

## RL DC motor

### Control laws design

Dynamics of DC motor

$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = -ax_2 - \mathbb{F} + bu(t) \end{cases} \quad \begin{cases} x_d = \theta_{desired} \\ x_1 = \theta_{actual} \\ x_2 = \dot{\theta}_{actual} = w_{actual} \end{cases}$$

Define the tracking error dynamics function

$$\begin{aligned} c &= x_d - x_1 \\ \dot{c} &= \dot{x}_d - \dot{x}_1 = \dot{x}_d - x_2 \\ \ddot{c} &= \ddot{x}_d - \ddot{x}_1 = \ddot{x}_d - \dot{x}_2 \Rightarrow \ddot{c} = \ddot{x}_d - [-ax_2 - \mathbb{F} + bu] \end{aligned}$$

Since the bristle state in LuGre model is challenged to derive or estimate, the feedforward compensation terms approximate the friction model by using **Columb friction model**. To compensate disturbances in error function, the control input can be designed as follows:

$$u(t) = v_{PID} + \alpha x_2 + \beta \ddot{\theta}_d(t) + \gamma_1 \text{sign}^+(\dot{\theta}(t)) + \gamma_2 \text{sign}^-(\dot{\theta}(t))$$

$$, \text{where } v_{PID} = \frac{1}{b} \left[ k_p c + k_d \dot{c} + k_i \int_0^t c(\tau) d\tau \right], \alpha = \frac{a}{b}, \beta = \frac{1}{b}, \gamma_1 = \frac{f_c^+}{b}, \gamma_2 = \frac{f_c^-}{b}$$

### Observation space

Num	Observation	Min	Max	Starting value
0	Motor Angular Position $\theta$ (rad)	-Inf	Inf	0
1	Motor Angular Velocity $\omega$ (rad/s)	-Inf	Inf	0
2	Motor Angular Position Error $c$ (rad)	-Inf	Inf	0
3	Error Backward Difference $\dot{c}$ (rad)	-Inf	Inf	0
4	Error integration $\int c dt$ (rad)	-Inf	Inf	0
5	Desired Motor Angular Velocity $\dot{\theta}_d$ (rad)	-Inf	Inf	0
6	Desired Motor Angular Acceleration $\ddot{\theta}_d$ (rad/s)	-Inf	Inf	0

### Action space

Num	Action	Min	Max
0	$k_p$	0	150
1	$k_i$	0	60
2	$k_d$	0	20
3	$\alpha$	0	0.519
4	$\beta$	0	0.061
5	$\gamma_1$	0	1.698
6	$\gamma_2$	0	1.622

### System ID. result

Para.	Value
$a$	8.4645
$b$	32.6486
$f_c^+$	27.7231
$f_c^-$	26.4779

$$\alpha = \frac{a}{b}, \beta = \frac{1}{b}$$

$$\gamma_1 = \frac{f_c^+}{b}, \gamma_2 = \frac{f_c^-}{b}$$