

# HUMBER ENGINEERING

MENG-3020

SYSTEMS MODELING & SIMULATION

LECTURE 2

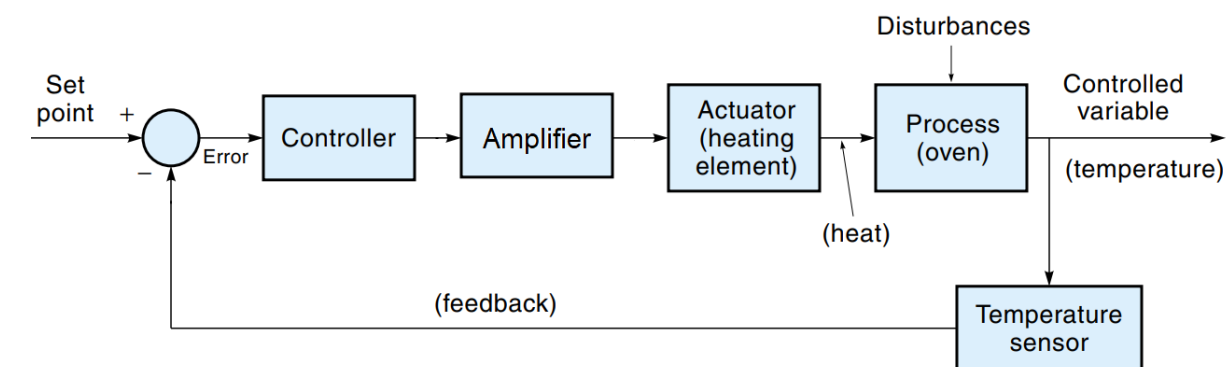
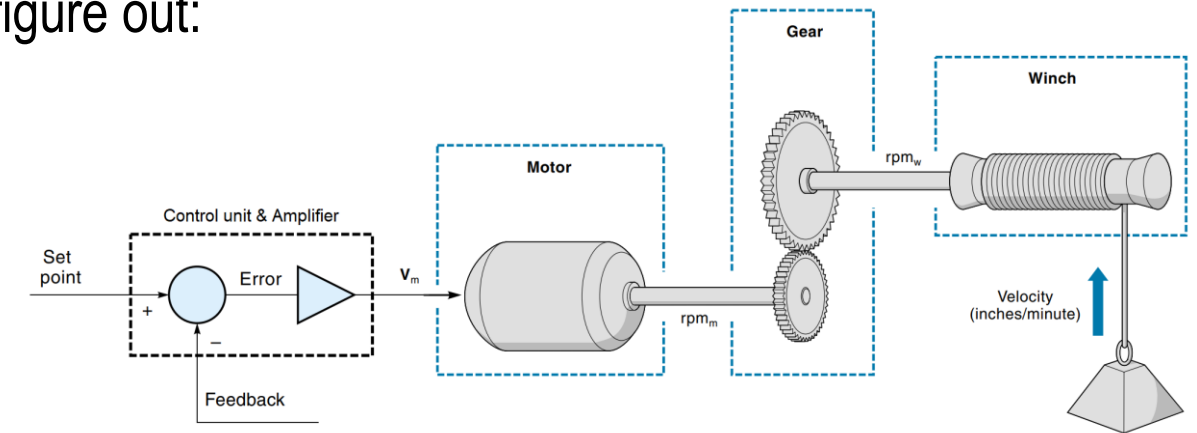
# LECTURE 2

## Translational Mechanical Systems

- Modeling of Translational Mechanical Systems
- Variables & Elements
- Element Laws
- Interconnection Laws
- Obtaining the System Model (Equation of Motion)
- Solving the Equation of Motion

# What We Already Know?

- A **dynamic system** is a collection of **components** and **circuits** connected together to perform a useful function.
- Each element in the system **converts energy** from one form to another.
  - For example, a **temperature sensor** as converting degrees to volts or a **motor** as converting volts to rpm.
- In order to design, analysis, and control of dynamic systems, we need to first understand the **input-output relationship** of the system elements and find a **model** for them. This helps us to figure out:
  - How components affect each other and the overall system.
  - How the output of the system will react to different inputs.
  - How to analyze, predict and control the system behavior.
- **System modeling** means finding a **mathematical equation** describing how the **output** of the system is related to its **input**.



How to find the system model?

# What We Already Know?

## □ Lump-Parametric Modeling

- Find the input-output relationships for systems by considering them to be composed of just a few **simple basic elements** and applying the **physical laws** from **first-principles**.
- Mainly used to model **electrical**, **mechanical**, and **electromechanical** systems.
- The model is obtained as a **differential equation**, then shown in any standard form of, **Transfer Function model**, **State-Space model** or **Block diagram model**.
- **Electrical systems** can be considered as compose of basic elements, which can be represented by **resistors**, **capacitors**, **inductors** and **op-amps**.
  - These are characterized by voltage –current relationships for components and the laws of interconnection **Kirchhoff's Voltage Law (KVL)** and **Current Law (KCL)**
- **Mechanical systems** can be considered as compose of basic elements, which can be represented by **springs**, **dampers** and **masses**, and are characterized by **Newton's Laws of motion**.



## □ Empirical Modeling

- An **experimental approach**, which mainly used to model **thermal** and **fluid (hydraulic and pneumatic)** processes.
- Some **experiments** are performed on the system to **collect input-output data**, a model is then fitted to the collected data by assigning suitable numerical values to its parameters.

# Modeling of Mechanical Systems

- The motion of elements of mechanical systems can be described as:
  - **Translational Motion**
  - **Rotational Motion**
- The equations governing the motion of mechanical systems are called the **equation of motion** that often directly or indirectly formulated by applying **Newton's law of motion** to the **free-body diagram** (FBD).

**Translational Motion**

$$\sum F_{ext} = Ma$$

$$\sum T_{ext} = J\alpha$$

**Rotational Motion**

- The number of **equations of motion** required is equal to the number of **linearly independent** motions or the number of **degrees of freedom**.
  - **Step 1:** Identify **reference point** and **positive direction** of motion.
  - **Step 2:** Draw a **free-body diagram** for each mass/point of motion.
  - **Step 3:** For each free-body diagram, find the forces acting on the body due only to its own motion and the forces create by the adjacent motion.
  - **Step 4:** Use **Newton's law** on each body to form the **differential equation of motion**.

# Translational Mechanical Systems: Variables & Elements

- The **translational motion** is defined as a motion that takes place along a **straight** or **curved** path.
- The **variables** that are used to describe the translational motion are:
  - $f(t)$ : Force (N)
  - $x(t)$ : Displacement (m)
  - $v(t)$ : Velocity (m/s)
  - $a(t)$ : Acceleration (m/s<sup>2</sup>)
- All these variables are function of time.
- **Displacements** are measured with respect to reference condition, which is the equilibrium position of the body.
- **Velocities** and **accelerations** are normally expressed as the derivatives of the corresponding **displacement**.

$$v(t) = \frac{dx(t)}{dt} = x'(t) = \dot{x}(t)$$

$$a(t) = \frac{d^2x(t)}{dt^2} = x''(t) = \ddot{x}(t)$$

- The **elements** that we include in translational systems are:
  - Inertia Element → **Mass**
  - Stiffness Element → **Spring**
  - Damping Element → **Damper**

# Translational Mechanical Systems: Example

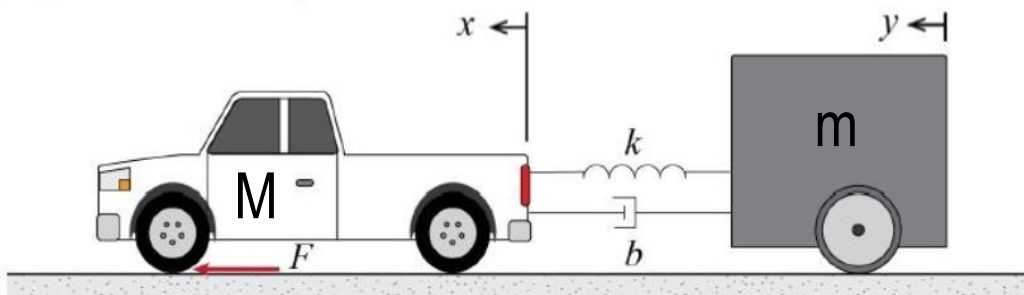
- Some real-world examples of translational motion systems.

- Truck Pulling a Cart

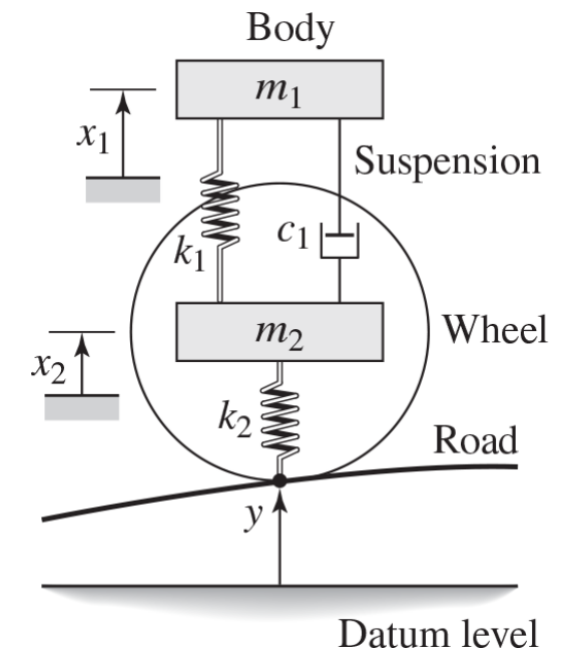
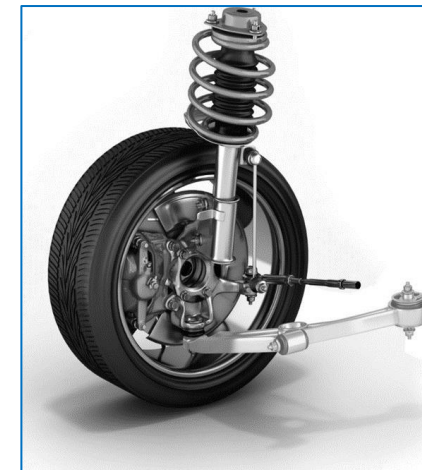


**Input:** Applied engine force

**Outputs:** Displacement of truck and cart



- Vehicle Suspension System



**Input:** Vertical displacement due to road bumps

**Outputs:** Vertical displacement of car

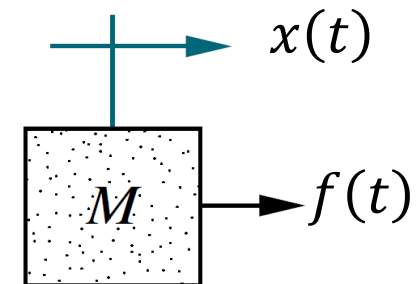


# Translational Mechanical Systems: Element Laws

## □ Inertia Element: Mass

- If a **force** is applied on a body, then it is opposed by an opposing force due to **inertia**.
- The inertia of a body can be represented by a **mass**.
- From the **Newton's second law**, the **applied force**  $f(t)$  is proportional to the **acceleration**  $a(t)$  of the body.
- The  $M$  is the **mass of the body**. The unit is (kg).

$$f(t) = Ma(t) = M \frac{dv(t)}{dt} = M \frac{d^2x(t)}{dt^2}$$



- **Energy** in a mass is stored as **kinetic energy** if the mass is in motion, and as **potential energy** if the mass has a vertical displacement relative to the reference point.

$$KE = \frac{1}{2} M v^2$$

$$PE = Mgh$$

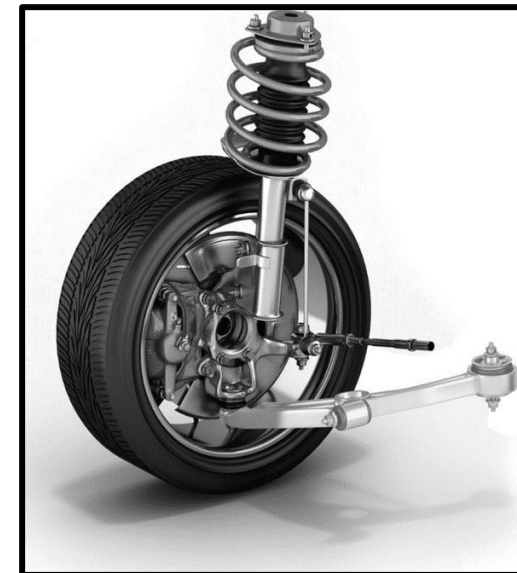
where  $g = 9.8 \text{ m/s}^2$  is gravitational acceleration and  $h$  is the height of mass above its reference position.



# Translational Mechanical Systems: Element Laws

## □ Stiffness Element

- All physical objects **deform** somewhat under the action of externally applied **forces**.
- When the **deformation is negligible** for the purpose of the analysis, we can treat the object as a **rigid body**.
- Sometimes, an elastic element is intentionally included in the system, as with a **spring in a vehicle suspension**.
- Sometimes the element is not intended to be elastic but **deforms** anyway because it is subjected to large forces, such as cables, beams and rods.
- This can be the case with the **boom or cables of a large crane that lifts a heavy load**.
- In such cases, we must include the deformation and corresponding forces in our analysis.



# Translational Mechanical Systems: Element Laws

## □ Stiffness Element: Spring

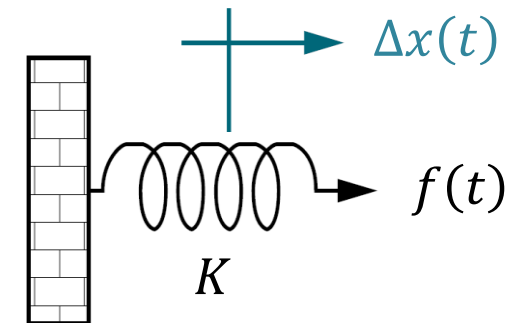
- Any mechanical element that undergoes a change in shape when subjected to a force can be characterized by a **stiffness element**, provided only that an **algebraic** relationship exists between the **elongation** and the **force**.
- The stiffness of an element can be represented by an **ideal spring**.
- If a **force** is applied to a spring, then it is opposed by an opposing force due to the **elasticity** of the spring.
- From the **Hooke's law**, the **applied force**  $f(t)$  to a spring is proportional to the **displacement**  $\Delta x(t)$  of the spring.
- The  $K$  is the **spring constant**. The unit is (N/m).

$$f(t) = K\Delta x(t)$$

- Potential energy stored in a spring** that has been stretched or compressed, and for a linear spring that energy is given by:

$$PE = \frac{1}{2} K (\Delta x)^2$$

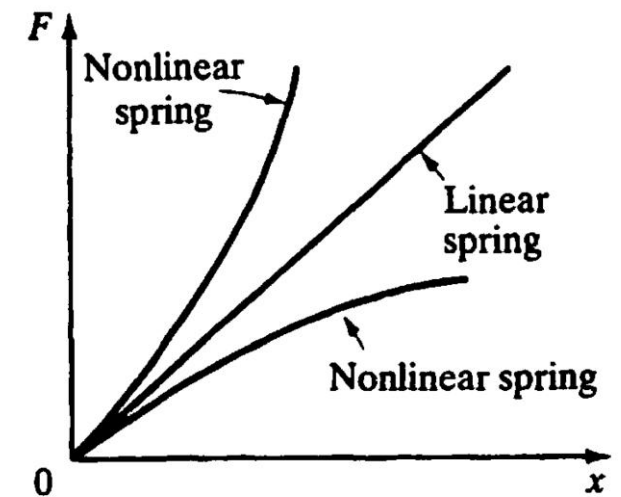
- An **ideal spring** element is massless.
- A **real spring** element can be represented by an ideal element either by neglecting its mass or by including it in another mass in the system.



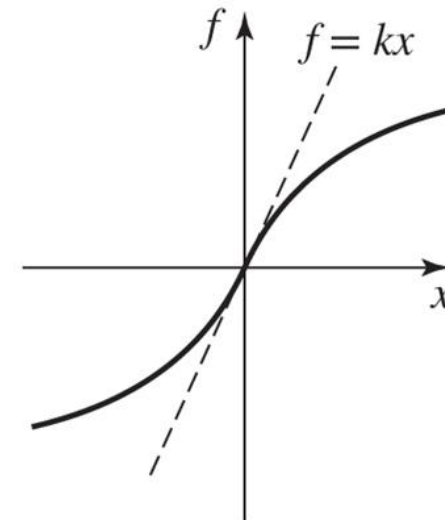
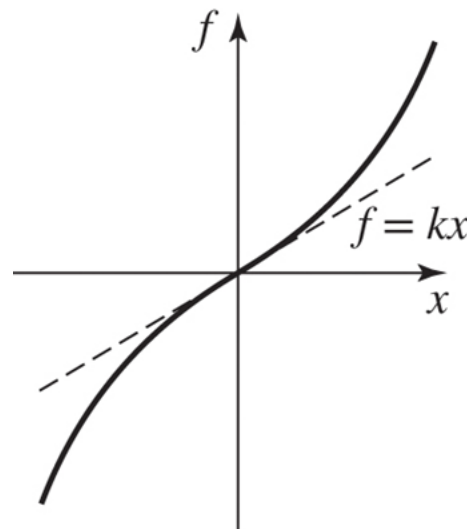
# Translational Mechanical Systems: Element Laws

## □ Properties of Spring

- For practical springs, the solution of linearity may be good only for relatively small net displacements.
- When a linear spring is stretched a point is reached in which the force per unit displacement begins to change and the spring becomes a **nonlinear spring**.
- Spring constants indicate stiffness of the spring:
  - Large value of spring constants correspond to a hard spring,
  - Small value of spring constants to a soft spring.
- The reciprocal of the spring constant is called **compliance** or **mechanical capacitance**.
- Mechanical capacitance indicates the softness of the spring.



Nonlinear  
characteristics of a  
**hardening** spring



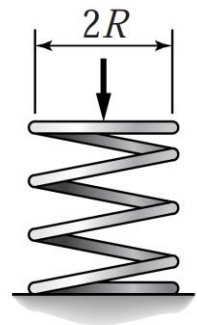
Nonlinear  
characteristics of a  
**softening** spring

# Translational Mechanical Systems: Element Laws

## □ Spring Constant

- The spring constant can be determined experimentally by a [tension test](#) or analytically from the [geometry and material properties](#).

Coil spring



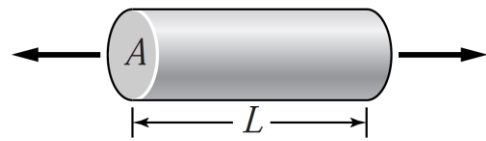
$$K = \frac{Gd^4}{64nR^3}$$

$d$  = wire diameter

$n$  = number of coils

$G$  = Shear modulus of elasticity

Solid rod



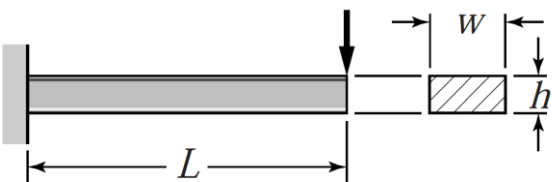
$$K = \frac{EA}{L}$$

$A$  = rod area

$L$  = rod length

$E$  = Modulus of elasticity

Cantilever beam



$$K = \frac{Ewh^3}{4L^3}$$

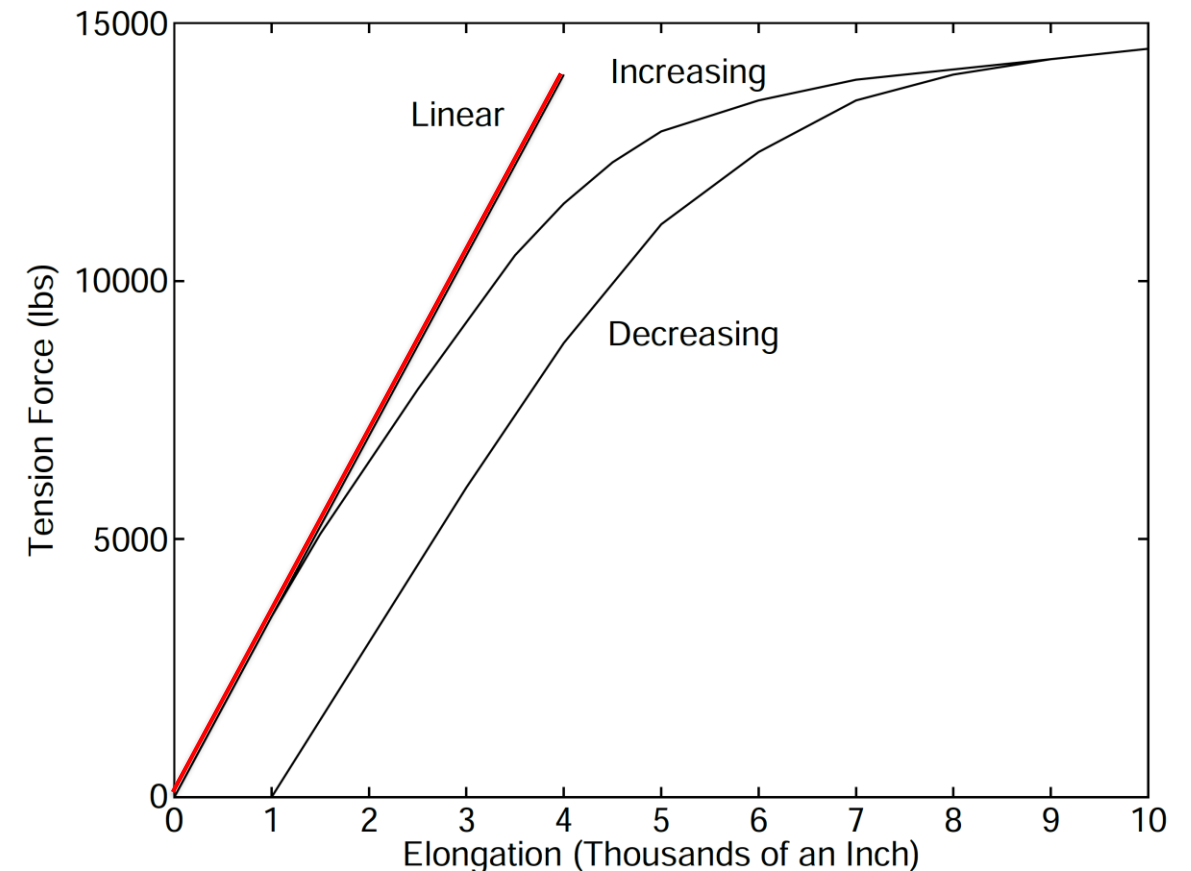
$w$  = beam width

$h$  = beam thickness

$L$  = beam length

$E$  = Modulus of elasticity

Plot of Tension Test Data





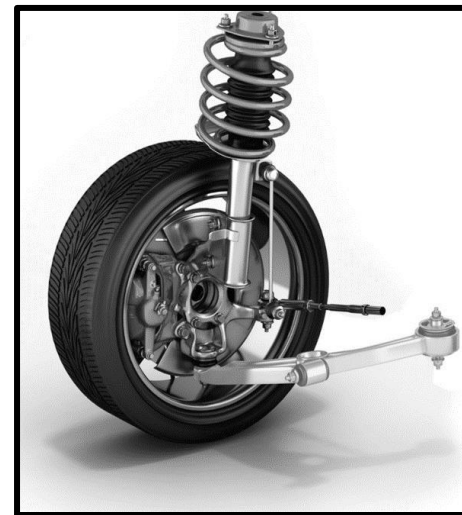
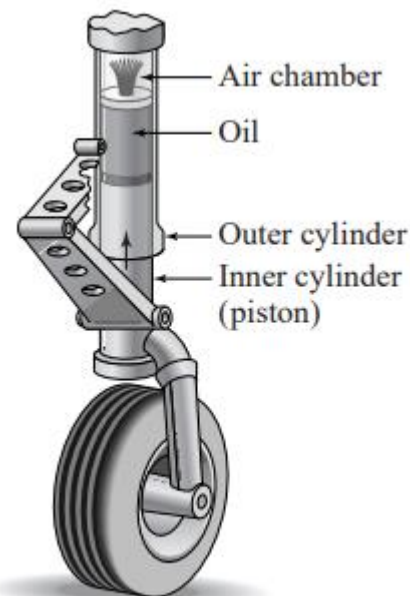
# Translational Mechanical Systems: Element Laws

## □ Damping Element

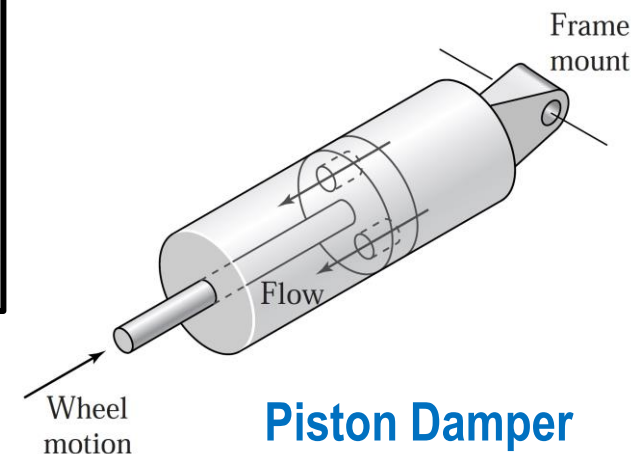
- A **damping element** or **damper** is an element that resists relative **velocity** across it.
- A common example of a damping element is a **dashpot (a shock absorber)**, which consists of a **piston** and an **oil filled cylinder**. Any relative motion between the piston rod and the cylinder is resisted by oil because oil must flow around the piston from one side to the other.
- An example from everyday life of a device that contains a damping element as well as a spring element is the **door closer**
- An **oleo strut** is a **pneumatic air–oil hydraulic shock absorber** used on the landing gear of most large aircraft and many smaller ones. This design cushions the impacts of landing and damps out vertical oscillations.



**Oleo Strut**



**Shock Absorber**



**Piston Damper**

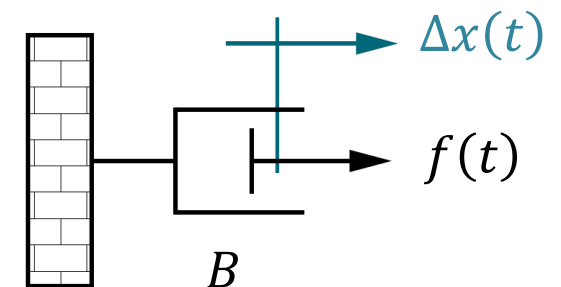


**Pneumatic Door Closer**

# Translational Mechanical Systems: Element Laws

## □ Damping Element

- Essentially, the damper **absorbs energy**, and the absorbed energy is **dissipated as heat** that flows away to the surroundings.
- Damping can exist whenever there is a **fluid resistance force** produced by a fluid layer moving relative to a solid surface.
- Engineering systems can exhibit damping in **bearings** and other **surfaces lubricated** to prevent wear.
- Damping elements can be deliberately included as part of the design.
- Drag friction or damping effect in a system can be represented by a linear **damper**.
- If a **force** is applied to a viscous damper, then it is opposed by an opposing force due to **viscus friction** of the damper.
- The **applied force**  $f(t)$  is proportional to the **velocity**  $v(t)$  of the motion.
- The  $B$  is the **viscus friction coefficient**. The unit is (N.s/m)

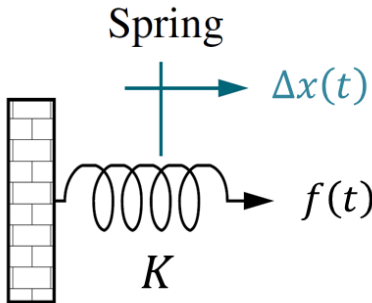
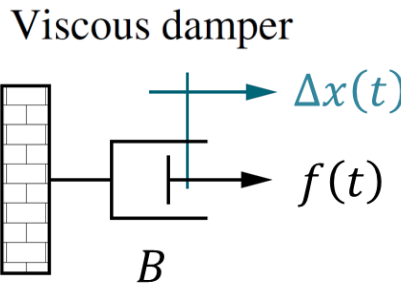
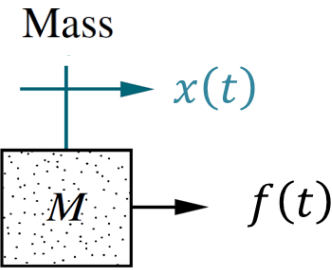


$$f(t) = B\Delta v(t) = B \frac{d\Delta x(t)}{dt}$$

# Translational Mechanical Systems: Element Laws

## □ Summary

- Table shows summary of the Force-velocity, and Force-displacement translational relationships for Spring, Viscous dampers, and Mass.

Element	Force-velocity	Force-displacement
<p>Spring</p> 	$f(t) = K \int_0^t \Delta v(t) dt$	$f(t) = K \Delta x(t)$
<p>Viscous damper</p> 	$f(t) = B \Delta v(t)$	$f(t) = B \frac{d\Delta x(t)}{dt}$
<p>Mass</p> 	$f(t) = M \frac{dv(t)}{dt}$	$f(t) = M \frac{d^2 x(t)}{dt^2}$



# Translational Mechanical Systems: Interconnection Laws

## □ Newton's Second Law

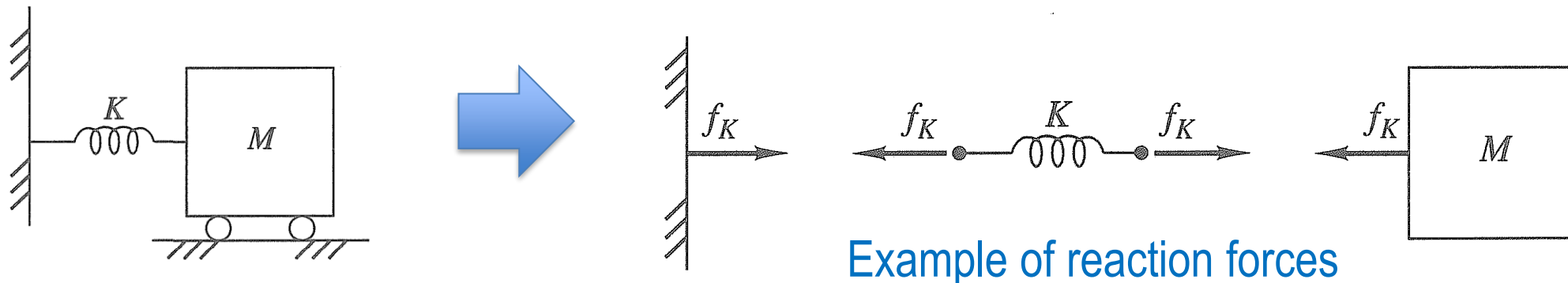
- Suppose that forces are acting on a body of mass  $m$ . If  $\sum F$  is the sum of all forces acting on mass  $m$  through the center of mass in a given direction, then,

$$\sum f_{ext} = ma$$

where  $a(t)$  is the resulting absolute acceleration in that direction.

## □ Newton's Third Law: The Law of Reaction Forces

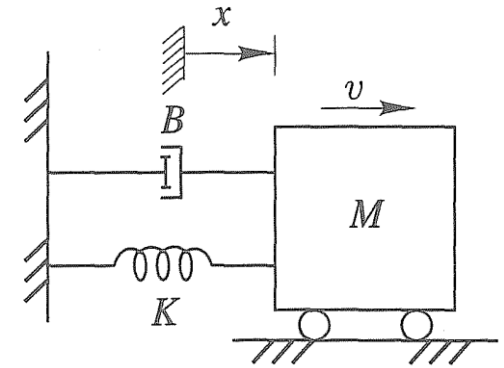
- In order to relate the forces exerted by the elements of friction and stiffness to the forces acting on a mass or junction point, we need Newton's third law regarding reaction forces.
- Accompanying any force of one element on another, there is a reaction force on the first element of equal magnitude and opposite direction.



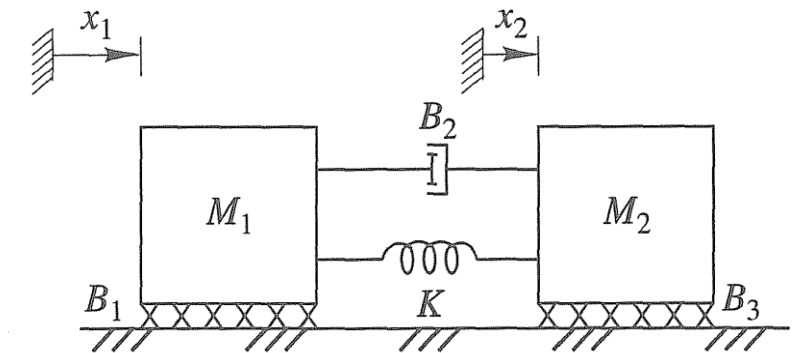
# Translational Mechanical Systems: Interconnection Laws

## □ The Law for Displacement

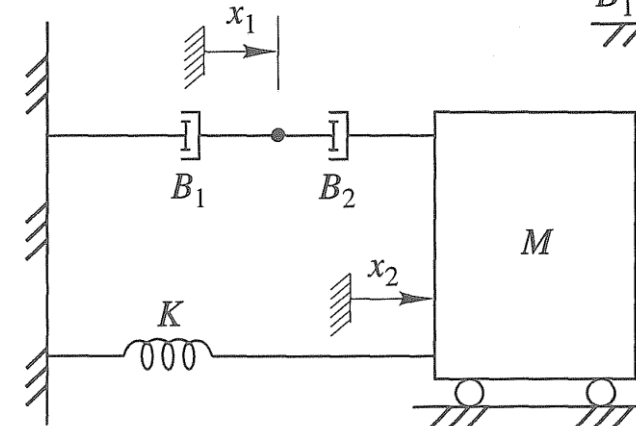
- If the ends of two elements are connected, those ends are forced to move with the **same displacement** and **velocity**.
- For example, because the damper and spring are both connected between the wall and the mass, the right ends of both elements have the same displacement  $x$  and move with the same velocity  $v$ .



- In this system, where  $B_2$  and  $K$  are connected between two moving masses, the elongation of both elements is  $x_2 - x_1$ .



- Let  $x_1$  and  $x_2$  denote displacements measured with respect to reference position. Then the respective elongations of  $B_1$ ,  $B_2$  and  $K$  are  $x_1$ ,  $x_2 - x_1$  and  $x_2$ .



# Modeling of Translational Mechanical Systems

## Example 1

Find the equation of motion for the given mass-spring-damper system. Assume that the input is the applied force, and the output is the displacement of the mass.

Assume that the positive direction for motion is to the right.

Draw the free-body diagram of the system for the mass  $M$ .

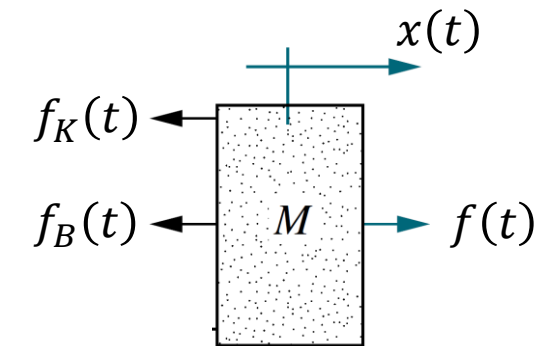
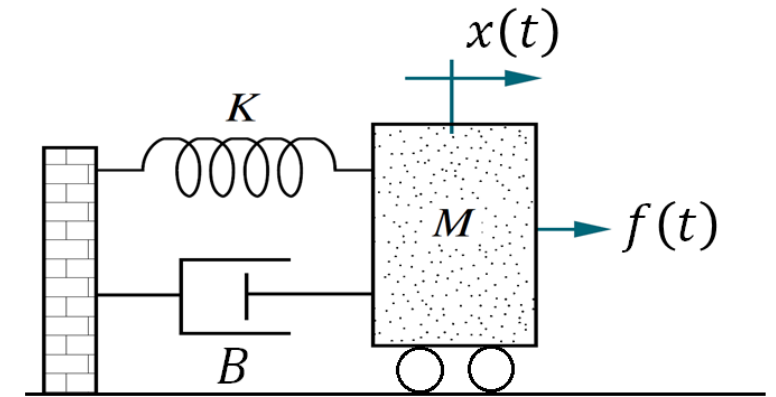
Apply Newton's second law to find the equation of motion.

$$\sum f_{ext} = ma \rightarrow f(t) - f_K(t) - f_B(t) = Ma(t)$$
$$f(t) - Kx(t) - B \frac{dx(t)}{dt} = M \frac{d^2x(t)}{dt^2}$$

The equation of motion is obtained as a second-order differential equation,

$$M \frac{d^2x(t)}{dt^2} + B \frac{dx(t)}{dt} + Kx(t) = f(t)$$

Second-order  
Differential Equation



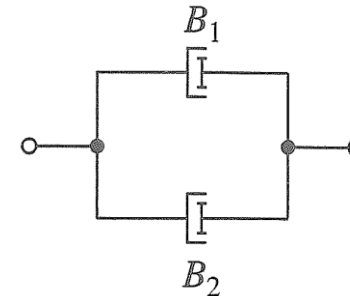
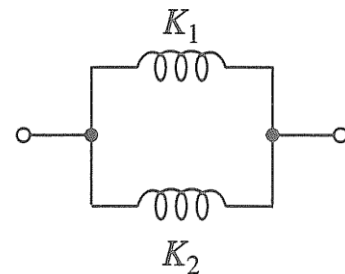
Free-body Diagram

# Modeling of Translational Mechanical Systems

## □ Parallel & Series Combination

- In some cases, two or more **springs** or **dampers** can be replaced by a single equivalent element.
- Two **springs** or **dampers** are said to be **in parallel** if the first end of each is attached to the same body and if the remaining ends are also attached to a common body.
- The key requirement for parallel elements is that **respective ends move with the same displacement**.

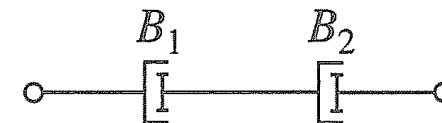
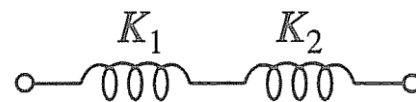
$$K_{eq} = K_1 + K_2$$



$$B_{eq} = B_1 + B_2$$

- Two **springs** or **dampers** are said to be **in series** if they are joined at only one end of each element and if there is **no other element connected to their common junction**.

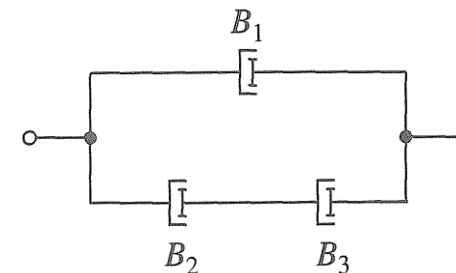
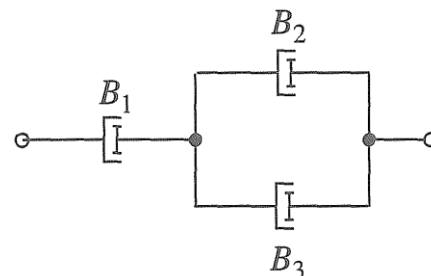
$$\frac{1}{K_{eq}} = \frac{1}{K_1} + \frac{1}{K_2}$$



$$\frac{1}{B_{eq}} = \frac{1}{B_1} + \frac{1}{B_2}$$

- It is also possible to have combination of series and parallel connections. For example:

$$B_{eq} = \frac{B_1(B_2 + B_3)}{B_1 + B_2 + B_3}$$



$$B_{eq} = B_1 + \frac{B_2 B_3}{B_2 + B_3}$$

# Modeling of Translational Mechanical Systems

## Example 2

Find the equation describing the motion of the mass in the translational system shown below. Show that the two springs can be replaced by a single equivalent spring, and the three friction elements by an equivalent element.

Assume that the **positive direction for motion** is to the **right**.

Draw the **free-body diagram** of the system for the mass  $M$ .

Apply **Newton's second law** to find the **equation of motion**.

$$\sum f_{ext} = ma$$

$$\text{Mass } M \rightarrow f_a(t) - K_1x - B_1\dot{x} - B_2\dot{x} - B_3\dot{x} - K_2x = M\ddot{x}$$

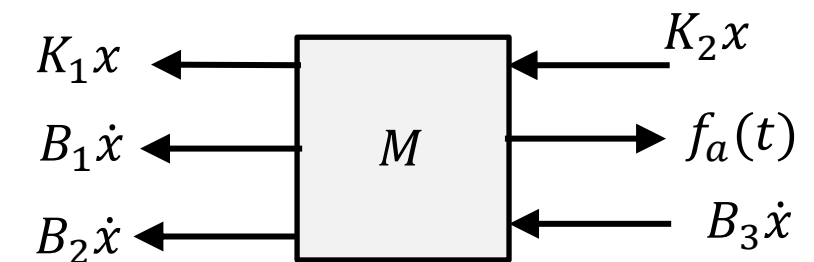
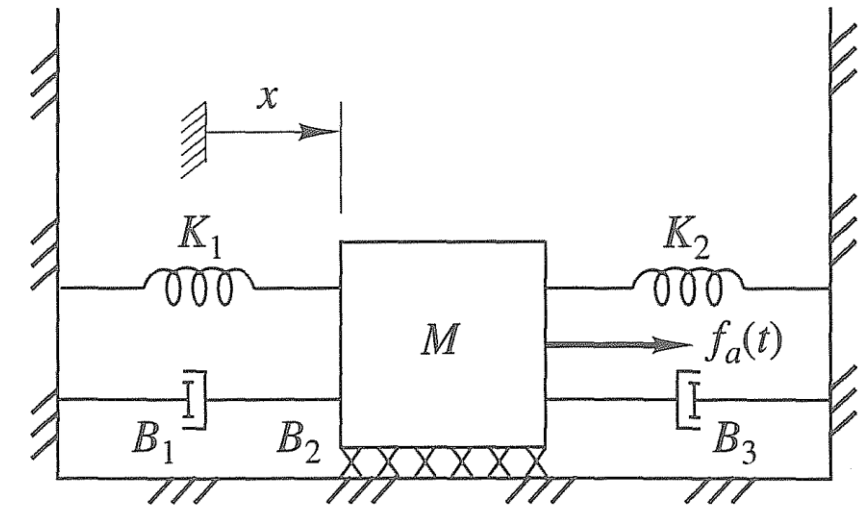
$$f_a(t) = M\ddot{x} + (B_1 + B_2 + B_3)\dot{x} + (K_1 + K_2)x$$

We can see that the two springs and the three damping elements can be replaced by an equivalent element.

$$f_a(t) = M\ddot{x} + B_{eq}\dot{x} + K_{eq}x$$

$$B_{eq} = B_1 + B_2 + B_3$$

$$K_{eq} = K_1 + K_2$$



Free-body Diagram

# Modeling of Translational Mechanical Systems

## Example 3

When  $x_1 = x_2 = 0$ , the two springs are neither stretched nor compressed. Draw free-body diagrams for the mass  $M$  and for the **massless junction A**, then write the equation of motion of the system. Find  $K_{eq}$  for a single spring that could replace the combination of  $K_1$  and  $K_2$ .

Assume that the **positive direction for motion** is to the **left**.

**Mass  $M \rightarrow$**   $f_a(t) - B\dot{x}_1 - K_1(x_1 - x_2) = M\ddot{x}_1$

**Junction A  $\rightarrow$**   $K_1(x_1 - x_2) = K_2x_2$

Solve the second equation for  $x_2$  in terms of  $x_1$  gives:

$$x_2 = \left( \frac{K_1}{K_1 + K_2} \right) x_1 \rightarrow \text{two displacement proportional to one another}$$

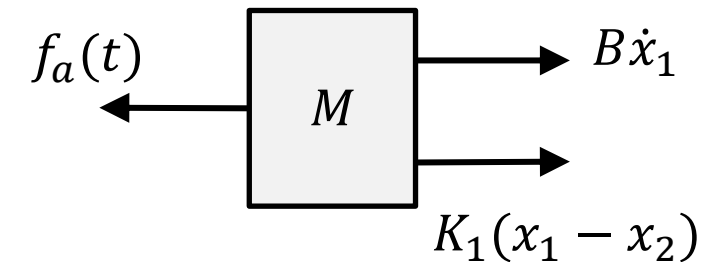
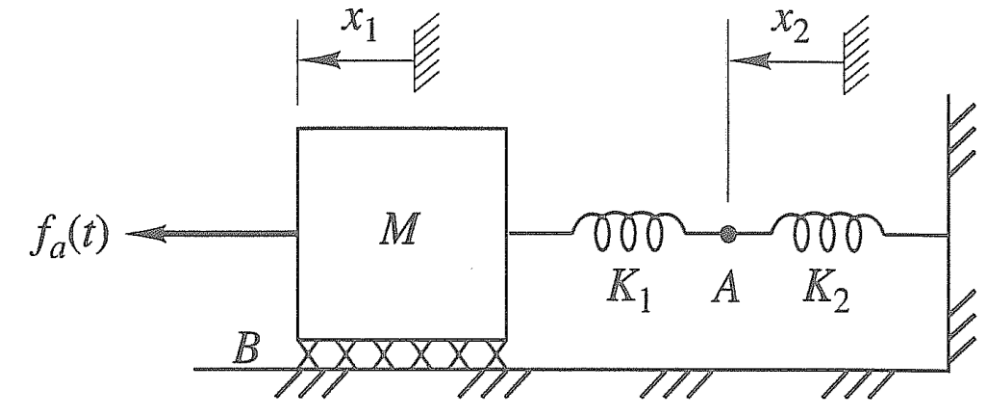
Substituting the  $x_2$  into the first equation we have:

$$f_a(t) - B\dot{x}_1 - K_1 \left( x_1 - \frac{K_1}{K_1 + K_2} x_1 \right) = M\ddot{x}_1 \rightarrow f_a(t) = M\ddot{x}_1 + B\dot{x}_1 + \frac{K_1 K_2}{K_1 + K_2} x_1$$

This equation describes the system formed when the two springs are replaced by a single spring for:

$$K_{eq} = \frac{K_1 K_2}{K_1 + K_2}$$

$$f_a(t) = M\ddot{x}_1 + B\dot{x}_1 + K_{eq}x_1$$



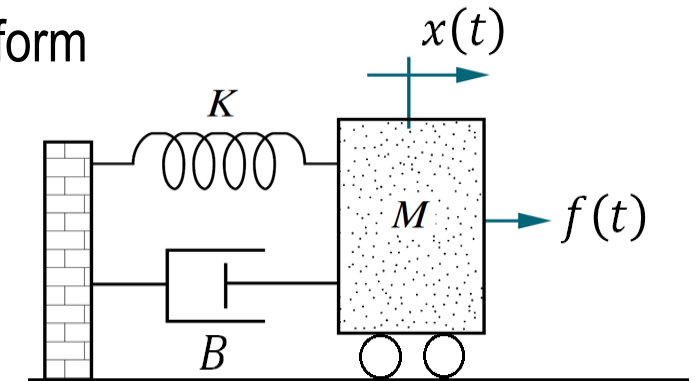
# Modeling of Translational Mechanical Systems

## □ Solving the Equation of Motion

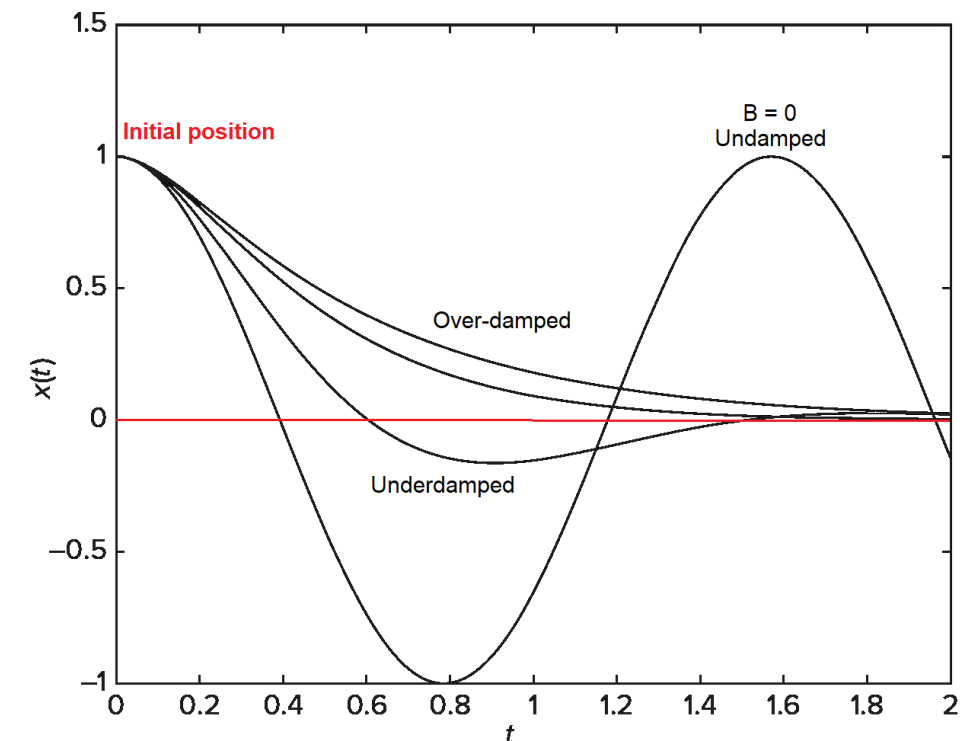
- We have seen that the **equation of motion** of mass-spring-damper systems has the general form of **second-order ODE**,

$$M\ddot{x}(t) + B\dot{x}(t) + Kx(t) = f(t)$$

where  $f(t)$  is an applied external force other than gravity.



- Solution of the **equation of motion** mainly depends on the value of the **damping element**.
- Assume that the applied force  $f(t)$  is **zero**, and we slightly moved and released the mass with the initial condition of  $x(0) = 1, \dot{x}(0) = 0$
- For **no damping or friction** ( $B = 0$ ), the system is **neutrally stable**, and the mass **oscillates** with a **constant amplitude** and the **natural frequency**.
- As **damping is increased** slightly, the system becomes **stable**, and mass **still oscillates** but with smaller frequency.
- As the damping is **increased further**, the mass **no longer oscillates** because the **damping force is large enough** to limit the velocity and prevent the mass from overshooting the equilibrium position.





# Modeling of Translational Mechanical Systems

## □ Review of ODE Trial-Solution

- Table shows a summary of the trial-solution for the **first-order** and **second-order** ODE for **constant input**:

Equation	Solution Form
<b>First order:</b> $\dot{x}(t) + ax(t) = b, \quad a \neq 0$	$x(t) = \frac{b}{a} + Ce^{-at}$
<b>Second order:</b> $\ddot{x}(t) + a\dot{x}(t) + bx(t) = c, \quad b \neq 0$  1. $(a^2 > 4b)$ distinct, real roots: $s_1, s_2$  2. $(a^2 = 4b)$ repeated, real roots: $s_1, s_1$  3. $(a = 0, b > 0)$ imaginary roots: $s = \pm j\omega_n, \quad \omega_n = \sqrt{b}$  4. $(a \neq 0, a^2 < 4b)$ complex roots: $s = \sigma \pm j\omega_d$ $\sigma = -\frac{a}{2}, \quad \omega_d = \frac{1}{2}\sqrt{4b - a^2}$	$x(t) = \frac{c}{b} + C_1 e^{s_1 t} + C_2 e^{s_2 t}$  $x(t) = \frac{c}{b} + (C_1 + C_2 t) e^{s_1 t}$  $x(t) = \frac{c}{b} + C_1 \sin \omega_n t + C_2 \cos \omega_n t$  $x(t) = \frac{c}{b} + e^{\sigma t} (C_1 \sin \omega_d t + C_2 \cos \omega_d t)$

- The coefficients  $C, C_1$  and  $C_2$  are determined from the given initial conditions  $x(0)$  and  $\dot{x}(0)$

# Modeling of Translational Mechanical Systems

## □ Review of Types of Response

- The first-order ODE dynamic models has the following general form, where  $f(t)$  is the **input** or **forcing function**, and  $x(t)$  is the **output** variable.

$$\dot{x}(t) + ax(t) = f(t)$$

- If the **forcing input is a constant**,  $f(t) = b$ , and **non-zero initial conditions**  $x(0)$ , the general solution can be shown as

$$\dot{x}(t) + ax(t) = b \quad \rightarrow \quad x(t) = \frac{b}{a} + Ce^{at}$$

- The coefficient  $C$  is determined from the initial conditions at  $t = 0$ :

$$x(0) = \frac{b}{a} + C \quad \rightarrow \quad C = x(0) - \frac{b}{a}$$

- Therefore, the general solution can be rearranged and shown as two terms:

$$x(t) = \frac{b}{a} + \left(x(0) - \frac{b}{a}\right)e^{at} \quad \rightarrow \quad x(t) = \underbrace{x(0)e^{-at}}_{\substack{\text{Free response} \\ \text{Zero-input response}}} + \underbrace{\frac{b}{a}(1 - e^{-at})}_{\substack{\text{Forced response} \\ \text{Zero-initial condition response}}}$$

- Free Response:** The part of the response that depends on the initial conditions.
- Forced Response:** The part of the response due to the forcing function.

# Modeling of Translational Mechanical Systems

## □ Review of Types of Response

- Consider the general solution of first-order ODE:

$$x(t) = x(0)e^{-at} + \frac{b}{a}(1 - e^{-at})$$

- The general solution can also be rearranged as follows to distinguish the **transient** and the **steady-state** responses:

$$x(t) = \underbrace{\frac{b}{a}}_{\text{Steady-state response}} + \underbrace{\left(x(0) - \frac{b}{a}\right)e^{-at}}_{\text{Transient Response}}$$

- Transient Response:** The part of the response that disappears with time.
- Steady-state Response:** The part of the response that remains with time.
- The same concepts are applicable for the response of the second-order ODE systems.

# Modeling of Translational Mechanical Systems

## □ Solving the Equation of Motion

### ○ Underdamped Response

In **underdamped** system, the damping force is not large enough to overcome the oscillation:

$$M\ddot{x}(t) + B\dot{x}(t) + Kx(t) = f(t)$$

Assume  $M = 50\text{kg}$ ,  $B = 30\text{ Ns/m}$  and  $K = 100\text{N/m}$  and the applied force is  $f(t) = 100\text{N}$  :

$$50\ddot{x}(t) + 30\dot{x}(t) + 100x(t) = 100 \quad \rightarrow \quad \ddot{x}(t) + 0.6\dot{x}(t) + 2x(t) = 2$$

- Solution of the equation of motion for zero initial condition  $x(0) = 0$ ,  $\dot{x}(0) = 0$ :

Characteristic Equation  $\rightarrow s^2 + 0.6s + 2 = 0$

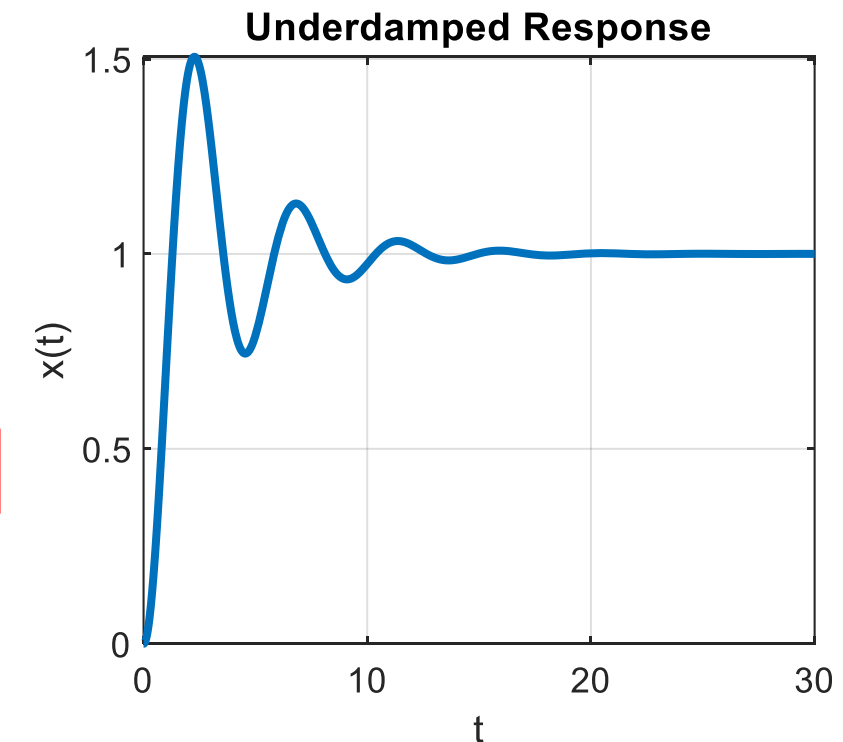
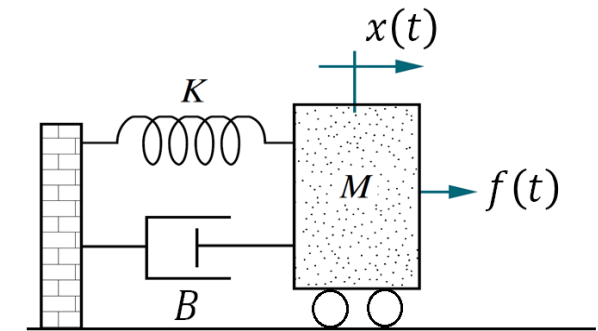
Characteristic Roots  $\rightarrow s_{1,2} = -0.3 \pm j1.38$  (Complex roots)

Solution  $\rightarrow x(t) = 1 - e^{-0.3t}(0.217 \sin(1.38 t) - \cos(1.38 t)), \quad t \geq 0$

Steady-state response

Transient Response

This solution shows that the mass oscillates with the **damped frequency**  $\omega_d$ , and the transient response will disappear with time due to the **exponential** term.



# Modeling of Translational Mechanical Systems

## □ Solving the Equation of Motion

### ○ Over-damped Response

In **over-damped** system, the damping force is large enough to limit the velocity and avoid the overshoot:

$$M\ddot{x}(t) + B\dot{x}(t) + Kx(t) = f(t)$$

Assume  $M = 50\text{kg}$ ,  $B = 300 \text{ Ns/m}$  and  $K = 100\text{N/m}$  and the applied force is  $f(t) = 100\text{N}$  :

$$50\ddot{x}(t) + 300\dot{x}(t) + 100x(t) = 100 \quad \rightarrow \quad \ddot{x}(t) + 6\dot{x}(t) + 2x(t) = 2$$

- Solution of the equation of motion for zero initial condition  $x(0) = 0$ ,  $\dot{x}(0) = 0$ :

Characteristic Equation  $\rightarrow s^2 + 6s + 2 = 0$

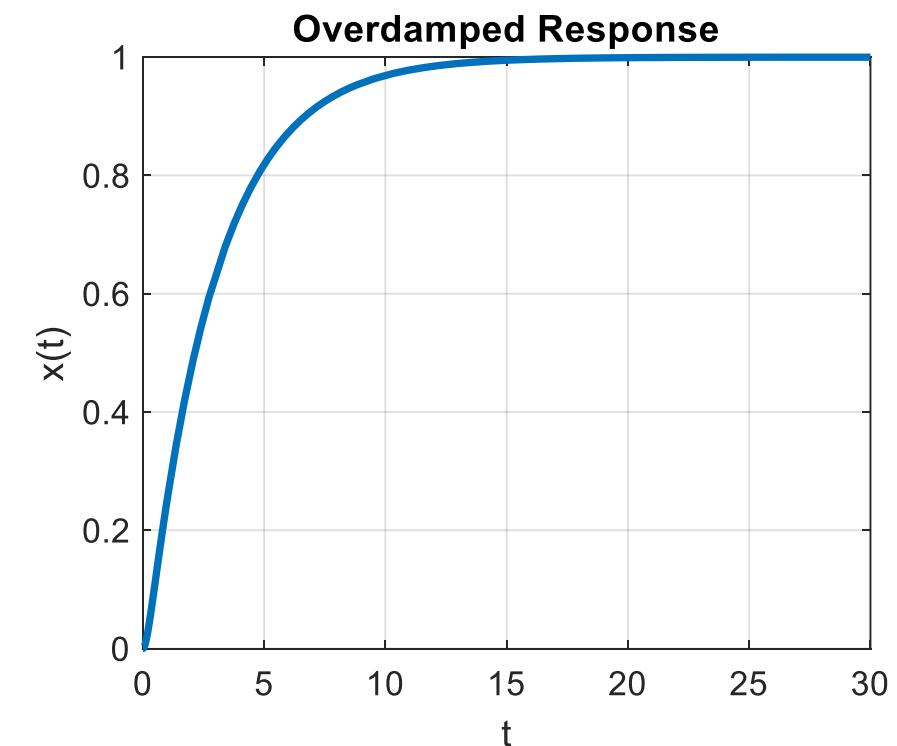
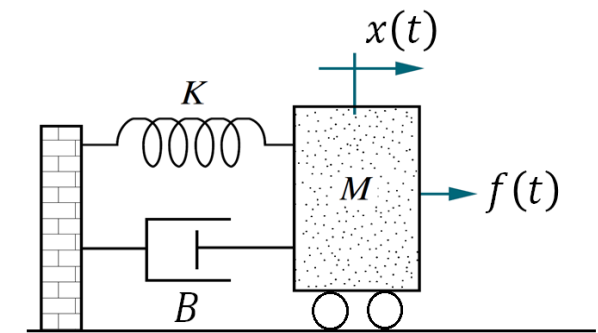
Characteristic Roots  $\rightarrow s_1 = -5.65$ ,  $s_2 = -0.35$  (Distinct, real roots)

Solution  $\rightarrow x(t) = 1 + 0.067e^{-5.65t} - 1.067e^{-0.35t}, \quad t \geq 0$

Steady-state response

Transient Response

The transient response consists of exponential terms, and the steady-state response is 1.



# Modeling of Translational Mechanical Systems

## □ Solving the Equation of Motion

### ○ No Damping (Undamped): $B = 0$

When there is no damping or friction, the system will be a simple **mass-spring** system:

$$M\ddot{x}(t) + Kx(t) = f(t)$$

Assume  $M = 50\text{kg}$ ,  $B = 0$  and  $K = 100\text{N/m}$  and the applied force is  $f(t) = 100\text{N}$ :

$$50\ddot{x}(t) + 100x(t) = 100 \quad \rightarrow \quad \ddot{x}(t) + 2x(t) = 2$$

Solution of the equation of motion for zero initial condition  $x(0) = 0$ ,  $\dot{x}(0) = 0$ :

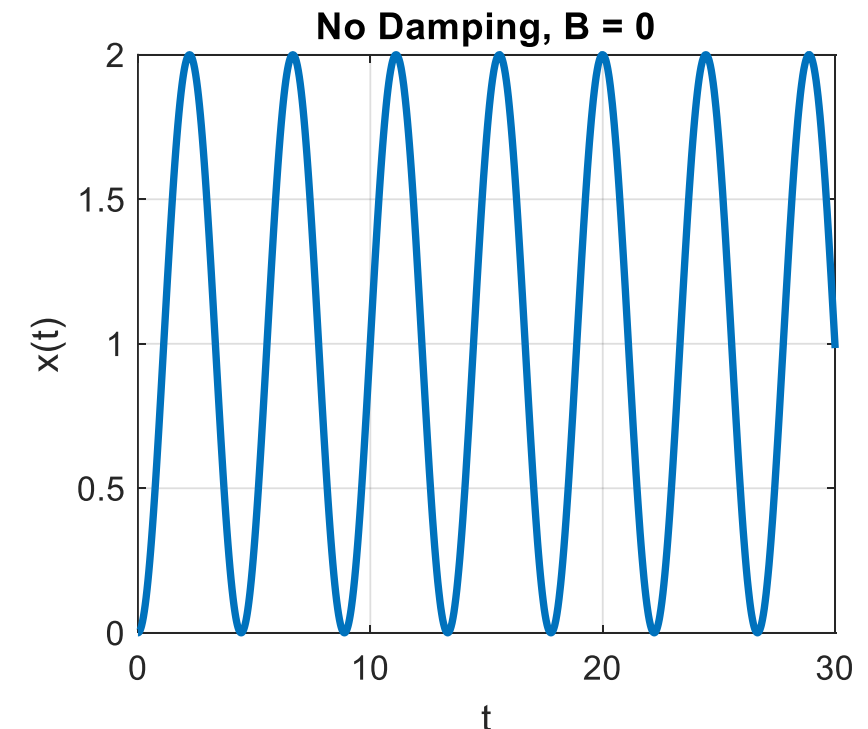
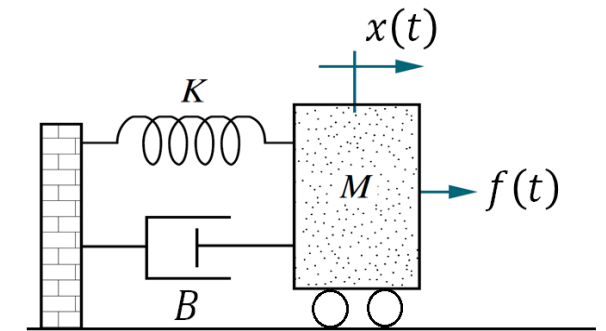
Characteristic Equation  $\rightarrow s^2 + 2 = 0$

Characteristic Roots  $\rightarrow s = \pm j\sqrt{2}$  (Imaginary roots)

Solution  $\rightarrow x(t) = 1 - \cos(\sqrt{2} t)$

This solution shows that the mass oscillates with the **natural frequency**  $\omega_n$ , and the transient response will not disappear with time.

$$\omega_n = \sqrt{\frac{K}{M}} = \sqrt{\frac{100}{50}} = \sqrt{2} \text{ rad/s}$$



# Modeling of Translational Mechanical Systems

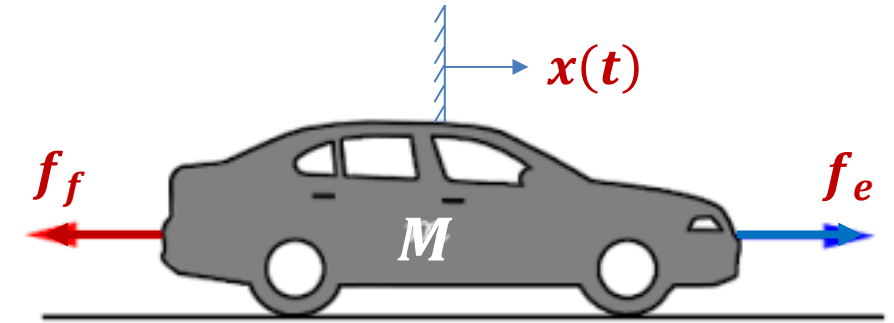
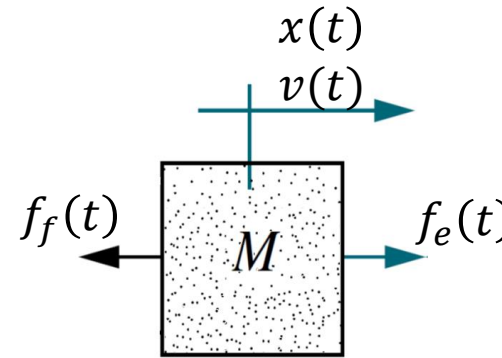
## Example 4

Consider the following simple cruise system. Assume that the engine applies a forward force of  $f_e(t)$  and air friction is proportional to the car's speed  $v(t)$ .

To obtain a system model we draw **free-body** diagrams

Apply **Newton's second law** as below

$$\sum f_{ext} = ma \quad \rightarrow \quad f_e(t) - f_f(t) = Ma(t)$$
$$f_e(t) - Bv(t) = Mv'(t)$$



**Input:** Applied force  $f_e(t)$

**Output:** Car speed  $v(t)$

The **differential equation** relating speed of the car  $v(t)$  to the engine force  $f_e(t)$  is determined as

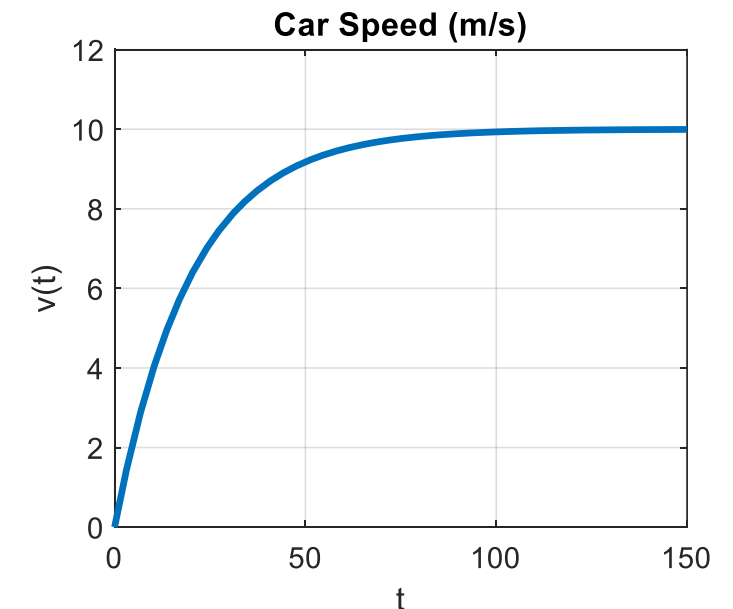
$$f_e(t) = Mv'(t) + Bv(t) \quad \text{First-order differential equation}$$

Assume  $M = 1000\text{kg}$  and  $B = 50\text{Ns/m}$  we have:

$$f_e(t) = 1000v'(t) + 50v(t)$$

Assume applied force is  $f(t) = 500\text{N}$ , and initial speed is zero. The solution of the first-order differential equation is:

$$v(t) = 10(1 - e^{-t/20})$$



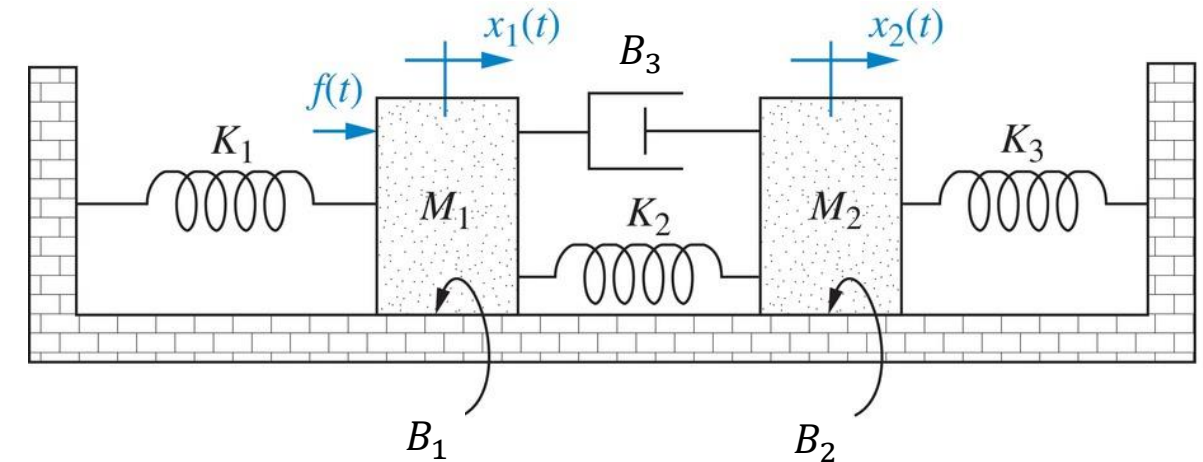


# Modeling of Translational Mechanical Systems

**Example 5** Draw the free-body diagrams and use Newton's second law to write two modeling equations for the given two-mass system.

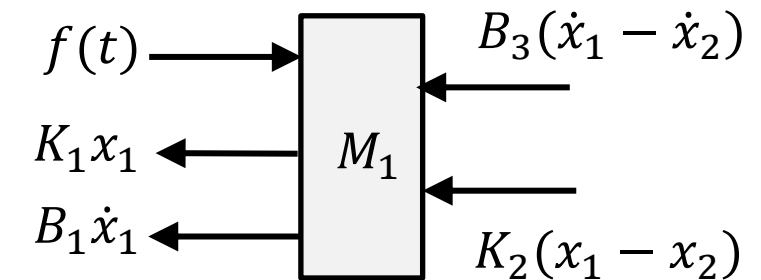
The system has **two degrees of freedom**, since each mass can be moved in the horizontal direction while the other is held still.

Draw the **free-body diagram** of mass body  $M_1$  and  $M_2$ .



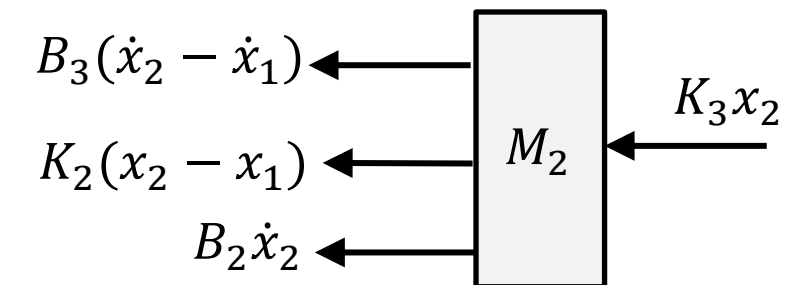
$$\text{Mass } M_1 \rightarrow f(t) - K_1 x_1 - B_1 \dot{x}_1 - B_3(\dot{x}_1 - \dot{x}_2) - K_2(x_1 - x_2) = M_1 \ddot{x}_1$$

$$\text{Mass } M_2 \rightarrow -B_3(\dot{x}_2 - \dot{x}_1) - K_2(x_2 - x_1) - B_2 \dot{x}_2 - K_3 x_2 = M_2 \ddot{x}_2$$



Rearrange the equations to find the **equations of motion**:

$$\begin{cases} \text{Mass } M_1 \rightarrow M_1 \ddot{x}_1 + (B_1 + B_3) \dot{x}_1 + (K_1 + K_2) x_1 - B_3 \dot{x}_2 - K_2 x_2 = f(t) \\ \text{Mass } M_2 \rightarrow M_2 \ddot{x}_2 + (B_2 + B_3) \dot{x}_2 + (K_2 + K_3) x_2 - B_3 \dot{x}_1 - K_2 x_1 = 0 \end{cases}$$



# Modeling of Translational Mechanical Systems

## □ Choosing the Equilibrium Position as Coordinate Reference

- Assume the mass-spring-damper system in **vertical motion**.
- Draw the **free-body diagram** of mass body  $M$  including the gravitational force.

$$\text{Mass } M \rightarrow f_a(t) + Mg - Kx - B\dot{x} = M\ddot{x} \rightarrow f_a(t) + Mg = M\ddot{x} + B\dot{x} + Kx$$

- Suppose that the applied force  $f_a(t)$  is **zero** and the mass is not moving.

Then  $x = x_0$  is the constant displacement caused by the gravitational force.

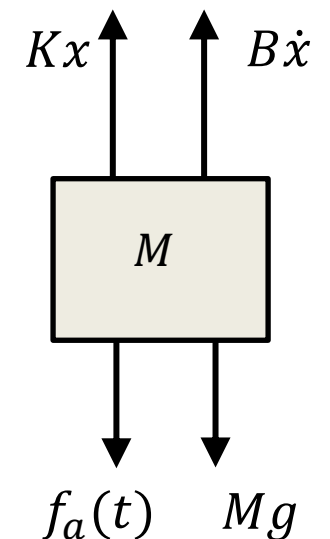
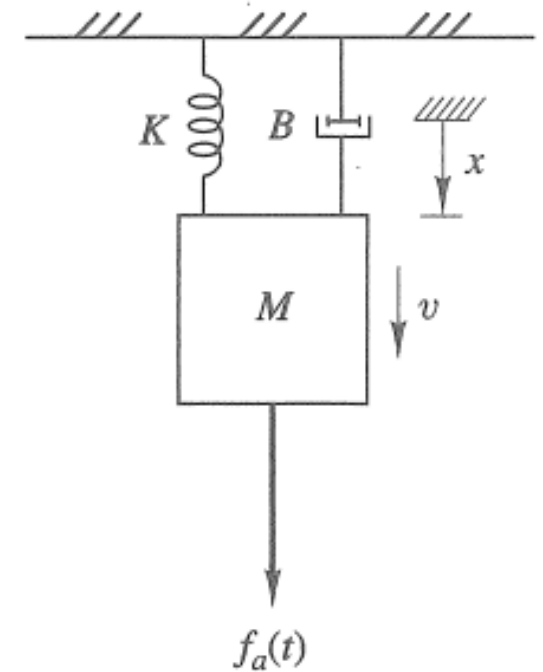
Since,  $\dot{x}_0 = \ddot{x}_0 = 0$  the equation of motion is  $\rightarrow Mg = Kx_0$

- Now reconsider the case when  $f_a(t)$  is **nonzero** and the mass is moving.

Then  $x = x_0 + z$ , where  $z$  is the additional displacement caused by  $f_a(t)$

$$f_a(t) + Mg = M\ddot{z} + B\dot{z} + K(x_0 + z) \rightarrow f_a(t) = M\ddot{z} + B\dot{z} + Kz$$

- For a mass connected to a spring element, the force due to gravity  $Mg$  is canceled out of the equation of motion by the force in the spring due to its static deflection, **as long the displacement of the mass is measured from the equilibrium position**.
- This means that if we are defined the vertical displacement from the **static-equilibrium position** caused by the gravitational force, then **no need to show the  $Mg$  force** in our free-body diagram.



# Modeling of Translational Mechanical Systems

## □ Displacement Input

### Example 6

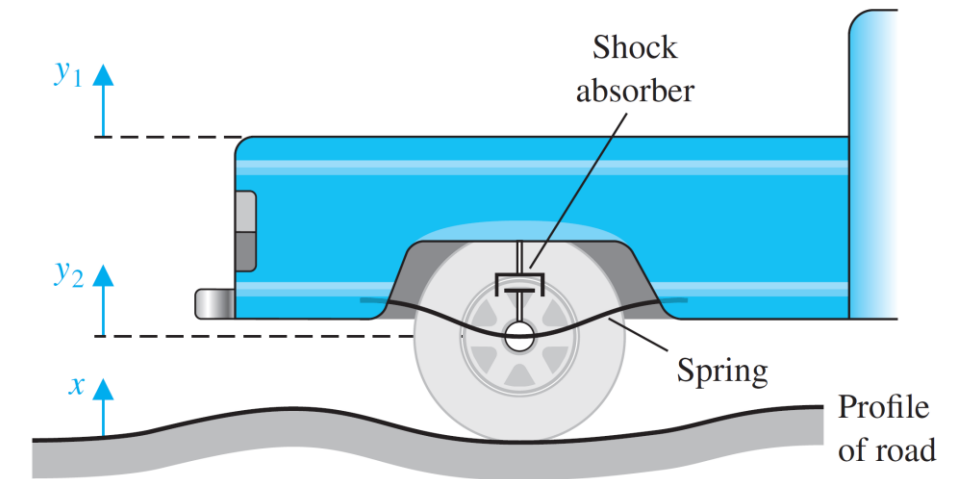
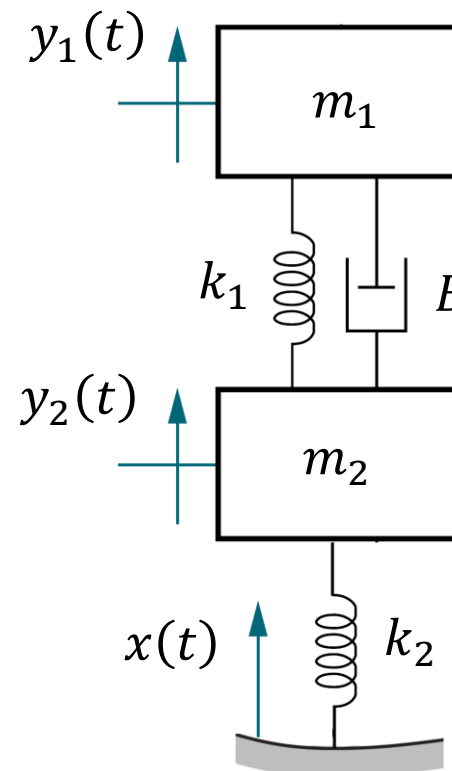
The suspension system for one wheel of an old-fashioned pickup truck is shown in the figure. The mass of the vehicle is  $m_1$  and the mass of the wheel is  $m_2$ . The suspension spring has a spring constant  $k_1$  and the tire has a spring constant  $k_2$ . The damping constant of the shock absorber is  $B$ . Derive the equations of motion for  $m_1$  and  $m_2$  in terms of the displacements from equilibrium,  $y_1$  and  $y_2$  with  $x(t)$  as the input.

Assume that the mass is traveling upward, the **suspension system** can be modeled as a following **mass-spring-damper system**.

The system has **two degrees of freedom**, since each mass can be moved in the vertical direction while the other is held still.

Draw the **free-body diagram** of the system for each mass.

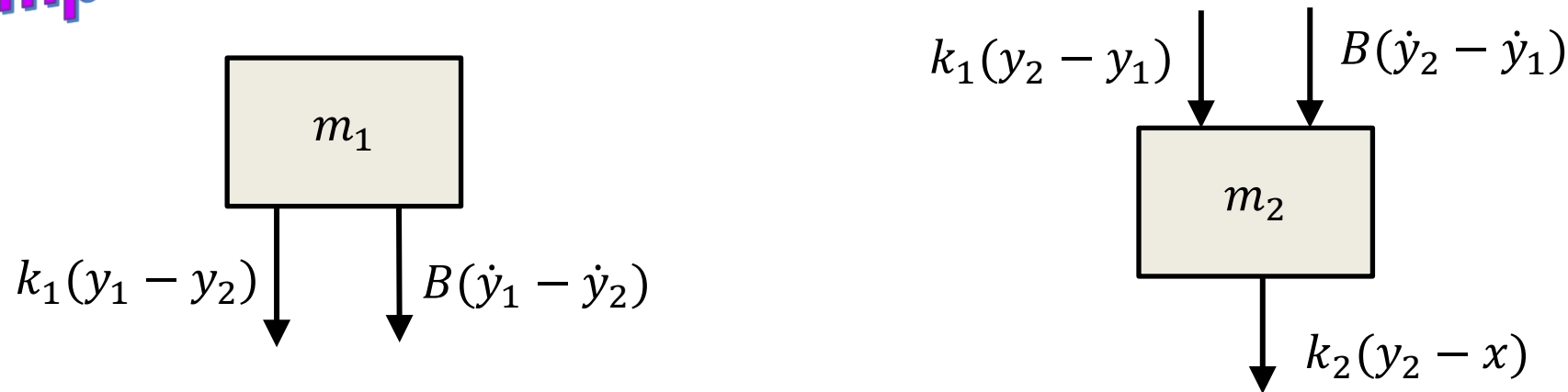
Place all the forces felt by the mass.



# Modeling of Translational Mechanical Systems

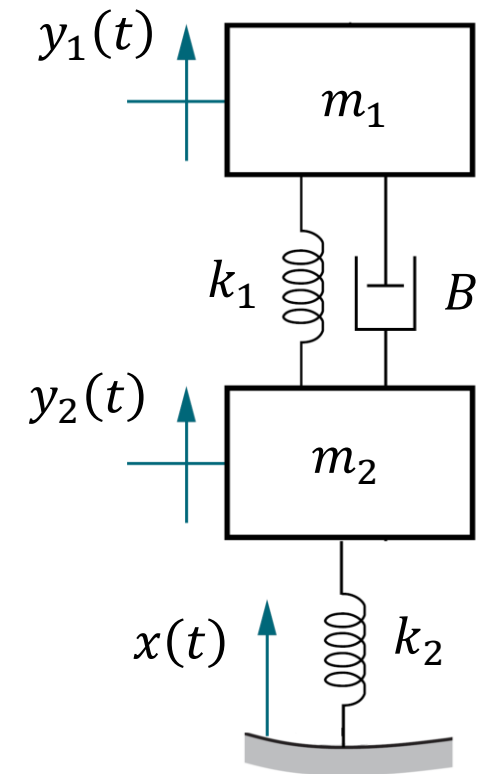
## Example 6

Draw the free-body diagram of mass body  $m_1$  and  $m_2$ .



For mass  $m_1 \rightarrow -k_1(y_1 - y_2) - B(\dot{y}_1 - \dot{y}_2) = m_1\ddot{y}_1$  **Eqn.1**

For mass  $m_2 \rightarrow -k_1(y_2 - y_1) - B(\dot{y}_2 - \dot{y}_1) - k_2(y_2 - x) = m_2\ddot{y}_2$  **Eqn. 2**



Note that since the **gravitational force** is canceled out by the **static spring force**, no need to include gravity in the equations.

Rearrange the equations to find the **equations of motion**:

$$\begin{cases} \text{For mass } m_1 & \rightarrow & m_1\ddot{y}_1 + B\dot{y}_1 + k_1y_1 - B\dot{y}_2 - k_1y_2 = 0 \\ \text{For mass } m_2 & \rightarrow & m_2\ddot{y}_2 + B\dot{y}_2 + (k_1 + k_2)y_2 - B\dot{y}_1 + k_1y_1 - k_2x = 0 \end{cases}$$

# THANK YOU