

# HUMBER ENGINEERING

MENG 3510 – Control Systems  
LECTURE 11

# LECTURE 11

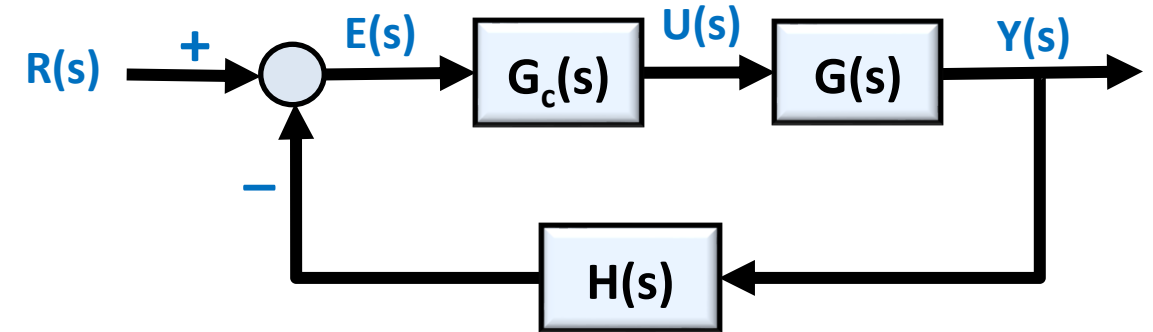
## Controller Design via Frequency Response

- Control System Design via Bode Diagram
  - Frequency Response of P, PI and PD Controllers
  - Proportional Controller Design
  - PD Controller Design
  - PI Controller Design

# Control System Design via Bode Diagram

- Consider the following closed-loop system with controller  $G_c(s)$

$$T(s) = \frac{Y(s)}{R(s)} = \frac{G_c(s)G(s)}{1 + G_c(s)G(s)H(s)}$$



- The goal is to **design the control system** using the **Bode diagram** of the **open-loop system**  $G_c(s)G(s)H(s)$ , to satisfy the desired performance criteria such as **gain margin**, **phase margin**, and **steady-state error**.
- We will focus on designing the PID family controllers via Bode plot.
  - Proportional Controller**
  - PI Controller**
  - PD Controller**

$$G_c(s) = K_p$$

$$G_c(s) = K_p \left( 1 + \frac{1}{T_i s} \right)$$

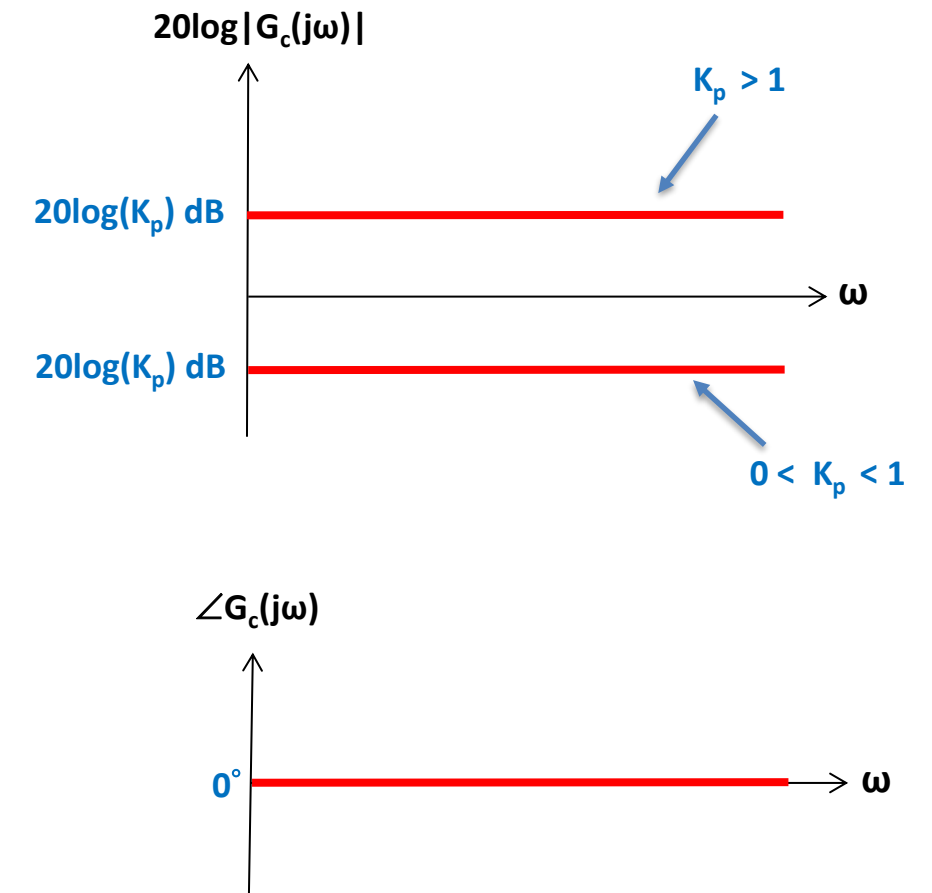
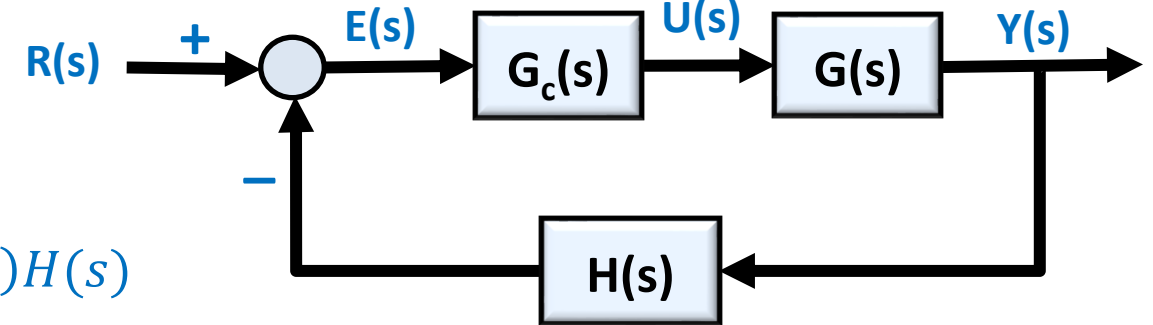
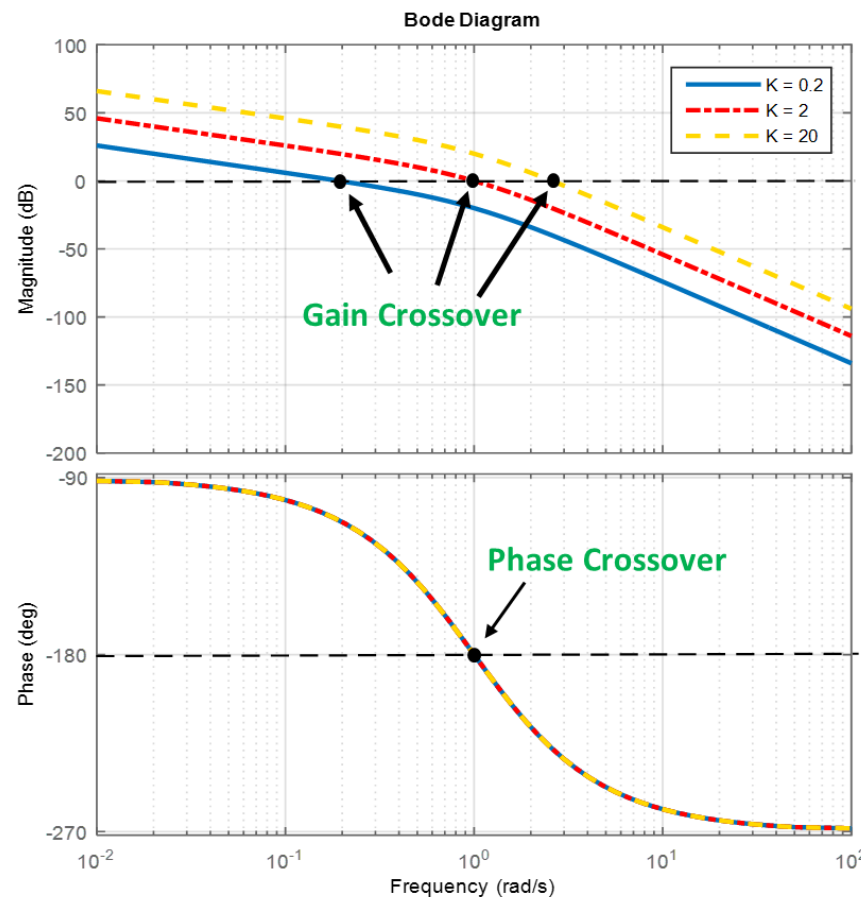
$$G_c(s) = K_p \left( 1 + \frac{T_d s}{\frac{T_d}{\beta} s + 1} \right)$$

# Proportional Controller

- The frequency response function of proportional controller

$$G_c(s) = K_p \rightarrow G_c(j\omega) = K_p$$

- Effect of a proportional controller on the Bode plot of the open-loop system  $G_c(s)G(s)H(s)$ 
  - Shifts the Bode magnitude graph up or down
  - Does not affect the Bode phase graph



# Proportional Controller Design

## Example 1

Consider the following fourth-order system. Determine the  $K_p$  value so that the phase margin is at least  $60^\circ$  and the gain margin is at least 15dB.

Desired performance characteristics:  $PM \geq 60^\circ$ ,  $GM \geq 15 \text{ dB}$

**Step 1:** Plot Bode diagram of the open-loop system  $K_p G(s)H(s)$ , and find **PM** and **GM**

- Plot the Bode diagram of open-loop system,  $K_p G(s)H(s)$ , for a convenient small value of the gain,  $K_p = 1$ .

$$K_p G(s)H(s) = \frac{K_p 60(s + 3)}{s(s + 2)(s + 4)(s + 7)}$$

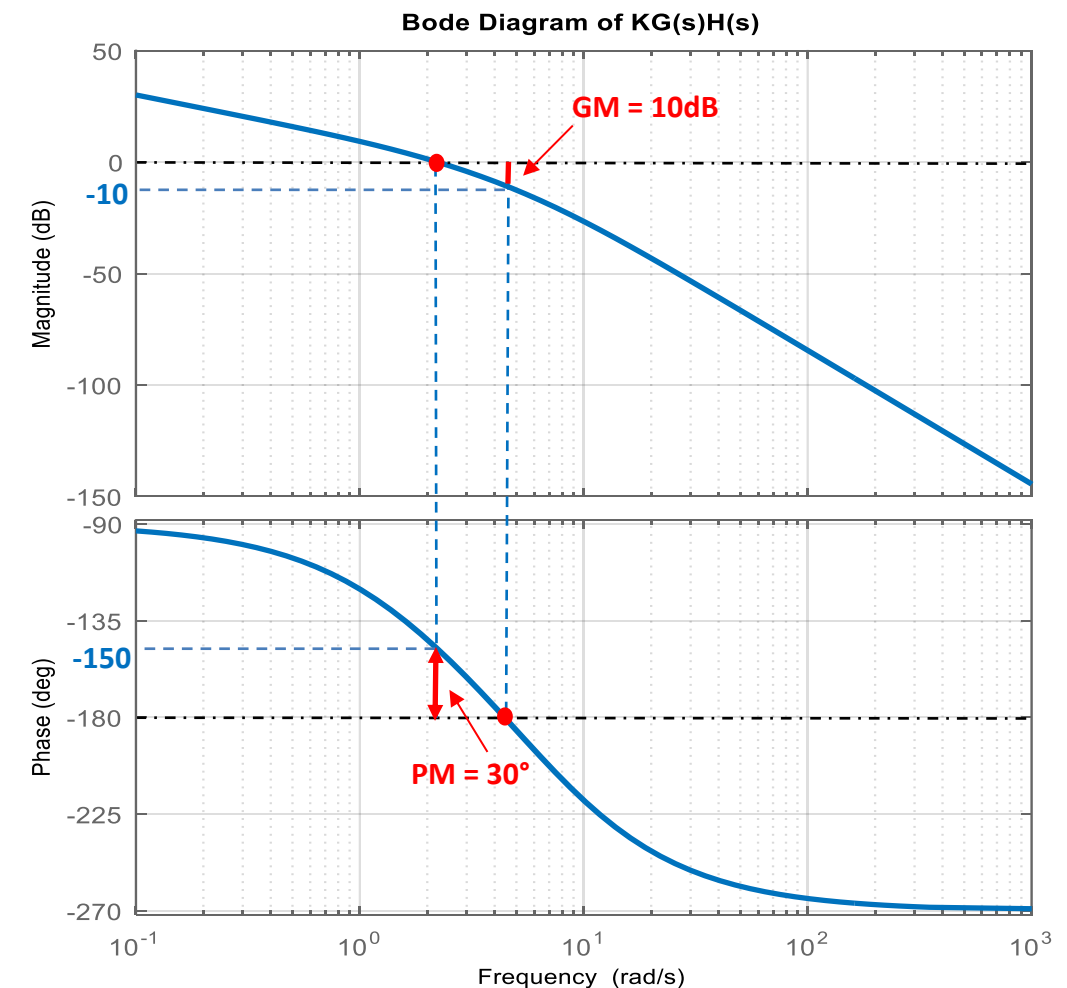
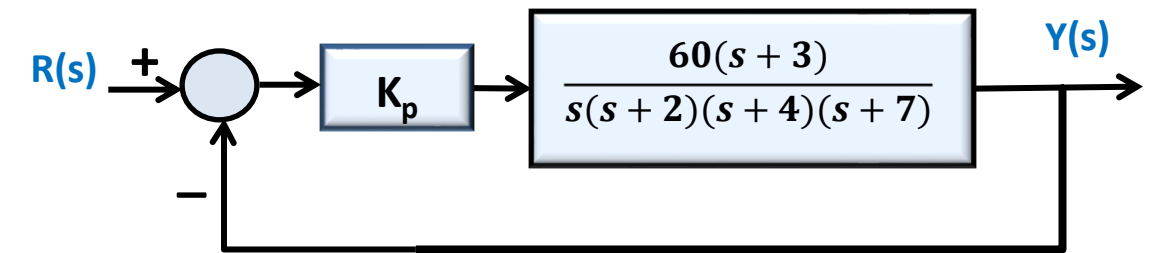
- Check the current **Phase Margin** and **Gain Margin**:

$$GM = 0\text{dB} - (-10\text{dB}) = 10\text{dB}$$

$$PM = 180^\circ + (-150^\circ) = 30^\circ$$

- Current  $GM$  and  $PM$  are not in the desired range.

$$PM = 30^\circ \quad \text{and} \quad GM = 10 \text{ dB}$$



# Proportional Controller Design

## Example 1

Consider the following fourth-order system. Determine the  $K_p$  value so that the phase margin is at least  $60^\circ$  and the gain margin is at least 15dB.

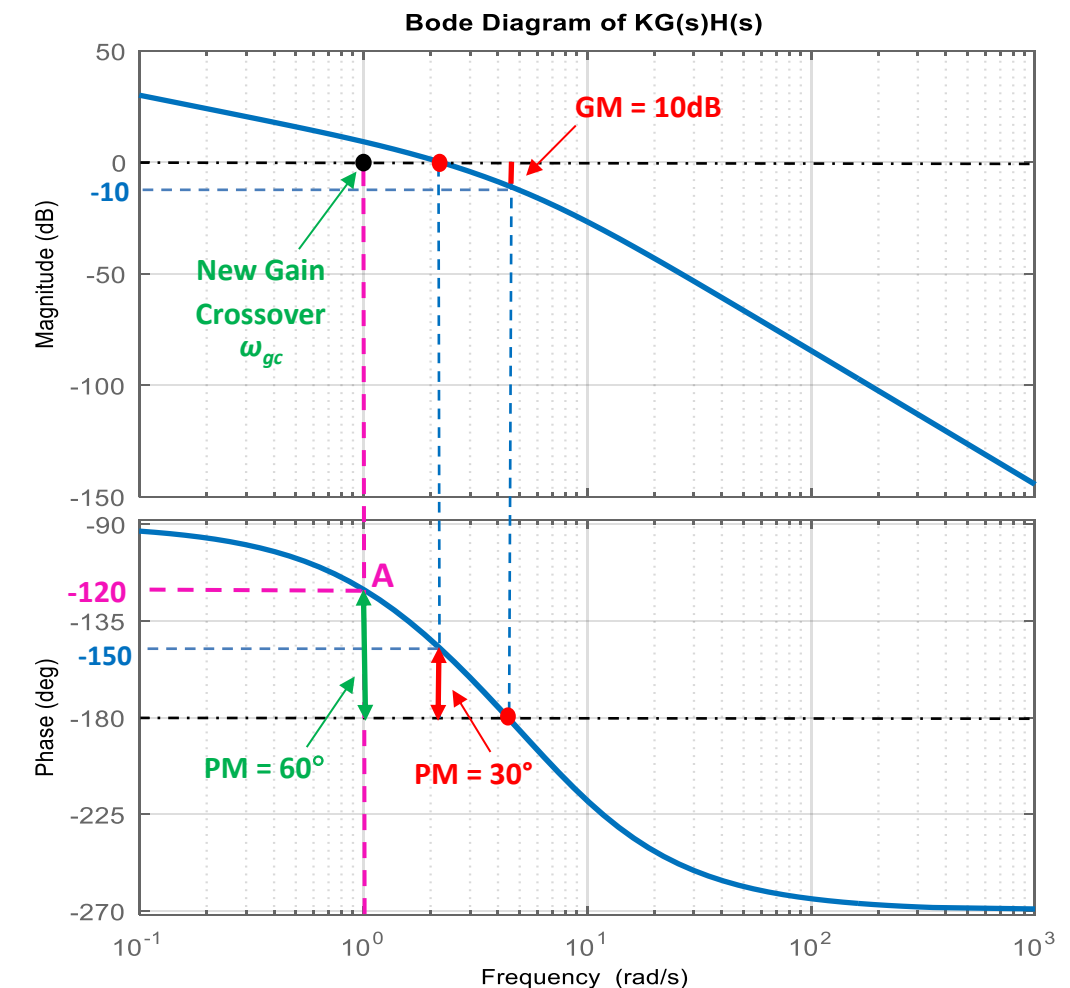
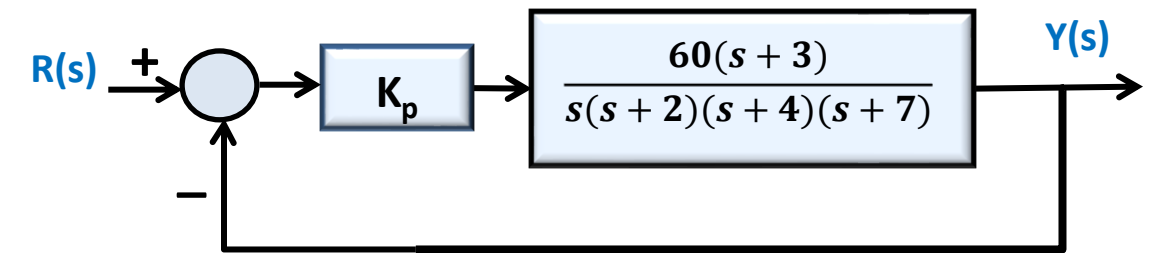
Desired performance characteristics:  $PM \geq 60^\circ$ ,  $GM \geq 15 \text{ dB}$

**Step 2:** Find the point on the **phase plot** to achieve the desired **PM**

$$PM_d = 180^\circ + \varphi \rightarrow \varphi = 60^\circ - 180^\circ = -120^\circ$$

- **Point A** on the Bode diagram shows the location which can give us the  $PM = 60^\circ$
- Find the **New Gain Crossover Frequency** at the desired PM:
 

$PM = 60^\circ \rightarrow \omega_g = 0.986 \text{ rad/s}$
- Therefore, we must **decrease the current gain  $K_p$**  to **shift down the magnitude** plot to achieve the desired gain crossover frequency and the desired  $PM$ .
- Note that by changing the gain value  $K_p$ , **only the magnitude plot** can be modified, and the phase plot is **not** affected.



# Proportional Controller Design

## Example 1

Consider the following fourth-order system. Determine the  $K_p$  value so that the phase margin is at least  $60^\circ$  and the gain margin is at least 15dB.

Desired performance characteristics:  $PM \geq 60^\circ$ ,  $GM \geq 15 \text{ dB}$

**Step 3:** Find the gain value at the new gain crossover frequency

$$\omega_{gc} = 0.986 \text{ rad/s}$$

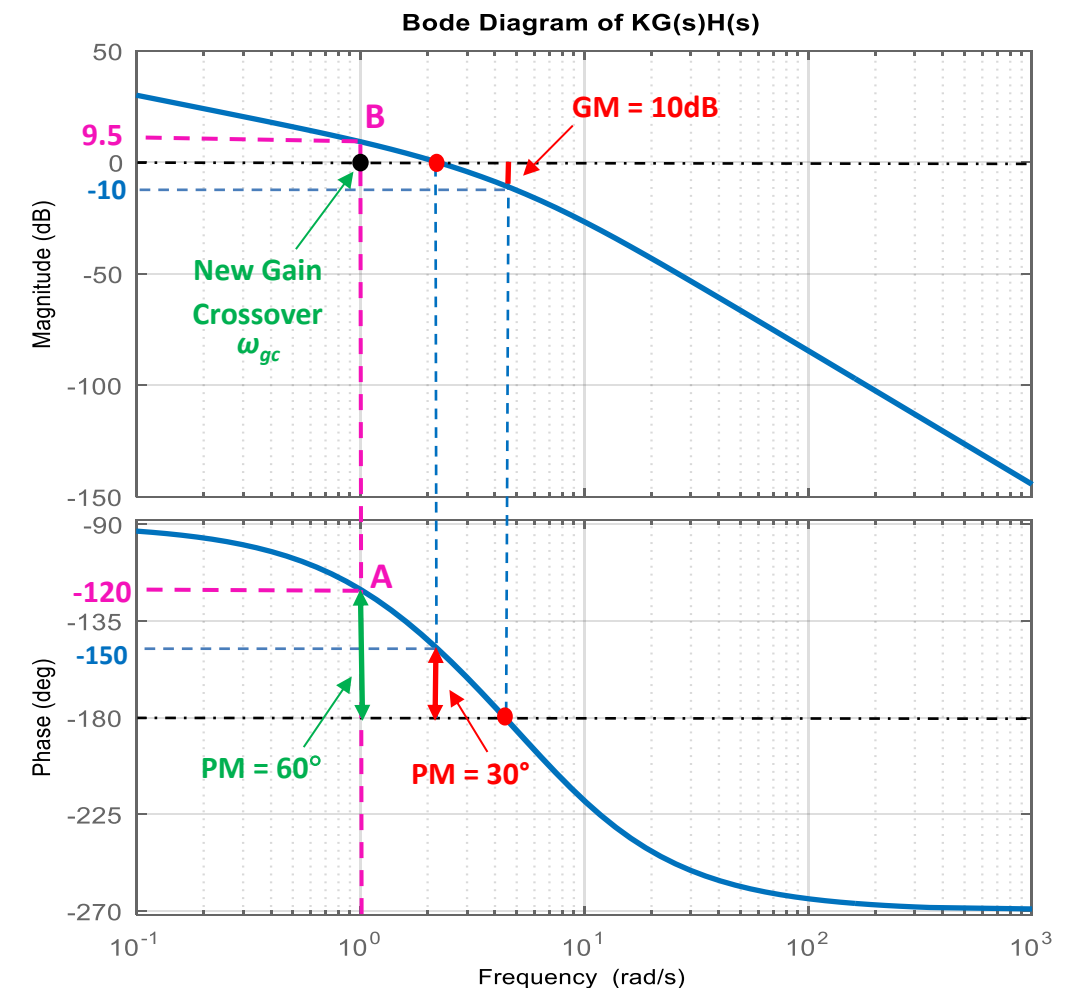
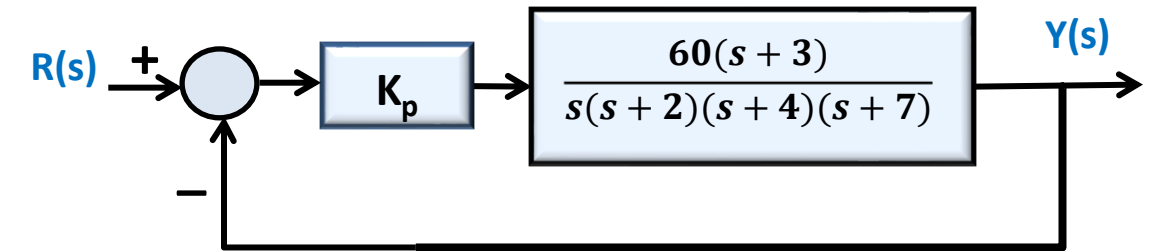
At point B  $\rightarrow 20\log |K_p G(s)H(s)| = 9.5\text{dB}$

We want to change the gain  $K_p$  to make the magnitude at point B equal to  $0\text{dB}$

Therefore, the new gain value must contribute the gain of  $-9.5\text{dB}$

$$20\log |K_{new}| = -9.5\text{dB} \rightarrow K_{new} = 10^{-9.5/20} = 0.335$$

**New Gain**



# Proportional Controller Design

## Example 1

Consider the following fourth-order system. Determine the  $K_p$  value so that the phase margin is at least  $60^\circ$  and the gain margin is at least 15dB.

Desired performance characteristics:

$$PM \geq 60^\circ, \quad GM \geq 15 \text{ dB}$$

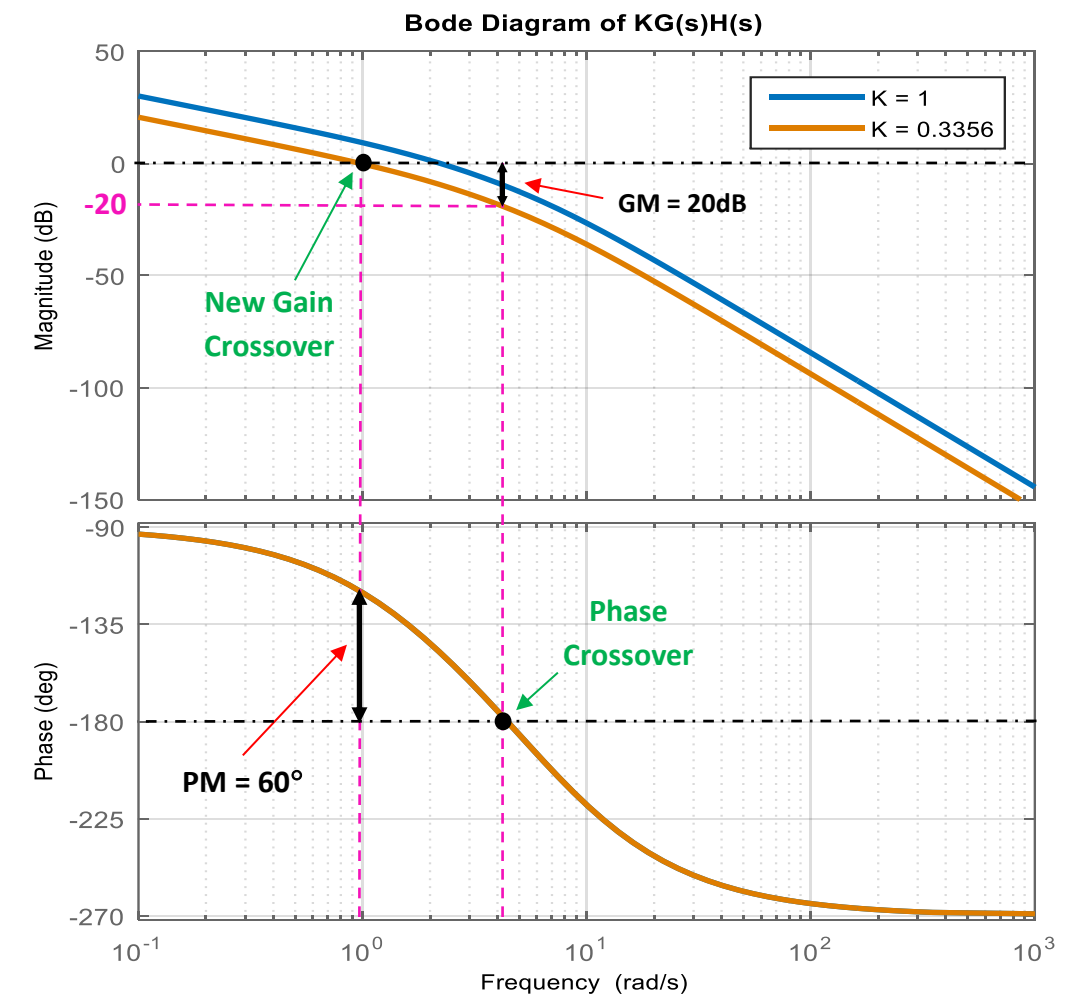
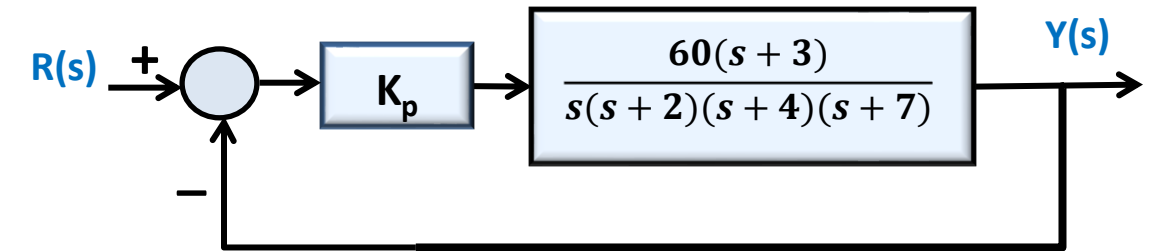
- We can plot the Bode diagram with the new gain to verify the result.

$$K_{\text{new}} = 0.335$$

- The gain margin and phase margin satisfy the required criteria

$$PM = 60^\circ$$

$$GM = 20 \text{ dB}$$





# Proportional Controller Design

## Example 1

Consider the following fourth-order system. Determine the  $K_p$  value so that the phase margin is at least  $60^\circ$  and the gain margin is at least 15dB.

Desired performance characteristics:

$$PM \geq 60^\circ, \quad GM \geq 15 \text{ dB}$$

- We can also plot the **unit-step response** of the closed-loop system with  $K_p = 0.335$  to check the performance of the system in time-domain.

$$K_{new} = 0.335$$

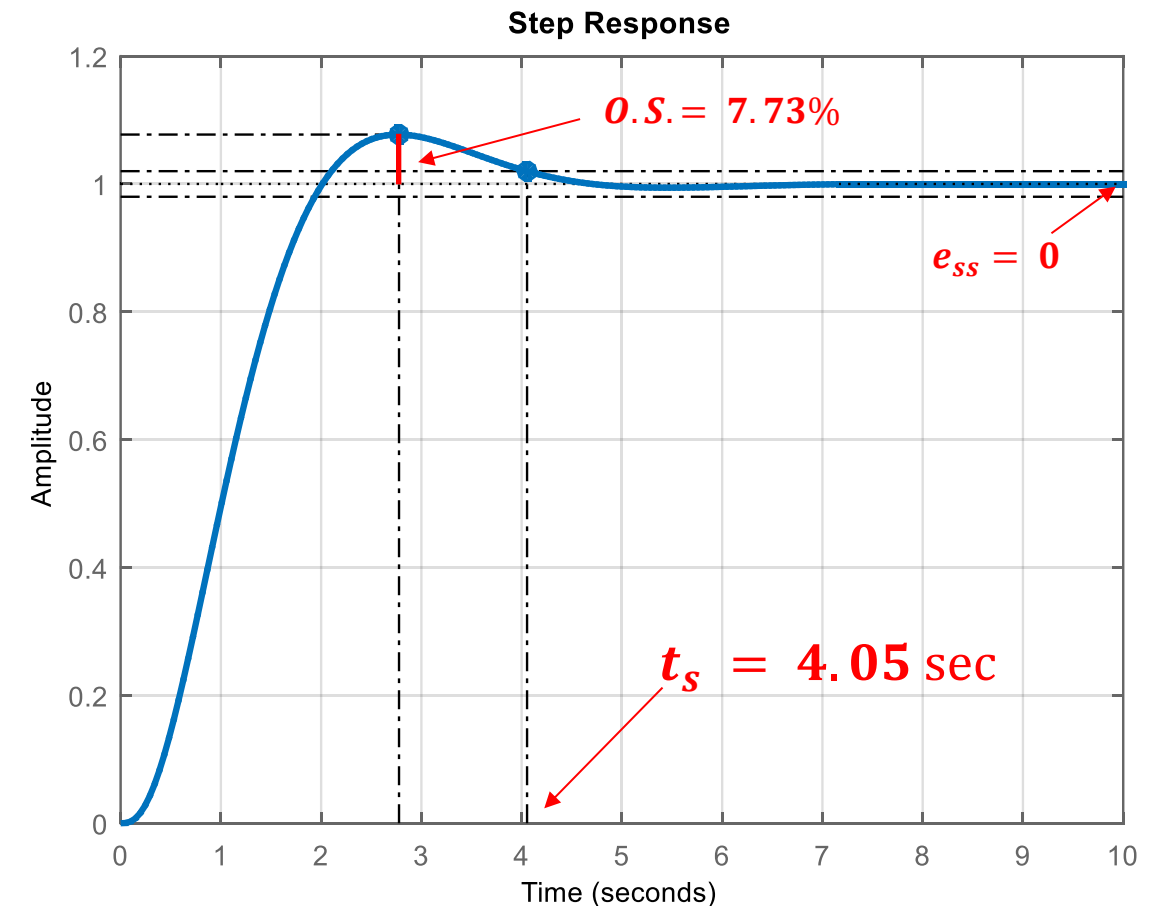
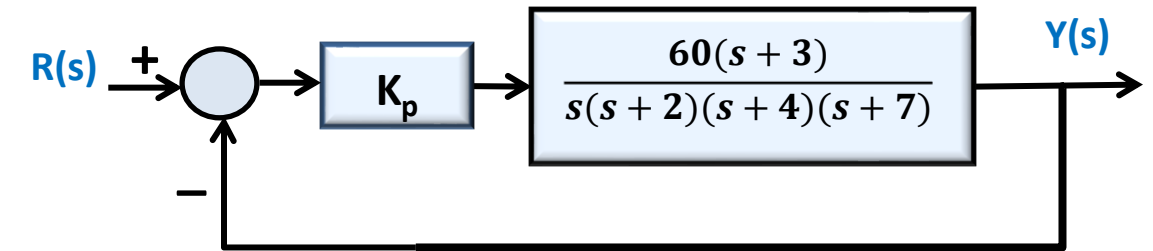
$$PM = 60^\circ$$

$$GM = 20 \text{ dB}$$

$$O.S. = 7.73\%$$

$$t_s = 4.05 \text{ sec}$$

$$e_{ss} = 0$$



# PI Controller Design via Bode Diagram

# PI Controller

- The frequency response function of PI controller

$$G_c(s) = K_P \left( 1 + \frac{1}{T_i s} \right) = K_p \left( \frac{T_i s + 1}{T_i s} \right) = K_p \left( \frac{1}{T_i s} \right) (T_i s + 1)$$

$$G_c(j\omega) = K_p \left( \frac{1}{jT_i \omega} \right) (jT_i \omega + 1)$$

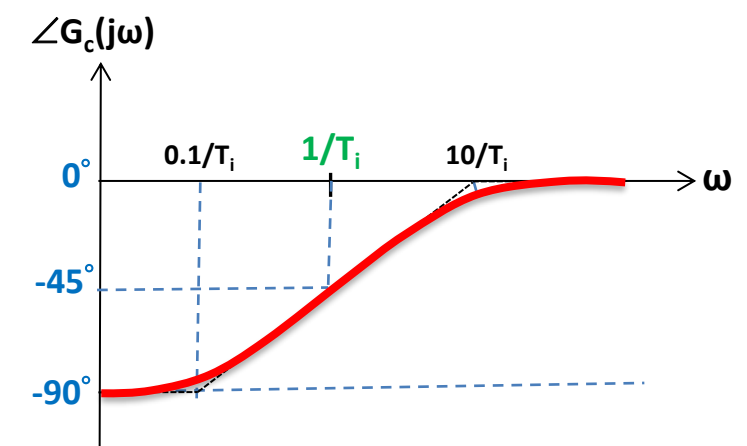
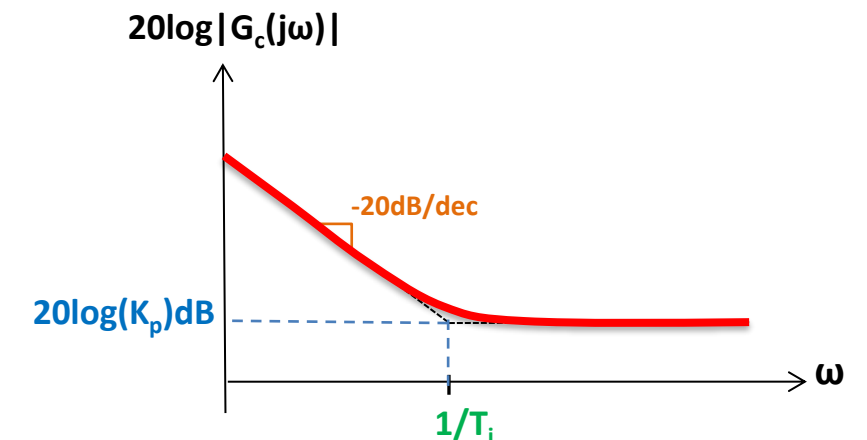
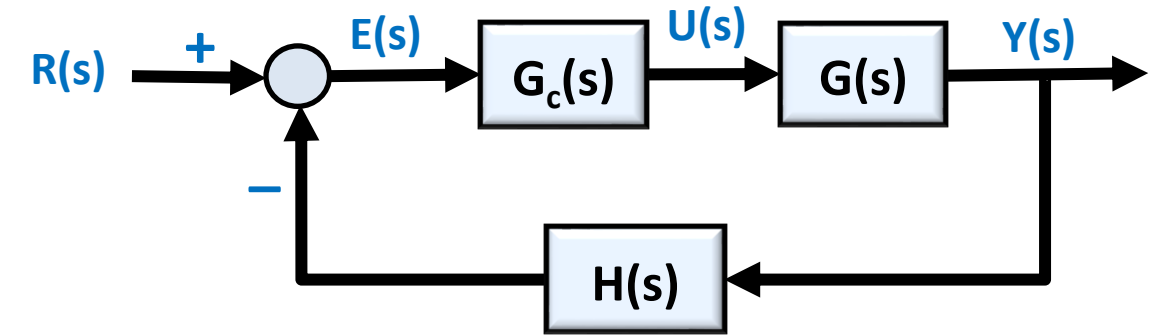
- The corner frequencies of single zero

$$\omega_z = \frac{1}{T_i}$$

- The low-frequency gain and the high-frequency gain

$$G_c(j0) = \infty \quad \text{and} \quad G_c(j\infty) = K_p$$

- Effect of a PI controller on the Bode plot of the open-loop system  $G_c(s)G(s)H(s)$ 
  - Eliminates steady-state error by applying infinite gain at low frequencies
  - Decreases the bandwidth by shifting the gain crossover frequency to the left, which makes slower transient response
  - Negative phase angle contribution (may increase phase lag)
- Negative phase must be kept at low frequencies far enough from the gain crossover frequency to not effect the  $PM$ .



# PI Controller Design

## □ PI Controller Design Steps via Bode Diagram

$$G_c(s) = K_P \left( 1 + \frac{1}{T_i s} \right)$$

**Step 1:** Plot Bode diagram of the open-loop system  $KG(s)H(s)$ , and find  $PM$  and  $GM$

**Step 2:** Find the required phase margin,  $PM_{req}$  →  $PM_{req} = PM_d + \alpha^\circ$

Safety factor ( $5^\circ \leq \alpha \leq 15^\circ$ )

**Step 3:** Determine the frequency on the Bode diagram to achieve the required phase margin  $PM_{req}$ . Select this frequency as the new gain crossover frequency,  $\omega_{gc}$

**Step 4:** Find the corner frequency of zero →  $\omega_z = 0.1\omega_{gc}$

**Step 5:** Select the integral time constant  $T_i$  →  $T_i = \frac{1}{\omega_z}$

**Step 6:** Select the proportional gain  $K_p$  to bring down the magnitude plot to  $0dB$  at the new crossover frequency  $\omega_{gc}$ .

# PI Controller Design

## Example 2

Consider the following third-order system

It is desired to design a PI controller to achieve the following performance characteristics

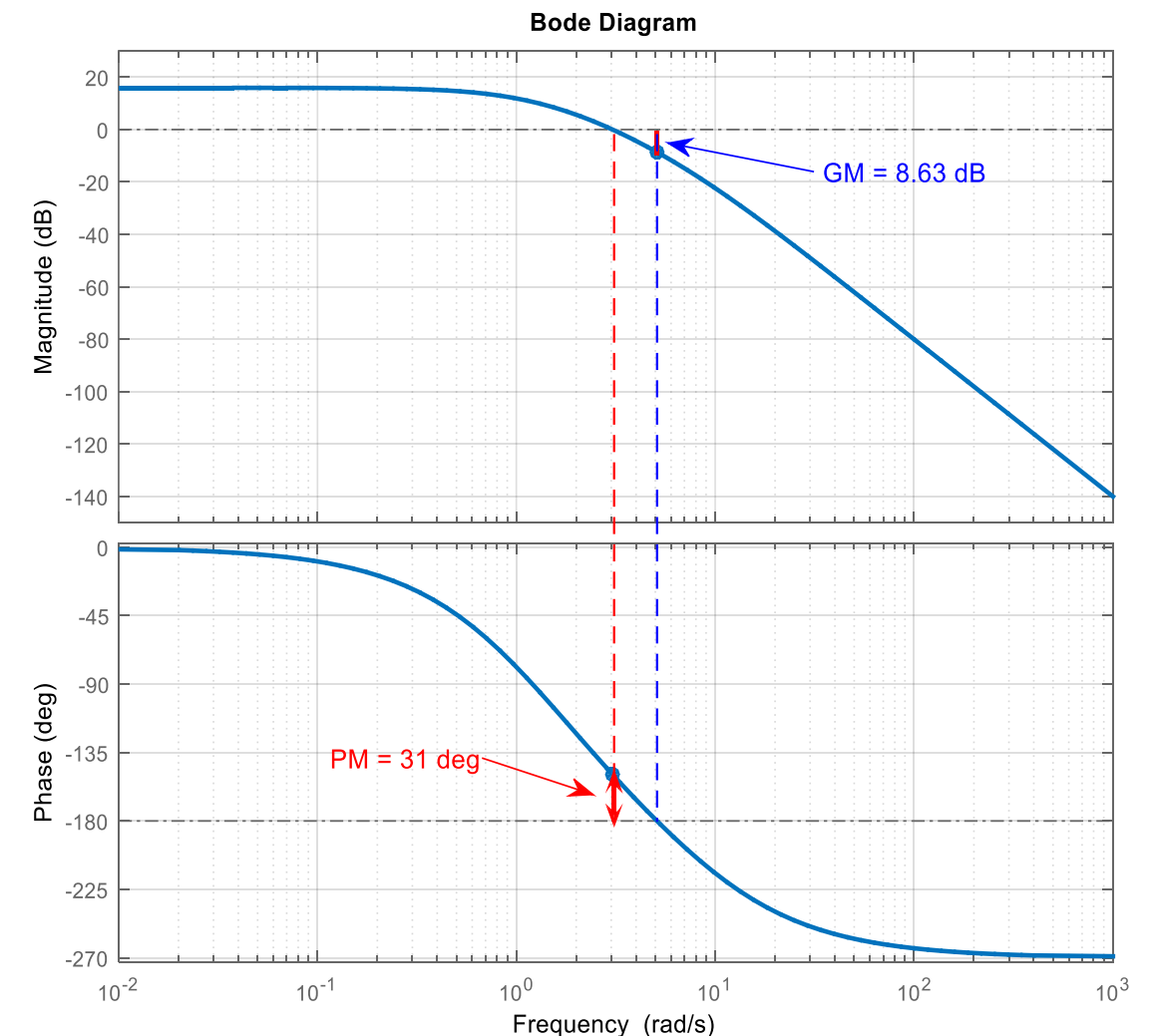
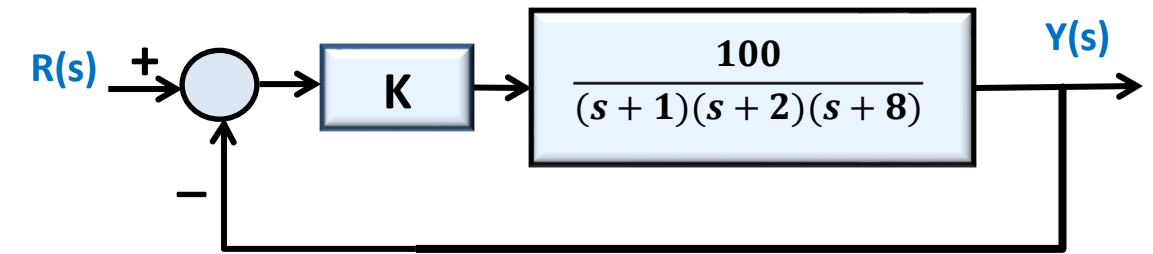
$$e_{ss} = 0, PM > 70^\circ, GM > 10dB$$

**Step 1:** Plot Bode diagram of the open-loop system  $KG(s)H(s)$ , and find  $PM$  and  $GM$

From the Bode diagram of the uncompensated system with  $K = 1$ , we have the following relative stability margins

$$PM = 31^\circ \quad \text{and} \quad GM = 8.63dB$$

Current  $PM$  and  $GM$  are not in the desired range.



# PI Controller Design

## Example 2

Consider the following third-order system

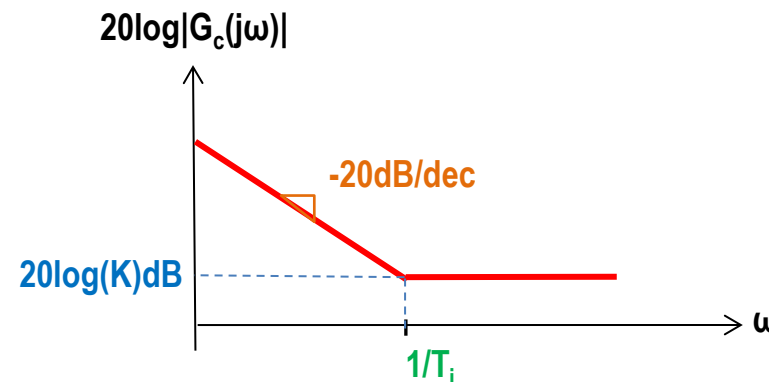
It is desired to design a PI controller to achieve the following performance characteristics

$$e_{ss} = 0, PM > 70^\circ, GM > 10dB$$

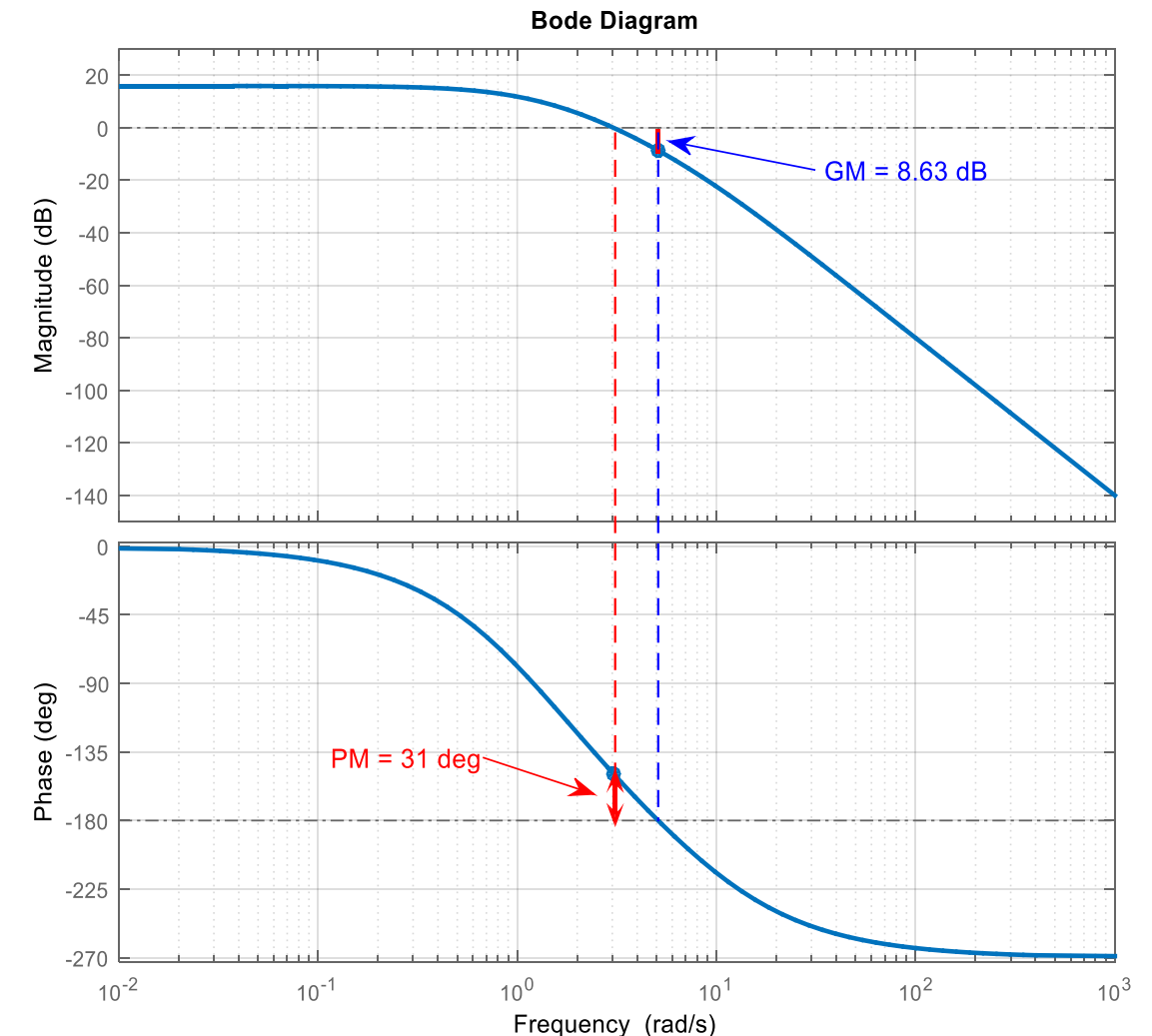
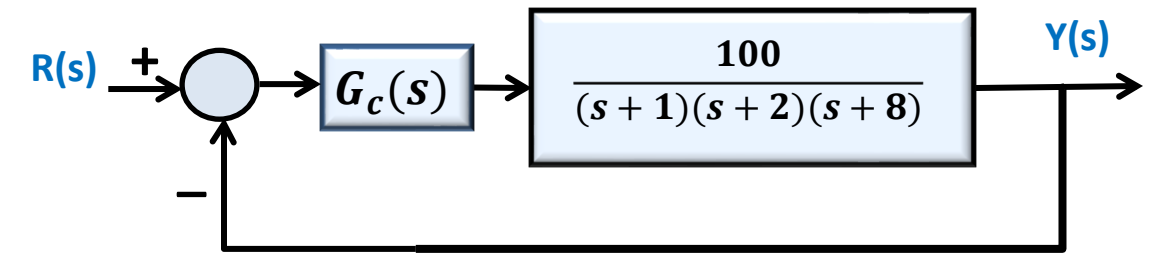
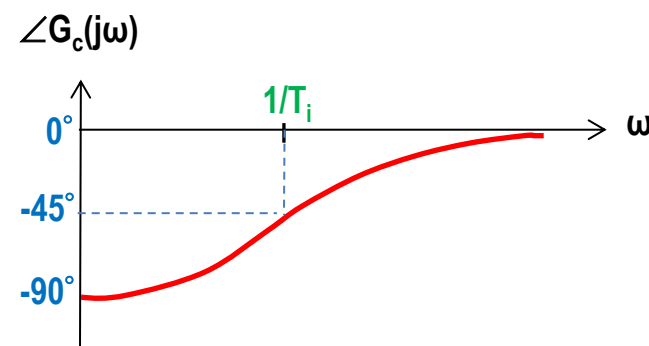
Next, design a PI Controller to achieve the desired  $PM$ .

$$G_c(s) = K_p \left( 1 + \frac{1}{T_i s} \right)$$

- PI controller modifies the both **magnitude** and **phase** plots by shifting the gain crossover to the **left**.



- To avoid the effect of **negative phase**, zero of the PI controller must be selected **one decade below** the new gain cross over frequency



# PI Controller Design

## Example 2

Consider the following third-order system

It is desired to design a PI controller to achieve the following performance characteristics

$$e_{ss} = 0, PM > 70^\circ, GM > 10dB$$

**Step 2:** Find the required phase margin,  $PM_{req}$

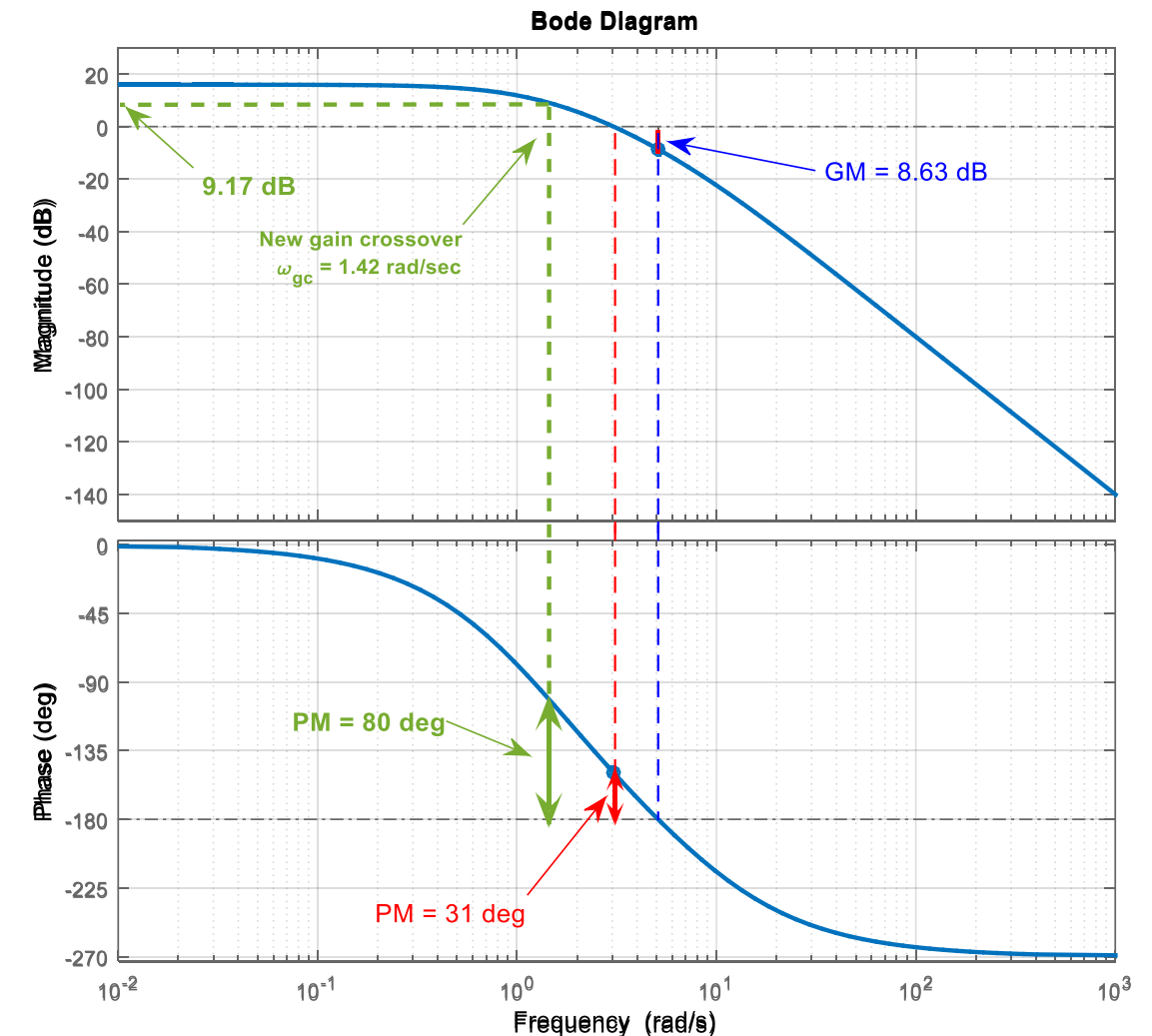
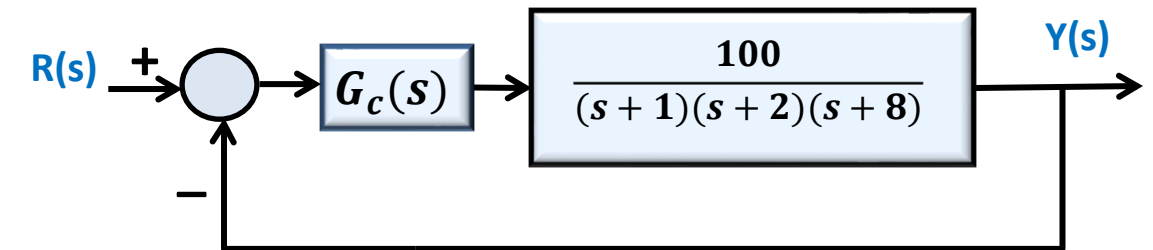
$$PM_{req} = PM_d + \alpha^\circ = 70^\circ + 10^\circ \rightarrow PM_{req} = 80^\circ$$

- A  $10^\circ$  safety factor is added to compensate the shifting in the gain crossover frequency

**Step 3:** Determine the frequency on the Bode diagram to achieve the required phase margin  $PM_{req}$ . Select this frequency as the new gain crossover frequency,  $\omega_{gc}$

$$PM_{req} = 80^\circ \rightarrow \omega_{gc} = 1.42 \text{ rad/s}$$

New Gain Crossover Frequency



# PI Controller Design

## Example 2

Consider the following third-order system

It is desired to design a PI controller to achieve the following performance characteristics

$$e_{ss} = 0, PM > 70^\circ, GM > 10dB$$

**Step 4:** Find the corner frequency of zero

$$\omega_z = 0.1\omega_{gc} = 0.142 \text{ rad/s}$$

**Step 5:** Select the integral time constant  $T_i$

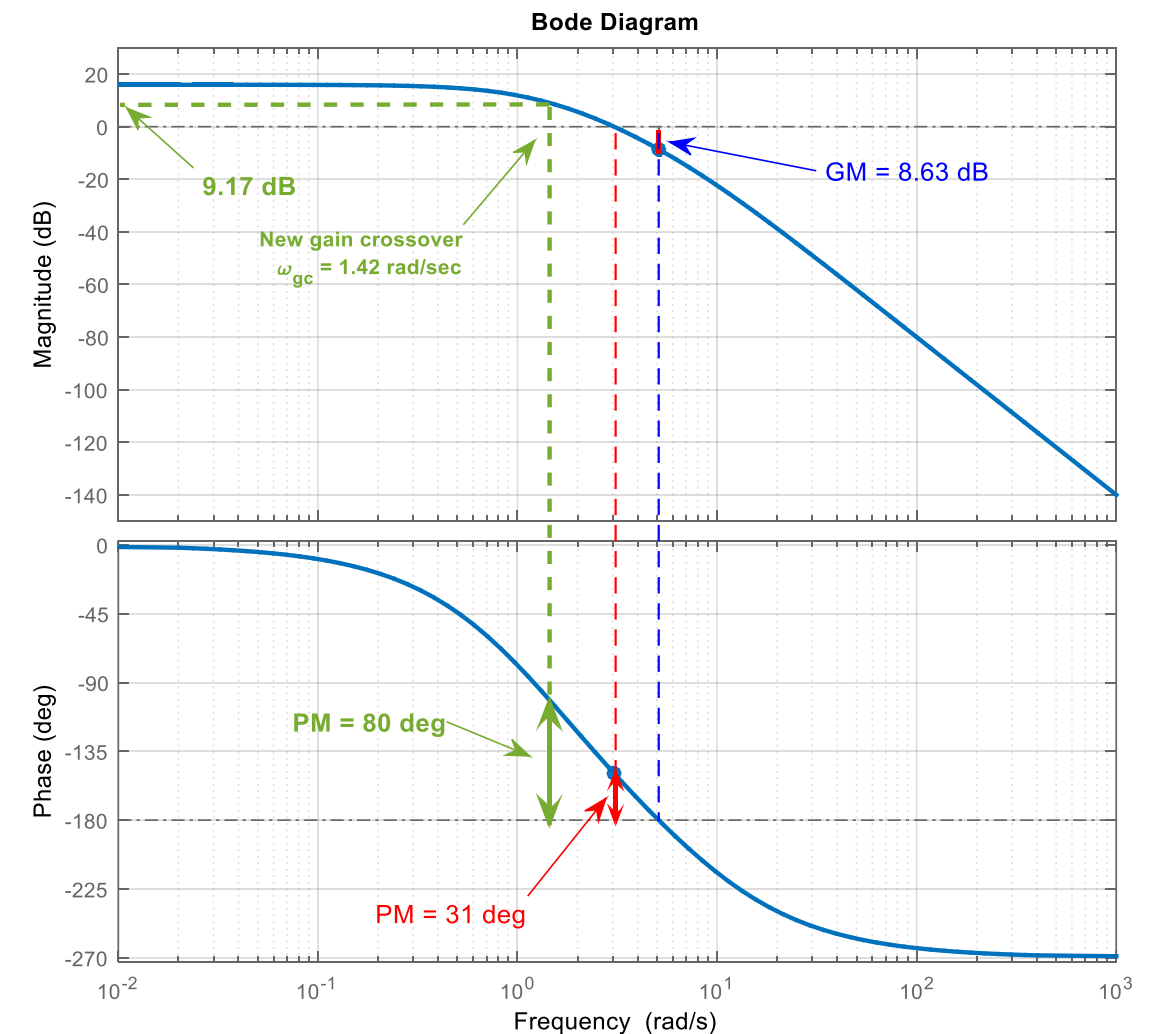
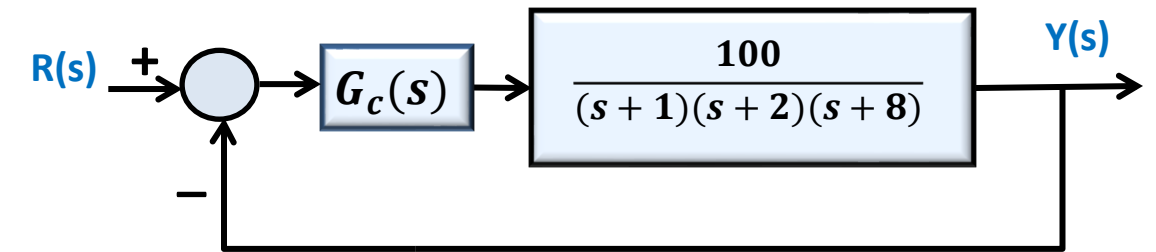
$$T_i = \frac{1}{\omega_z} \rightarrow T_i = 7.04 \text{ sec}$$

**Step 6:** Select the proportional gain  $K_p$  to bring down the magnitude plot to 0dB at the new crossover frequency.

- From the Bode plot the magnitude at the new gain crossover is

$$\omega_{gc} = 1.42 \rightarrow 9.17 \text{ dB}$$

$$20\log(K_p) = -9.17\text{dB} \rightarrow K_p = 10^{-9.17/20} = 0.35$$





# PI Controller Design

## Example 2

Consider the following third-order system

It is desired to design a PI controller to achieve the following performance characteristics

$$e_{ss} = 0, PM > 70^\circ, GM > 10dB$$

Designed PI Controller

$$G_c(s) = 0.35 \left( 1 + \frac{1}{7.04s} \right)$$

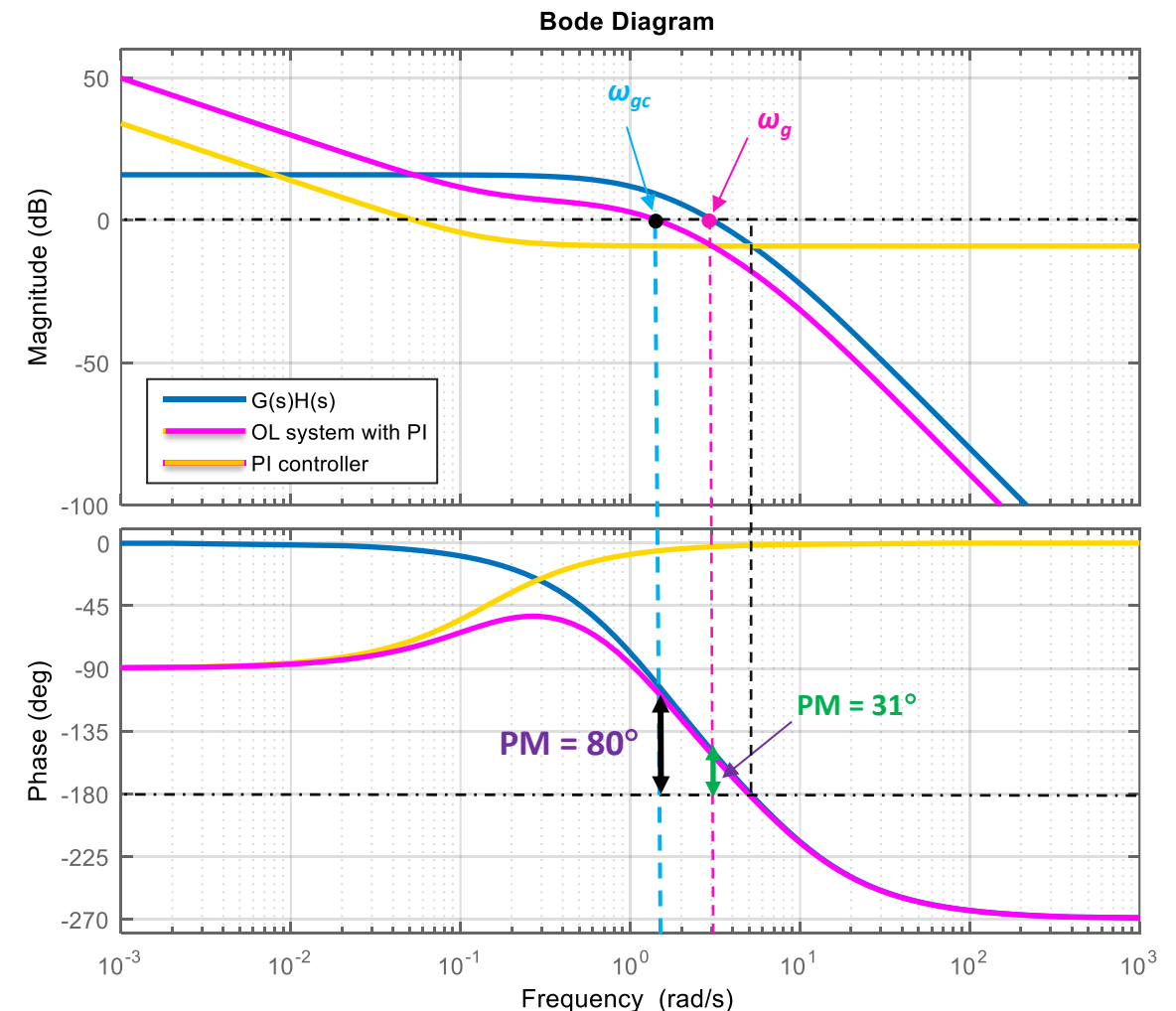
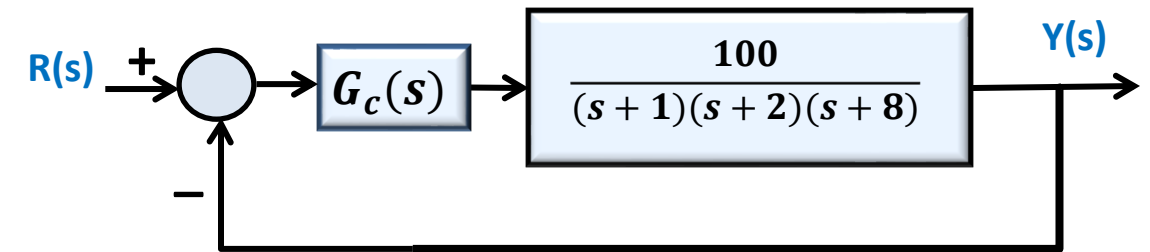
- Graph shows Bode plot of the following systems

$$G(s)H(s) = \frac{100}{(s+1)(s+2)(s+8)}$$

$$G_c(s)G(s)H(s) = 0.35 \left( 1 + \frac{1}{7.04s} \right) \frac{100}{(s+1)(s+2)(s+8)}$$

$$G_c(s) = 0.35 \left( 1 + \frac{1}{7.04s} \right)$$

- The PI controller decreases the bandwidth of the system that results in slower transient response.
- The  $\omega_z$  must be selected far enough from the new gain crossover frequency  $\omega_{gc}$  to not effect the designed phase margin.



# PD Controller Design via Bode Diagram

# Ideal PD Controller

- The frequency response function of PD controller

$$G_c(s) = K_p(1 + T_d s) \rightarrow G_c(j\omega) = K_p(1 + jT_d \omega)$$

- The corner frequency of single zero

$$\omega_z = \frac{1}{T_d}$$

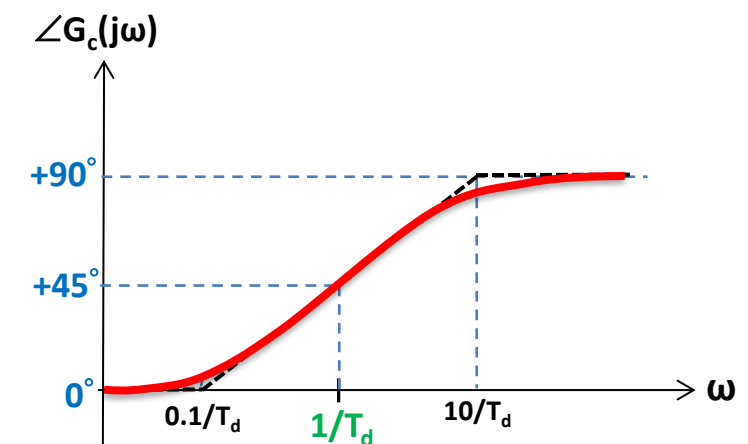
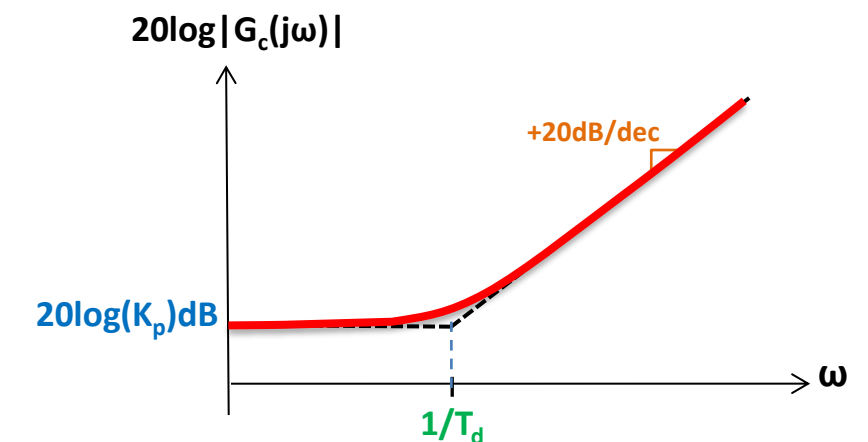
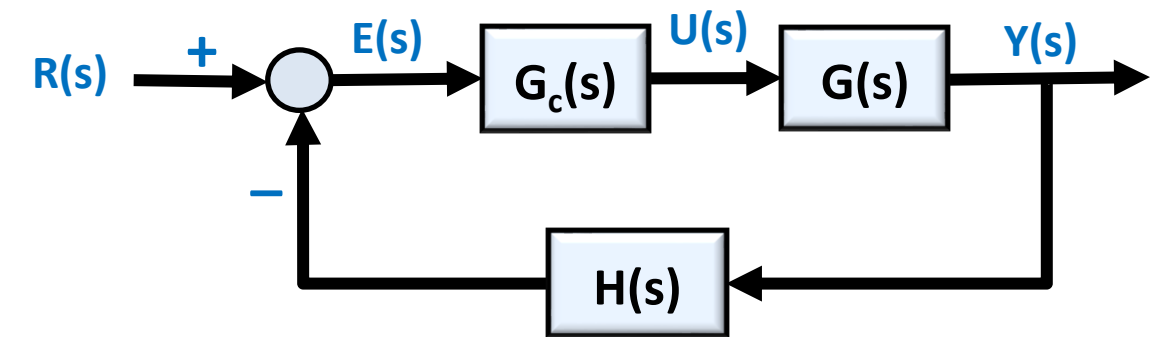
- The low-frequency gain and the high-frequency gain

$$G_c(j0) = K_p \quad \text{and} \quad G_c(j\infty) = \infty$$

- Effect of a PD controller on the Bode plot of the open-loop system  $G_c(s)G(s)H(s)$

- Increases the bandwidth by shifting the gain crossover frequency to the right, which makes faster transient response
- Positive phase angle contribution, which helps to increase the PM, which makes less overshoot and enhances the stability

- Ideal PD controller amplifies the high frequency noise.



# Practical PD Controller

- In practical applications, to avoid of the amplifying high frequency noise, the high frequency gain is limited by adding a **pole** to the controller

$$G_c(s) = K_p \left( 1 + \frac{T_d s}{\frac{\beta}{T_d} s + 1} \right), \quad 10 \leq \beta \leq 100$$

- The **parameter**  $\beta$  determines the distance between the **pole** and the **zero**.
- The **corner frequency** of the **single pole** and the **single zero**

$$\omega_p = \frac{\beta}{T_d} \quad \text{and} \quad \omega_z = \frac{\beta}{(1 + \beta)T_d} \approx \frac{1}{T_d}$$

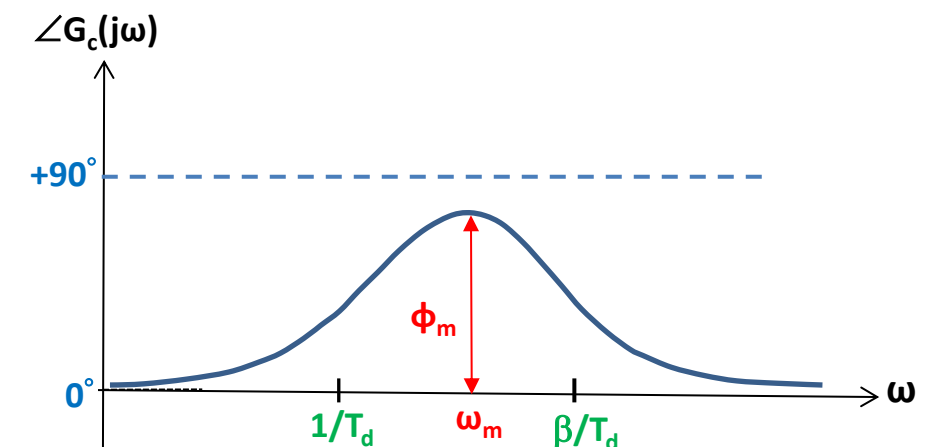
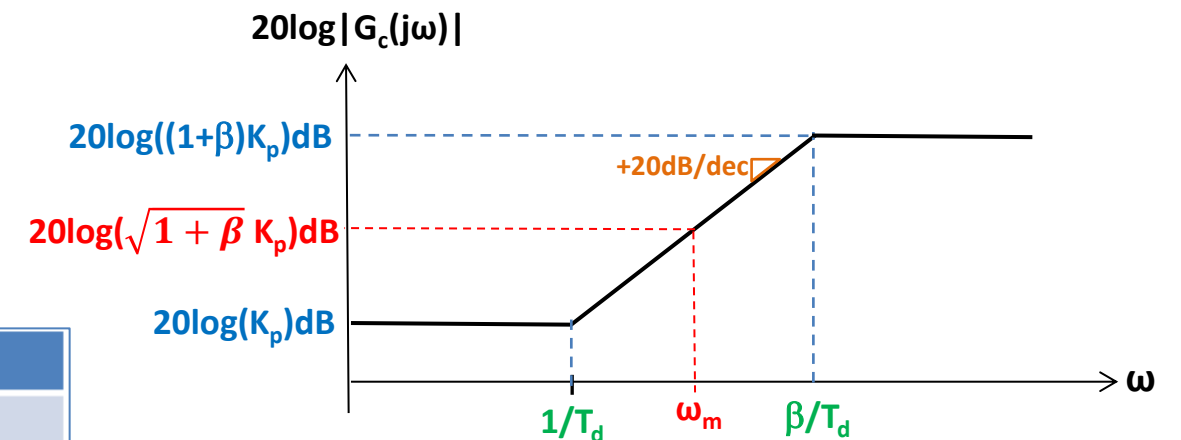
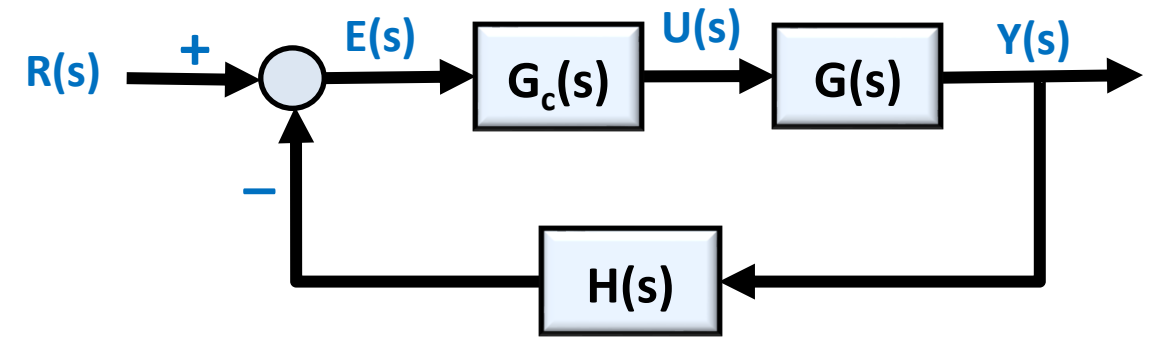
- The **low-frequency gain** and the **high-frequency gain**

$$G_c(j0) = K_p \quad \text{and} \quad G_c(j\infty) = (1 + \beta)K_p$$

- The **maximum phase frequency** and **maximum phase angle**

$$\omega_m = \sqrt{\omega_p \cdot \omega_z} = \frac{\sqrt{\beta}}{T_d} \quad \phi_m = \sin^{-1} \left( \frac{\beta - 1}{\beta + 1} \right)$$

Practical PD controller is also called **phase-lead controller**



$\beta$	$\phi_m$
10	55°
20	65°
30	70°
40	72°
50	74°
60	75°
70	76°
80	77°
90	78°
100	78.5°

# PD Controller Design

## □ PD Controller Design Steps via Bode Diagram

**Step 1:** Determine the proportional gain  $K_p$  to satisfy the desired steady-state error.

**Step 2:** Plot Bode diagram of the open-loop system with proportional gain  $K_p G(s)H(s)$ , and find PM and GM.

**Step 3:** Find the maximum phase lead angle,  $\phi_m$  to be added to the system to achieve the desired PM criteria.

$$\phi_m = PM_d - PM + \alpha^\circ$$

Safety factor ( $5^\circ \leq \alpha \leq 15^\circ$ )

**Step 4:** Select the appropriate factor of  $\beta$  based on the  $\phi_m$  value.

**Step 5:** Find the new gain crossover frequency  $\omega_{gc}$  where the magnitude is  $-20 \log \sqrt{1 + \beta}$

**Step 6:** Assign the maximum phase frequency  $\omega_m$  at the new gain crossover frequency  $\omega_{gc}$  value.

$$\omega_m = \omega_{gc}$$

**Step 7:** Assign the derivative time constant  $T_d$  value as

$$T_d = \frac{\sqrt{\beta}}{\omega_m}$$

$$G_c(s) = K_p \left( 1 + \frac{T_d s}{\frac{T_d}{\beta} s + 1} \right)$$

$$\phi_m = \sin^{-1} \left( \frac{\beta - 1}{\beta + 1} \right)$$

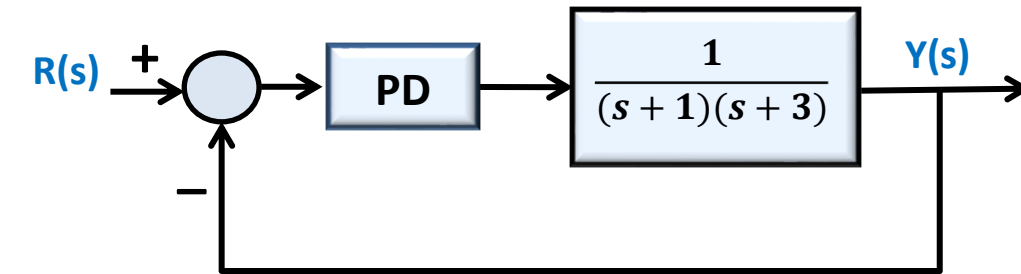
$\beta$	$\phi_m$
10	55°
20	65°
30	70°
40	72°
50	74°
60	75°
70	76°
80	77°
90	78°
100	78.5°

# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$



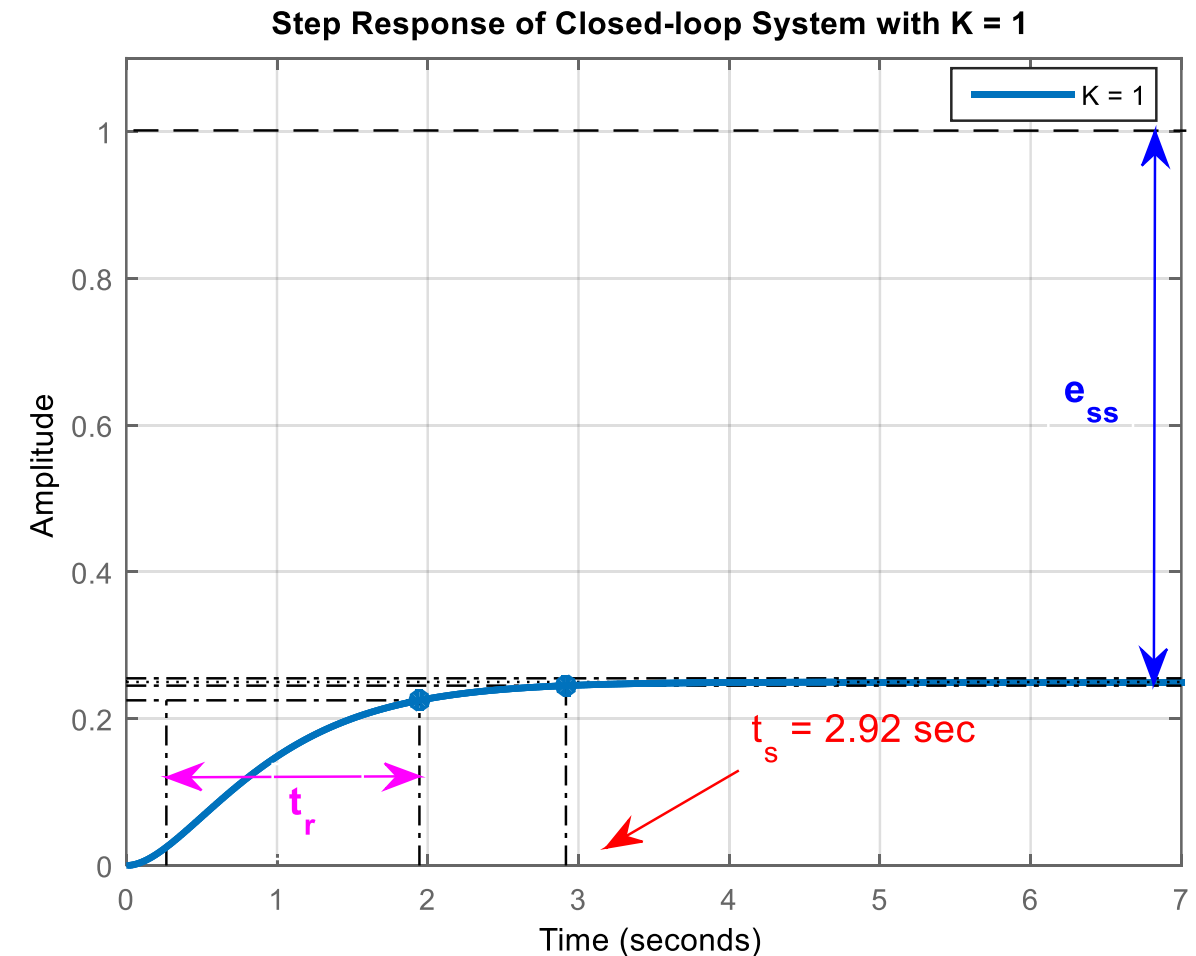
### Predesign Performance Study

- First, check the unit-step response of the closed-loop system with proportional gain of  $K_p = 1$ .
- The results show that  $G(s)$  is a **slow system** with a **large steady-state error**.

$$t_r = 1.68 \text{ sec}$$

$$t_s = 2.92 \text{ sec}$$

$$e_{ss} = 0.75 = 75\%$$

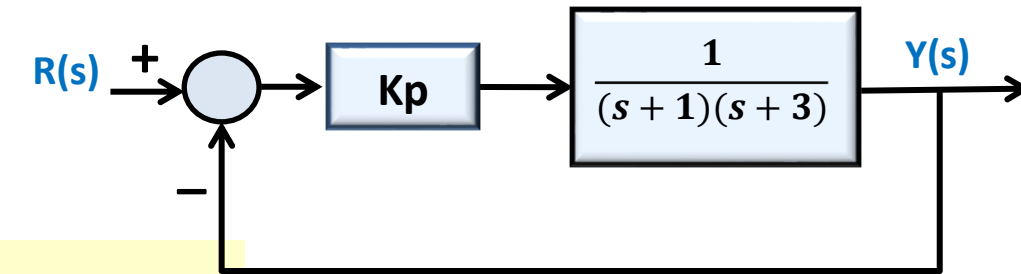


# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$



**Step 1:** Determine the proportional gain  $K_p$  to satisfy the desired steady-state error of unit-step response

- First, find the step-error constant,  $k_p$  based on the desired steady-state error.

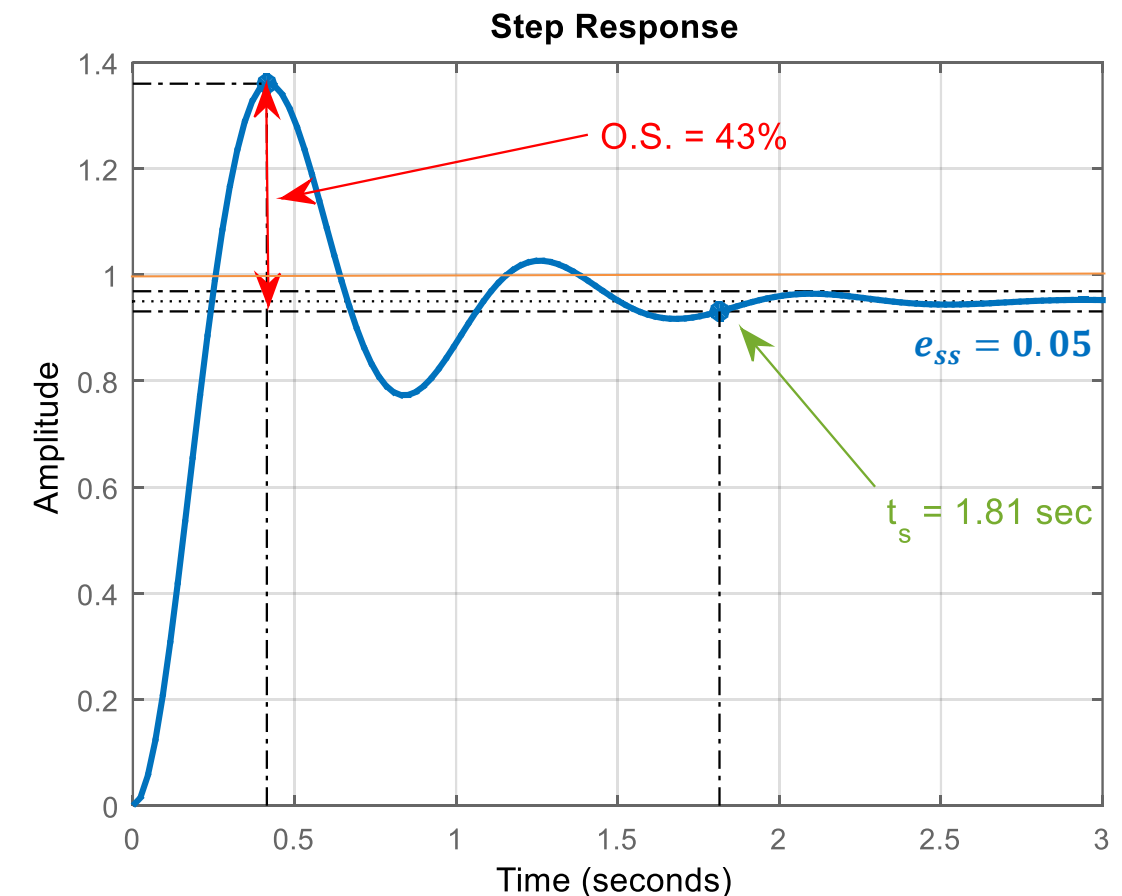
$$e_{ss} = \frac{R}{1 + k_p} \rightarrow 0.05 = \frac{1}{1 + k_p} \rightarrow k_p = 19$$

$$k_p = \lim_{s \rightarrow 0} K_p G(s) H(s) \rightarrow 19 = \lim_{s \rightarrow 0} K_p \left( \frac{1}{(s+1)(s+3)} \right)$$

$$19 = \frac{K_p}{3} \rightarrow K_p = 57$$

$$K_p = 57$$

**Desired Proportional Gain**

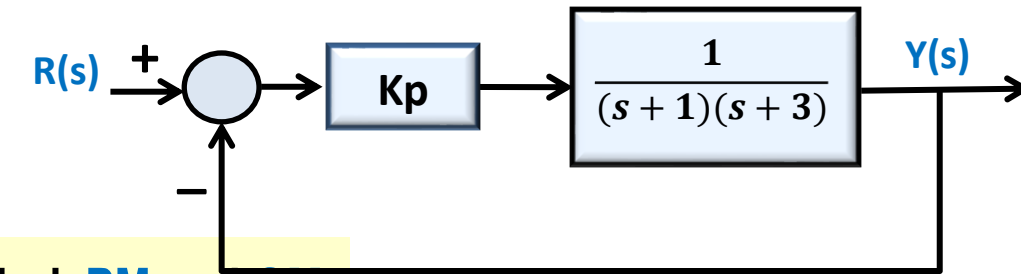


# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$



**Step 2:** Plot Bode diagram of the open-loop system with proportional gain  $K_p G(s)H(s)$ , and find PM and GM

- Open-loop system with desired proportional gain

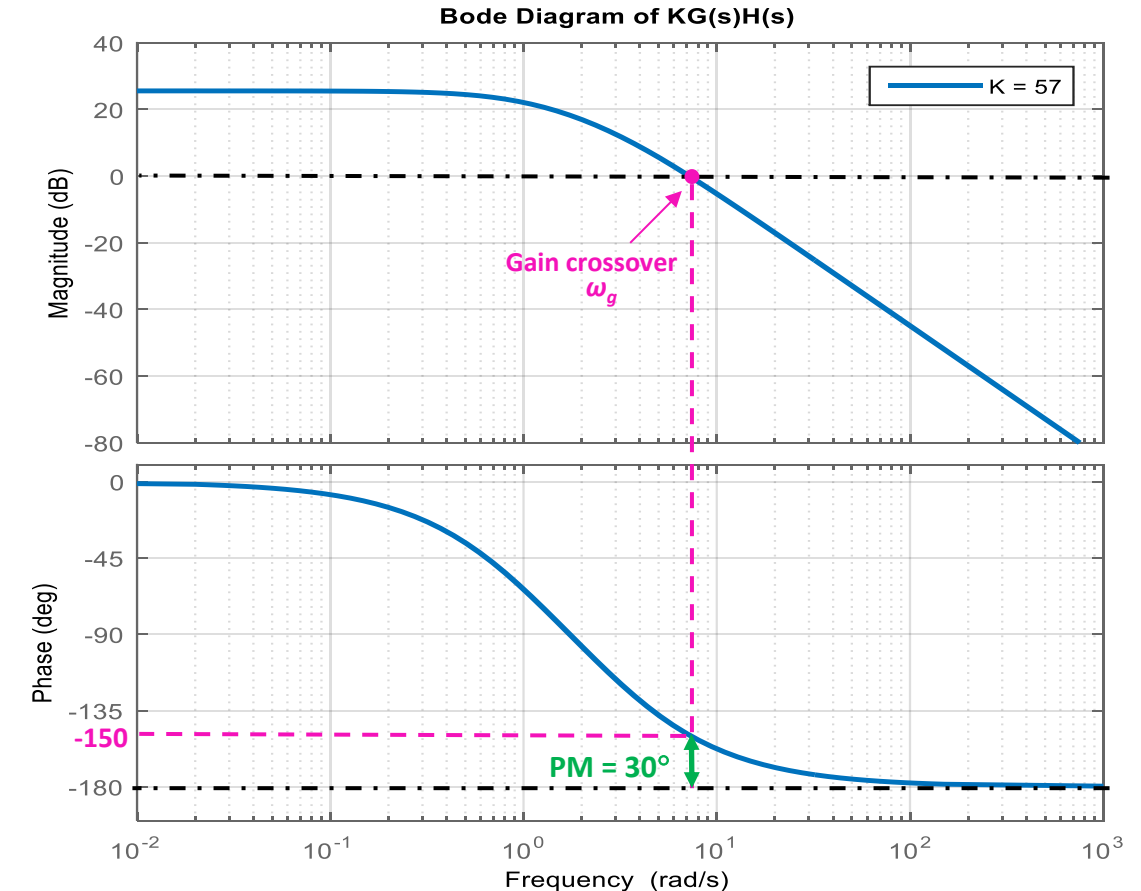
$$K_p G(s)H(s) = \frac{57}{(s+1)(s+3)}$$

- From the Bode diagram the gain crossover frequency, the phase margin and gain margin of the system with  $K_p = 57$

$$\omega_g = 7.22 \text{ rad/sec}$$

$$PM = 30^\circ, GM = +\infty$$

- The desired PM is not satisfied by only proportional gain of  $K_p = 57$ . Therefore; we have to add the derivative part to increase the PM.





# PD Controller Design

## Example 3

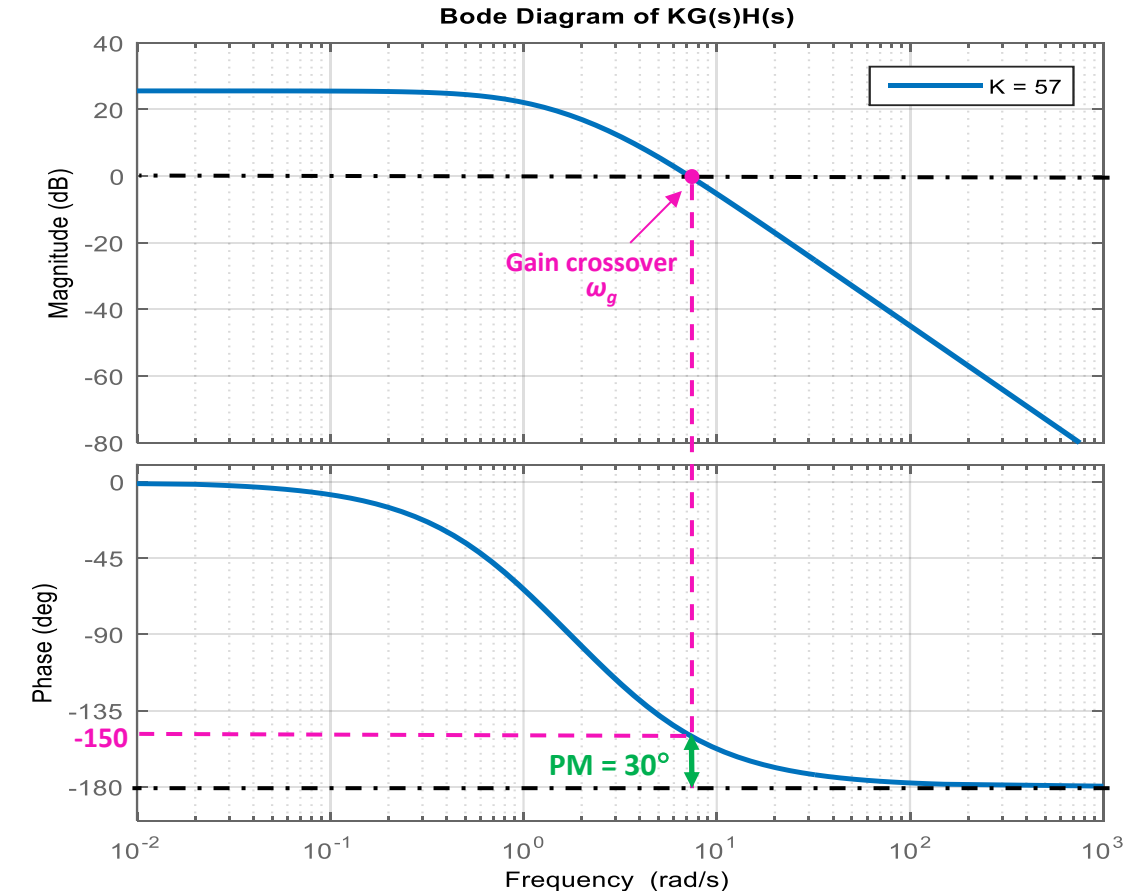
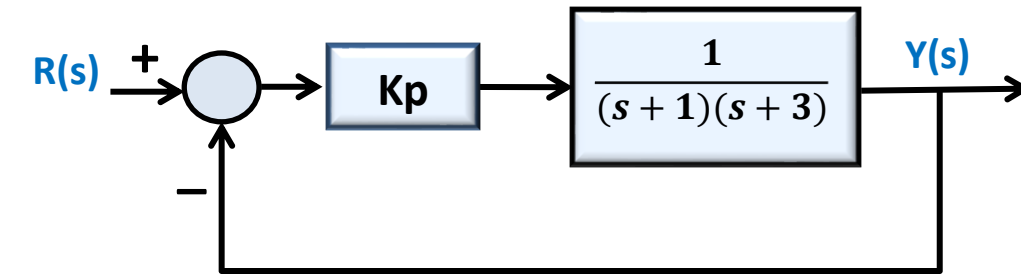
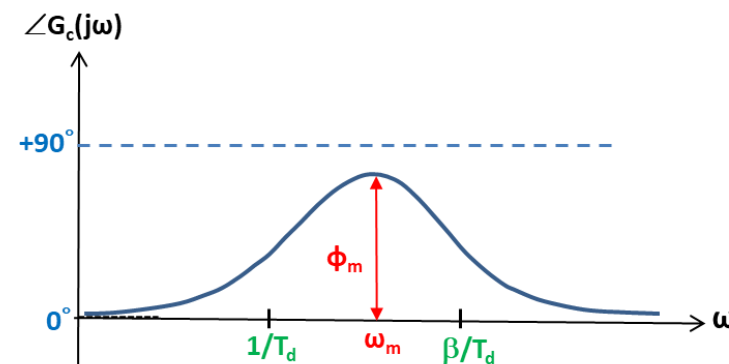
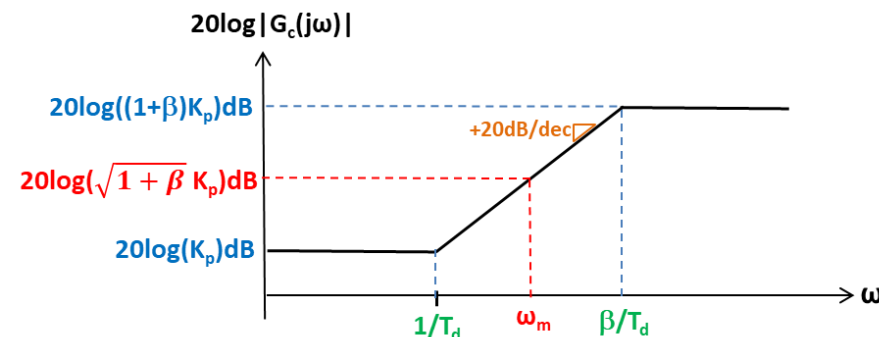
Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$

Next, design a PD Controller to achieve the desired PM.

$$G_c(s) = K_P \left( 1 + \frac{T_d s}{\frac{T_d}{\beta} s + 1} \right)$$

- Adding the lead compensator modifies both magnitude and phase plots.
- The magnitude plot shifts up, thus the gain crossover frequency  $\omega_g$  will be shifted to the right.

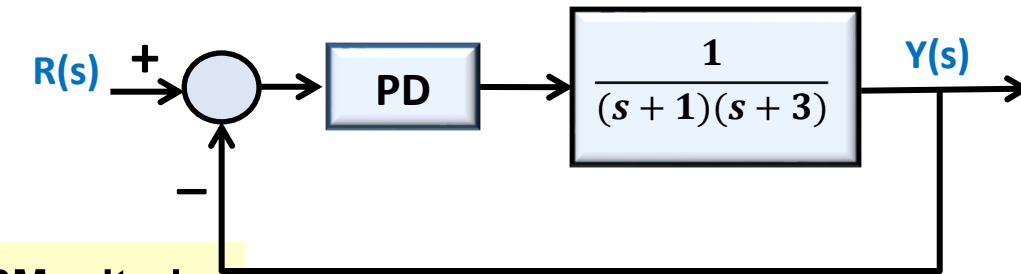


# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$



**Step 3:** Find the maximum phase angle,  $\phi_m$  to be added to the system to achieve the desired PM criteria

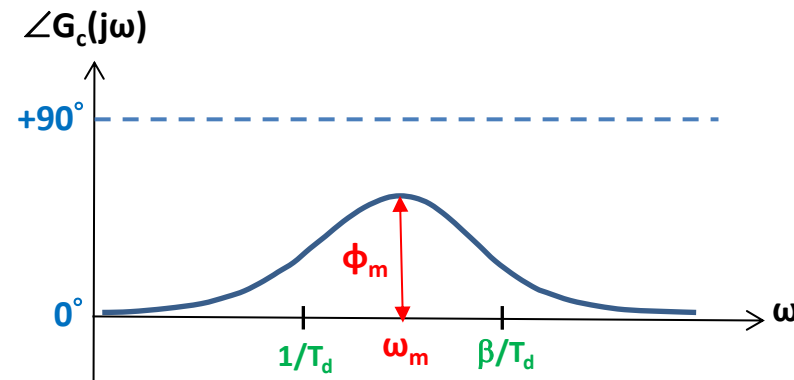
$$\phi_m = PM_d - PM + 10^\circ = 60^\circ - 30^\circ + 10^\circ = 40^\circ$$

$$\phi_m > 40^\circ$$

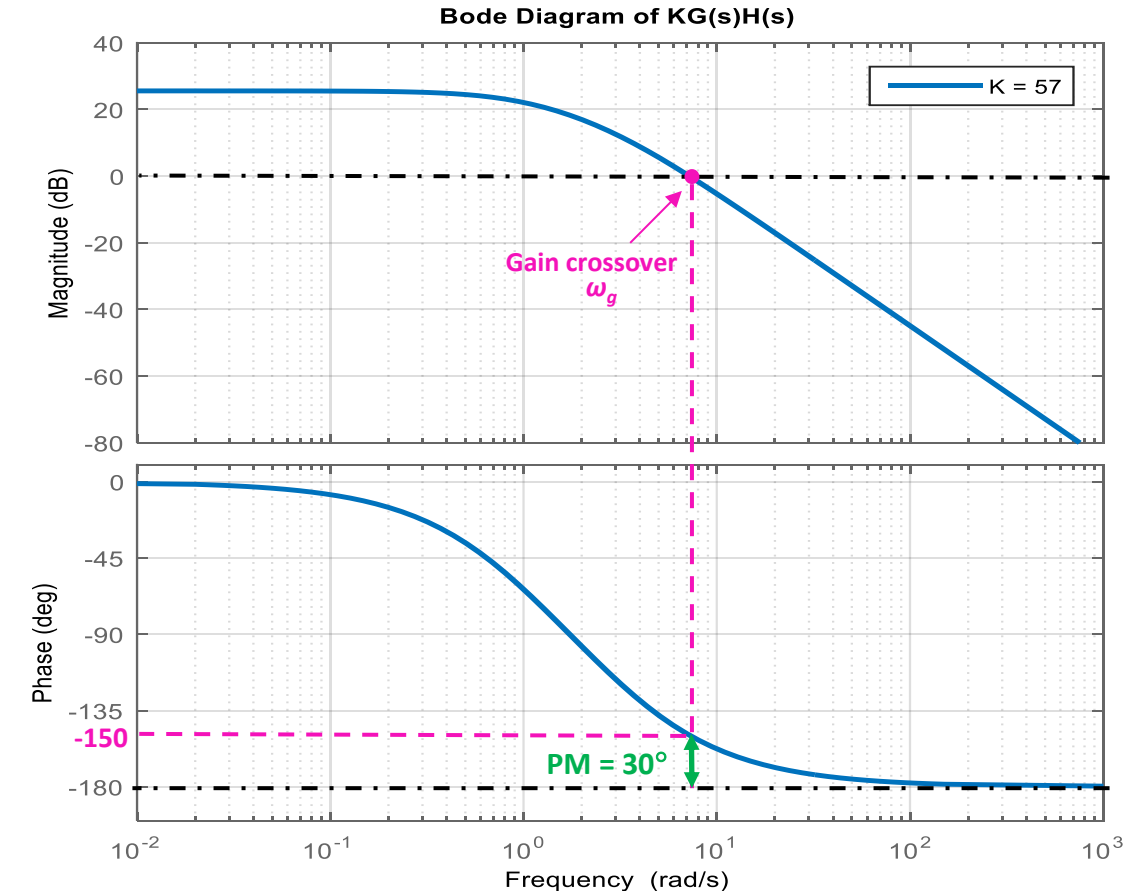
**Step 4:** Select the appropriate factor of  $\beta$  based on the  $\phi_m$  value

$$\beta = 10$$

$$\phi_m = 55^\circ$$



$\beta$	$\phi_m$
10	55°
20	65°
30	70°
40	72°
50	74°
60	75°
70	76°
80	77°
90	78°
100	78.5°

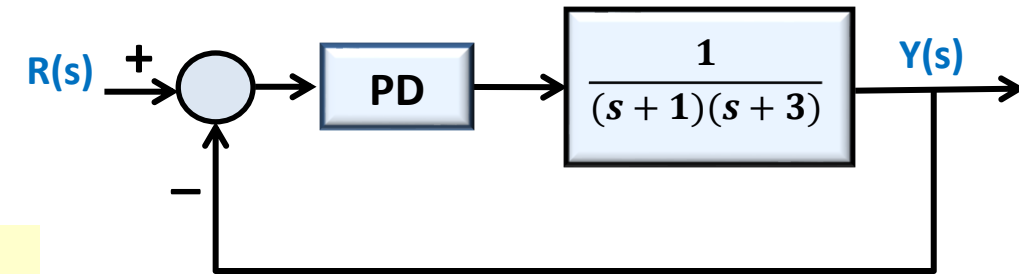


# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$



**Step 5:** Find the new gain crossover frequency  $\omega_{gc}$  where the magnitude is  $-20 \log \sqrt{1 + \beta}$

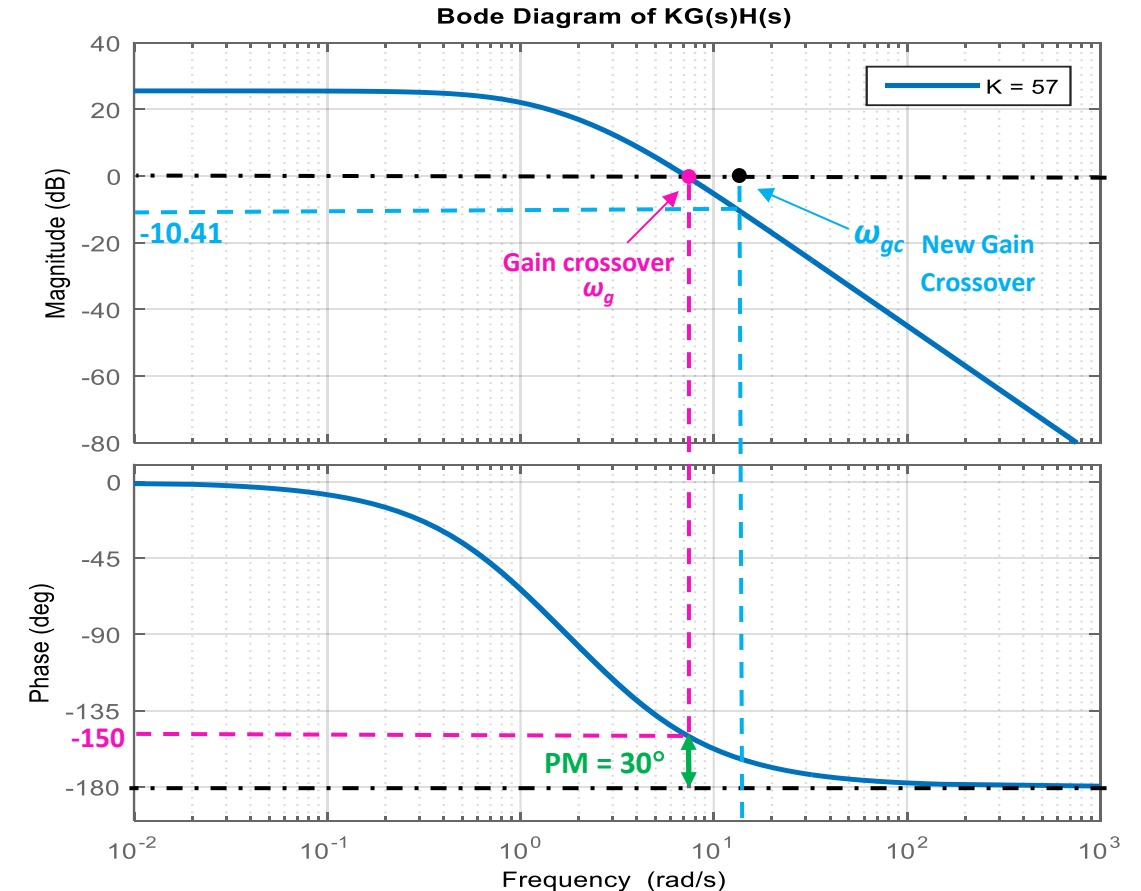
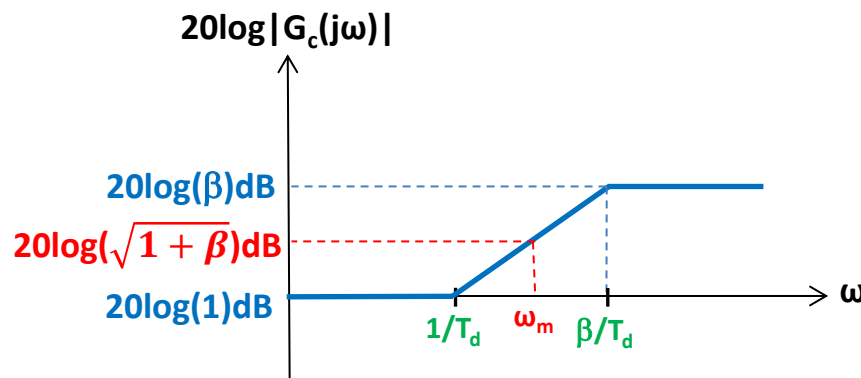
- The new gain crossover frequency,  $\omega_{gc}$ , can be determined from the Bode diagram at the magnitude of  $-20 \log \sqrt{1 + \beta}$ .

$$-20 \log \sqrt{1 + \beta} = -20 \log \sqrt{11} = -10.41 \text{ dB}$$



$$\omega_{gc} = 13.5 \text{ rad/sec}$$

New Gain Crossover Frequency

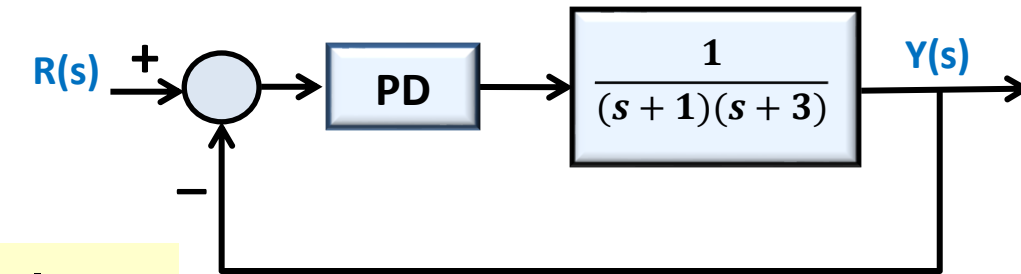


# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$



**Step 6:** Assign the maximum phase frequency  $\omega_m$  at the new gain crossover frequency  $\omega_{gc}$  value

$$\omega_m = \omega_{gc} = 13.5 \text{ rad/sec}$$

**Step 7:** Assign the derivative time constant  $T_d$  value

$$T_d = \frac{\sqrt{\beta}}{\omega_m} \rightarrow T_d = \frac{\sqrt{10}}{13.5} \rightarrow T_d = 0.23$$

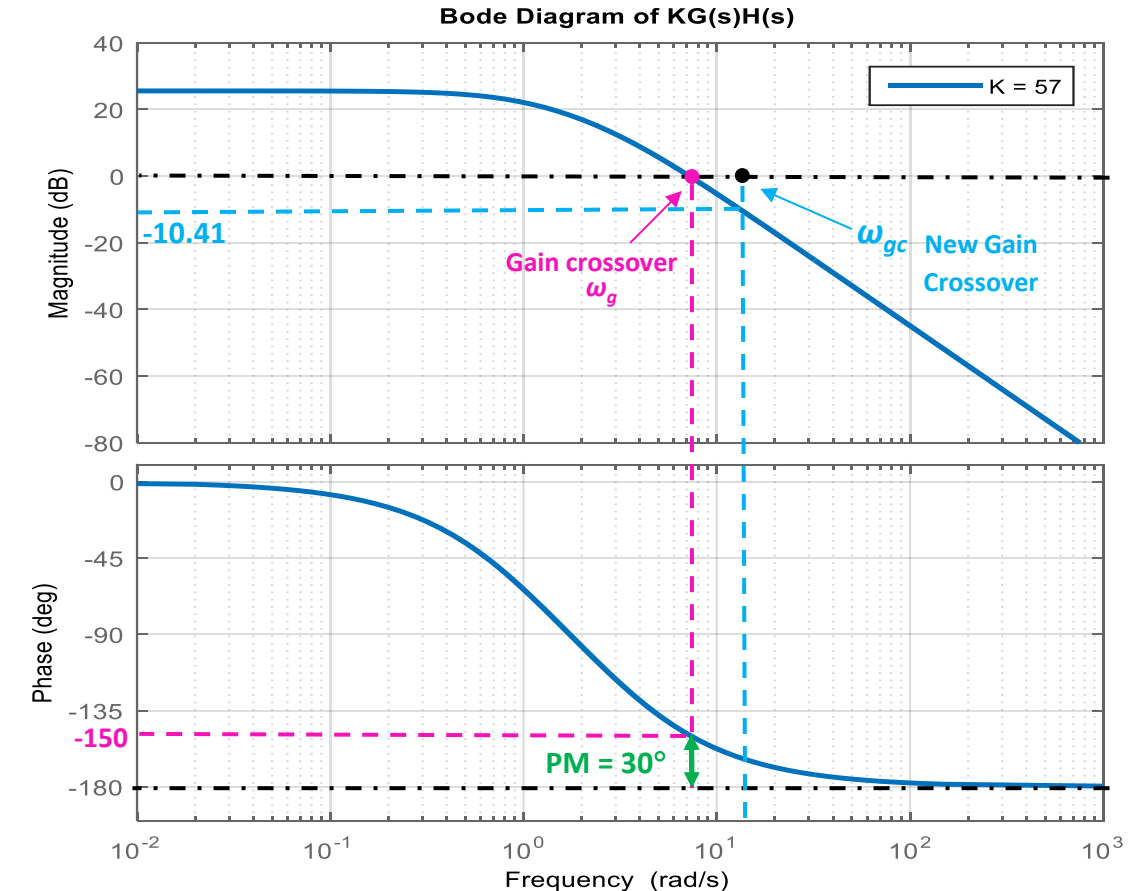
- The designed PD controller is obtained as

$$K_p = 57$$

$$T_d = 0.23$$

$$\beta = 10$$

$$G_c(s) = 57 \left( 1 + \frac{0.23s}{0.023s + 1} \right)$$



# PD Controller Design

## Example 3

Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$

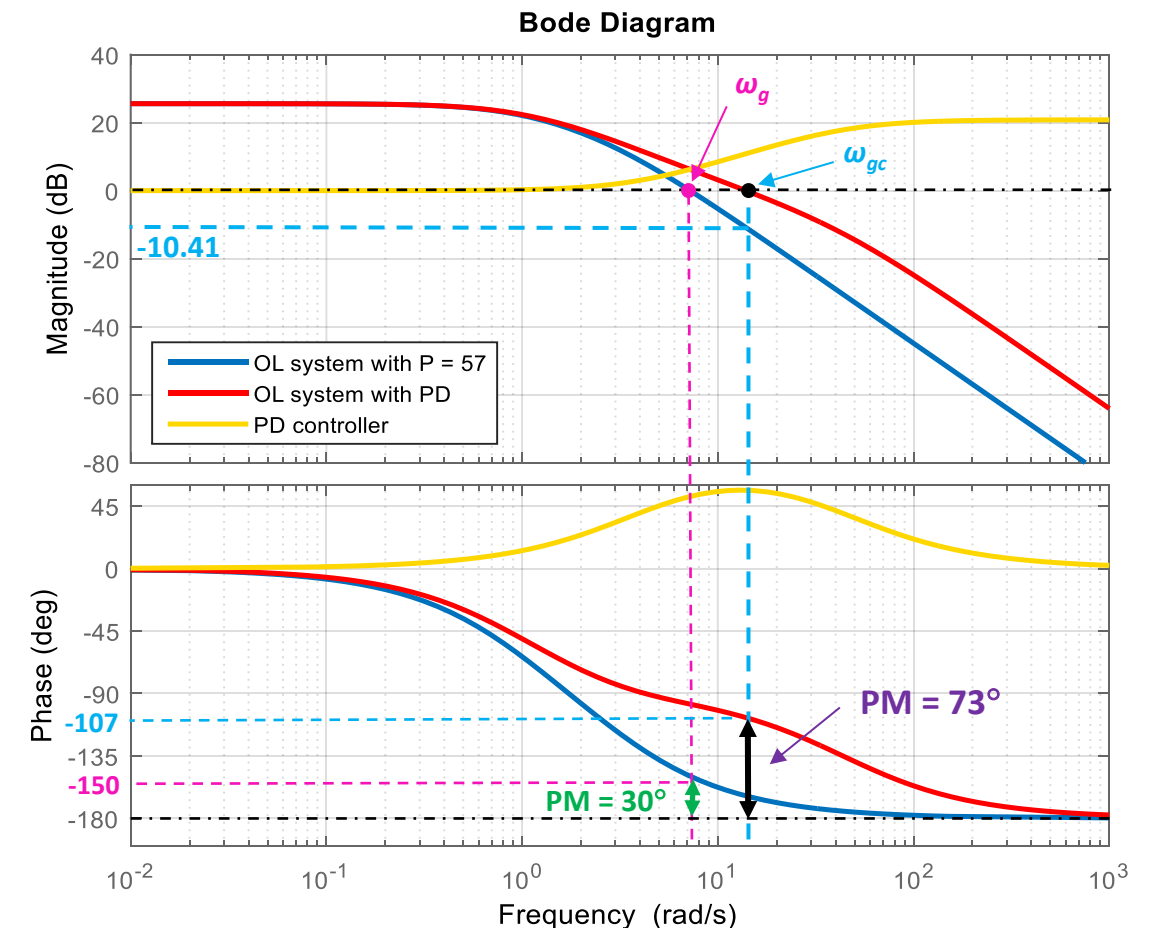
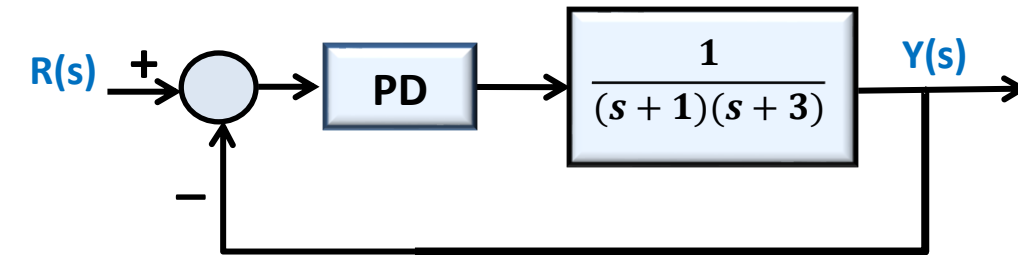
- Graph shows Bode plot of the open-loop system with proportional controller only, the open-loop system with PD controller, and the PD controller

$$K_p G(s)H(s) = \frac{57}{(s+1)(s+3)}$$

$$G_c(s)G(s)H(s) = 57 \left( 1 + \frac{0.23s}{0.023s+1} \right) \frac{1}{(s+1)(s+3)}$$

$$G_c(s) = 57 \left( 1 + \frac{0.23s}{0.023s+1} \right)$$

- The new gain crossover frequency is located at the frequency of the maximum peak of the designed lead compensator at  $\omega_m$ .
- PD controller **increases the phase margin** of the system by contributing the **positive phase**.
- PD controller **increases the bandwidth** of the system that results in **faster transient response**.



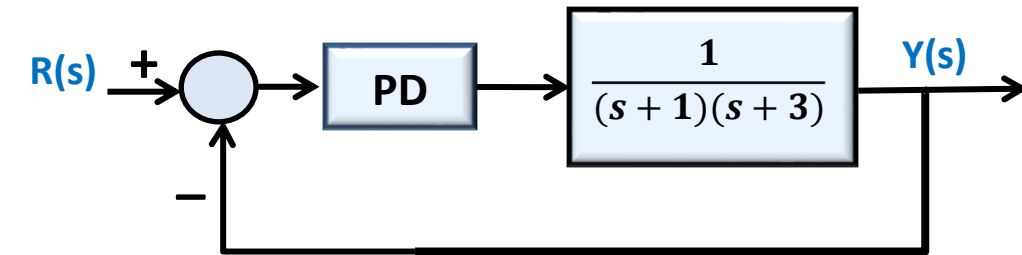
# PD Controller Design

## Example 3

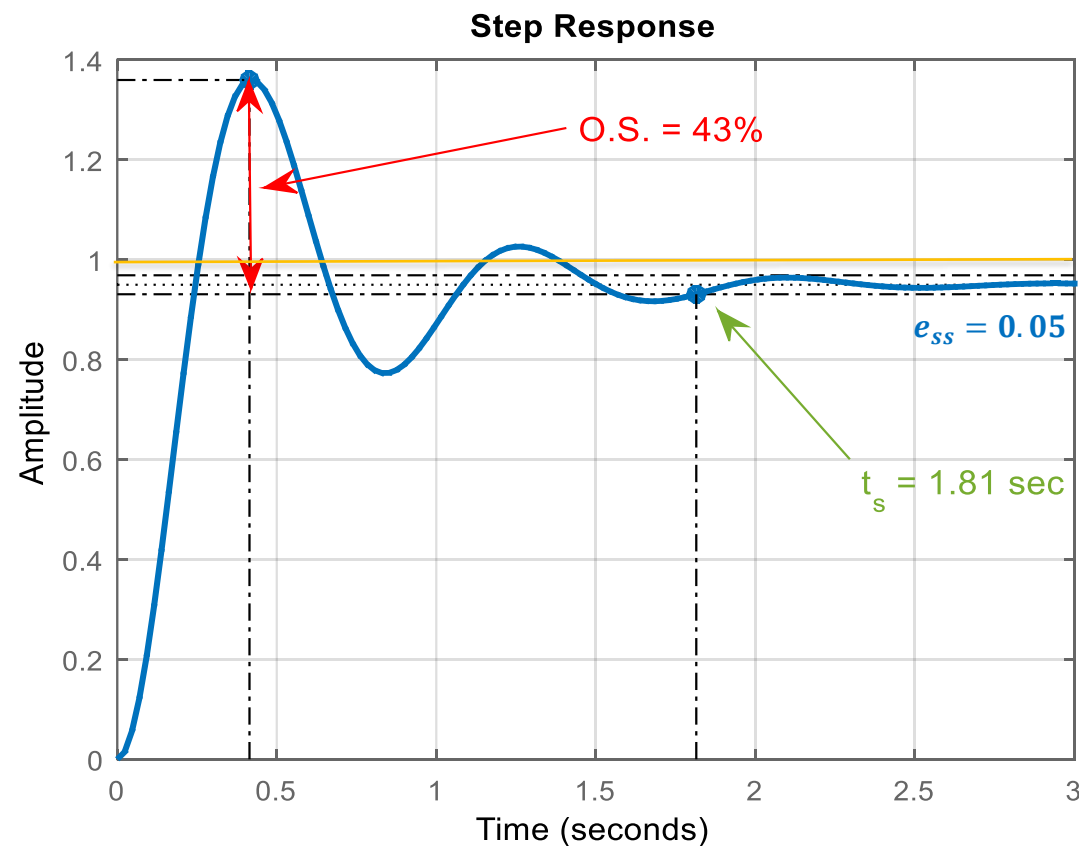
Consider the following second-order system. It is desired to design a PD controller to achieve the following performance characteristics

$$e_{ss} = 0.05, PM > 60^\circ, GM > 10\text{dB}$$

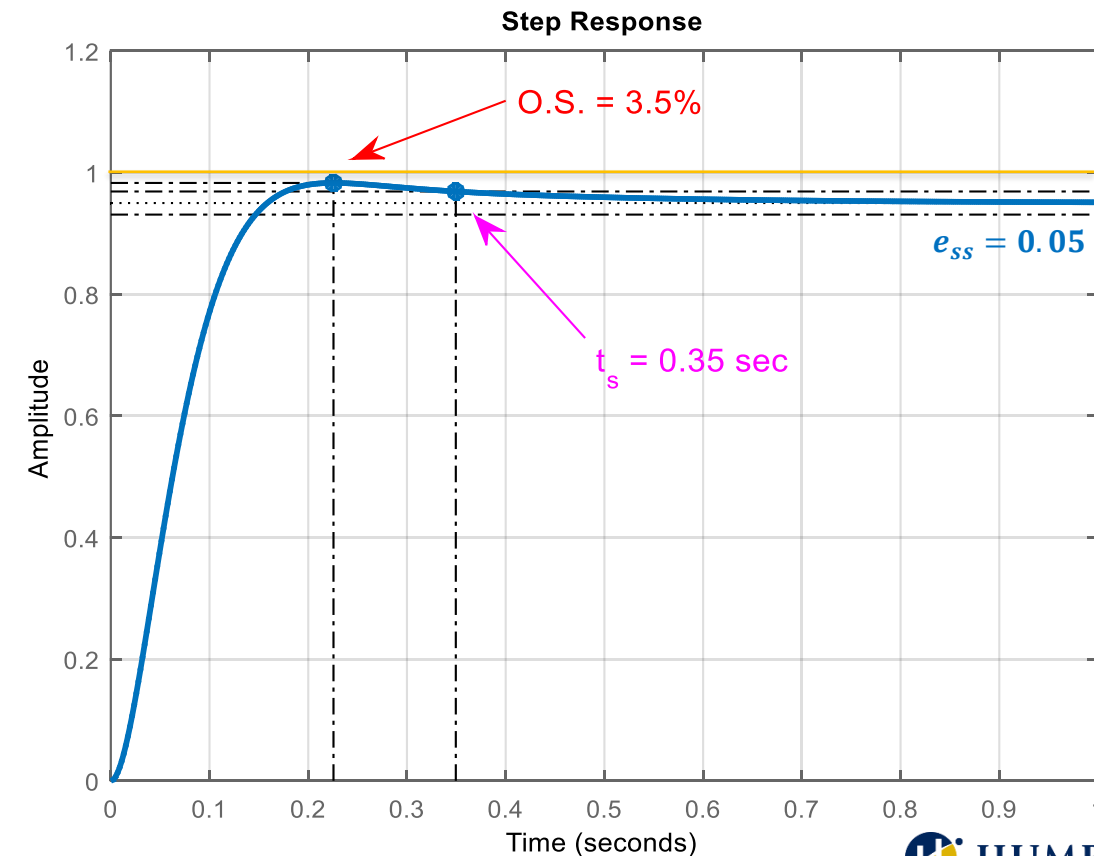
- Graphs show unit-step response of the closed-loop systems with P only controller  $K_p = 57$  and with the designed PD controller



Closed-loop system with P only  $K_p = 57$



Closed-loop system with the PD Controller



# THANK YOU