Root-Locus for $K \in [0, +\infty)$

| Magnitude Condition: $ KG(s)H(s) = 1$ | Angle Condition: $\angle (KG(s)H(s)) = \pm (2i+1)180^{\circ}$ |
|--|--|
| Number of asymptote lines: $Relative \ degree = n - m$ | Angle of asymptote lines: |
| Intersection of asymptote lines with real axis: | Intersection of root locus with imaginary axis: |
| $\alpha = \frac{\sum_{i=1}^{n} p_i - \sum_{i=1}^{m} z_i}{n - m}$ | Assume $s = j\omega$ and compute the cross points and K value from characteristic equation |

Break-away (or break-in) points:

$$1 + KG(s)H(s) = 0 \quad \to \quad K = \frac{-1}{G(s)H(s)} \quad \to \quad \frac{dK}{ds} = 0 \quad \to \quad \text{solve for } s$$

Angle of departure from the complex pole:

180° – (sum of the angles of vectors drawn to this pole from other poles) + (sum of the angles of vectors drawn to this pole from zeros)

Angle of arrival to the complex zero:

 180° – (sum of the angles of vectors drawn to this zero from other zeros) + (sum of the angles of vectors drawn to this zero from poles)

| $G(s) = \frac{K_{dc}\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$ | Overshoot: $O. S. = e^{-\zeta \pi/\sqrt{1-\zeta^2}}$ |
|---|---|
| Settling-time (2%): $t_{\scriptscriptstyle S} = \frac{4}{\zeta \omega_n}$ | Damping ratio from overshoot: $\zeta = \frac{-\ln(O.S.)}{\sqrt{\pi^2 + \ln^2(O.S.)}}$ |
| Rise-time: $t_r \cong \frac{0.8 + 2.5 \zeta}{\omega_n}$ | Step-error-constant: $k_p = \lim_{s \to 0} G(s) \to e_{ss} = \frac{R}{1 + k_p}$ |
| Peak-time: $t_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}}$ | Ramp-error-constant: $k_v = \lim_{s \to 0} sG(s) \to e_{ss} = \frac{R}{k_v}$ |
| Resonant peak: $M_r = K_{dc} \frac{1}{2\zeta\sqrt{1-\zeta^2}}$ | Resonant frequency: $\omega_r = \omega_n \sqrt{1-2\zeta^2}$ |
| Initial-value Theorem: $f(0^+) = \lim_{t \to 0^+} f(t) = \lim_{s \to \infty} sF(s)$ | Final-value Theorem: $f(\infty) = \lim_{t \to \infty} f(t) = \lim_{s \to 0} sF(s)$ |

PD Controller (Frequency Domain):

$$G_c(s) = K_P \left(1 + \frac{T_d s}{\frac{T_d}{\beta} s + 1} \right)$$
 , $0 < \beta < 1$

$$\omega_m = \frac{\sqrt{\beta}}{T_d}$$
, $\sin(\phi_m) = \frac{\beta - 1}{\beta + 1}$

PI Controller:

$$G_c(s) = K_p \left(1 + \frac{1}{T_i s} \right)$$

PD Controller:

$$G_c(s) = K_p(1 + T_d s)$$

PID Controller:

$$G_c(s) = K_p \left(1 + \frac{1}{T_i s} + T_d s \right)$$

Lag Compensator:

$$G_c(s) = K_c \frac{s+z}{s+p}$$
 , $z > p > 0$

Lead Compensator:

$$G_c(s) = K_c \frac{s+z}{s+p}$$
 , $p > z > 0$

State space equations:

$$\begin{cases} \dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) \\ \mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}\mathbf{u}(t) \end{cases}$$

Controllability matrix:

$$Q_c = [B \quad AB \quad A^2B \quad A^3B \quad \cdots \quad A^{n-1}B]$$

Characteristics Equation:

$$\det(sI - A) = 0$$

Transfer function formula:

$$G(s) = C(sI - A)^{-1}B + D$$

Closed-loop system with state feedback control:

$$\begin{cases} \dot{\mathbf{x}}(t) = (\mathbf{A} - \mathbf{B}\mathbf{K})\mathbf{x}(t) + \mathbf{B}r(t) \\ y(t) = (\mathbf{C} - \mathbf{D}\mathbf{K})\mathbf{x}(t) + \mathbf{D}r(t) \end{cases}$$

Closed-loop system with state feedback with integrator control:

$$\begin{cases} \begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{q}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{A} - \mathbf{B}\mathbf{K} & \mathbf{B}k_i \\ -\mathbf{C} + \mathbf{D}\mathbf{K} & -\mathbf{D}k_i \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ q(t) \end{bmatrix} + \begin{bmatrix} \mathbf{0} \\ \mathbf{1} \end{bmatrix} r(t) \\ y(t) = \begin{bmatrix} \mathbf{C} - \mathbf{D}\mathbf{K} & \mathbf{D}k_i \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ q(t) \end{bmatrix} \end{cases}$$

Matrix inversion for 2×2 matrix:

$$\mathbf{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \quad \rightarrow \qquad \mathbf{A}^{-1} = \frac{1}{a_{11}a_{22} - a_{21}a_{12}} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix}$$

Mason's Formula:

$$\frac{Y_{out}}{Y_{in}} = \frac{1}{\Delta} \sum_{k=1}^{N} M_k \Delta_k$$

 $N = \text{Total number of forward paths between } Y_{in} \text{ and } Y_{out}$

 $M_k = \text{Gain of the } k \text{th forward path between } Y_{in} \text{ and } Y_{out}$

 $\Delta = 1$ – (sum of all loop gains)

- + (sum of products of all combinations of two non-touching loops)
- (sum of products of all combinations of three non-touching loops)
- + (sum of products of all combinations of four non-touching loops)

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 $\Delta_{\mathbf{k}}=$ the Δ of the SFG non-touching with the forward path M_k when M_k has been removed