TS2 Custom Rate Constants

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1 Introduction

This document builds on the TS1 Custom Rate Constants document, adding treatments for custom rate constant functions used in the TS2 mechanism that are not also present in TS1.

2 Note on [M] in Troe reactions



Figure 1: Example of a Troe reaction in the Chemistry Café.

The species 'M' seems to be included in most (maybe all?) standard Troe reactions as a reactant and a product. However, the CAM preprocessor appears to ignore 'M' as a species, and instead includes it in the calculation of the rate constant:

```
/cam/src/chemistry/pp_trop_strat_mam4_ts2/m_spc_id.F90 (27,27)
     integer, parameter :: id_C2H2 = 25
/cam/src/chemistry/pp_trop_strat_mam4_ts2/m_spc_id.F90 (295,295)
     integer, parameter :: id_OH = 293
/cam/src/chemistry/pp_trop_strat_mam4_ts2/m_rxt_id.F90 (324,324)
     integer, parameter :: rid_C2H2_OH_M = 322
/cam/src/chemistry/pp_trop_strat_mam4_ts2/mo_setrxt.F90 (928,930)
     ko(:) = 5.5e-30_r8
     kinf(:) = 8.3e-13_r8 * itemp(:)**(-2._r8)
     call jpl( rate(:,322), m, 0.6_r8, ko, kinf, n )
/cam/src/chemistry/mozart/mo_jpl.F90 (9,39)
     subroutine jpl( rate, m, factor, ko, kinf, ncol )
        ... Calculate JPL troe rate
     use shr_kind_mod, only : r8 => shr_kind_r8
     implicit none
        ... Dummy args
     integer, intent(in) :: ncol
     real(r8), intent(in) ::
                               factor
     real(r8), intent(in) :: ko(ncol)
     real(r8), intent(in) :: kinf(ncol)
     real(r8), intent(in) ::
                               m(ncol)
     real(r8), intent(out) :: rate(ncol)
     ... Local variables
```

Is it ok to always ignore 'M' as a species in Troe reactions (with it included in the rate constant calculation)?

3 usr_ISOPNO3_NOa and usr_ISOPNO3_NOn

```
/cam/src/chemistry/mozart/mo_usrrxt.F90 (1213,1231)
                      ... ISOPNO3_NOn Temp/Pressure Dependent Nitrate Yield
            _____
                    if( usr_ISOPNO3_NOn_ndx > 0 ) then
                             nyield = (1._r8-0.135_r8)/0.135_r8
                             natom = 9.0_r8
                             exp_natom = exp( natom )
                             acorr = (2.0e-22_r8*exp_natom*2.45e19_r8)/(1._r8+((2.0e-22_r8* & 2.45e19_r8))/(1._r8+((2.0e-22_r8* &
                                                                 exp_natom*2.45e19_r8)/(0.43_r8*(298._r8*(1._r8/293._r8))**8._r8)))* &
                                                                 0.41_r8**(1._r8/(1._r8+(log10((2.0e-22_r8*exp_natom*2.45e19_r8)/ \&
                                                                 (0.43_r8*(298._r8*(1._r8/293._r8))**8._r8)))**2._r8))
                             aterm(:) = (2.0e-22_r8*exp_natom*m(:,k))/(1._r8+((2.0e-22_r8* & 
                                                                 exp_natom*m(:,k))/(0.43_r8*(298._r8*tinv(:))**8._r8)))* &
                                                                 0.41_r8**(1._r8/(1._r8+(log10((2.0e-22_r8*exp_natom*m(:,k)))/ &
                                                                 (0.43_r8*(298._r8*tinv(:))**8._r8)))**2._r8))
                             call comp_exp( exp_fac, 360._r8*tinv, ncol )
                             rxt(:,k,usr_ISOPNO3_NOn_ndx) = 2.7e-12_r8 * exp_fac(:)*aterm(:)/(aterm(:)+acorr*nyield)
                             rxt(:,k,usr_ISOPNO3_NOa_ndx) = 2.7e-12_r8 * exp_fac(:)*acorr*nyield/(aterm(:)+acorr*nyield)
                    end if
```

This appears to be based on eqs (1)–(6) of [1], which define the rate constant for each branch as a function of four parameters (X, Y, Z, n):

$$k_{nitrate} = \left(Xe^{-Y/T}\right) \left(\frac{A(T, [\mathbf{M}], n)}{A(T, [\mathbf{M}], n) + Z}\right)$$

$$k_{alkoxy} = \left(Xe^{-Y/T}\right) \left(\frac{Z}{Z + A(T, [\mathbf{M}], n)}\right)$$

$$A(T, [\mathbf{M}], n) = \frac{2 \times 10^{-22} e^{n} [\mathbf{M}]}{1 + \frac{2 \times 10^{-22} e^{n} [\mathbf{M}]}{0.43(T/298)^{-8}}} 0.41^{(1 + [log(\frac{2 \times 10^{-22} e^{n} [\mathbf{M}]}{0.43(T/298)^{-8}})]^{2})^{-1}}$$
(1)

where T is temperature (K) and [M] is the number density of air (molecules cm⁻³). To retain the detail of the current implementation of these rate constant functions, Z is defined as a function of two parameters (α_0, n) :

Table 1: Wennberg NO + RO₂ rate constant parameters by custom rate constant function name

Function name	X	Y	a_0	n
usr_ISOPB1O2_NO	2.7×10^{-12}	-360	0.14	6
usr_ISOPB4O2_NO	2.7×10^{-12}	-360	0.13	6
usr_ISOPD1O2_NO	2.7×10^{-12}	-360	0.12	6
usr_ISOPD4O2_NO	2.7×10^{-12}	-360	0.12	6
usr_ISOPZD1O2_NO	2.7×10^{-12}	-360	0.12	6
usr_ISOPZD4O2_NO	2.7×10^{-12}	-360	0.12	6
usr_ISOPNO3_NO	2.7×10^{-12}	-360	0.135	9
usr_MVKO2_NO	2.7×10^{-12}	-360	0.04	6
usr_MACRO2_NO	2.7×10^{-12}	-360	0.06	6
usr_IEPOXOO_NO	2.7×10^{-12}	-360	0.025	8
usr_ISOPN1DO2_NO	2.7×10^{-12}	-360	0.084	11
usr_ISOPN2BO2_NO	2.7×10^{-12}	-360	0.065	11
usr_ISOPN3BO2_NO	2.7×10^{-12}	-360	0.053	11
usr_ISOPN4DO2_NO	2.7×10^{-12}	-360	0.165	11
usr_ISOPNBNO3O2_NO	2.7×10^{-12}	-360	0.203	11
usr_ISOPNOOHBO2_NO	2.7×10^{-12}	-360	0.141	12
$usr_ISOPNOOHDO2_NO$	2.7×10^{-12}	-360	0.045	12
usr_NC4CHOO2_NO	2.7×10^{-12}	-360	0.021	11

$$Z(\alpha_0, n) = A(T = 293K, [M] = 2.45 \times 10^{19} \frac{\text{molec}}{\text{cm}^3}, n) \frac{(1 - \alpha_0)}{\alpha_0}$$
 (2)

This reaction has been added to Music Box as WENNBERG_NO_RO2. The usr_ISOPNO3_NOn and usr_ISOPNO3_NOa rate constants can then be calculated according to the above equations with $X=2.7\times 10^{-12},\,Y=-360,\,\alpha_0=0.135,\,$ and $n=9,\,$ with usr_ISOPNO3_NOn corresponding to $k_{nitrate}$ and usr_ISOPNO3_NOa corresponding to k_{alkoxy} .

Similar custom rate constant functions are summarized in Table 1.

4 usr_ISOPZD1O2

This appears to be based on eq. (12) of [1]:

$$k_{tunneling} = Ae^{-B/T}e^{C/T^3} (3)$$

with $A=5.05\times 10^{15},\ B=12200,\ {\rm and}\ C=1\times 10^8.$ This reaction has been added to Music Box as WENNBERG_TUNNELING.

$5 \quad usr_TERPAPAN_M$

```
/cam/src/chemistry/mozart/mo_usrrxt.F90 (971,971)
     call comp_exp( exp_fac, -14000._r8*tinv, ncol )
```

Following the same logic as for usr_PBZNIT_M, the tag_TERPACO3_NO2_ndx reaction is identified as:

```
{
  "type": "TROE",
  "kO_A": 9.7e-29,
  "kO_B": -5.6,
  "kinf_A": 9.3e-12,
  "N": 1.5,
  "reactants": {
     "TERPACO3": { },
     "M": { }
  },
  "products": {
     "TERPAPAN": { },
     "M": { }
  },
}
```

and can be rearranged as a Troe reaction:

$$k = \frac{k_0[M]}{1 + k_0[M]/k_{inf}} F_C^{(1+1/N[log_{10}(k_0[M]/k_{inf})]^2)^{-1}}$$

$$k_0 = A_0 e^{\left(\frac{C_0}{T}\right)} \left(\frac{T}{300}\right)^{B_0}$$

$$k_{inf} = A_{inf} e^{\left(\frac{C_{inf}}{T}\right)} \left(\frac{T}{300}\right)^{B_{inf}}$$
(4)

where $F_C = 0.6$, N = 1.5, $A_0 = 9.7 \times 10^{-29} \times 1.111 \times 10^{28}$, $B_0 = -5.6$, $C_0 = -14000$, $A_{inf} = 9.3 \times 10^{-12} \times 1.111 \times 10^{28}$, $B_{inf} = 0$, and $C_{inf} = -14000$.

6 usr TERPA2PAN M

```
else
    rxt(:,k,usr_TERPA2PAN_M_ndx) = 0._r8
end if
end if
```

Following the same logic as for usr_PBZNIT_M, the tag_TERPA2CO3_NO2_ndx reaction is identified as:

```
{
  "type": "TROE",
  "kO_A": 9.7e-29,
  "kO_B": -5.6,
  "kinf_A": 9.3e-12,
  "N": 1.5,
  "reactants": {
    "TERPA2CO3": { },
    "M": { }
  },
  "products": {
    "TERPA2PAN": { },
    "M": { }
  }
}
```

and can be rearranged as a Troe reaction:

$$k = \frac{k_0[M]}{1 + k_0[M]/k_{\inf}} F_C^{(1+1/N[log_{10}(k_0[M]/k_{\inf})]^2)^{-1}}$$

$$k_0 = A_0 e^{\left(\frac{C_0}{T}\right)} \left(\frac{T}{300}\right)^{B_0}$$

$$k_{inf} = A_{inf} e^{\left(\frac{C_{inf}}{T}\right)} \left(\frac{T}{300}\right)^{B_{inf}}$$
(5)

where $F_C=0.6,~N=1.5,~A_0=9.7\times 10^{-29}\times 1.111\times 10^{28},~B_0=-5.6,~C_0=-14000,~A_{inf}=9.3\times 10^{-12}\times 1.111\times 10^{28},~B_{inf}=0,~{\rm and}~C_{inf}=-14000.$

7 usr_TERPA3PAN_M

Following the same logic as for usr_PBZNIT_M, the tag_TERPA3CO3_NO2_ndx reaction is identified as:

```
{
  "type": "TROE",
  "k0_A": 9.7e-29,
  "k0_B": -5.6,
  "kinf_A": 9.3e-12,
  "N": 1.5,
  "reactants": {
    "TERPA3CO3": { },
    "M": { }
  },
  "products": {
    "TERPA3PAN": { },
    "M": { }
  },
  "M": { }
},
```

and can be rearranged as a Troe reaction:

$$k = \frac{k_0[M]}{1 + k_0[M]/k_{inf}} F_C^{(1+1/N[log_{10}(k_0[M]/k_{inf})]^2)^{-1}}$$

$$k_0 = A_0 e^{\left(\frac{C_0}{T}\right)} \left(\frac{T}{300}\right)^{B_0}$$

$$k_{inf} = A_{inf} e^{\left(\frac{C_{inf}}{T}\right)} \left(\frac{T}{300}\right)^{B_{inf}}$$
(6)

where $F_C = 0.6$, N = 1.5, $A_0 = 9.7 \times 10^{-29} \times 1.111 \times 10^{28}$, $B_0 = -5.6$, $C_0 = -14000$, $A_{inf} = 9.3 \times 10^{-12} \times 1.111 \times 10^{28}$, $B_{inf} = 0$, and $C_{inf} = -14000$.

8 usr_ISOPZD4O2

This appears to be a WENNBERG_TUNNELING reaction:

$$k_{tunneling} = Ae^{-B/T}e^{C/T^3} \tag{7}$$

with $A = 2.22 \times 10^9$, B = 7160, and $C = 1 \times 10^8$.

9 References

References

[1] Paul O. Wennberg et al. "Gas-Phase Reactions of Isoprene and Its Major Oxidation Products". In: Chemical Reviews 118.7 (2018). PMID: 29522327, pp. 3337-3390. DOI: 10.1021/acs.chemrev.7b00439. eprint: https://doi.org/10.1021/acs.chemrev.7b00439. URL: https://doi.org/10.1021/acs.chemrev.7b00439.