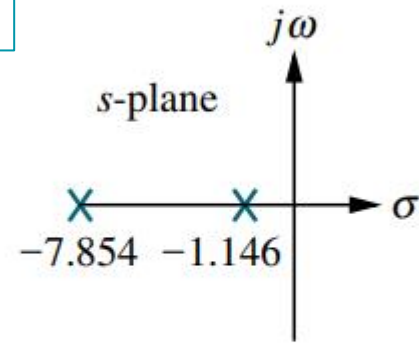
# Introduction to Stability

## Example 2

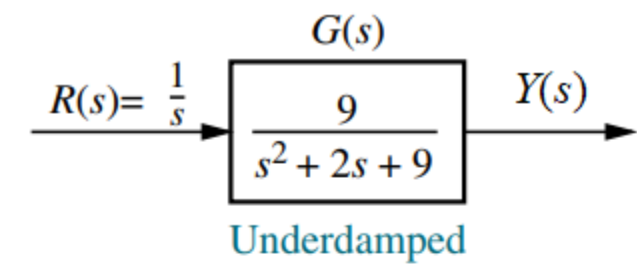
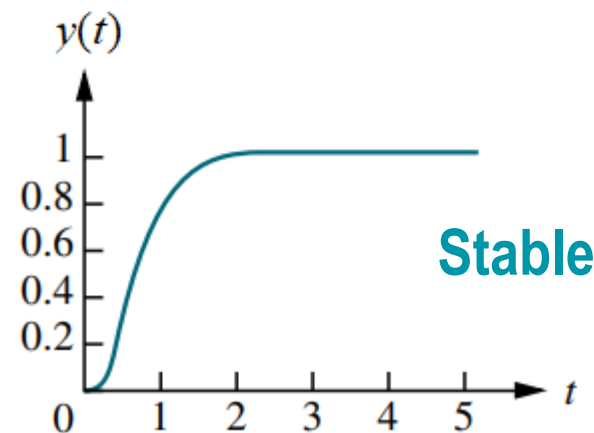
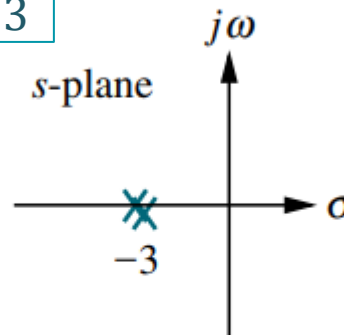
This example shows relationship of the step response, pole locations and stability in a second-order system.



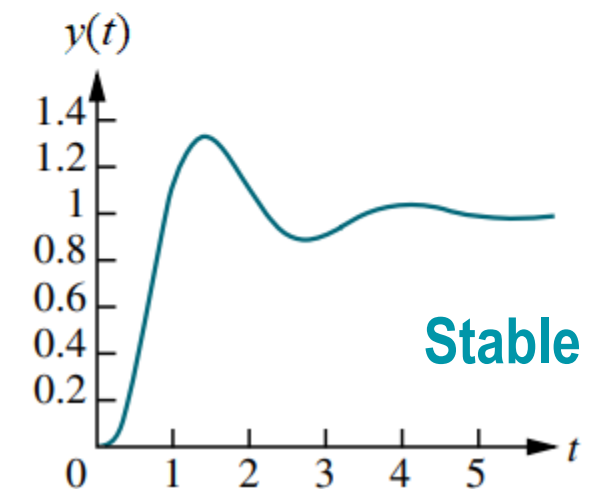
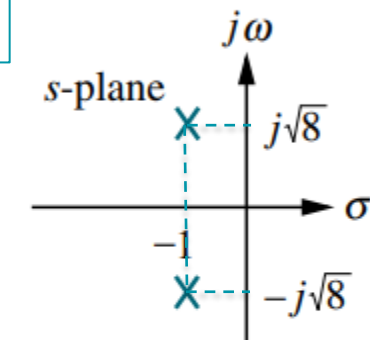
$$\zeta = 1.5$$
$$s_1 = -7.854,$$
$$s_2 = -1.146$$



$$\zeta = 1$$
$$s_1 = s_2 = -3$$



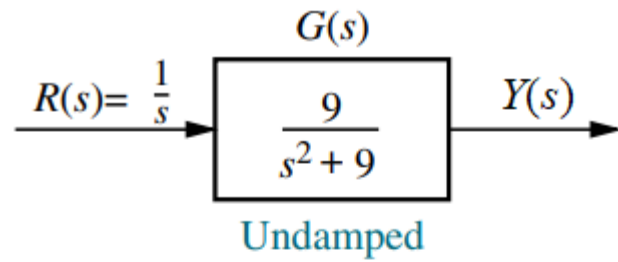
$$\zeta = 0.33$$
$$s_{1,2} = -1 \pm j\sqrt{8}$$



# Introduction to Stability

## Example 2

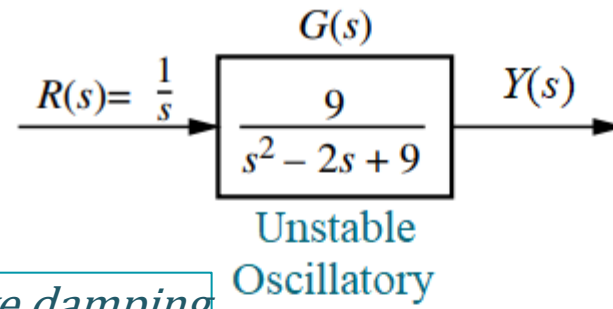
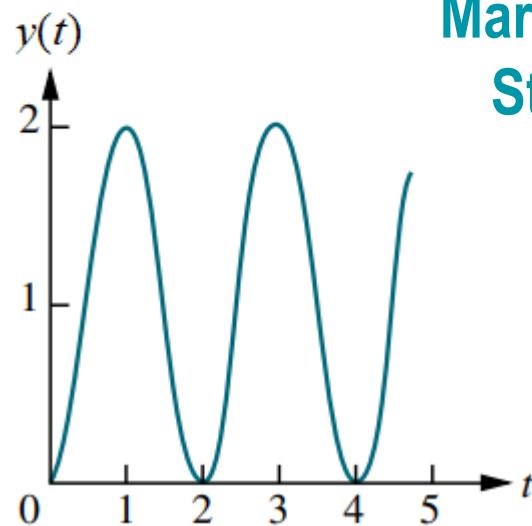
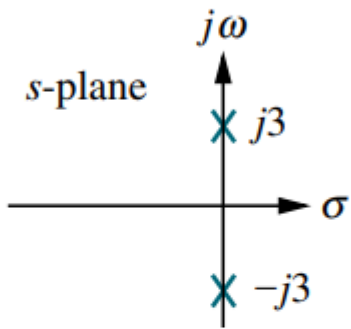
This example shows relationship of the step response, pole locations and stability in a second-order system.



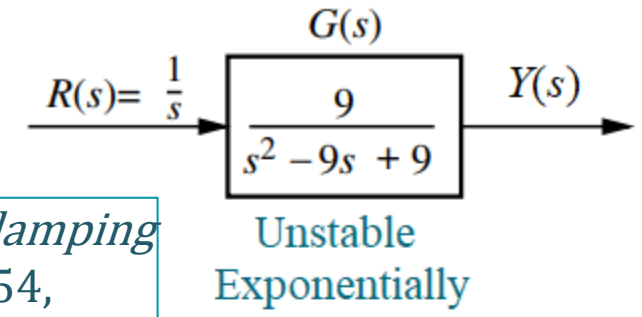
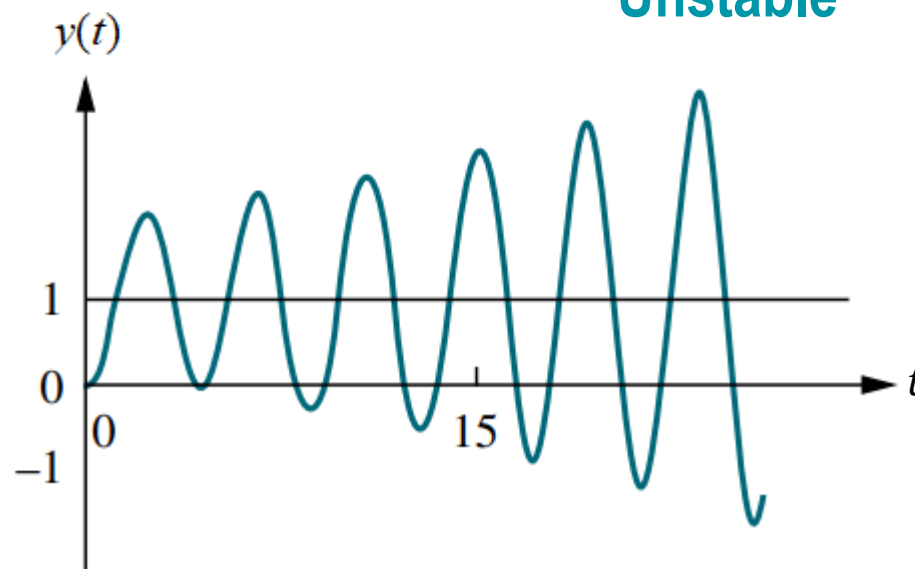
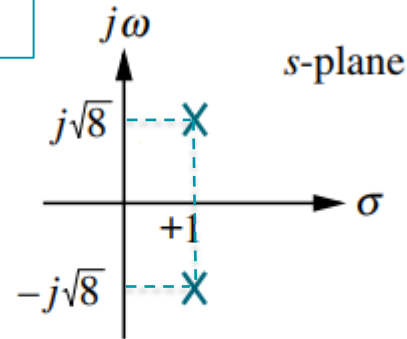
No damping

$$\zeta = 0$$

$$s_{1,2} = \pm j3$$

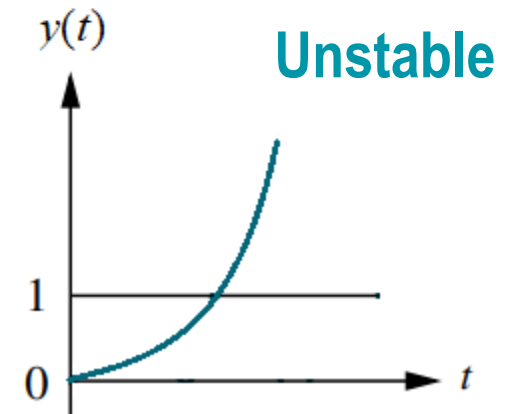
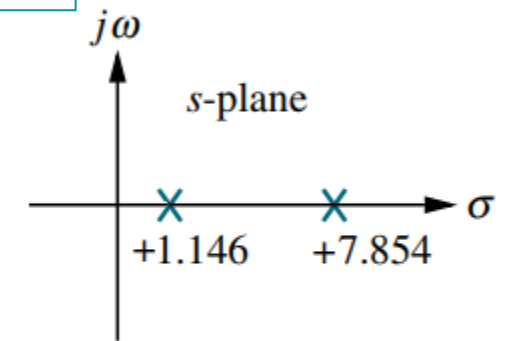


Negative damping

$$s_{1,2} = +1 \pm j\sqrt{8}$$


Negative damping

$$s_1 = +7.854,$$

$$s_2 = +1.146$$


# Methods of Determining Stability

- There are several methods to determine the stability of LTI systems **without** involving root solving.



- Routh-Hurwitz Criterion
- Root Locus Diagram
- Bode Diagram
- Nyquist Criterion

## □ Routh-Hurwitz Criterion

- Consider the following polynomial with **real coefficients**:

$$a_n s^n + a_{n-1} s^{n-1} + a_{n-2} s^{n-2} + \dots + a_1 s + a_0 = 0$$

- **Routh-Hurwitz Criterion** is an **algebraic method** to find the **number of roots** of the polynomial in the **right-half s-plane**.
- **Routh-Hurwitz Criterion** gives the **necessary** and **sufficient** condition for stability.



# Routh-Hurwitz Stability Criterion

1) Write the polynomial with real coefficients in the following form:

$$a_n s^n + a_{n-1} s^{n-1} + a_{n-2} s^{n-2} + \dots + a_1 s + a_0 = 0$$

2) If any of the coefficients are **zero** or **negative**, the polynomial has **roots** on the **right-half s-plane**.

## Example 3

Determine stability of the following LTI systems

$$G_1(s) = \frac{1}{3s^3 + s + 5}$$



Characteristic equation  $\rightarrow 3s^3 + 0s^2 + s + 5 = 0 \rightarrow G_1(s)$  is unstable

$$G_2(s) = \frac{1}{s^2 - 2s + 9}$$



Characteristic equation  $\rightarrow s^2 - 2s + 9 = 0 \rightarrow G_2(s)$  is unstable

$$G_3(s) = \frac{1}{3s^3 + s^2 + 2s + 1}$$



?

We have to create the **Routh-Hurwitz** table to check the stability.

# Routh-Hurwitz Stability Criterion

3) If all coefficients are **positive** arrange them in a table according to the following pattern, which is called **Routh-Hurwitz** table.

For example, for  $n = 6$  we have:

$$a_6s^6 + a_5s^5 + a_4s^4 + a_3s^3 + a_2s^2 + a_1s + a_0 = 0$$

4) Check **number of sign changes** in the **first column**.

$a_6$
$a_5$
$b_1$
$c_1$
$d_1$
$e_1$
$f_1$

Number of **sign changes** in the **first column** is equal to the number of **roots** in the **right-half s-plane**

$s^6$	$a_6$	$a_4$	$a_2$	$a_0$
$s^5$	$a_5$	$a_3$	$a_1$	0
$s^4$	$b_1 = \frac{-\begin{vmatrix} a_6 & a_4 \\ a_5 & a_3 \end{vmatrix}}{a_5}$	$b_2 = \frac{-\begin{vmatrix} a_6 & a_2 \\ a_5 & a_1 \end{vmatrix}}{a_5}$	$b_3 = \frac{-\begin{vmatrix} a_6 & a_0 \\ a_5 & 0 \end{vmatrix}}{a_5}$	0
$s^3$	$c_1 = \frac{-\begin{vmatrix} a_5 & a_3 \\ b_1 & b_2 \end{vmatrix}}{b_1}$	$c_2 = \frac{-\begin{vmatrix} a_5 & a_1 \\ b_1 & b_3 \end{vmatrix}}{b_1}$	$c_3 = \frac{-\begin{vmatrix} a_5 & 0 \\ b_1 & 0 \end{vmatrix}}{b_1}$	0
$s^2$	$d_1 = \frac{-\begin{vmatrix} b_1 & b_2 \\ c_1 & c_2 \end{vmatrix}}{c_1}$	$d_2 = \frac{-\begin{vmatrix} b_1 & b_3 \\ c_1 & c_3 \end{vmatrix}}{c_1}$	$d_3 = \frac{-\begin{vmatrix} b_1 & 0 \\ c_1 & 0 \end{vmatrix}}{c_1}$	0
$s^1$	$e_1 = \frac{-\begin{vmatrix} c_1 & c_2 \\ d_1 & d_2 \end{vmatrix}}{d_1}$	$e_2 = \frac{-\begin{vmatrix} c_1 & c_3 \\ d_1 & d_3 \end{vmatrix}}{d_1}$	$e_3 = \frac{-\begin{vmatrix} c_1 & 0 \\ d_1 & 0 \end{vmatrix}}{d_1}$	0
$s^0$	$f_1 = \frac{-\begin{vmatrix} d_1 & d_2 \\ e_1 & e_2 \end{vmatrix}}{e_1}$	$f_2 = \frac{-\begin{vmatrix} d_1 & d_3 \\ e_1 & e_3 \end{vmatrix}}{e_1}$	$f_3 = \frac{-\begin{vmatrix} d_1 & 0 \\ e_1 & 0 \end{vmatrix}}{e_1}$	0

# Routh-Hurwitz Stability Criterion

## Example 4

Determine stability of the following transfer function

$$G(s) = \frac{1}{3s^3 + s^2 + 2s + 1}$$

Characteristic eqn.  $\rightarrow 3s^3 + s^2 + 2s + 1 = 0 \rightarrow$  The tabular is needed

The Routh-Hurwitz table for this polynomial is as below:

$s^3$	3	2
$s^2$	1	1
$s^1$	-1	0
$s^0$	1	0

$$b_1 = \frac{-\begin{vmatrix} 3 & 2 \\ 1 & 1 \end{vmatrix}}{1} = \frac{-(3 \times 1 - 2 \times 1)}{1} = -1$$

$$c_1 = \frac{-\begin{vmatrix} 1 & 1 \\ -1 & 0 \end{vmatrix}}{-1} = \frac{-(1 \times 0 - 1 \times (-1))}{-1} = 1$$

There are two sign changes in first column.

System is unstable and it has two poles in the right-half s-plane.

# Routh-Hurwitz Stability Criterion

## Example 5

Check whether roots of the following polynomial are in the right-half s-plane.

$$2s^4 + s^3 + 3s^2 + 5s + 10 = 0$$

The Routh-Hurwitz table for this polynomial is as below:

$s^4$	2	3	10
$s^3$	1	5	0
$s^2$	-7	10	0
$s^1$	$\frac{45}{7}$	0	0
$s^0$	10	0	0

There are **two** sign changes in first column.

System is **unstable** and it has **two poles** in the right-half s-plane.

$$b_1 = \frac{-\begin{vmatrix} 2 & 3 \\ 1 & 5 \end{vmatrix}}{1} = \frac{-(2 \times 5 - 3 \times 1)}{1} = -7$$

$$b_2 = \frac{-\begin{vmatrix} 2 & 10 \\ 1 & 0 \end{vmatrix}}{1} = \frac{-(2 \times 0 - 10 \times 1)}{1} = 10$$

$$c_1 = \frac{-\begin{vmatrix} 1 & 5 \\ -7 & 10 \end{vmatrix}}{-7} = \frac{-(1 \times 10 - 5 \times (-7))}{-7} = \frac{45}{7}$$

$$d_1 = \frac{-\begin{vmatrix} -7 & 10 \\ \frac{45}{7} & 0 \end{vmatrix}}{\frac{45}{7}} = \frac{-((-7) \times 0 - \frac{45}{7} \times 10)}{\frac{45}{7}} = 10$$

# Routh-Hurwitz Stability Criterion

## □ Special Cases

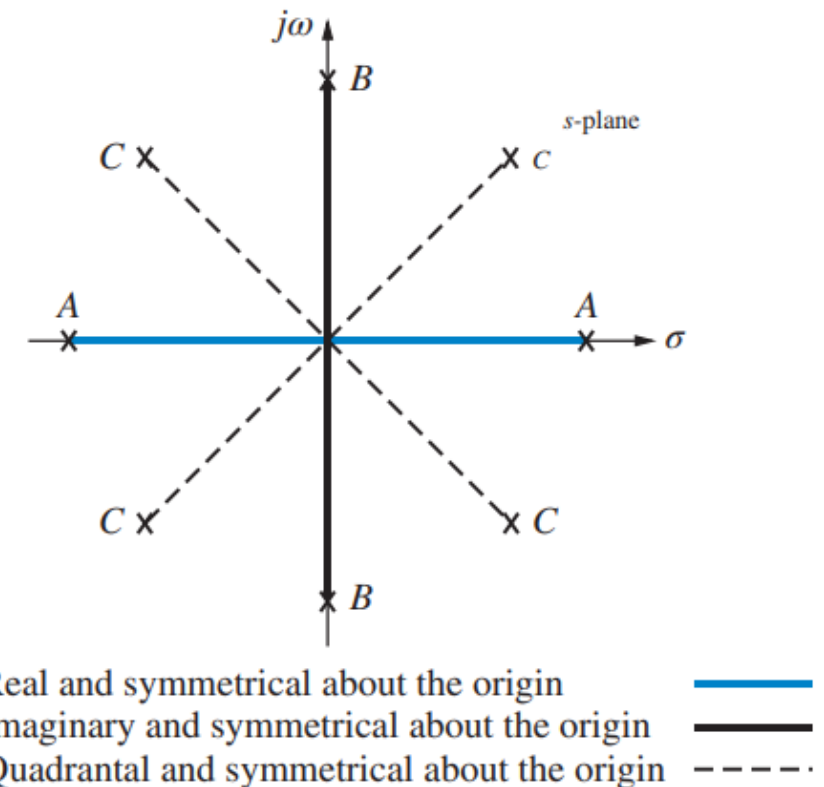
- Two special cases can arise when creating a Routh-Hurwitz table:

### 1) A zero in only the first column of a row

- Divide-by-zero problem when forming the next row.
- If a zero appears in the first column
  1. Replace the zero with a very small positive number  $\varepsilon > 0$
  2. Complete the Routh-Hurwitz table as usual
  3. Take the limit as  $\varepsilon \rightarrow 0$
  4. Evaluate the sign of the first-column entries

### 2) An entire row of zeros

- Indicates the presence of pairs of poles that are mirrored about the imaginary axis.
- If an entire row of zeros appears in a Routh-Hurwitz table
  1. Create an auxiliary polynomial from the row above the row of zeros, skipping every other power of  $s$
  2. Differentiate the auxiliary polynomial with respect to  $s$
  3. Replace the zero row with the coefficients of the resulting polynomial
  4. Complete the Routh-Hurwitz table as usual
  5. Evaluate the sign of the first-column entries



# Routh-Hurwitz Stability Criterion

## ❑ Special Case1: Only First Term in a Row is Zero

### Example 6

Check whether roots of the following polynomial are in the right-half s-plane.

$$s^4 + s^3 + 2s^2 + 2s + 3 = 0$$

The Routh-Hurwitz table for this polynomial is as below:

$s^4$	1	2	3
$s^3$	1	2	0
$s^2$	0	3	0
$s^1$	$\infty \rightarrow$	Not acceptable	
$s^0$			

$$b_1 = \frac{-\begin{vmatrix} 1 & 2 \\ 1 & 2 \end{vmatrix}}{1} = \frac{-(1 \times 2 - 1 \times 2)}{1} = 0$$

$$b_2 = \frac{-\begin{vmatrix} 1 & 3 \\ 1 & 0 \end{vmatrix}}{1} = \frac{-(1 \times 0 - 3 \times 1)}{1} = 3$$

$$c_1 = \frac{-\begin{vmatrix} 1 & 2 \\ 0 & 3 \end{vmatrix}}{0} = \frac{-(1 \times 3 - 2 \times 0)}{0} = \infty$$

If only the first term in any row is zero, but the next term in the row is nonzero or there is no remaining term, then the zero term is replaced by a very small positive number ( $\varepsilon > 0$ ) and the rest of the array evaluated as before.

# Routh-Hurwitz Stability Criterion

## ❑ Special Case1: Only First Term in a Row is Zero

### Example 6

Check whether roots of the following polynomial are in the right-half s-plane.

$$s^4 + s^3 + 2s^2 + 2s + 3 = 0$$

The Routh-Hurwitz table for this polynomial is as below:

$s^4$	1	2	3
$s^3$	1	2	0
$s^2$	$\epsilon$	3	0
$s^1$	$\frac{-3}{\epsilon}$		
$s^0$	3	0	0

Zero replaced by  $\epsilon > 0$

Zero replaced by  $\epsilon > 0$

$$b_1 = \frac{-\begin{vmatrix} 1 & 2 \\ 1 & 2 \end{vmatrix}}{1} = \frac{-(1 \times 2 - 1 \times 2)}{1} = 0$$

$$b_2 = \frac{-\begin{vmatrix} 1 & 3 \\ 1 & 0 \end{vmatrix}}{1} = \frac{-(1 \times 0 - 3 \times 1)}{1} = 3$$

$$c_1 = \frac{-\begin{vmatrix} 1 & 2 \\ \epsilon & 3 \end{vmatrix}}{\epsilon} = \frac{-(1 \times 3 - 2 \times \epsilon)}{\epsilon} \approx \frac{-3}{\epsilon}$$

$$d_1 = \frac{-\begin{vmatrix} \epsilon & 3 \\ \frac{-3}{\epsilon} & 0 \end{vmatrix}}{\frac{-3}{\epsilon}} = \frac{-(\epsilon \times 0 - 3 \times (\frac{-3}{\epsilon}))}{\frac{-3}{\epsilon}} = 3$$

There are two sign changes in first column.

System is unstable and it has two poles in the right-half s-plane.

# Routh-Hurwitz Stability Criterion

## □ Special Case2: All Terms in a Row are Zero

### Example 7

Check number of roots of the following polynomial are in the right-half s-plane.

$$s^5 + 2s^4 + 24s^3 + 48s^2 - 25s - 50 = 0$$

The Routh-Hurwitz table for this polynomial is as below:

$s^5$	1	24	-25
$s^4$	2	48	-50
$s^3$	0	0	0
$s^2$			
$s^1$			
$s^0$			

All zero row

$$b_1 = \frac{-\begin{vmatrix} 1 & 24 \\ 2 & 48 \end{vmatrix}}{2} = \frac{-(1 \times 48 - 2 \times 24)}{2} = 0$$

$$b_2 = \frac{-\begin{vmatrix} 1 & -25 \\ 2 & -50 \end{vmatrix}}{2} = \frac{-(1 \times (-50) - 2 \times (-25))}{2} = 0$$

If **all of the terms** in a row are zero, first an **auxiliary equation** is formed from the previous non-zero row, then the all-zero row is **replaced** by **coefficients of the derivative of the auxiliary equation** and the rest of the array evaluated as before.



# Routh-Hurwitz Stability Criterion

## □ Special Case2: All Terms in a Row are Zero

### Example 7

Check number of roots of the following polynomial are in the right-half s-plane.

$$s^5 + 2s^4 + 24s^3 + 48s^2 - 25s - 50 = 0$$

The Routh-Hurwitz table for this polynomial is as below:

$s^5$	1	24	-25
$s^4$	2	48	-50
$s^3$	8	96	0
$s^2$			
$s^1$			
$s^0$			

$$b_1 = \frac{-\begin{vmatrix} 1 & 24 \\ 2 & 48 \end{vmatrix}}{2} = \frac{-(1 \times 48 - 2 \times 24)}{2} = 0$$

$$b_2 = \frac{-\begin{vmatrix} 1 & -25 \\ 2 & -50 \end{vmatrix}}{2} = \frac{-(1 \times (-50) - 2 \times (-25))}{2} = 0$$

The zeros are replaced by 8 and 96

The auxiliary equation is:

$$A(s) = 2s^4 + 48s^2 - 50$$

Take derivative of A(s):

$$\frac{dA(s)}{ds} = 8s^3 + 96s$$

# Routh-Hurwitz Stability Criterion

## □ Special Case2: All Terms in a Row are Zero

### Example 7

Check number of roots of the following polynomial are in the right-half s-plane.

$$s^5 + 2s^4 + 24s^3 + 48s^2 - 25s - 50 = 0$$

The Routh-Hurwitz table for this polynomial is as below:

$s^5$	1	24	-25
$s^4$	2	48	-50
$s^3$	8	96	0
$s^2$	24	-50	0
$s^1$	112.7	0	0
$s^0$	-50	0	0

$$c_1 = \frac{-\begin{vmatrix} 2 & 48 \\ 8 & 96 \end{vmatrix}}{8} = \frac{-(2 \times 96 - 8 \times 48)}{8} = 24$$

$$c_2 = \frac{-\begin{vmatrix} 2 & -50 \\ 8 & 0 \end{vmatrix}}{8} = \frac{-(2 \times 0 - (-50) \times 8)}{8} = -50$$

$$d_1 = \frac{-\begin{vmatrix} 8 & 96 \\ 24 & -50 \end{vmatrix}}{24} = \frac{-(8 \times (-50) - 24 \times 96)}{24} = 112.7$$

$$e_1 = \frac{-\begin{vmatrix} 24 & -50 \\ 112.7 & 0 \end{vmatrix}}{112.7} = \frac{-(24 \times 0 - (-50) \times 112.7)}{112.7} = -50$$

There are **one** sign change in first column.

System is **unstable** and it has **one pole** in the right-half s-plane.

# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 8

Consider the following transfer function of a system.

$$G_p(s) = \frac{1}{s^3 + s^2 + 2s - 4}$$

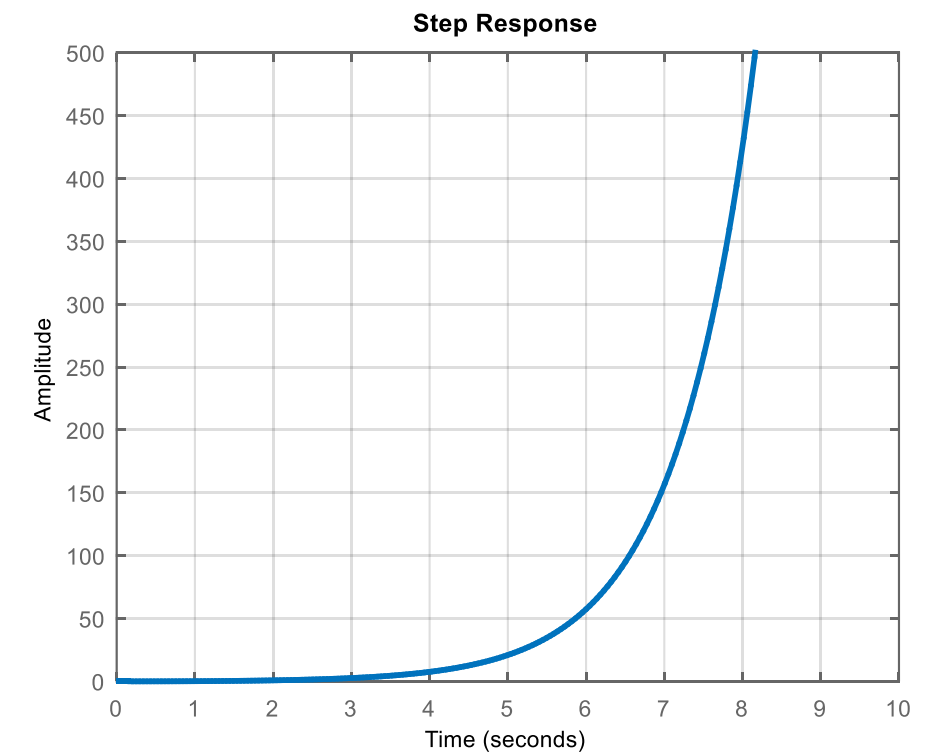
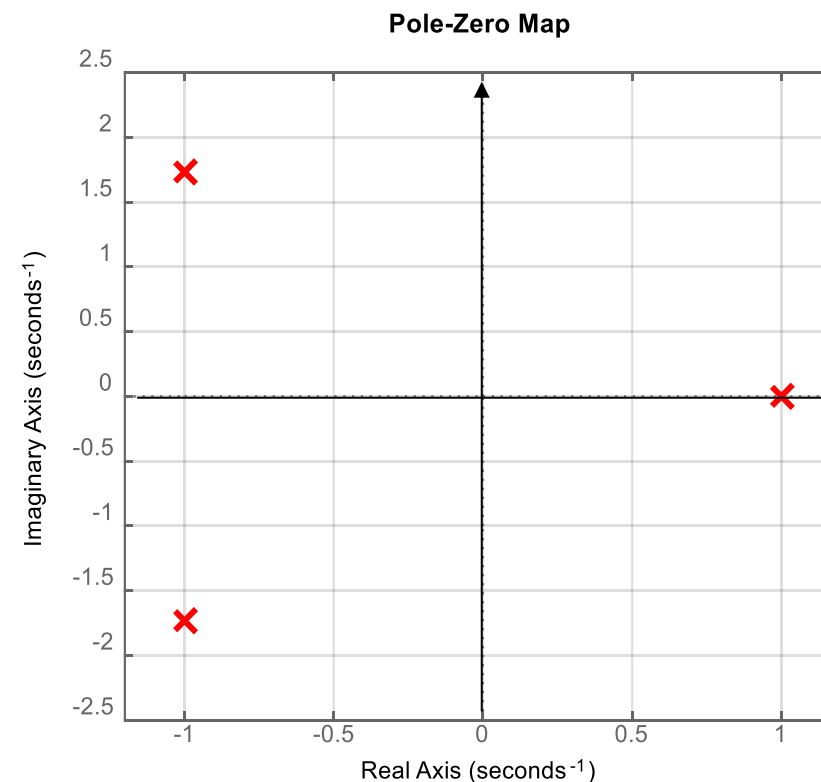
a) Determine stability of the system by Routh-Hurwitz criterion.

Characteristic equation  $\rightarrow s^3 + s^2 + 2s - 4 = 0 \rightarrow G_p(s)$  is an unstable system

We can also check the pole locations and the step response of the system using MATLAB



```
num = [1];  
den = [1 1 2 -4];  
G = tf(num,den);  
  
pzmap(G)  
  
step(G)
```



Unstable System

# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 8

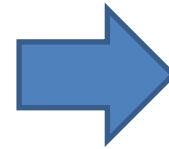
Consider the following transfer function of a system.

$$G_p(s) = \frac{1}{s^3 + s^2 + 2s - 4}$$

b) Determine the range of the variable gain  $K_p$  for closed-loop stability.

First, find the closed-loop transfer function

$$\frac{Y(s)}{R(s)} = \frac{K_p G_p(s)}{1 + K_p G_p(s)} = \frac{\frac{K_p}{s^3 + s^2 + 2s - 4}}{1 + \frac{K_p}{s^3 + s^2 + 2s - 4}}$$

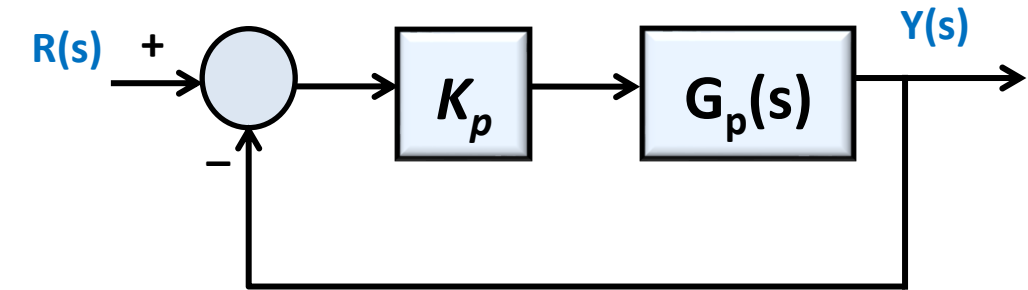


$$\frac{Y(s)}{R(s)} = \frac{K_p}{\underbrace{s^3 + s^2 + 2s - 4 + K_p}_{\text{Characteristic equation of the closed-loop system}}}$$

Characteristic equation of the closed-loop system

$$s^3 + s^2 + 2s - 4 + K_p = 0$$

- The closed-loop characteristic equation and closed-loop poles are dependent on the gain  $K_p$ .
- Therefore, we can obtain a stable closed-loop system by selecting an appropriate range of gain  $K_p$  for stability.



# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 8

Consider the following transfer function of a system.

$$G_p(s) = \frac{1}{s^3 + s^2 + 2s - 4}$$

b) Determine the range of the variable gain  $K_p$  for closed-loop stability.

Next, apply the Routh-Hurwitz criterion to the closed-loop characteristic equation.

$s^3$	1	2
$s^2$	1	$-4 + K_p$
$s^1$	$6 - K_p$	0
$s^0$	$-4 + K_p$	0

$$s^3 + s^2 + 2s - 4 + K_p = 0$$

$$b_1 = \frac{-\begin{vmatrix} 1 & 2 \\ 1 & -4 + K_p \end{vmatrix}}{1} = \frac{-(1 \times (-4 + K_p) - 2 \times 1)}{1} = 6 - K_p$$

$$c_1 = \frac{-\begin{vmatrix} 1 & -4 + K_p \\ 6 - K_p & 0 \end{vmatrix}}{6 - K_p} = \frac{-(1 \times 0 - (-4 + K_p)(6 - K_p))}{6 - K_p} = -4 + K_p$$

For stability, all terms in the first column must be positive:

$$6 - K_p > 0 \rightarrow K_p < 6$$

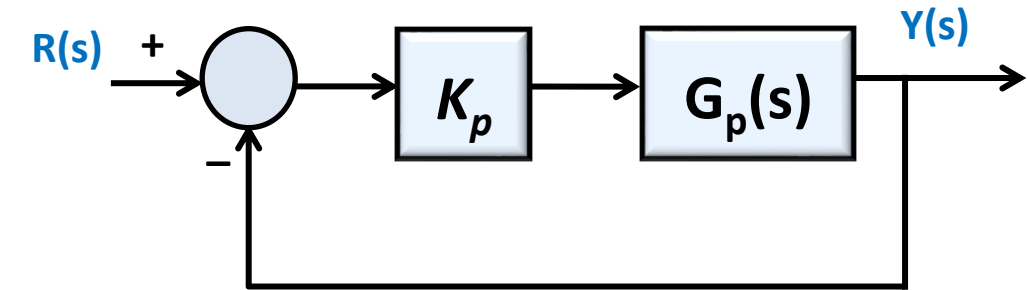
$$-4 + K_p > 0 \rightarrow K_p > 4$$



$$4 < K_p < 6$$

Necessary and sufficient condition for stability

- For  $K_p = 4$  and  $K_p = 6$  the closed-loop system is marginally stable.
- For  $K_p < 4$  and  $K_p > 6$  the closed-loop system is unstable.



# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 8

Consider the following transfer function of a system.

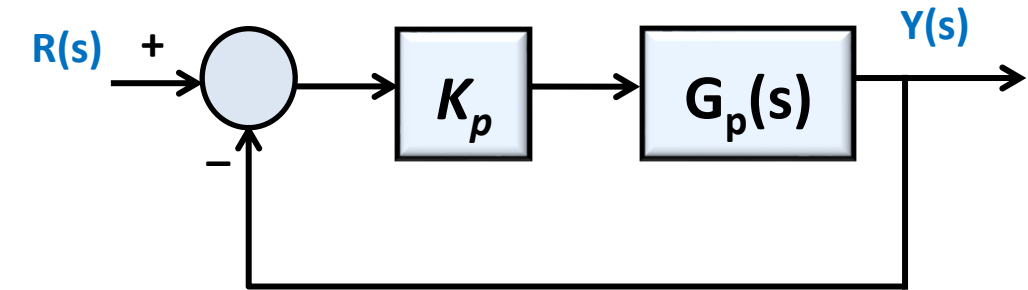
$$G_p(s) = \frac{1}{s^3 + s^2 + 2s - 4}$$

b) Determine the range of the variable gain  $K_p$  for closed-loop stability.

Closed-loop Transfer Function



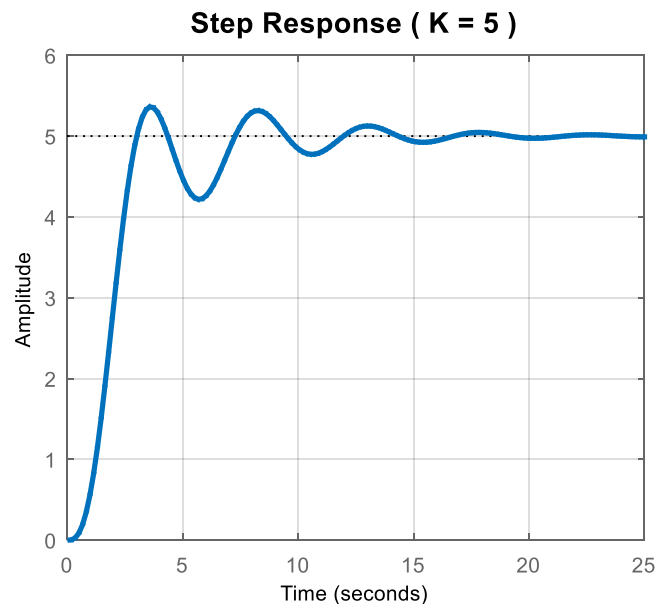
$$\frac{Y(s)}{R(s)} = \frac{K_p}{s^3 + s^2 + 2s - 4 + K_p}$$



We can check the step response of the closed-loop system for the following range of gain values

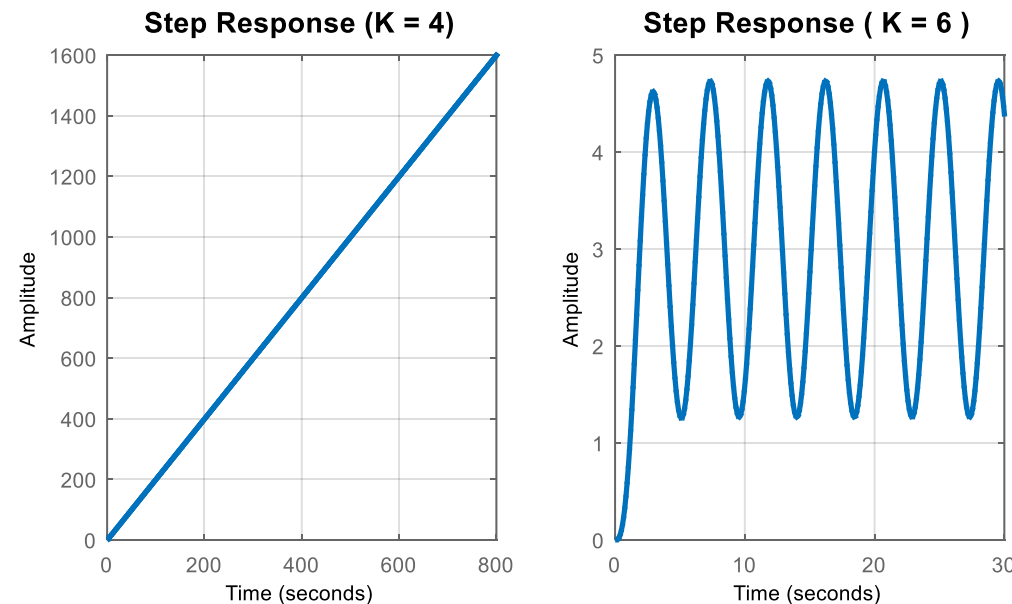
$$4 < K_p < 6$$

Stable System



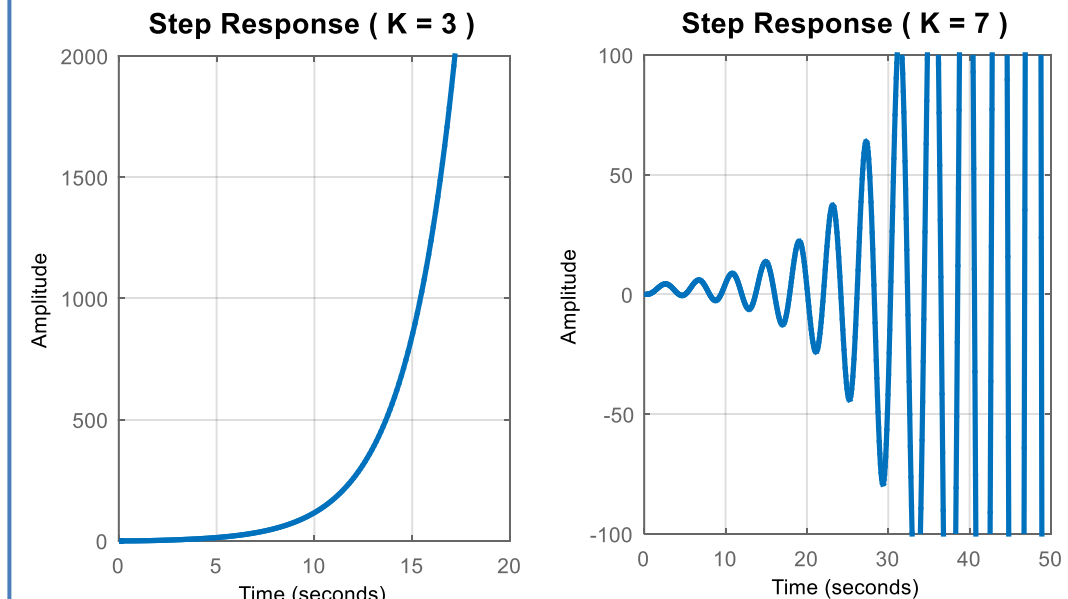
$$K_p = 4 \text{ and } K_p = 6$$

Marginally Stable System



$$K_p < 4 \text{ and } K_p > 6$$

Unstable System

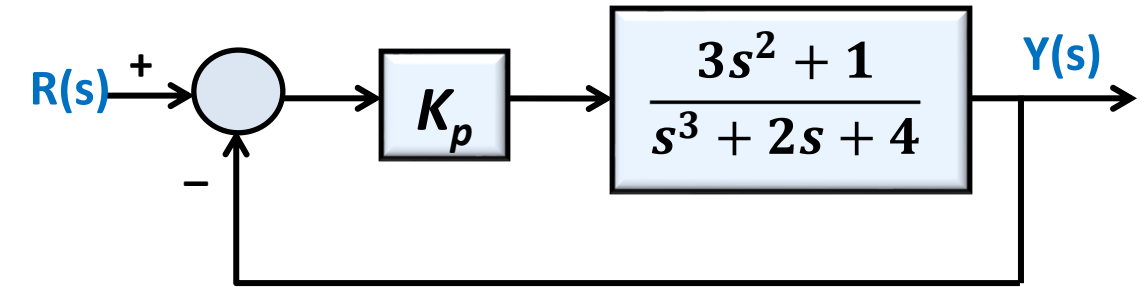


# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 9

Consider the following unity-feedback closed-loop system

$$G(s) = \frac{K_p(3s^2 + 1)}{s^3 + 2s + 4}, \quad H(s) = 1$$



a) Determine order and type of the open-loop system.

$G(s)$  is a third order, type 0 system with characteristic equation of

$$s^3 + 2s + 4 = 0 \rightarrow n = 3, \quad \text{Type 0}$$

b) Determine stability of the open-loop system.

$$s^3 + 0s^2 + 2s + 4 = 0 \rightarrow \text{Based on the Routh-Hurwitz criterion, } G(s) \text{ is unstable.}$$

c) Determine the closed-loop transfer function.

Transfer function of the closed-loop system is

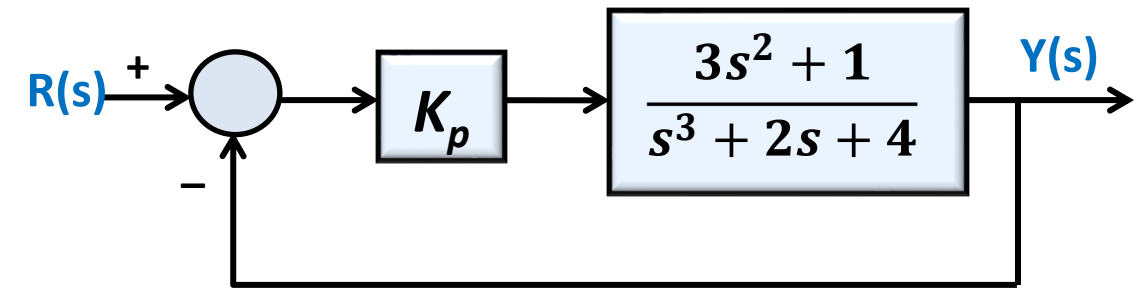
$$T(s) = \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)} = \frac{\frac{K_p(3s^2 + 1)}{s^3 + 2s + 4}}{1 + \frac{K_p(3s^2 + 1)}{s^3 + 2s + 4}} = \frac{K_p(3s^2 + 1)}{s^3 + 3K_p s^2 + 2s + K_p + 4}$$

# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 9

Consider the following unity-feedback closed-loop system

$$G(s) = \frac{K_p(3s^2 + 1)}{s^3 + 2s + 4}, \quad H(s) = 1$$



d) Determine range of the  $K_p$  for closed-loop stability.

Closed-loop system characteristic equation

$$\rightarrow s^3 + 3K_p s^2 + 2s + K_p + 4 = 0$$

The Routh-Hurwitz table:

$s^3$	1	2
$s^2$	$3K_p$	$K_p + 4$
$s^1$	$\frac{5K_p - 4}{3K_p}$	0
$s^0$	$K_p + 4$	0

For stability, all terms in the first column must be positive:

$$3K_p > 0 \rightarrow K_p > 0$$

$$5K_p - 4 > 0 \rightarrow K_p > 0.8$$

$$K_p + 4 > 0 \rightarrow K_p > -4$$

$$K_p > 0.8$$

**Stability Condition**

- For  $K_p = 0.8$  the closed-loop system is **marginally stable**.
- For  $K_p < 0.8$  the closed-loop system is **unstable**.

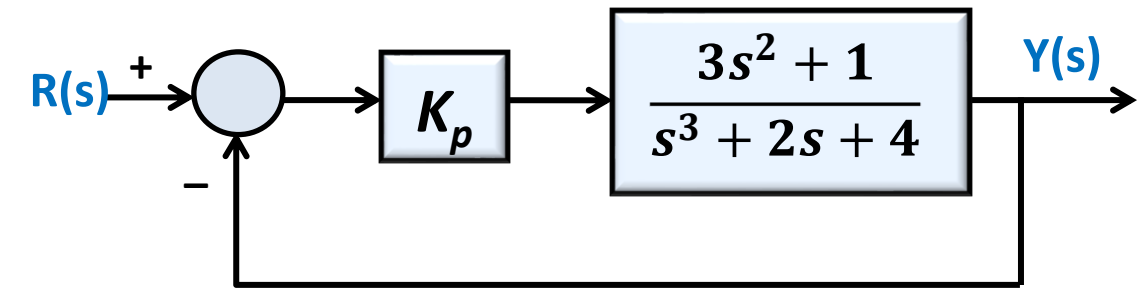


# Control Systems Stability Analysis via Routh-Hurwitz Criterion

## Example 9

Consider the following unity-feedback closed-loop system

$$G(s) = \frac{K_p(3s^2 + 1)}{s^3 + 2s + 4}, \quad H(s) = 1$$



e) Determine the gain  $K_p$  so that to achieve 5% steady-state error for unit-step input.

Step-error constant and steady-state error for unit-step input:

$$k_p = \lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \frac{K_p(3s^2 + 1)}{s^3 + 2s + 4} = \frac{K_p}{4}$$

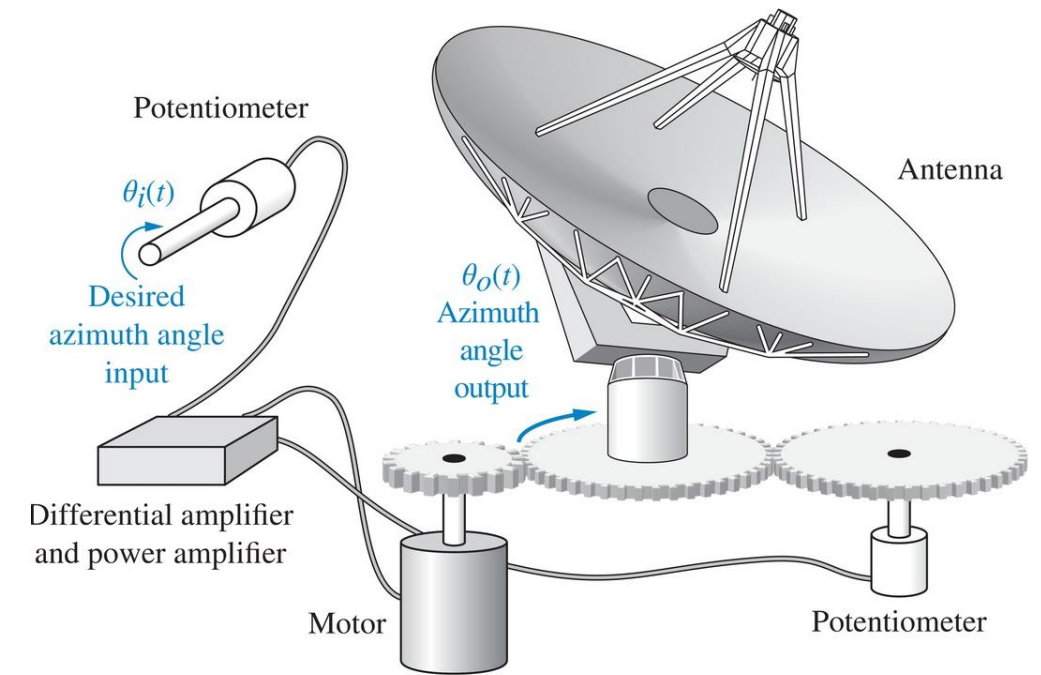
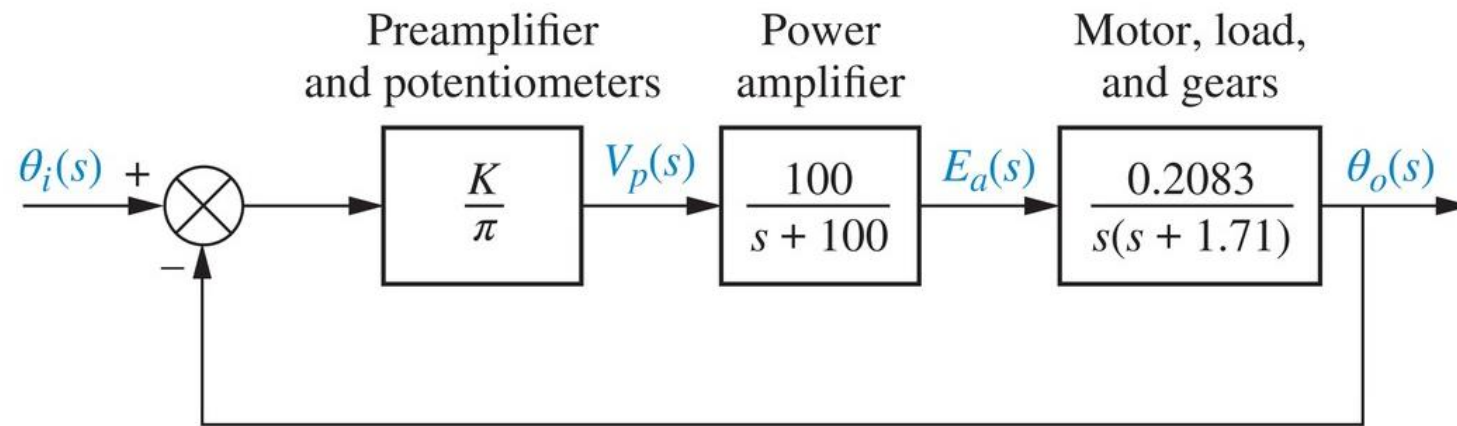
$$e_{ss} = \frac{R}{1 + k_p} = \frac{1}{1 + \frac{K_p}{4}} = \frac{4}{4 + K_p}$$

The required gain value to achieve the desired steady-state error of 5% is obtained as below

$$0.05 = \frac{4}{4 + K_p} \rightarrow 0.2 + 0.05K_p = 4 \rightarrow K_p = \frac{3.8}{0.05} \rightarrow \boxed{K_p = 76}$$

# Case Study: Antenna Control System

- Consider the *motor-driven antenna azimuth position control system* example from Lecture 1.
- We determined the block diagram of the control system as below:

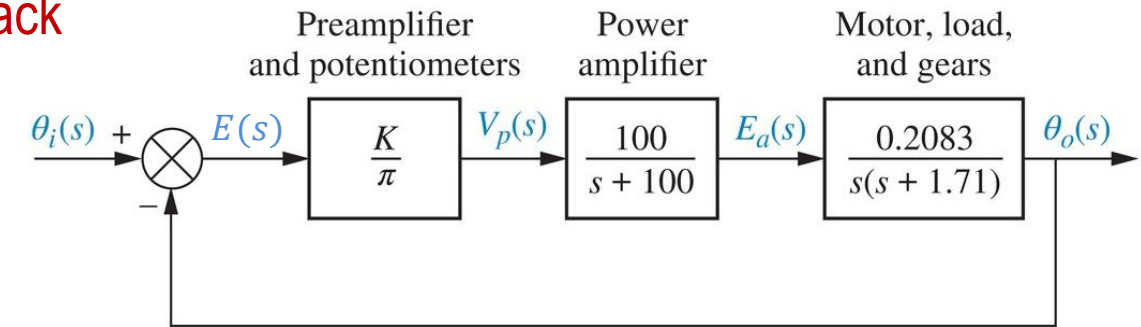


- In this part, we will find the range of preamplifier gain  $K$  required to keep the closed-loop system stable.

# Case Study: Antenna Control System

For the antenna azimuth position control system with the given simplified unity-feedback block diagram model:

Find the range of preamplifier gain  $K$  required to keep the closed-loop system stable.



First, derive the closed-loop transfer function and the characteristic equation.

$$T(s) = \frac{6.63K}{s^3 + 101.71s^2 + 171s + 6.63K}$$

Create the **Routh-Hurwitz** table for the characteristic equation.

$s^3$	1	171
$s^2$	101.71	$6.63K$
$s^1$	$17392.41 - 6.63K$	0
$s^0$	$6.63K$	0

For stability, all terms in the first column must be positive:

$$17392.41 - 6.63K > 0 \rightarrow K < 2623$$

$$6.63K > 0 \rightarrow K > 0$$



$$0 < K < 2623$$

**Stability Condition**

- For  $K = 2623$  the closed-loop system is **marginally stable**.
- For  $K > 2623$  and  $K < 0$  the closed-loop system is **unstable**.

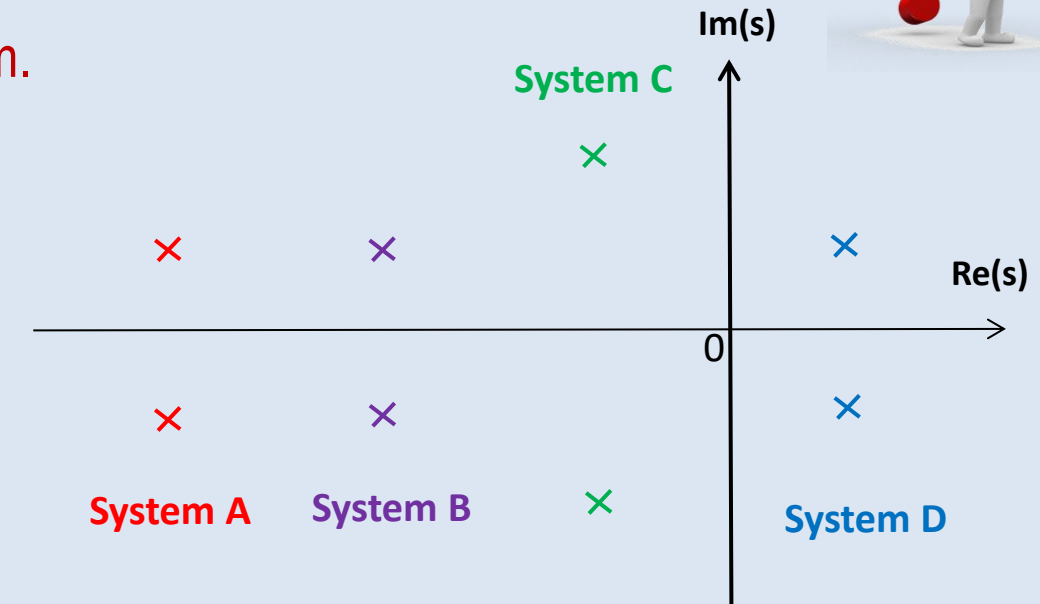
# Quick Review

1) Answer the questions based on the given pole locations for each second order system.

- Which system has largest percent overshoot ?
- Which system has longest settling-time?
- Which system has shortest settling time?
- Which system is unstable?
- Which system has smallest percent overshoot?

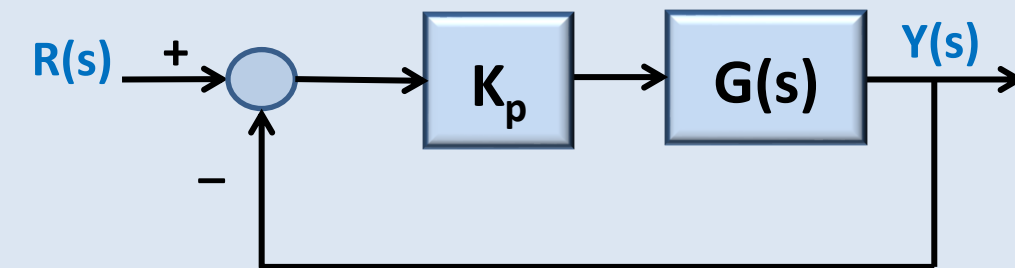
$$t_s \approx \frac{4}{\zeta \omega_n}$$

$$O.S. = e^{-\zeta \pi / \sqrt{1-\zeta^2}}$$



$$s_{1,2} = -\zeta \omega_n \pm j \omega_n \sqrt{1-\zeta^2}$$

2) Determine range of the gain  $K_p$  for closed-loop stability.



$$G(s) = \frac{1}{(s-1)(s+5)}$$

# Stability Analysis of LTI State-Space Models

## □ Transfer Function from State-space Model

- Determining the **transfer function** from the **state space representation** is called **reconstruction**.
- Consider a LTI system with the state space representation

$$\begin{cases} \dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) \\ \mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}\mathbf{u}(t) \end{cases}$$

- Take Laplace transform of the state space equations assuming the **zero initial condition**

$$\begin{cases} s\mathbf{X}(s) = \mathbf{A}\mathbf{X}(s) + \mathbf{B}\mathbf{U}(s) \\ \mathbf{Y}(s) = \mathbf{C}\mathbf{X}(s) + \mathbf{D}\mathbf{U}(s) \end{cases} \begin{matrix} \longrightarrow \\ \longrightarrow \end{matrix} \begin{cases} (s\mathbf{I} - \mathbf{A})\mathbf{X}(s) = \mathbf{B}\mathbf{U}(s) \\ \mathbf{Y}(s) = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}\mathbf{U}(s) + \mathbf{D}\mathbf{U}(s) \end{cases} \begin{matrix} \longrightarrow \\ \longrightarrow \end{matrix} \begin{cases} \mathbf{X}(s) = (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}\mathbf{U}(s) \\ \mathbf{Y}(s) = [\mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}]\mathbf{U}(s) \end{cases}$$

$$\mathbf{Y}(s) = \underbrace{[\mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}]}_{\text{Transfer Function Matrix}} \mathbf{U}(s)$$

**Transfer Function Matrix**

- For **single-input-single-output (SISO)** LTI systems the transfer function is obtained as below,

$$G(s) = \frac{Y(s)}{U(s)} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$$

# Stability Analysis of LTI State-Space Models

## Reminder: Matrix Inverse

$$A^{-1} = \frac{\text{adj}(A)}{\det(A)}$$

### For $2 \times 2$ matrix:

$$A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \rightarrow A^{-1} = \frac{1}{a_{11}a_{22} - a_{21}a_{12}} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix}$$

### For $3 \times 3$ matrix:

$$A = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}$$

$$\det(A) = a_{11}(a_{22}a_{33} - a_{23}a_{32}) - a_{12}(a_{21}a_{33} - a_{23}a_{31}) + a_{13}(a_{21}a_{32} - a_{22}a_{31})$$

$$\text{adj}(A) = \begin{bmatrix} a_{22}a_{33} - a_{23}a_{32} & -(a_{12}a_{33} - a_{13}a_{32}) & a_{12}a_{23} - a_{13}a_{22} \\ -(a_{21}a_{33} - a_{23}a_{31}) & a_{11}a_{33} - a_{13}a_{31} & -(a_{11}a_{23} - a_{21}a_{13}) \\ a_{21}a_{32} - a_{22}a_{31} & -(a_{11}a_{32} - a_{12}a_{31}) & a_{11}a_{22} - a_{12}a_{21} \end{bmatrix}$$

# Stability Analysis of LTI State-Space Models

## Example 10

Consider the following state space representation of a system  
Determine transfer function of the system.

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} -4 & -3 \\ 1 & -5 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 3 \\ 6 \end{bmatrix} u(t)$$

$$y(t) = \begin{bmatrix} 1 & 2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \end{bmatrix} u(t)$$

The transfer function is determined by the following formula

$$G(s) = \frac{Y(s)}{U(s)} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$$

$$(s\mathbf{I} - \mathbf{A})^{-1} = \frac{\text{adj}(s\mathbf{I} - \mathbf{A})}{\det(s\mathbf{I} - \mathbf{A})}$$

First, find the  $(s\mathbf{I} - \mathbf{A})^{-1}$

$$s\mathbf{I} - \mathbf{A} = \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} -4 & -3 \\ 1 & -5 \end{bmatrix} = \begin{bmatrix} s+4 & 3 \\ -1 & s+5 \end{bmatrix} \rightarrow (s\mathbf{I} - \mathbf{A})^{-1} = \frac{1}{s^2 + 9s + 23} \begin{bmatrix} s+5 & -3 \\ 1 & s+4 \end{bmatrix}$$

Substitute the  $(s\mathbf{I} - \mathbf{A})^{-1}$ ,  $\mathbf{C}$ ,  $\mathbf{B}$  and  $\mathbf{D}$  in the transfer function formula

$$\frac{Y(s)}{U(s)} = \frac{1}{s^2 + 9s + 23} \begin{bmatrix} 1 & 2 \end{bmatrix} \begin{bmatrix} s+5 & -3 \\ 1 & s+4 \end{bmatrix} \begin{bmatrix} 3 \\ 6 \end{bmatrix} = \frac{1}{s^2 + 9s + 23} \begin{bmatrix} 1 & 2 \end{bmatrix} \begin{bmatrix} 3s-3 \\ 6s+27 \end{bmatrix} = \frac{1}{s^2 + 9s + 23} (3s-3+12s+54)$$

$$\frac{Y(s)}{U(s)} = \frac{15s + 51}{s^2 + 9s + 23}$$

Transfer Function

# Stability Analysis of LTI State-Space Models

## □ Characteristic Polynomial and Eigenvalues

- Consider a LTI system with the following state space equations

$$\begin{cases} \dot{\mathbf{x}}(\mathbf{t}) = \mathbf{A}\mathbf{x}(\mathbf{t}) + \mathbf{B}\mathbf{u}(\mathbf{t}) \\ \mathbf{y}(\mathbf{t}) = \mathbf{C}\mathbf{x}(\mathbf{t}) + \mathbf{D}\mathbf{u}(\mathbf{t}) \end{cases}$$

- Characteristic polynomial** of the system matrix is obtained as below

Characteristic Polynomial  $\det(\lambda\mathbf{I} - \mathbf{A}) = 0$

- Given matrix  $\mathbf{A}_{n \times n}$  with **real** arrays, the **characteristic polynomial** is a  $n$ th order **monic** polynomial with **real** coefficients

$$\det(\lambda\mathbf{I} - \mathbf{A}) = \lambda^n + c_{n-1}\lambda^{n-1} + \cdots + c_1\lambda + c_0$$

- The **roots of the characteristic equation** are called **eigenvalues** of the matrix  $\mathbf{A}$ .
- The eigenvalues are always **real** or **complex conjugate** numbers.



# Stability Analysis of LTI State-Space Models

- Consider a LTI system with the following state-space equations and characteristic polynomial

$$\begin{cases} \dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t) \\ \mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t) \end{cases}$$

$$\det(\lambda\mathbf{I} - \mathbf{A}) = 0$$

Characteristic Polynomial

- Recall the **reconstruction** formula to obtain the transfer function:

$$\frac{Y(s)}{U(s)} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D} \quad \Rightarrow \quad \frac{Y(s)}{U(s)} = \mathbf{C} \left( \frac{\text{adj}(s\mathbf{I} - \mathbf{A})}{\det(s\mathbf{I} - \mathbf{A})} \right) \mathbf{B} + \mathbf{D} = \frac{\mathbf{C} \text{adj}(s\mathbf{I} - \mathbf{A})\mathbf{B} + \mathbf{D} \det(s\mathbf{I} - \mathbf{A})}{\underbrace{\det(s\mathbf{I} - \mathbf{A})}_{\text{Characteristic Equation}}}$$

Characteristic Equation

- Therefore,  $\det(s\mathbf{I} - \mathbf{A}) = 0$  is the **characteristic equation** of the system, which is identical to the **characteristic polynomial** of the matrix  $\mathbf{A}$
- Therefore, the **eigenvalues of the matrix  $\mathbf{A}$**  are identical to the **system's poles** with no pole-zero cancellation.

Stability of the system is analyzed by checking the **eigenvalues of matrix  $\mathbf{A}$**

# Stability Analysis of LTI State-Space Models

## Example 11

Determine stability of the following system

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u(t)$$

First, find the **characteristic polynomial** of the matrix **A**

$$s\mathbf{I} - \mathbf{A} = \begin{bmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix} = \begin{bmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 6 & 11 & s + 6 \end{bmatrix}$$

$$\det(s\mathbf{I} - \mathbf{A}) = \begin{vmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 6 & 11 & s + 6 \end{vmatrix} = \boxed{s^3 + 6s^2 + 11s + 6} \quad \text{Characteristic Polynomial}$$

Next, create the **Routh-Hurwitz** table for the characteristic equation.

$s^3$	1	11
$s^2$	6	6
$s^1$	10	0
$s^0$	6	0

Since there is **no sign change** in the first column all the eigenvalues are located on the left-half of the s-plane.

Therefore, the system is **stable**.

# Stability Analysis of LTI State-Space Models

## Example 11

Determine stability of the following system

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u(t)$$

We can also determine the characteristic polynomial and the eigenvalues in **MATLAB**

```
A = [0 1 0; 0 0 1; -6 -11 -6];  
poly(A)  
ans =  
    1.0000    6.0000   11.0000    6.0000  
  
eig(A)  
ans =  
   -1.0000  
   -2.0000  
   -3.0000
```

$$\lambda^3 + 6\lambda^2 + 11\lambda + 6$$

Characteristic Polynomial

$$\lambda_1 = -1,$$

$$\lambda_2 = -2,$$

$$\lambda_3 = -3$$

Eigenvalues

# Quick Review

1) A system is represented by state-space model of  $\dot{\mathbf{x}} = A\mathbf{x} + B\mathbf{u}$ .

The values of  $K$  for a stable system are:

- a)  $K < 1/2$
- b)  $K > 1/2$
- c)  $K = 1/2$
- d) The system is stable for all  $K$ .

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -5 & -K & -10 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u(t)$$



# THANK YOU