# Temperature dependence of rock thermal properties

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# Contents

1	Introduction							
2	Rui	Running koft.pro						
	2.1	Overview	3					
	2.2	Sequence to prepare coefficents for KRC	4					
3	Thermal conductivity $\lambda(T)$ : koft.pro							
	3.1	Extending measurements to lower temperatures	6					
	3.2	$\lambda$ of Ice	7					
	3.3	Other materials	8					
4	Spe	Specific heat $C_P(T)$ : specheat.pro						
	4.1	$C_P$ of $H_2O$ Ice	9					
	4.2	Other materials	10					
5	Thermal properties main program: koftop.pro							
	5.1 Functional fit for KRC use							
	5.2	2 Modifiable parameters						
	5.3	Action guide						
	5.4	4 Typical use						
	5.5	Fitting Cp of T for Mars temperature range						
	5.6	Fitting $\lambda$ of T for Mars temperature range						
	5.7	Extension of $\lambda$ for Mars temperature range	16					
6	Particulate materials							
	6.1	SP09A: Piqueux unconsolidated model	17					
		6.1.1 SPSPREAD: Piqueux Spreadsheet for cemented particles. OBSOLETE	18					
		6.1.2 Calling from koftop	18					
	6.2	PARTCOND: Kieffer analytic model for cemented particles	19					
		6.2.1 Calling from koftop	20					
7	Pap	pers on hand	21					
	7.1	Rocks and minerals	21					

	7.2	Carbon dioxide gas	22
8	Rar	ndom notes during literature search	23
	8.1	SWK	25
	8.2	Palankovski Dissertation	25
		8.2.1 3.2.4 Thermal Conductivity	25
		8.2.2 3.2.4 Specific heat	25
	8.3	From Vosteen 2003 Section 4:	26
		8.3.1 Mottaghy08	26
	8.4	Clauser & Huenges 1995	26
	8.5	Other papers	27
9	Ack	knowledgments	30
$\mathbf{L}$	ist	of Figures	
	1	$\lambda$ big picture. kex.jpg jpg=color version	6
	2	$\lambda$ for several materials. 34a.jpg	7
	3	$\lambda$ from Petrunin. 34b.jpg	7
	4	$\lambda$ data points. 35.jpg	8
	5	$C_P$ for several materials. Cp9.jpg	10
	6	$\lambda$ for un-cemented soils	19
	7	$\lambda$ for temperature-dependent cemented soils	21
	8	Thermal inertia for temperature-dependent cemented soils.	22

### Abstract

The temperature dependence of the specific heat  $C_p$  and thermal conductivity  $\lambda$  for geologic materials are extracted from the literature. Measurements below 0° are rare, especially for  $\lambda$ . These data and methods to extend to cover the temperature range for Mars have been coded into IDL routines. Model of unconsolidated [50] and cemented [38] particulates are used to generate the effective thermal conductivity of these materials and hence the thermal inertia as a function of temperature. For all materials, the coefficients ready for inclusion in the KRC thermal model, a third-degree polynomial in scaled temperature, can be generated. Apart from mm and larger uncemented grains, the intrinsic thermal variation of the bulk properites has a significantly larger effect on the temperature dependance of thermal inertia of particulates than does grain size.

### 1 Introduction

I did not set out for this to become so involved:

Life is what happens while you are busy making other plans.

John Lennon

In theory there is no difference between theory and practice. In practice there is.  $Yogi\ Berra$ 

If we knew what it was we were doing, it would not be called research, would it?  $Albert\ Einstein$ 

It doesn't make a difference what temperature a room is, it's always room temperature.  $Steven\ Wright$  This document covers the background for inclusion of temperature-dependent thermal properties capability of the KRC thermal model.

To aid in choosing the form for incorporating temperature dependence, I searched the literature for information on the variation of both thermal conductivity  $(k \text{ or } \lambda)$  and specific heat  $(C_P)$  with temperature. Any variation of density  $(\rho)$  with temperature, which is commonly characterized through the linear thermal expansion coefficient, was ignored as this coefficient of order 1.E-5 per Kelvin; e.g., [25, Fig.8].

Whereas there is quite a bit of information on  $C_P(T)$  at temperatures appropriate for the martian surface, most work on  $\lambda(T)$  of geologic materials has been directed toward study of the Earth's crust and mantle, and hence is at room temperature and above. I had little success finding conductivity measurements in the 100-273 K range.

A number of suggested analytic forms for  $C_P(T)$  and  $\lambda(T)$  were coded, along with the listed coefficients for a number of materials. In addition, for a few materials, original measurement data were found, and these are also included.

For each material or relation, the temperature range of measurements and an estimated range of applicability is assigned; the latter is subjective and only a guide. These values are returned by the thermal-properties routines.

The KRC thermal model is in Fortran. All the code for generating the coefficients is in IDL.

Major IDL routines are effectively large case statements; the coding style is described in -xtex/idlstyle.tex. The @here refers to specific elments of a case statement identified by its case control index, kon

The thermal properties are covered by two routines;

**koft.pro** for thermal conductivity, see  $\S 3$ 

**specheat.pro** for specific heat, see §4

This routine also include k(T) for  $H_2O$  ice because of source table structure.

These two routines are accessed by the main program **koftop.pro**, see §5, which can fit the returned values to the standard form chosen for KRC, a cubic polynomial to scaled temperature, and print the coefficients in a form ready for cut-and-paste into a KRC input file.

Unfortunately,  $C_p$  and  $\lambda$  are not both available for many materials, and for none of expected Martian materials. Thus, the defaults listed in §2.2 may seem strange; thay are chosen to hopefully be close to likely Martian surface materials.

A user could incorporate additional relations or materials by adding a section to the appropriate thermal properties routine, and running **koftop** for the desired temperature range.

Although virtually all the literature research and coding of thermal properties is for materials of higher thermal inertia (TI) than common on Mars, §6 uses these to derive the temperature-dependent properties for particulates, covering the common TI range for Mars.

§8 is an unstructured set of notes, and will be of little interest to most readers.

Many of the figures are more usefully viewed in color; change the extension on the file name that ends the caption to .jpg. They are also listed in the List of Figures.

# 2 Running koft.pro

### 2.1 Overview

Typical sequence of actions using **koftop.pro** 

A temperature range is chosen, and a spacing within this range adequate to support representative polynomial fits of order 3 (or more).

For either  $C_P$  or  $\lambda$ , a source index and sub-index is selected. The appropriate routine, specheat or koft, respectively, is called to supply the values V at these temperatures.

These values are fit with a functional form that matches KRC; currently a cubic polynomial for both properties.

Fit uses scaled (or unscaled) temperature

Could choose any order of 2 or larger

Also available are forms 1/(A+BT), useful for conductivity, and  $c_0 + c_1/\sqrt{T} + c_2/T^2 + c_3/T^3$ , only for unscaled temperature.

The polynomial representation is tested uniformly across the desired temperature range and a RMS residual reported. Sample applications that are coded:

- The conductivity values for two materials can be used for the grains and cement of a particulate conduction model and the resulting effective conductivity fit with a cubic.
- The cubic coefficients for a conductivity and a specific heat can be used to compute a thermal inertial table versus temperature.

### 2.2 Sequence to prepare coefficients for KRC

in IDL: .rnew koftop. This will automatically do several initialization steps

@71... Defaults for Particulates

Sets the parameter groups: park, parp, to their firm-code defaults, shown in §5.2

Set the default materials for the grains and the particulate cement

Conductivity: matk BasicRocks:Zoth88, limestone

Specific heat: matp Sphene, clinochlore:Fe=0.89

**@**25... Setup T

Set the temperature range parr [11:13] to the defaults shown in §5.2

Set the temperature scaling to defaults. DO NOT CHANGE

@260.. Empty XYY storage. This will store data for materials used

@60... Initiate bbb. This will store interpolated points

@5.... x=scaled T. Use scaled (versus absolute) temperature as the independent variable

@856.. Set colors to a nice set of six.

Option: Change temperature range and resolution: @16 Modify [11:13]. Then @25, @5

Option: Change properties of the Grains: Do C and K below. Then do @710 to store as grain properties

C: Option: change material for specific heat. You may need to look at SPECHEAT for details.

@15 parc: Change any of the following

[1:2] Set material index and sub-index, as listed in §4

If Material =1, then set [3]= Debye temperature in K and [5]= $C_P$  at  $0^{\circ}$  C

@41 Transfer parameters and call SPECHEAT

@33 Compute cubic fit coefficents

@57: Save coef as: Cp

K: Option: change material for conductivity. You may need to look at KOFT for details.

@12 pari: Change any of the following

[1:2] Set material index and sub-index, as listed in §3

If more than one material listed, the sub-index is the 0-based count in the order listed.

[7:8] Cold extension method and number of points. Change not recommended

@31 Transfer parameters and call KOFT

@32 Extend to lower temperatures. Will do nothing if not needed.

@33 Compute cubic fit coefficents

**@**56: Save coef as:  $\lambda$ 

Choice 1: treat as pure solid:

For both  $C_P$  and  $k=\lambda$ , Cut and paste the coefficients printed @33

between the > and < into KRC input for upper or lower material

@59 Will print thermal inertia table

Choice 2: treat as uncemented: [do not need cement properties at all]

[ @36 Will print SP90A parameters for a default set of inputs]

@16 parr: Change any of the following

0: Grain radius, micrometer

1: Pressure in Pascal

2: Porosity fraction. Routine is based on 0.259 to 0.476

4: Density of a grain

8: Point-contact conductivity.

@37 Run Piqueux unconsolidated model

@377 Prepare results for fit

Choice 3: treat as cemented:

Option: Change properties of the cement: Do C and K above.

Then do @711 to store as cement properties

@16 parr: Change any of the following

4: Density of a grain

5: Cement volume fraction

7: Density of cement

@701 Modify PARTCOND parameters

1: grain radius, micrometer

Do not change items 2:5, these will be replaced for each temperature

The rest can generally be left at their defaults.

@72 Run Kieffer cemented model

After choice 2 or 3:

@74 Cubic fit to conductivity

Cut and paste the values for  $C_P$  and  $k=\lambda$  into KRC input for upper or lower material

@75 Print thermal inertia table

# 3 Thermal conductivity $\lambda(T)$ : koft.pro

At very low temperatures, typically below about 20K and not of interest here, expect a  $T^3$  relation. Above this and over most of the range below the Debye temperature, expect for crystals a 1/T relation according to the 3-phonon scattering Umklapp effect Kittel76=[41]. The temperature dependence for glasses is quite different, usually increasing with temperature, e.g. Birch40=[10] Figure. 4, crystalline rocks, versus, Fig. 6, glasses.

Measurements of probable Mars materials under Mars-appropriate conditions are rare.

A relation  $1/\lambda = A + BT$  has been found to be a rough fit for minerals Petrunin95=[49]. A linear fit to  $1/\lambda$  for several published data are shown in Figure 1 and 2 of Petrunin95=[49]; I estimated the values at 200 and 800 K in these figures, from which A and B are derived and which allows extension over the range of Martian temperatures.

Relations coded, only 2 and 5 are algebraically different from 1/(A+BT).

1: Horai70b 1/[A + B(T - 300)]

Dunite, Pyroxenite, Diabase, Gabbro, Anorthosite, Albitite, Granite

2: Zoth88  $A + B/(350 + T_c)$ 

RockSalt, Limestones, Metamorphics, AcidRocks, BasicRocks, Ultra-basics, Aveof5types

- 3: Sass92 elaborate form of 1/(A+BT)
- 4: Clauser 95 1/(A+BT)

gneiss, metabasite

5: Seipold98  $1/(A + BT_c) + CT_c^3$ 

paragneiss, amphibolite

 $T_c^3$  term is clearly inappropriate below 0°C.

6: Vosteen03  $1/[0.99 + T_c(A - B/k_0)]$ 

crystalline, sedimentary

7: Petrunin95 1/(A+BT)

Fig 1: labradorite, microcline, garnet, pyroxenite, SynGalGarnet, garnet, SynOlivine, olivine, alpha-SiO2

Fig 2: Granite, Diorite, Diabase, Dunite, Gabbro, Serpentenite, Eclogite, mica

For all these, the lower limit of applicability was arbitrarily set at 123K.

Data points

11: Kanamori 1968

quartz001, quartz001, olivine, periclase

- 12: Yang 1981, NaCl
- 13: Birch 1940, silica glass

- 14: Glassbrenner 1964, pure Si and Ge
  These ideal materials, measured over wide range, are instructive for typical behaviour.
- 15: Abdulagatov 2006 Sandstone, Limestone, Amphibolite, Granulite, Pyroxene-Granulite
- 16: Slack 1971 Grossularite

Some of these are shown in Figure 1

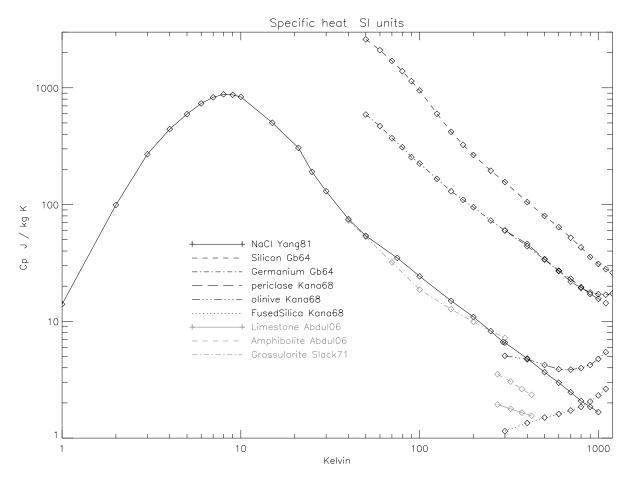


Figure 1: Measured values of thermal conductivity versus temperature. NaCl displays the transition from  $T^3$  at very low temperatures to 1/T over planetary surface temperature range.  $\lambda$  begins to increase near the Debye temperature, as shown for Olivine and Germainium (which is otherwise indistinguishable from Periclase). The rocks Limestone and Amphibolite, measured over 273-423 K, are lower than all minerals. The garnet Grossularite is similar to NaCl. kex.eps

### 3.1 Extending measurements to lower temperatures

Conductivity measurements of geologic materials commonly do not extend below laboratory ambient. Where analytic relations are given, here they are simply used for low temperatures. For data-point sets, a cubic spline is used to interpolate between data points; a "natural spline" is specified for extrapolation. For extension of data points to lower temperatures; **koft** can be called a second time with the material index set to:

- 21: a linear extension of the coldest two measured points
  - Mathematically robust, but amplifies errors.
- 22: a  $1/\lambda = A + BT$  exact fit to the coldest two measured points Tends to generate a pole and wild extensions
- 24: a  $1/\lambda = A + BT$  fit to the coldest N=pari[8] measured points (uses Simplex method) Both coefficients limited to  $>10^{-8}$  to avoid poles, and these limits are commonly hit!

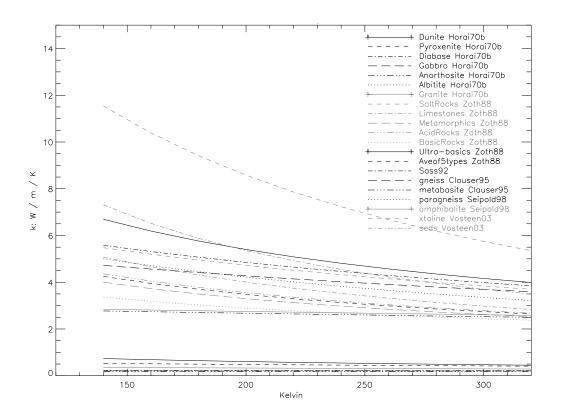


Figure 2: Thermal conductivity versus temperature for several of the pre-coded materials. 34a.eps

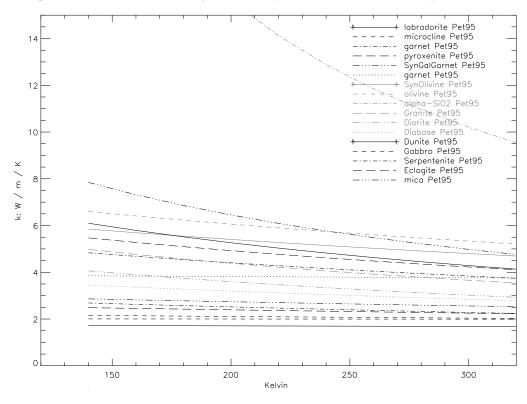


Figure 3: Thermal conductivity versus temperature relations from Petrunin95=[49]. 34b.eps

### 3.2 $\lambda$ of Ice

Note,  $\lambda(T)$  for H<sub>2</sub>O ice returned by **specheat** with arg2=9 and arg3=4

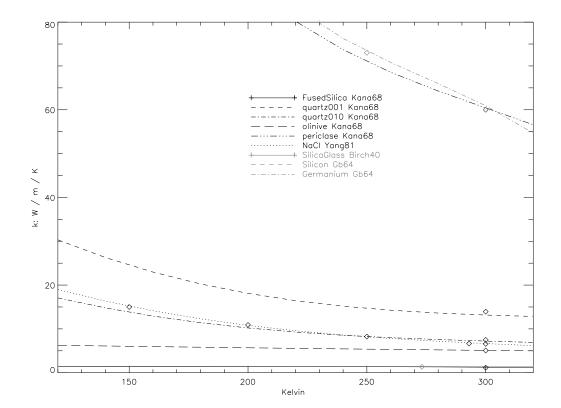


Figure 4: Thermal conductivity versus temperature for data-points (diamonds) for several materials. The lines represent cubic fit to points within 120:320 K. 35.eps

Theoretical expectation is for a 1/T relation; as discussed by Slack80=[64]. The relation used of this form is taken from Figure 5.7 in Hobbs; k = 0.4685 + 488.19/T. Because ice Ih is anisotropic, can't really expect different lab measurements of polycrystalline ice to agree within a few percent. Action sequence: 138, which sets T range to 120:280 by 10 and sets the sequence:

```
25... Setup T
48... H20 k into arg4
481.. yin=arg4
315.. Plot one material
5.... x=scaled T
33... Cubic coefficents for KRC
335.. Oplot fit
56... Save coef as: k
Gives results:
0.00784 > 2.685262 -0.9664988 0.4933776 -0.3767982 < H2O:Ice Hobbs
RMS fit residual represents 0.3% of the value at 220K.
```

### 3.3 Other materials

To include additional materials, add a section to the case statement in koft.pro

# 4 Specific heat $C_P(T)$ : specheat.pro

Specific heat increases with temperature across the temperature range of our interest. Representations range from linear with T (for  $H_2O$ ) to the Debye form:

 $C_v=9Nk\left[rac{T}{T_D}
ight]^3\int_0^{T_D/T}rac{x^4e^x}{(e^x-1)^2}dx$  where  $T_D$  is the Debye temperature for a material.

Berman85=[5] explicitly address extension below 298.15K=25C but their interest is focused on Earth-interior temperatures. They use the form  $C_p = k_0 + k_1 T^{-0.5} + k_2 T^{-2} + k_3 T^{-3}$  T in Kelvin, and provide in Table 3 these coefficient for an extensive set of minerals based on prior reported measurements. This form is widely used.

Waples04=[71] shows in Fig 2 typical  $C_P(T)$  for 0-800C. Table 1 list  $C_P$  for about 250 minerals, mostly at 20C or "room temperature". Based on an empirical fit to many minerals and non-porous rocks over 0-1200C, they propose a normalized temperature relations:  $C_{Pn}(T) = 8.95E - 10T^3 - 2.13E - 6T^2 + 0.00172T + 0.716$ . However, they do not discuss the range below 0C, so that at most the slope of this relation at 0C is relevant for martian temperatures.

Index [and sub-index] and Materials:

- 1: Debye theory Debye12=[17], presented in Chapter 5 of Kittel76=[41] Debye temperature, and arg4 is  $C_p$  at 0C
- 3: Apollo lunar samples, Horai70=[33]
  - 0: sample 10020; fine-grained vesicular crystalline igneous
  - else: sample 10046; breccia

Both also output  $\lambda$ 

- 4: Sphene, King54=[40]
- 5: Chlorites: clinochlore chamosite
  - 0,1,2,3 are index of four specific Fe abundances, listed below. 4.x is x fraction FE

Four Fe/(Fe+Mg) ratios: 0, 0.116, 0.889, 1.0 . 143-623K Bertoldi01=[6]

Analytic function tends to derivative=0 at 120K

Mg and Fe end-members measured over 5:500K Bertoldi07=[7]

Data table at 10K interval up to 300K

- 6: Lunar material to high T, Ledlow92=[44]
- 8: Normalized relation for solid rocks, Waples04=[71]

Reference temperature in C

- 9:  $H_2O$  ice, including some  $\lambda$  values. arg3=:
  - 0: Spline interpolation of Giauque 36=[21]
  - 1: Hobbs Figure 5.7, straight line
  - 2: Table of  $C_P$  [and k, and  $\rho$ ] from http://www.engineeringtoolbox.com/
  - 3: Giauque36=[21] 16:267 K
  - 4: Haida<br/>74=[24] 119:230  ${\rm K}$
  - 5: Yamamuro87=[73] 13:164 K
  - 6: k from web table
  - 7: Concatenation of those in 3:5 that are within range of request T.
  - 8: Plot of 1:5 above

Temperature curves for a number of materials are generated by @44, the results are shown in Figure 5 and in color image CP9.jpg. Measurements of probable Mars materials under Mars-appropriate conditions are rare.

### 4.1 $C_P$ of $H_2O$ Ice

**specheat** includes tables of measurements for ice Ih taken by Giauque36=[21], Haida74=[24], and Yamamuro87=[73]. A cubic fit was done to the aggregate of their data over 120K to 273K, with an RMS residual of 0.23%

Running to get H<sub>2</sub>O ice Cp, using all data sources, Do 139, which creates:

49... Cp H2O data points Will all be below OC

491.. move T points into ttt

315.. Plot one material

5.... x=scaled T

33... Cubic coefficents for KRC

25... Setup T

5.... x=scaled T

482.. Make points on uniform T

335.. Oplot fit

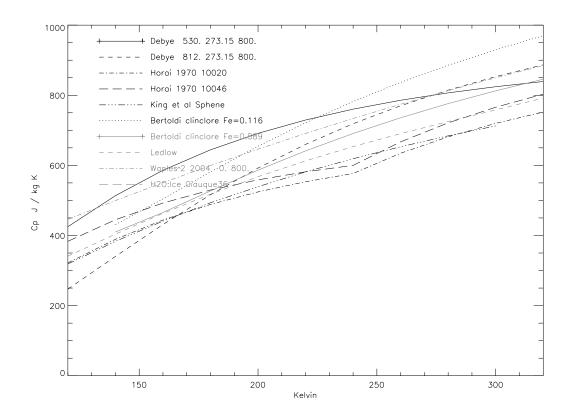


Figure 5: Specific heat versus temperature for several of the pre-coded materials. The inflection for the Horai Apollo sample comes from his recommendation to use the Debye relation below 240K.  $H_2O$  ice is off the top of this plot. Cp9.eps

57... Save coef as: Cp 3.95779 > 1710.648 721.8740 57.44873 24.37532 < H2O:Ice 3sources

### 4.2 Other materials

To include additional materials, add a section to the case statement in **specheat.pro** 

# 5 Thermal properties main program: koftop.pro

All data are firm-coded into subroutines, so the koftop uses no files.

New routines: KOFTOP, KOFT, SPECHEAT, FIT\_ABX, PARTCOND, SPSPREAD

**XYY5** is a package that allows storage of un-equal length arrays, in this case temperature-values data points for  $C_P$  or  $\lambda$ . It has a plot function for displaying these data.

### 5.1 Functional fit for KRC use

A set of uniformly-spaced points over the request temperature range is generated, and these are fit with a 3rd order polynomial.

### 5.2 Modifiable parameters

12: Cond. Ints: pari
Limits= -1 999

```
0
             6 Last @34
             5 Material index
      1
      2
            2 Secondary index
            3 Fit kode @51
      3
             0 bbb index, -=auto
      4
             8 Size of bbb.
      5
      6
            0 Ylog flag @73
      7
            24 Cold extension: KofT action
             4 " Max points to use
13: PARTCOND: parm
            0.00000 edit: flag -=stop >1=help
      1
            100.000 Rg: grain radius, mu m
      2
            250.000 T: temperature, K
      3
           0.937000 kh: grain thermal conductivity
          0.00300000 kg: gas cond. J m^-1 s^-1 k^-1
      4
      5
            2.00000 kc: cement cond. =SI
      6
           0.980000 emis: grain emissivity
           0.900000 G: host grain cond. factor -1=ave -2=geomean
      7
          0.0100000 B: Cement contact angle, radian
      8
            77.7700 vvvv:--numerical parameters
      9
     10
            0.00000 flag: test integrals
           0.100000 beta: SMX limit radian
     11
     12
            30.0000 nLo: steps along cement [Int]
            100.000 nHi: steps along gap [Int]
     13
            0.00000 DP: Flag, double precision
     14
     15  0.00100000  B1: Initial B
     16
            1.10000 Brat: ratio for loop
14: FitPlot: parg
          0.0100000 Fit toler \ FIT_ABX
      0
          0.0500000 Frac.Scale / > Amoeba
      1
      2
          -7.00000 ----spare
           -7.00000 ----spare
      3
      4
            20.0000 Plot Ymax for k
      5
            1000.00 " " for Cp
      6
            220.000 @76 X left \ Normaliz | middle Xval
      7
           0.800000 Y of first | locations| offset units of char height
      8
            1.00000 Delta Y | for | c.size LABEL_CURVE
            1.00000 Line Lenght/ Guide | c.thick
      9
     10
            1.00000
                                         |leave: 0=clear
15: Cp values: parc
            2500.00 Density, SI
            5.00000 Material index
      1
            5.00000 Secondary index
      2
            850.000 Debye Temp. K
      3
            20.0000 Reference temperature C
      4
      5
            700.000 Reference Cp
           6
           0.930000 Y of first | locations
      7
      8 -0.0240000 Delta Y | for
          0.0800000 Line Lenght / Guide
16: Cond. values: parr
           -1.00000 Rg: Grain radius, micron -=table
```

```
1
             600.000 P: pressure Pascal
      2
            0.350000 phi: Porosity fraction
      3
            0.937000 host grain conductivity
                      " " density
      4
             2400.00
      5
         -0.00100000 Cement fraction -=table
             2.00000 " conductitity
      6
      7
             1400.00 " density
          0.00100000 Point-contact conduct.
      8
      9
             4.00000 k @25C for Sass92
            0.700000 @632 YplotMax
      10
     11
             120.000 T min, Kelvin
                      " max
     12
             320.000
     13
             20.0000 " delta
     14
            -7.77000 vvv-Beware-vvv
             220.000 T scaling offset
     15
     16
           0.0100000 " " multiplier
17 GrainCemK: park
             2.77401 Grain K ConCof
      0
      1
           -0.535400 Grain K LinCof
      2
            0.204288 Grain K ^2 Cof
          -0.0710305 Grain K ^3 Cof
      3
      4
             3.79146 Cement K ConCof
      5
            -1.29785 Cement K LinCof
      6
            0.345378 Cement K ^2 Cof
      7
          -0.0386713 Cement K ^3 Cof
177 GrainCemCp: parp
      0
             581.378 Grain Cp ConCof
      1
             198.189 Grain Cp LinCof
      2
            -52.2628 Grain Cp ^2 Cof
      3
             12.0520 Grain Cp ^3 Cof
             636.157 Cement Cp ConCof
      4
      5
             272.547 Cement Cp LinCof
      6
            -28.1283 Cement Cp ^2 Cof
      7
            -39.3450 Cement Cp ^3 Cof
```

### 5.3 Action guide

```
Actions:
```

```
@0.... Stop  
@112.. kons=[25,5,34,64] Do conductivity: Group 1  
@113.. kons=[34,64] Group 2  
@114.. kons=[35,64,-1,64,655] data points  
@115.. kons=[12,15,16,25,60,41,5,51,55,61,62] Do one specific heat fit  
@116.. kons=[25,50,44,64] Do specific heat family  
@117.. kons=[72,74,75,76,-1,73,-1] k(T) solids in partcond,  
@118.. kons=[260,60,31,261,32,33,61,62,1182,651,88] loop for big picture  
@1182. increment  
@131.. kons=[15,25,41,315,5,33,335,57] Cp for one material  
@132.. kons=[12,25,31,315,5,33,335,56,710] k for one material  
@138.. kons=[25,48,481,315,5,33,335,56] H2O k  
@139.. kons=[49,491,315,5,33,25,5,482,335,57] Use H2O Cp data points
```

- @123.. Start auto-script
- @12... Integers: pari
- @13... PARTCOND: parm
- @14... Fit, plot: parg
- @15... Cp values: parc
- @16... Cond. values: parr
- @17... Partic K of T: park
- @177.. Partic Cp of T: parp
- @18... Guides and help
- @25... Setup T
- @260.. Empty XYY storage
- @261.. Add material data to XYY
- @31... Thermal conductivity of minerals
- @315.. Plot one material
- @32... Extend data sets to lower T REQ 31
- @33... Cubic coefficients for KRC
- @335.. Oplot fit
- @34... Test all analytic K for all their materials
- @35... Test all data-set materials
- @36... SP09a parameters
- @37... Particulates
- @41... Specific heat capacity of minerals
- @44... Test many SPECHEAT options
- @48... H2O k into arg4
- @481.. yin=arg4
- @482.. Make points on uniform T
- @49... Cp H2O data points
- @491.. Move T points into ttt
- @50... x=Kelvin
- @5.... x=scaled T
- @51... Fit to Tk
- @52... Use DoublePrec.
- @55... Print fit results
- @56... Save coef as: k
- **@**57... Save coef as: Cp
- **@**59... Print Inertia(T)
- @60... Initiate bbb
- @61... Plot data
- @62... Plot fit
- @631.. CHART cement k
- @632.. Plot rrr,ggg UPDATE
- @64... Plot of bbb
- @65... Data plot
- @651.. Big picture
- @655.. Overplot
- @70... Constant solid conductivity
- @701.. Modify PARTCOND params only
- @71... Defaults for Particulates
- @710.. Set Grain coefs.
- @711.. Set Cement coefs
- @72... Compute particulate k for 1 or set cement volumes
- @73... CLOT partCond
- @735.. oCLOT
- @738.. Plot gas conds
- @74... Calc and Print coefficients
- @75... Print thermal inertia table

```
@76... CLOT inertia
    @-3... — KON91 null
    @-1... Wait
    @-9... Stop in KON91 —
    @122.. Modify kons sequence
    @121.. + Reset to null
    @801.. TV2LP
    @803.. TV2JPG
    @8.... Start Graph to file and printer
    @80... Reset plot output device
    @85... Set Color, line, symbol scheme
    @87... Close plot device, no spawn of plot
    @88... Add subtitle to plot
    @9.... End a plot, save and print the file
Details
@31
    @49 gets the points, non-monotonic
    @491 moves data-point T into normal uniform T vector
    @51 does the fit to T
        kfit=pari[3] 2:n are polynomial, -4=Berman form for Cp, -2=1/(A+BT) for k.
    @25 restores normal T vector
    @482 generates uniform points
    @5 Specifies normalized T
    @33 does cubic fit to T'
@33
    Call SPSPREAD to get kgas
    call PARTCOND to get cement volume fraction
    For each grain size
```

### 5.4 Typical use

Control sequences for doing one material conductivity or specific Heat are preset.

@131 for specific heat. Default is, Bertoldi clinclore Fe fraction 0.89.

@132 for conductivity. Default is: BasicRocks Zoth88

Call SPSPREAD results into ddd Call PRESLEY results into ggg Call PARTCOND results into ppp

After doing these two, the results can be for either the grain material @710 or the cement material @711. Or, @70 will load the defaults for  $\lambda$  and  $C_P$  for both materials

For the Kieffer09=[38] particulate model then do the sequence

### 5.5 Fitting Cp of T for Mars temperature range

Below are examples of some cubic fits to scaled temperature martian temperatures; done at @44. The fits were restricted to the valid temperature range specified in the **specheat** routine.

```
T range and delta=
                         120.000
                                      320,000
                                                    20,0000
 Values between > < are the coefficents
 Value before > is the Standard Deviation of fit
Std.Dev
                                             T'^2
                                                           T'^3
               constant
                             Linear
                                                                      Material
0.85597 >
               730.3778
                             171.1534
                                          -97.36093
                                                         35.92560 < Debye 530. 273.15 800.
1.67749 >
               658.1685
                             318.4424
                                          -93.07760
                                                         1.813520 < Debye 812. 273.15 800.
```

8.68950	> 559.6317	178.1158	-15.88013	39.01124 <	Horai 1970 10020
11.85039	> 590.3480	166.5212	12.34777	46.07032 <	Horai 1970 10046
0.18631	> 581.3780	198.1888	-52.26276	12.05196 <	King et al Sphene
1.82517	> 719.6918	319.2454	-62.06202	-8.264219 <	clinclore Bert01 Fe=0.116
1.81581	> 639.2908	261.6666	-44.44849	-12.14468 <	clinclore Bert01 Fe=0.889
1.75006	> 642.4306	245.8746	-37.44404	-13.46644 <	clinclore Bert01 Fe=1.000
0.92818	> 646.6275	246.6678	-49.82160	7.951969 <	Chlorite Bert07 Fe=0.89
0.99128	> 611.7469	214.1993	-46.28867	11.27204 <	Ledlow
0.00000	> 690.9838	218.3245	-25.39334	0.9999385 <	Waples^2 2004 0.800.
2.96565	> 1711.052	728.0281	26.30519	-22.12386 <	H2O:Ice Giauque36

# 5.6 Fitting $\lambda$ of T for Mars temperature range

Results of @34

Т	range and	delta= 12	20.000 320	.000 20.0	0000	
	Std.Dev	constant	Linear	T'^2	T'^3	Material
	0.00038 >	0.5727402	-0.1567263	0.04650183	-0.01300548 <	Dunite Horai70b
	0.00002 >	0.4669398	-0.06774209	0.01004124	-0.001465128 <	Pyroxenite Horai70b
	0.00000 >	0.2209081	-0.002332719	2.464336e-05	-2.588600e-07 <	Diabase Horai70b
	0.00000 >	0.2053396	-0.0003023222	4.537213e-07	1.835347e-09 <	Gabbro Horai70b
	0.00000 >	0.1717570	0.004935535	0.0001419527	4.088490e-06 <	Anorthosite Horai70b
	0.00000 >	0.2071287	-0.005126931	0.0001269907	-3.158598e-06 <	Albitite Horai70b
	0.00001 >	0.3213432	-0.03948743	0.004927245	-0.0006079461 <	Granite Horai70b
	0.01602 >	7.844152	-3.343426	1.275726	-0.4435667 <	SaltRocks Zoth88
	0.00581 >	3.738380	-1.211992	0.4624507	-0.1607930 <	Limestones Zoth88
	0.00382 >	3.120837	-0.7963225	0.3038468	-0.1056470 <	Metamorphics Zoth88
	0.00437 >	3.353852	-0.9115353	0.3478075	-0.1209317 <	AcidRocks Zoth88
	0.00257 >	2.774009	-0.5354000	0.2042885	-0.07103046 <	BasicRocks Zoth88
	0.00700 >	5.078216	-1.460490	0.5572681	-0.1937604 <	Ultra-basics Zoth88
	0.00417 >	3.289425	-0.8697424	0.3318611	-0.1153873 <	Aveof5types Zoth88
	0.00097 >	4.646508	-0.9689192	0.2114329	-0.04462963 <	Sass92
	0.00024 >	4.142231	-0.6348214	0.09965667	-0.01537151 <	gneiss Clauser95
	0.00000 >	2.642703	-0.1536450	0.008963052	-0.0005217241 <	metabasite Clauser95
	0.00172 >	4.010569	-0.9906328	0.2589533	-0.06405231 <	paragneiss Seipold98
	0.00000 >	2.720438	-0.1448558	0.007374227	-0.0001738053 <	amphibolite Seipold98
	0.00118 >	4.511555	-0.9920732	0.2295133	-0.05116162 <	xtaline Vosteen03
	0.01894 >	4.898468	-1.988685	0.9858879	-0.4227412 <	seds Vosteen03
	0.00000 >	1.701741	-0.02365008		-4.536606e-06 <	labradorite Pet95
	0.00000 >	2.095118	-0.07242709	0.002506750	-8.661032e-05 <	microcline Pet95
	0.00019 >	4.278776	-0.6132959	0.08976835	-0.01293881 <	garnet Pet95
	0.00034 >	4.767582	-0.7651988	0.1261028	-0.02038259 <	pyroxenite Pet95
	0.00433 >	6.086648	-1.697102	0.5148059	-0.1468391 <	SynGalGarnet Pet95
	0.00000 >	3.806140	-0.05311756	0.0007416263	-1.065313e-05 <	garnet Pet95
	0.00013 >	5.272266	-0.6485804	0.08102152	-0.01000797 <	SynOlivine Pet95
	0.00019 >	5.899489	-0.7830707	0.1058212	-0.01411335 <	olivine Pet95
	0.11737 >	14.00425	-6.624243	4.223161	-2.169872 <	alpha-SiO2 Pet95
	0.00062 >	4.217541	-0.8062869	0.1600958	-0.03091895 <	Granite Pet95
	0.00042 >	3.464935	-0.6342483	0.1201894	-0.02220582 <	Diorite Pet95
	0.00007 >	3.118103	-0.3743126	0.04559595	-0.005495317 <	Diabase Pet95
	0.00127 >	5.032161	-1.097111	0.2514201	-0.05555261 <	Dunite Pet95
	0.00000 >	1.998668	-0.006657808	2.226491e-05	-8.915301e-08 <	Gabbro Pet95
	0.00003 >	2.467480	-0.2516543	0.02593687	-0.002652605 <	Serpentenite Pet95
	0.00000 >	2.362759	-0.1460787	0.009066172	-0.0005610733 <	Eclogite Pet95

### -0.1885311

### Extension of $\lambda$ for Mars temperature range

Used method 24 as described in §3.1 Fit to data points. FIT\_ABX preceding a material line are the values used for the cold extension based on a fit to the lowest 4 measured points; reports: A, B, # iterations, and  $\sum (y_f - y_m)^2$ . With unrestricted coefficients, can get some wild results.

Using 120 to 320 K with 10° interval, and with both coefficients restricted to be >1.e-8, get:

```
FIT_ABX out:
                 0.71640 1.0000e-08
                                       37.
                                             0.1212117
                                                             -0.1581136 < FusedSilica Kana68
  9 0.03898 >
                    1.412375
                                0.02452806
                                              -0.1340093
FIT_ABX out:
             1.0000e-08
                          0.00027364
                                       32.
                                              6.716378
  9 0.30994 >
                                                             -1.124730 < quartz001 Kana68
                    16.41876
                                 -7.531681
                                                5.085024
FIT_ABX out: 1.0000e-08 0.00048602
                                             0.6877223
                                       28.
  9 0.12127 >
                    9.264705
                                 -4.216154
                                                2.689451
                                                             -0.8292275 < quartz010 Kana68
                                            0.01092515
FIT_ABX out:
                 0.13603 0.00019892
                                       18.
  9 0.00834 >
                    5.561930
                                -0.6203964
                                              0.06161419
                                                          -0.008579915 < olinive Kana68
FIT_ABX out:
             1.0000e-08 5.6226e-05
                                              11.04964
                                       31.
  9 0.56404 >
                    80.26309
                                 -36.46237
                                                21.45405
                                                              -8.871257 < periclase Kana68
  9 0.13921 >
                    9.597675
                                 -5.494487
                                                2.905688
                                                             -0.8641065 <
                                                                          NaCl Yang81
FIT_ABX out:
                 0.68838 1.0000e-08
                                       34.
                                            0.01593368
                                             -0.02221565
                                                             0.01746422 <
                                                                          SilicaGlass Birch40
 11 0.01750 >
                    1.448836
                               -0.03569783
 11
    9.19763 >
                    223.8652
                                 -129.5840
                                                159.1353
                                                              -120.5962 <
                                                                          Silicon Gb64
    1.79470 >
                    83.58900
                                 -41.13925
                                                             -17.77364 <
                                                                          Germanium Gb64
 11
                                                29.67271
FIT_ABX out:
                 0.40525 0.00034224
                                       22.0.0001146897
  4 0.00097 >
                    2.081675
                                -0.1465059
                                             0.005840617
                                                           -0.007324098 < Sandstone Abdul06
FIT_ABX out:
                 0.27817
                         0.00087337
                                       23.0.0001096941
  4 0.00095 >
                    2.126523
                                -0.3922069
                                              0.07423300
                                                           -0.01850849 < Limestone Abdul06
FIT_ABX out:
                0.026575
                          0.00094168
                                       21. 0.001022004
  4 0.01386 >
                    4.262733
                                 -1.704368
                                               0.8369164
                                                             -0.3302984 < Amphibolite Abdul06
FIT_ABX out:
                 0.33794 0.00053873
                                       19.8.725863e-05
  4 0.00069 >
                    2.190314
                                -0.2586301
                                              0.03525489
                                                          0.0006817337 < Granulite Abdul06
FIT_ABX out:
                         1.0000e-08
                                       28. 0.002000614
                 0.41154
  4 0.00572 >
                    2.428892
                               -0.01149608 -0.009635572
                                                           0.003171192 < Pyroxene-Granulite Abdul06
```

#### Particulate materials 6

Use the relations from Piqueux09a=[50] for Knudsen number and its influence on effective gas conductivity.

Their relation for  $k_0$ , the large-volume conductivity of  $CO_2$  gas, differs by only a few percent from the fit to Johnston46=[36]. The effective gas conductivity in pores is  $k_{gas} = \frac{k_0}{1+e^{xi(Kn^{-1})}}$  where  $\xi\left(Kn^{-1}\right) = \frac{\log_{10}\left(Kn^{-1}\right)-2.15}{0.55}$ is derived from their numerical model.

The Knudsen number is the ratio of mean free path to the pore size;  $Kn = \frac{k_B T}{\sqrt{2\pi}\theta^2 LP}$  where  $k_B$  is the gas Boltzmann's constant,  $\theta$  is the molecule collision diameter,  $L \approx \sqrt[3]{\frac{\phi}{1-\phi}} \cdot r$  is the pore size  $(\phi$  is the porosity) and P is the pressure [all in SI units].

Piqueux09b=[51] does not provide a simple algorithmic approximation to his finite element model of cemented soils, so I will use my simple analytic model Kieffer09=[38], which displays the same general behavior.

Overview of sequence:

select grain size, cement fraction, environment conditions

Call **PP\_CO2** to get gas conductivity

Call PARTCOND once to get relation between indices for various cement volumes.

Compute effective gas conductivity

Loop over grain size calling SPSPREAD and PRESLEY for a set of temperatures loop over temperature calling PARTCOND to get net conductivity For each grain size and cement fraction, fit particulate K to cubic in T'

### 6.1 SP09A: Piqueux unconsolidated model

Summary of Piqueux09a=[50]

Contact conductivity is expected to be <.001, assumed to be zero [27.5]

Radiative conductivity goes as  $T^3$  described by Eqs 2,3,4

While mentioned at [5.8], never explicitly added into k???

Unconfined gas conductivity  $k_0$  follows fit to experimental data, Eq. 14

Effective gas conductivity  $k_{qas}$  expected to depend on Knundsen number. Eq. 12

Major numerical model to relate net conductivity to gas conductivity

Model run for simple cubic(SC) and close cubic(CC)cells

Results shown in Fig 8.

Results fit with rational functions, Eq. 26 coefficients in Table 1, rows 2 and 3

For other pore fractions, linear interpolation between SC and CC results, Eq. 28

I did fit to CO<sub>2</sub> gas measurements of Johnston46=[36] with form  $\ln \lambda = a + b \ln T$ ; get  $\lambda = 5.46772e - 06T^{1.407266}$  This agrees closely with http://encyclopedia.airliquide.com/Encyclopedia.asp?GasID=26 thermal conductivity (1.013 bar and 0 C ): 14.65 mW/(m.K)

Can call **sp09a** for any set of:

Temperature: negative yields default set [150.,230.,315] Grain radius in micrometer: negative yields default set [10.,50.,200.] Pressure in torr: negative yields default set [0.5,5,10.]

Optional Pore fraction: negative yields default set [0.30,0.35,0.4,0.45]

absence yields 0.35

16 output items for each set of input conditions:

i	name	value	Description
-2	kcontact	0.0000	Contact conductivity; assumed
-1	kgrain	0.93700	Solid grain conductivity; assumed
0	R um	100.00	Grain radius, micrometer. Input
1	Phi	0.35000	Porosity. Input
2	T	240.00	Temperature, K. Input
3	Pa	500.00	Pressure, Pa. Input
4	MFP	7.0493e-06	Mean Free path, m. Eq 7
5	KO	0.012183	Bulk gas conductivity. Eq 14
6	Pore	8.1523e-05	Typical length of Pore. Eq 11
7	Kn	0.086470	Knudsen Number, Eq 7
8	xi	-1.9761	Exponent in kgas. Eq 29,30,31
9	Kgas	0.0014831	Gas thermal conductitivy, Eq. 32
10	KeffCC	0.015480	Effective gas conductivity, close cubic Eq 25
11	KeffSC	0.049761	Effective gas conductivity, simple cubic
12	keff	0.029856	Effective gas conductivity, interpolated to porosity Eq 27
13	krad	0.00036468	Radiative part of conductivity
14	knet	0.030221	Total conductivity
15	kVasa	0.0013620	Vasavada 99 relation for radiative term

Sample results, default radii set:  $10 \ \mu m$  to  $50 \ mm$ 

```
Tmin,Tmax, Tdel= 120.000 320.000 20.0000
   Grain Cp > 581.3780 198.1888 -52.2628 12.0520 <Sphene

1000|err| c0 c1 c2 c3 Ind.Param
0 0.02347 > 0.008292 0.001725 -0.000119 0.000019 < 10.0</pre>
```

```
1
   0.03971 >
              0.012572
                        0.002880 -0.000214
                                            0.000038 <
                                                               20.0
 2
   0.07774 >
              0.021995
                        0.005493 -0.000459
                                            0.000096 <
                                                               50.0
                        0.008660 -0.000788
 3
   0.11164 >
              0.032834
                                            0.000183 <
                                                               100.
 4
   0.12810 >
              0.047054
                        0.013195 -0.001242
                                            0.000320 <
                                                               200.
 5
   0.10286 >
              0.069647
                        0.021717 -0.001770
                                            0.000553 <
                                                               500.
 6
   0.06743 >
              0.087617
                        0.030218 -0.001627
                                            0.000740 <
                                                           1.00e+03
 7
   0.03380 >
              0.104917
                        0.040653 -0.000353 0.000983 <
                                                           2.00e+03
 8
   0.04042 >
              0.127544
                        0.059495
                                   0.004676
                                             0.001686 <
                                                           5.00e+03
9
   0.05149 >
                        0.082637
                                   0.013420
                                             0.002938 <
              0.148618
                                                           1.00e+04
10
   0.05040 >
              0.181254
                        0.123653
                                  0.030915
                                             0.005528 <
                                                           2.00e+04
   0.03781 >
              0.268984
                        0.240701
                                  0.083247
                                             0.013403 <
                                                           5.00e+04
         T 120.0 140.0 160.0 180.0 200.0 220.0 240.0 260.0 280.0 300.0 320.0
 GasK*1000
            4.8
                   5.9
                         7.0
                               8.2
                                     9.5
                                         10.8
                                               12.2
                                                     13.6
                                                            15.1
            0.9
                   0.9
                         0.9
                               0.9
                                     0.9
                                           0.9
                                                 0.9
                                                       0.9
                                                             0.9
  Grain k
                                                                   0.9
 Grain Cp 318.9 383.2 441.0 493.0 539.6 581.4 619.0 653.1 684.1 712.7 739.4
Ind.Param
               _____ Thermal inertia ____
           56.6
                 63.9 70.4 76.4 81.8 86.7 91.3 95.6 99.6 103.3 106.9
      20.0 68.5 77.7 86.0 93.6 100.4 106.8 112.6 118.1 123.2 128.1 132.7
      50.0 89.1 101.6 112.9 123.1 132.6 141.2 149.3 156.8 163.8 170.5 176.9
      100. 107.4 123.0 137.1 149.9 161.7 172.6 182.6 192.0 200.8 209.2 217.2
      200. 126.8 145.8 163.0 178.8 193.2 206.6 219.0 230.5 241.4 251.7 261.6
      500. 150.6 174.4 196.0 216.0 234.3 251.3 267.2 282.0 296.1 309.5 322.5
  1.00e+03 165.5 192.6 217.5 240.5 261.9 281.9 300.6 318.4 335.3 351.5 367.3
  2.00e+03 176.9 207.0 234.9 260.9 285.4 308.5 330.4 351.4 371.6 391.3 410.6
  5.00e+03 188.0 221.5 253.2 283.3 312.2 340.1 367.2 393.8 420.0 446.1 472.3
  1.00e+04 195.0 231.4 266.5 300.6 334.1 367.1 400.0 433.0 466.2 499.9 534.4
  2.00e+04 203.2 243.6 283.7 323.9 364.3 405.4 447.4 490.4 534.6 580.2 627.5
  5.00e+04 220.9 271.0 323.0 377.4 434.3 493.9 556.4 621.7 690.1 761.6 836.3
```

### 6.1.1 SPSPREAD: Piqueux Spreadsheet for cemented particles. OBSOLETE

Reverse engineer Sylvain Piqueux thermal conductivity spreadsheet emailed 2008nov11 and described in a two-page 2008nov16 email from him, into IDL. Also coding of his two-page equations explicitly.

Can call with same flexability of inputs as **sp09a**. Output array(row,19) of all the spreadsheet columns in order. Rows are formed by looping over the above four parameters, pore fraction fastest, temperature slowest. Internally:

 $\tt ddd$  are values based on reverse engineering of spreadsheet

Then reformatted for gg

www are values based on 2-page writeup.

If dbug is set, will print all results for the first row. Then prints a comparison of spreadsheet versus writeup: starting at -1, columns of

i: Row count

labw[i]: Piqueux ID of computed parameter

 $www[0,i] \colon values \ for \ first \ row$ 

qq[i]: gg[0,select], based on 2-page writeup

labp[ii[i]]: Brief ID of item ii[i]: Location in gg

Some disagreements between spreadsheet and writeup:

 $k_0$ : Eq 1. versus Column E in 2nd version

 $k_{gas}$ : Eq. 5 versus column O of first version. (not in 2nd)

### 6.1.2 Calling from koftop

Parr 1 through 8 set inputs to particulate models.

parr[0] sets grain radius, or negative invokes a large set

parr[5] sets cement volume, or negative invokes a large set

An inner loop runs through a range of temperatures, replacing the bulk materials  $C_P$  and  $\lambda$  with values derived

above, and outer loop run over a range of grain sizes.

Results for a wide range of grain sizes are shown in Figure 6; these are at porosity=.35 and pressure of 500 Pa.

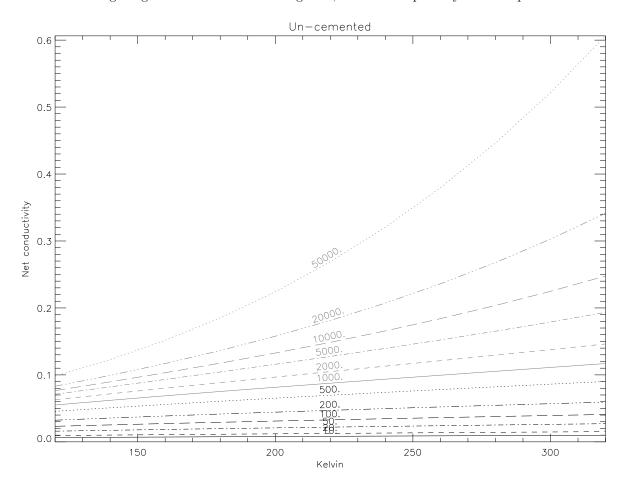


Figure 6: Results the Piqueux un-cemented particulate model. Grain size ranges from 10  $\mu$ m to 50 mm. The grain conductivity is a constant

### 6.2 PARTCOND: Kieffer analytic model for cemented particles

The IDL routine **partcond.pro** implements the model of cemented particles described in Kieffer09=[38] [available upon request]. This routine requires a gas conductivity, which is obtained by calling **PP\_CO2** and selecting the Hilsenrath60=[26] relation given by Piqueux09a=[50].

Input parameters are defined under 13: PARTCOND in  $\S 5.2$ . Lacking good  $C_P$  values for carbonates, I choose to use the values for clinclore: Fe=0.89 based upon its similarity with limestone near 300K.

### partcond is written as a large case statement

konc=[16,43,-4]; return [vol,knet] 16 modify values 20: [auto] begin; Set limits and constants 43: Numerical integration for all B; first evaluate the parts: cement, gas, radiation, for all radii; Then integrate the cement outward and the others inward; Sum to get the results for all values of B

returns [nB,2] where 0]=volume fraction cement, 1]=net conductivity, and nB is the total number of cement contact angles =parm[12]+parm[13]

Sample results; 10 ppb to 10% cement volume

```
Grain Cp >
                            581.3780 198.1888
                                                                      -52.2628
                                                                                             12.0520 < Sphene
                                                                                         -39.3450 < clinclore:Fe=0.89
  Cement Cp >
                            636.1573
                                                 272.5468
                                                                      -28.1283
    1000|err|
                                     c0
                                                          c1
                                                                               c2
                                                                                                   с3
                                                                                                                      Ind.Param
       0.12972 >
                              0.114758
                                                   0.030359
                                                                       0.002328 -0.001066 <
                                                                                                                          1.00e-08
       0.07328 >
                              0.183835
                                                   0.016928 0.007453 -0.002852 <
  1
                                                                                                                          1.00e-06
      0.04431 >
                              0.256925 0.002279 0.013186 -0.004888 <
                                                                                                                          1.00e-05
       0.05256 >
                              0.388408 -0.026003 0.024181 -0.008647 <
                                                                                                                          0.000100
                              4
       0.02827 >
                                                                                                                            0.00100
  5
       0.03033 >
                              1.098480 -0.189480 0.080076 -0.026705 <
                                                                                                                              0.0100
  6
      0.03544 >
                              1.305149 -0.236999 0.095629 -0.031734 <
                                                                                                                              0.0200
  7
        0.04390 >
                              1.650960 -0.316747
                                                                        0.121512 -0.039990 <
                                                                                                                               0.0500
  8 0.05213 >
                              1.989642 -0.395644
                                                                        0.146817 -0.047868 <
                                                                                                                                 0.100
Doing ---->
                                                        75
                  T 120.0 140.0 160.0 180.0 200.0 220.0 240.0 260.0 280.0 300.0 320.0
                                                                                                               13.6
                                                                                                                            15.1
  GasK*1000
                           4.8
                                       5.9
                                                   7.0
                                                                8.2
                                                                            9.5
                                                                                     10.8
                                                                                                  12.2
                                                                                                                                        16.6 18.1
    Grain k
                          3.6
                                       3.4
                                                   3.2
                                                                3.0
                                                                            2.9
                                                                                         2.8
                                                                                                     2.7
                                                                                                                  2.6
                                                                                                                               2.5
                                                                                                                                           2.4
                                                                                                                                                       2.4
                          5.5
                                                                4.4
                                                                            4.1
                                                                                         3.8
                                                                                                     3.5
                                                                                                                  3.3
                                                                                                                               3.1
                                                                                                                                           3.0
                                                                                                                                                       2.8
    Cement k
                                       5.1
                                                   4.7
  Grain Cp 318.9 383.2 441.0 493.0 539.6 581.4 619.0 653.1 684.1 712.7 739.4
  Cement Cp 374.8 420.3 471.0 525.2 580.8 636.2 689.2 738.2 781.1 816.0 841.2
Ind.Param _____ Thermal inertia _____
    1.00e-08 187.6 211.1 232.7 252.8 271.7 289.7 306.8 323.2 339.0 354.2 368.9
    1.00e-06 266.6 291.7 313.3 332.6 350.2 366.6 382.1 396.7 410.7 424.1 437.0
    1.00e-05 330.7 358.1 380.7 400.3 417.6 433.4 448.1 461.8 474.7 487.1 498.7
    0.000100 423.5 454.8 479.6 500.0 517.5 532.9 546.9 559.7 571.5 582.6 592.8
      0.00100 559.4 597.2 626.0 648.7 667.1 682.7 696.2 708.1 718.8 728.3 736.8
        0.0100\ 753.3\ 801.2\ 836.7\ 863.8\ 884.9\ 902.0\ 916.0\ 927.7\ 937.6\ 945.8\ 952.4
        0.0200\ 830.0\ 881.6\ 919.9\ 948.9\ 971.4\ 989.41004.01016.01025.91033.91039.9
        0.0500\ 956.61013.61056.01088.41113.51133.51149.51162.51172.81180.61185.9
          0.1001087.31148.31194.61230.41258.51281.01299.11313.61324.71332.71337.21231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.012311.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231.01231
```

### Calling from koftop

2 0.00000 >

3 0.00000 >

Grain and cement materials = BasicRocks

1.107043

2.004842

The program koftop can call partcond with temperature-dependent (cubic in T) conductivity for the solids (grains and cement). Using the relations for BasicRocks for grains and Limestone for cement yields the results in Figure 7. The cubic coefficient values for the solids and cemented mix are:

limestone

```
Tmin,Tmax, Tdel=
                      120.000
                                    320.000
                                                 20.0000
    sigResid
                      c0
                                                   c2
                                                                сЗ
                                                                           cem.Vol
                                     с1
BasicRocks >
                   2.797455
                                -0.5733288
                                               0.1525714
                                                            -0.01708314 <
 limestone >
                                                            -0.03867132 <
                   3.791455
                                 -1.297852
                                               0.3453778
 0 0.00002 >
                              -0.03036693
                                                          -0.002487207 < 0.000100
                  0.3911251
                                              0.01817816
                                                          -0.004121674 < 0.001000
 1 0.00001 >
                  0.6414463
                              -0.09064570
                                              0.03389244
                                                          -0.006863785 < 0.010000
   0.00001 >
                   1.107040
                                -0.2033801
                                              0.06119198
 3 0.00001 >
                   2.004835
                                -0.4204147
                                               0.1133001
                                                           -0.01237263 < 0.100000
Setting the solid temperature dependence to zero yields nearly T-independent behavior \begin{verbatim}
    sigResid
                      c0
                                     c1
                                                   c2
                                                                сЗ
                                                                           cem.Vol
BasicRocks >
                   2.797455
                                  0.000000
                                                0.000000
                                                               0.000000 <
  limestone >
                   3.791455
                                  0.000000
                                                0.000000
                                                               0.000000 <
 0 0.00001 >
                  0.3911375
                                0.03798161
                                             0.001679920 - 0.0004527534 < 0.000100
 1 0.00001 >
                  0.6414520
                                0.03236581
                                             0.002237705 - 0.0004111509 < 0.001000
                               0.02312554
```

0.01198547

0.002075447 - 0.0002425569 < 0.010000

0.001259117 -9.197257e-05 < 0.100000

Results for a wide range of cement volumes are shown in Figure 7; the corresponding thermal inertias are in Figure 8. The opposing slopes in these two figures is the result of the temperature dependence of specific heat being the larger effect.

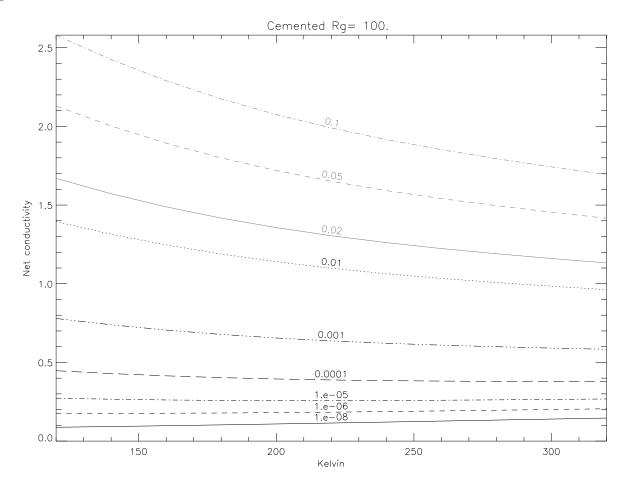


Figure 7: Thermal conductivity results using temperature-dependent solids in the Kieffer cemented particulate model. Cement volume fraction ranges from 10 ppb to 10%. If the temperature dependance of the solids conductivity, but not the gas, is set to zero, net conductivity increases slightly with temperature; 10% for 0.1% cement[Dashed lines on color version only.] cemk.eps

# 7 Papers on hand

Articles that I could find and access through the ASU system. and a few articles on lunar surface materials for which I had hard-copy.

### 7.1 Rocks and minerals

 $\begin{tabular}{l} Abdul06=[1], Andersson94=[2], Aurangzeb07=[4], vdBerg01=[68], Berman85=[5], Bertoldi01=[6], Bertoldi05=[8] \\ Bertoldi07=[7], Birch40=[10], Birch40b=[9], Clauser95=[15], Cahill89=[11], Cahill92=[12], Carruthers92=[13], \\ Cermak82=[16], Fountain70=[19], Ghormley68=[20], Giauque36=[21], Giesting02=[22], Glassbrenner64=[23], \\ Haida74=[24], Heuze83=[25], Hofmeister01=[28], Hofmeister04=[31], Hofmeister06=[29], Hofmeister07=[30] \\ Horai69=[34], Horai70b=[35], Kanamori68=[37], SWKieffer79=[39], Klug91=[42], Ledlow92=[44], McGaughey04=[46], \\ Mottaghy08=[47], Petrunin95=[49], Popov03=[52], Presley97=[53], Presley97b=[54], Pribnow93=[55], \\ Sass71=[58], Sass84=[59], Seipold98=[63], Seipold98g=[62], Slack80=[64], Sugasaki68=[66], \\ Vosteen03=[70], Waples04=[71], Whittington09=[72], Yamamuro87=[73] \\ \end{tabular}$ 

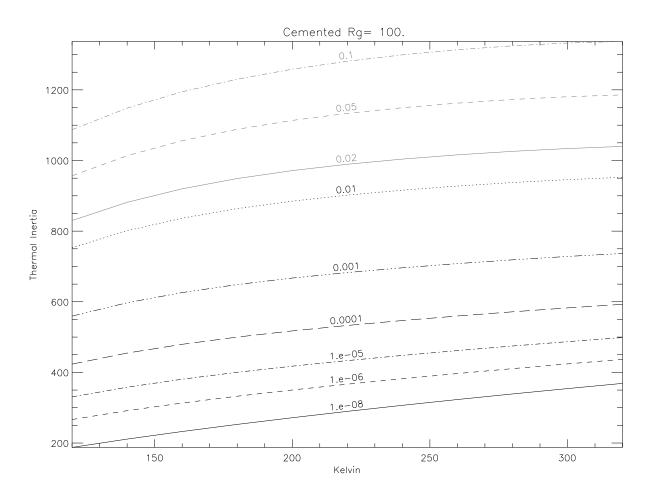


Figure 8: Thermal inertia results using temperature-dependent solids in the Kieffer cemented particulate model. Cement volume fraction ranges from 10 ppb to 10%. cemi.eps

These files are in /work2/rockReprints/; the file names are typically first author name followed by the last two digits of the year.

I found no access to, or only abstracts for: Cermak82=[16], Chai96=[14], Diment88=[18], Jessop 2008, Linvill84=[45], Robie68=[56], Yang94=[74]

### 7.2 Carbon dioxide gas

Articles on gas conductivity:

Johnston46=[36] has original measurements. I have used these in IDL routine pp\_co2.pro

Vesovic90=[69] is synthesis addressing high pressures.

Seiferlin96=[61] Used crushed commercial dry ice; results in Fig. 15 suggest  $\lambda$  0.03 to 0.06 W/m-K at 140K . Sumarokov03=[67] Measurements 1.5 to 35K. They show points up to 100 K from L. A. Koloskova, I. N. Krupskii, V. G. Manzhelii, B. Ya. Gorodilov, and Yu. G. Kravchenko, Fiz. Tverd. Tela Leningrad 16,3089 1974 Sov. Phys. Solid State 16, 1993 1975 (Amer. Inst. Phys indicates available, but I can't locate)

Scalabrin06=[60] Develop 30-term (6 are zero) function to fit massive set of observations from the literature. Eq. 7 with coefficents in Table 3; validity range 216.59-1000K, up to 200 Mpa. Table 11 has three low pressure (0.01MPa) points at 225,250,275K; 11.037 12.849, 14.727 mW m-1 K-1. Figure 5 indicates that Johnston and Grilly have quadratic deviation from this new relation, +3.2% at 186K, 0 at about 280, +1.9% at 380. This is similar form, but about twice the magnitude, of deviation from my fit using  $\ln \lambda = a + b * \ln T$ 

Konstan06=[43] shows large decrease in  $\lambda$  of solid CO<sub>2</sub> with a few percent inert gas as solid solution. Although

their work at 140Mpa, the physical explanation seems relevent for CO<sub>2</sub>/ Ar on Mars.

### 8 Random notes during literature search

Aurangzeb07=[4] present  $\rho C_P$  for limestone over 293:443K, but the figure is difficult to follow and the errors are stated to be 10%. The average value of  $C_P$  at 293K is about 880.

Slack71=[65] Fig. 2 shows conductivity for 5 natural garnets, Table V lists the measured values for Grossularite, which had the highest values In Waples, neither Fig 13 or 14 seems to agree with equation 18

Pribnow93=[55] has short table of conductivities, uses linear and harmonic means, weighting by volume fraction, as upper and lower limits for mixtures.

$$\lambda_u = \sum_{i=1}^n \phi_i \lambda_i$$
 and  $\frac{1}{\lambda_L} = \sum_{i=1}^n \frac{\phi_i}{\lambda_i}$  and  $\lambda_G = \sqrt{\lambda_U \lambda_L}$ 

Following Sass71, for a two phase system (cuttings in water), uses

$$\lambda_r = \lambda_w \left(\frac{\lambda_m}{\lambda_w}\right)^{\frac{1}{1-\phi}}$$

where  $\lambda_w$  is thermal conductivity of water,  $\lambda_m$  thermal conductivity of the mixture,  $\phi$  the volume fraction of water in the mixture, and  $\lambda_r$  the thermal conductivity of the dry rock. And then the square-root of their product as a general representation

Title CRC handbook of physical properties of rocks. Volume III Creator/Author Carmichael, R.S. Publication Date 1984 Jan 01 No access

The estimation of rock thermal conductivity from mineral content: an ... MJ Drury, AM Jessop - Zentralbl. Geol. Palaeontol, 1983 No access

```
99577 Bertoldi01.pdf http://www.springerlink.com/content/mea9vg4j4363vmx8/
1957679 ClauserHuenges95.pdf http://www.geophysik.rwth-aachen.de/html/publikationen.htm
882459 vasavada99merc.pdf
370463 Vosteen03.pdf 0-500C conductivity \lambda Eq 4,5
```

 $Yang 94 = [74] \ no\ access. Thermal\ expansion\ properties\ of\ synthetic\ orthopyroxenes\ (Fe 0.20 Mg 0.80) SiO3\ , (Fe 0.40 Mg 0.60) SiO3\ , (Fe 0.50 Mg 0.50) SiO3\ , (Fe 0.75 Mg 0.25) SiO3\ and\ (Fe 0.83 Mg 0.17) SiO3\ from\ 296\ to\ 1300 K.\ ...\ The\ thermal\ Debye\ temperatures\ are\ composition-dependent\ , decreasing\ linearly\ from\ 812\ (Mg SiO3)\ to\ 561\ K\ (Fe SiO3)\ , and\ are\ systematically\ higher\ than\ the\ corresponding\ acoustic\ Debye\ temperatures\ .$ 

Eventually located Birch40=[10]. Figs 2,3,4 show approximate 1/T for several minerals and rocks. Fig 5 shows Anorthosite and gabbro nearly independent of T, Fig 6 shows k of silica glass, increasing nearly linear over 50-300C

For the first time this notion was introduced by the German physicist Paul Debye to express the connection between heat capacity of poly-atomic solid and its elastic coefficient.

$$(C_v)_{T\to 0} = 77.938 \cdot 3R \left(\frac{T}{\theta}\right)^3$$

where:  $C_v$ - substance heat capacity, R gas constant, T absolute temperature.

The Debye temperature is constant for a given (present) substance, and defines the maximum frequency in the spectrum of particle vibration of the solid.  $\theta = \frac{h\nu_{max}}{k}$ 

h Planck's constant, k Boltzmann's constant,  $\nu_{max}$  maximal frequency of vibration of solid.

http://journals.lww.com/soilsci/Citation/1962/12000/

Specific\_Heat\_Capacity\_of\_Soils\_and\_Minerals\_As.7.aspx

Specific Heat Capacity of Soils and Minerals As Determined With A Radiation Calorimeter BOWERS, S. A.; HANKS, R. J.

Soil Science: December 1962 - Volume 94 - Issue 6 - ppg 392-396

http://ccm.geoscienceworld.org/cgi/content/abstract/53/4/380

Bertoldi05=[8]

 $C_p = 610.72 - 5140.0xT^{-0.5} - 5.88486x10e6T^{-2} + 9.5444x10e8T^{-3}$  is recommended for thermodynamic calculations above 298 K involving berthierine.

Bertoldi07=[7] 40 to 40 temperature points from 5 to 300K with logarithmic spacing, smoothed into Table 2 covering 5-900K

Determination of specific heat capacity on rock fragments Ueli Schrli and Ladislaus Rybach Geothermics Volume 30, Issue 1, February 2001, Pages 93-110

Cermk, V., Rybach, L., 1982. Thermal properties. In: Angenheister, G. (Ed.), Landolt-Brnstein, Numerical Data and Functional Relationships in Science and Technology, Vol. 1a: Physical Properties of Rocks, Springer-Verlag, Berlin, pp. 305-343.

Touloukian, Y.S., Roy, R.F., Beck, A.E., 1981. Thermophysical properties of rocks. In: Touloukian, Y.S., Ho, C.Y. (Eds.), Physical Properties of Rocks and Minerals. Cindas data series on material properties, Vol. II-2, pp. 409-502.

Thermodynamic properties of minerals and related substances at 298.15 K and 1 bar (10/sup 5/ pascals) pressure and at higher temperatures Robie, R.A.; Hemingway, B.S.; Fisher, J.R. 1978 USGS-BULL-1452

Heat capacity, relative enthalpy, and calorimetric entropy of silicate minerals; an empirical method of prediction Gilpin R. Robinson, and John L. Haas
American Mineralogist; June 1983; v. 68; no. 5-6; p. 541-553

SUPCRT92: a software package for calculating the standard molal thermodynamic properties of minerals, gases, aqueous species, and reactions from 1 to 5000 bar and 0 to 1000 degree C.

Johnson, James W | Oelkers, Eric H | Helgeson, Harold C Computers & Geosciences. Vol. 18, no. 7, pp. 899-947. 1992 in Fortran, SPRONS92.DAT, database

followup: http://www.geology.wisc.edu/flincs/fi/disc/supcrt.html

JAMES W. JOHNSON, ERIC H. OELKERS, and HAROLD C. HELGESON
Earth Sciences Department, L-219, Lawrence Livermore National Laboratory,
Livermore, CA 94550 and Laboratory of Theoretical Geochemistry,
Department of Geology and Geophysics, University of California,
Berkeley, CA 94720, U.S.A.

Need to login: Soil Science

Christian.Bertholdi@sbg.ac.at Universitat Salzburg bottom page 381

standard entropy: $S_o = \int_0^{298.15} \frac{C_p}{T} dT$ 

bottom page 381 ... low-T Cp-T data into three parts fitting each to a  $C_p$  polynomial of the form:  $Cp = ko + k1T^{-0.5} + k2T^{-2} + k3T^{-3}(+k4T + k5T^2 + k6T^3)$ 

http://hyperphysics.phy-astr.gsu.edu/Hbase/solids/phonon.html#c2

Derived Debye specific heat (also in Kittel Eq.31)

$$U = \frac{9NkT^4}{T_D^3} \int_0^{T_D/T} \frac{x^3}{e^x - 1} dx$$

 $C_v = 9Nk \left[\frac{T}{T_D}\right]^3 \int_0^{T_D/T} \frac{x^4 e^x}{(e^x - 1)^2} dx$  where  $T_D$  is the Debye temperature for a material.

Law of Dulong and Petit: Upper limit is:  $C_v = 3kN_A = 24.94$  / mole K

### 8.1 SWK

SWKieffer79=[39]

 $C_v = C_p - TV\epsilon^2 B$  3 Eq 29 where:  $\epsilon$  is the volume coefficient of thermal expansion. B is the bulk modulus and V is the specific volume. Many in Clark[1966]

 $(C_P - C_V)/C_V$  generally i 1% at 100K and about 4% at 700K. Exception is halite, about 5% at 300K (page 43.8b)

### 8.2 Palankovski Dissertation

Palankovski00=[48]

Simulation of Heterojunction Bipolar Transistors

Vassil Palankovski Dec. 2002

http://www.iue.tuwien.ac.at/phd/palankovski/node34.html

### 8.2.1 3.2.4 Thermal Conductivity

The temperature dependence of the basic materials and insulators is modeled by a simple power law

$$\kappa_{\rm L}(T_{\rm L}) = \kappa_{300} \cdot \left(\frac{T_{\rm L}}{300{\rm K}}\right)^{\alpha}$$

Table 3.5: Parameter values for thermal conductivity

Material  $\kappa_{300}$  [W/K m]  $\alpha$  Reported  $\kappa_{300}$  [W/K m] References

 $SiO_2$  1.38 0.33 1.4 [85,86]

### **8.2.2 3.2.4** Specific heat

The specific heat capacity  $c_{\rm L}$  is modeled by:

$$c_{\rm L}(T_{\rm L}) = c_{300} + c_1 \cdot \frac{X - 1}{X + \frac{c_1}{c_{300}}}$$

where 
$$X = \left(\frac{T_L}{300\text{K}}\right)^{\beta}$$

Parameter values for the specific heat

Material  $c_{300}$  [J/K kg]  $c_1$  [J/K kg]  $\beta$  Reported  $c_{300}$  [J/K kg] References

 $SiO_2$  709 696 1.5 1000

### 8.3 From Vosteen 2003 Section 4:

in abstract, T in C., k in W / m / K

$$\lambda(T) = \frac{\lambda(0)}{0.99 + T(a - b/\lambda(0))} \qquad \text{eq: V3}$$

0-500C for crystalline  $a=0.0030\pm0.0015$ ,  $b=0.0042\pm0.0006$ 0-300C for sedimentary:  $a=0.0043\pm0.0006$ ,  $b=0.0039\pm0.0014$ 

Vosteen03=[70] Section 4: cite Zoth88=[75] who suggest form  $k(T) = \frac{A}{350+T} + B$ 

Zoth88=[75] Manage to display using Google books.

### 8.3.1 Mottaghy08

Mottaghy08.pdf Mottaghy08=[47]

They cite for Vosteen 03: using Kx for  $\lambda(x)$ 

for crystalline, alpine rocks:  $K0 = 0.53K25 + \frac{1}{2}\sqrt{1.13K25^2 - 0.42K25}$ , using Eq. 1

For Kola samples:  $K0 = 0.52K25 + \frac{1}{2}\sqrt{1.09K25^2 - 0.36K25}$ , and Eq. 1 is modified slightly in that the constant is 0.99.

Table 2 has k,  $\rho$ , and  $C_P$  for 7 rocks, presumably at 25C.

Cite Seipold98=[63] for:  $\kappa(T) = 1/(A+BT) + CT^3$ ;  $10^{-6} \text{ m}^2 \text{ s}^{-1}$ 

A=1.25, B=2.13E-3 C=1.25E-10 for amphibolite MUST BE WRONG

A=0.779, B=2.55E-3, C=1.15E-10 for paragneiss

However, in Seipold98=[63] have: thermal diffusivity of amphibolites result in  $(0.8 \ 0.2)$  E-6 m<sup>2</sup> s<sup>-1</sup> under ambient conditions.

Form:  $\lambda = 1/(A + BT) + CT^3$ , T in C.

Fig 5: shows steeper Tc dependence for paragneiss A=0.282~B=6.17E-4~C=1.91E-9. values at 200C about 2.4, checked relation

Fig 6: Amphibolite A=0.378 B=1.96 E-4 C=0.24 E-9 values at 200C about 2.4

Seipold98g=[62] tries several simple modifications of the Eucken law

WLF1:  $K \equiv \lambda = 1/(A + BT)$ 

WLF2:  $K = 1/(A' + B'T) + C'T^3$ 

WLF3:  $K = D'/T^n$ 

WLF4: K = T/(E + FT)

Table 1 has A and B for 8 rock types. They state extrapolation better with WLF4 than WLF1. Form WLF1 is better for thermal diffusivity

Makes an error in treating  $T^3$  as a radiation term when T is in  ${}^{\circ}$ C

### 8.4 Clauser & Huenges 1995

Clauser95 = [15]

http://www.geophysik.rwth-aachen.de/html/publikationen.htm has clauser pubs

page 110: Zoth & Hanel (1988)  $\Lambda(T)=A+\frac{B}{350+Tk}$  Eq. 3a Zoth88 derived, using form K=X/(Tc+77)+Y, with X,Y, High T= \qi 474., 1.18, 1100 for basic rocks Fig 10.5

```
\qi 807 0.64, 1300 for acid rocks Fig 10.4
\qi 705,0.75, 1200 for metamorphic Fig 10.3
\qi 1073,0.13, 500 for limestones Fig 10.2
\qi 2960,-2.11, 350 salt rocks Fig 10.1
\qi 1293,0.73, 1380 Ultra basics Fig 10.6
```

page 112: Values of A and B for Eq 3a nearly all OC and higher

Buntebarth(1991) 1/k = D+ET Eq 3b

metamorphics: D=0.16+- 0.03 m K W E=0.37+-0.03 mK/W

Sass et al(1992) propose empirical relation:

$$\lambda \equiv k(T) = \frac{\lambda(0)}{1.007 + T\left(0.0036 - \frac{0.0072}{\lambda(0)}\right)}$$
 where  $\lambda(0) = \lambda(25) \left[1.007 + 25\left(0.0037 - \frac{0.0074}{\lambda(25)}\right)\right]$ 

### 8.5 Other papers

Although some papers propose models by which k can be derived from vibration spectra, e.g. Giesting02=[22], I did not code up these models.

Aurang08=[3] aurangzebbabar@yahoo.com

The thermal conductivity, thermal diffusivity, and heat capacity per unit volume of dunite rocks taken from Chillas near Gilgit, Pakistan, have been measured simultaneously using the transient plane source technique. The temperature dependence of the thermal transport properties was studied in the temperature range from 303 K to 483 K. Different relations for the estimation of the thermal conductivity are applied. A proposed model for the prediction of the thermal conductivity as a function of temperature is also given. It is observed that the values of the effective thermal conductivity predicted by the proposed model are in agreement with the experimental thermal conductivity data within 9%.

Several papers by Anne Hofmeister, Hofmeister99=[27], Hofmeister06=[29], Hofmeister07=[30]

Hofmeister01=[28]; Eq. 19 indicates k proportional to Cv

Hofmeister04pre. high-temperature partial derivative of k. Separates lattice from radiation.

Hofmeister06 Fig 7 has k(t) for Grossular derived from diffusivity, density and specific heat 0-1500K. k for Grossular peaks near 100, Pyrope 250K uses form  $D = A + B/T + C/T^2$ , but says later that at moderate temperatures  $1/D = A + BT + CT^2$  is best representation.

Hofmeister07 Concentrates on diffusivity

Hofmeister, A.; Whittington, A. G.; Nabelek, P. I. Not attained

Horai70b=[35] cites Birch40 for thermal resistivity linear with temperature, and gives coefficients for 7 rocks in Table 2.  $R \equiv 1/K = a + b(T - 300)$ , R in cm sec deg /cal, T in K

Horai71=[32] Has table of many minerals, but no discussion of T-dependence.

Roufosse74=[57] Theory only; says lattice component (versus radiative component) of minerals should follow  $\lambda \propto 1/T$ 

Models of thermal conductivity of crystalline rocks. Alan M. Jessop International Journal of Earth Sciences Volume 97, Number 2 / April, 2008 Terrestrial heat flow: Recent advances in modeling and interpretation % ASU not registered

Abdul06=[1] measures thermal conductivity of sandstone, limestone, amphibolite, granulite, and pyroxene-granulite over 273-473K and up to 1500MPa. Data at every 100C in Table 1. However, values for granulite, and pyroxene-

granulite are identical at all T and P, where as Figs 3 4 shows pyroxene-granulite with much higher k and consistent; I use the later.

Giesting02=[22]k calculated from spectra, modified Debye. No figures nor tables of k versus T. Table III of k does not list temperature

vdBerg01=[68] Eq 1 is from: Hofmeister99=[27]

$$k(T, P) = k_0 (298/T)^a \exp\left[-(4\gamma + 1/3)\alpha(T - 298)\right] \left(1 + \frac{K_0'P}{K_0}\right) + \sum_{i=0}^3 b_i T^i$$

where  $k_0 = 4.7$  W K<sup>-1</sup>m<sup>-1</sup>, T is in Kelvin, Grueneisen parameter  $\gamma = 1.2$ , thermal expansivity  $\alpha = 2.0$ E-5 K<sup>-1</sup>, the bulk modulus  $K_0 = 261$  GPa, pressure derivative of bulk modulus  $K'_0 = 5$ . Radiative contribution given by coeff.  $b_i$  from least squares fit to spectra of overtones. The fitting parameter a is 0.9 for oxides and 0.3 to 0.4 for silicates.

Cahill89=[11] Zr-, Hf, Y-doped and Y<sub>66</sub> boron crystals measured from 30K to 1000K

Cahill92=[12] Measures from 30K to ambient using  $3\omega$  method[19]. Mostly non-geologic materials, but has several feldspars, data from Linvill. Largest conductivity for nearly pure Albite, Ab<sub>99</sub>An<sub>1</sub>

M.L. Linvill 1987, unpublished PhD thesis, Cornell University

I could not find in Cornell Library search

Also: M.L. Linvill R.O. Pohl, in Thermal conductivity 18 (Ed. T.Ashworth and D.R. Smith) 1985, p653

Also: M.L. Linvill and J.W. Vandersande and R.O. Pohl, Thermal conductivity of feldspars. Bulletin de Mineralogie. 107,p521-527, 1984

The thermal conductivity of several alkali and plagioclase feldspars was measured over the range 0.3-500 K. Between 10 and 100 K the conductivity decreases by over one order of magnitude from albite to bytownite. In some of the feldspars, the conductivity above 100 K approaches that of glass of composition Ab50An50, indicating very strong phonon scattering. It is tentatively suggested that this scattering occurs at lamellar structures with a spacing of tens of A found within intergrowths in feldspars.-R.A.H.

The Bulletin de Minralogie ceased publication in 1989. Along with the S.F.M.C., the D.M.G. (Deutsche Mineralogische Gesellschaft) and the S.I.M.P. (Societ Italiana di Mineralogia e Petrologia) renounced to their national publications and launched the European Journal of Mineralogy.

Cited by: Abdulagatov, I.M., Emirov, S.N., Abdulagatova, Z.Z. Effect of pressure and temperature on the thermal conductivity of rocks (2006) Journal of Chemical and Engineering Data and: Ray, L., Forster, H.-J., Schilling, F.R. Thermal diffusivity of felsic to mafic granulites at elevated temperatures (2006) Earth and Planetary Science Letters

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Degiovanni, A. and Andre, S. and Maillet, D. in Thermal Conductivity 22 (ed. Tong, T. W.) 623-633 (Technomic, 1994). Could not find

Richard B. Stephens Intrinsic low-temperature thermal properties of glasses Phys. Rev. B 13, 852-865 1976 All near 1K Joseph Callaway Model for Lattice Thermal Conductivity at Low Temperatures Phys. Rev. 113, 1046-1051, 1959 Germanium. predict roughly proportinal to  $T^-(3/2)$  for normal material but T^-2 for single isotope material in the range 50-100K M. G. Holland Analysis of Lattice Thermal Conductivity Phys. Rev. 132, 2461-2471, 1963 Fit silicon and Germanium, 2-1000K use G.A.Slack & C. Glassbrenner Phys Rev, 120 782,1960 and TBPub M.G.Holland and Neuringer ? Bull. Am. Phys Soc. 8,15,1963 T.T.Geballe & G.W.Hull Phys Rev 110 773 1958 GEORGE S. DIXON and VALENTINA A. STEPHEN and SURINDER K. SAHAI A pulse method for studying thermal transport properties of sedimentary rocks Tectonophysics, 148 (1988) 317-322 limestone diffusivity linear between 20C,11.5 and 130C,7.5 x1.e-3 cm<sup>2</sup>/s Popov03.pdf Include materials from Ries impact structure. http://www.osti.gov/energycitations/product.biblio.jsp?osti\_id=5659536 Lagedrost, J.F.; Capps, W. Creator/Author Publication Date 1983 Dec 01 Thermal expansions ... Associated rocks were from 0.6 to 1.6 percent. Basalts were close to 0.3 percent at 500 C. http://www.britannica.com/EBchecked/topic/505970/rock/80194/Thermal-expansion rock type linear-expansion coefficient (in 1.E-6 per degree Celsius) granite and rhyolite 8 +- 3 andesite and diorite 7 +- 2 basalt, gabbro, diabase 5.4 +- 1 sandstone 10 +- 2 8 +- 4 limestone 7 +- 2 marble 9 +- 1 slate Lindroth, D.P.; Krawza, W.G. Heat content and specific heat of six rock types at temperatures to 1000 C Rep. Invest. - U.S., Bur. Mines; (United States); Journal Volume: 7503

1971 Apr 01 26 pages

Bertoldi01=[6]; Measured 143 to 623 K units= J / mol-K

; fit to Berman and Brown's (1985) form for heat capacities.

Bertoldi07=[7] measured five chlorites of different Fe-Mg composition over 5-303K (data in file Bertoldi07Ap.doc) and presents in Table 2 the smoothed values for  $C_P$  from 5 to 900K for the two end-members.

Stolen, S., Glockner, R., Gronvold, F., Atake, T. and Izumisawa, S. (1996) Heat capacity and nearly stoichiometric wustite from 13 to 450 K. American Mineralogist, 81, 973-981.

Major peak in Cp near 190K

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