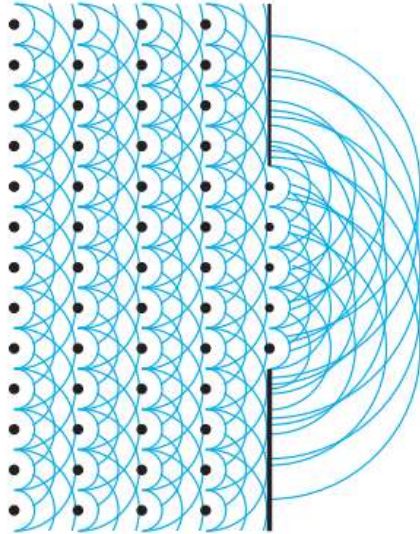


# Integral da propagação Fresnel-Huygens



Cada ponto na abertura  $[f(x', y')]$  é tratado como uma fonte de onda esférica  
Dentro da aproximação Fresnel o integral representa a sobreposição destas fontes.

$$\mathcal{E}(x, y, z) = \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(x', y') e^{ik[(x-x')^2 + (y-y')^2]/2z} dx' dy'$$

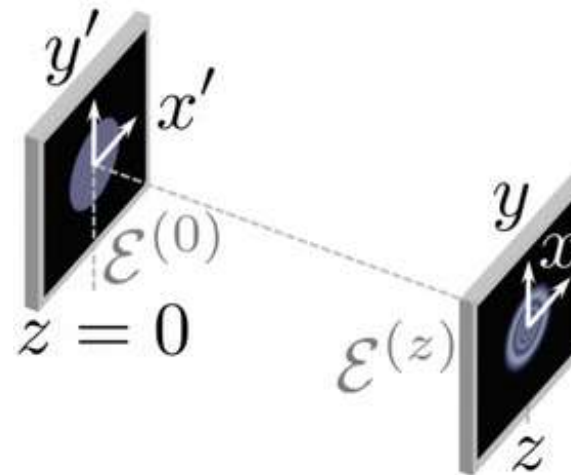
Efetivamente uma soma infinita de fasores

$$r_p^2 = (x - x')^2 + (y - y')^2 + z^2$$

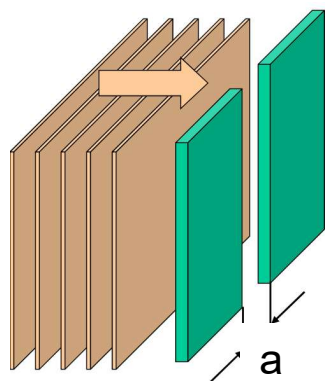
$$r_p \approx z + \frac{(x - x')^2 + (y - y')^2}{2z}$$

Aproximação Fresnel  
(paraxial)

$$z \gg x, y, x', y'$$



# Integral sobre $y'$



$$\mathcal{E}(x, y, z) = \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} \int_{-a/2}^{a/2} e^{\{ik(x-x')^2/2z\}} dx' \int_{-\infty}^{\infty} e^{\{ik(y-y')^2/2z\}} dy'$$

$$\int_{-\infty}^{\infty} e^{ik(y-y')^2/2z} dy' = \int_{-\infty}^{\infty} e^{-\pi(y-y')^2/i\lambda z} dy' = \sqrt{i\lambda z}$$

Integral Gaussiano  $\int_{-\infty}^{\infty} du e^{-\beta(u-u_0)^2} = \sqrt{\frac{\pi}{\beta}} \quad \text{Re}(\beta) \geq 0$

$$\mathcal{E}(x, y, z) = \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} \int_{-a/2}^{a/2} e^{\{ik(x-x')^2/2z\}} dx'$$

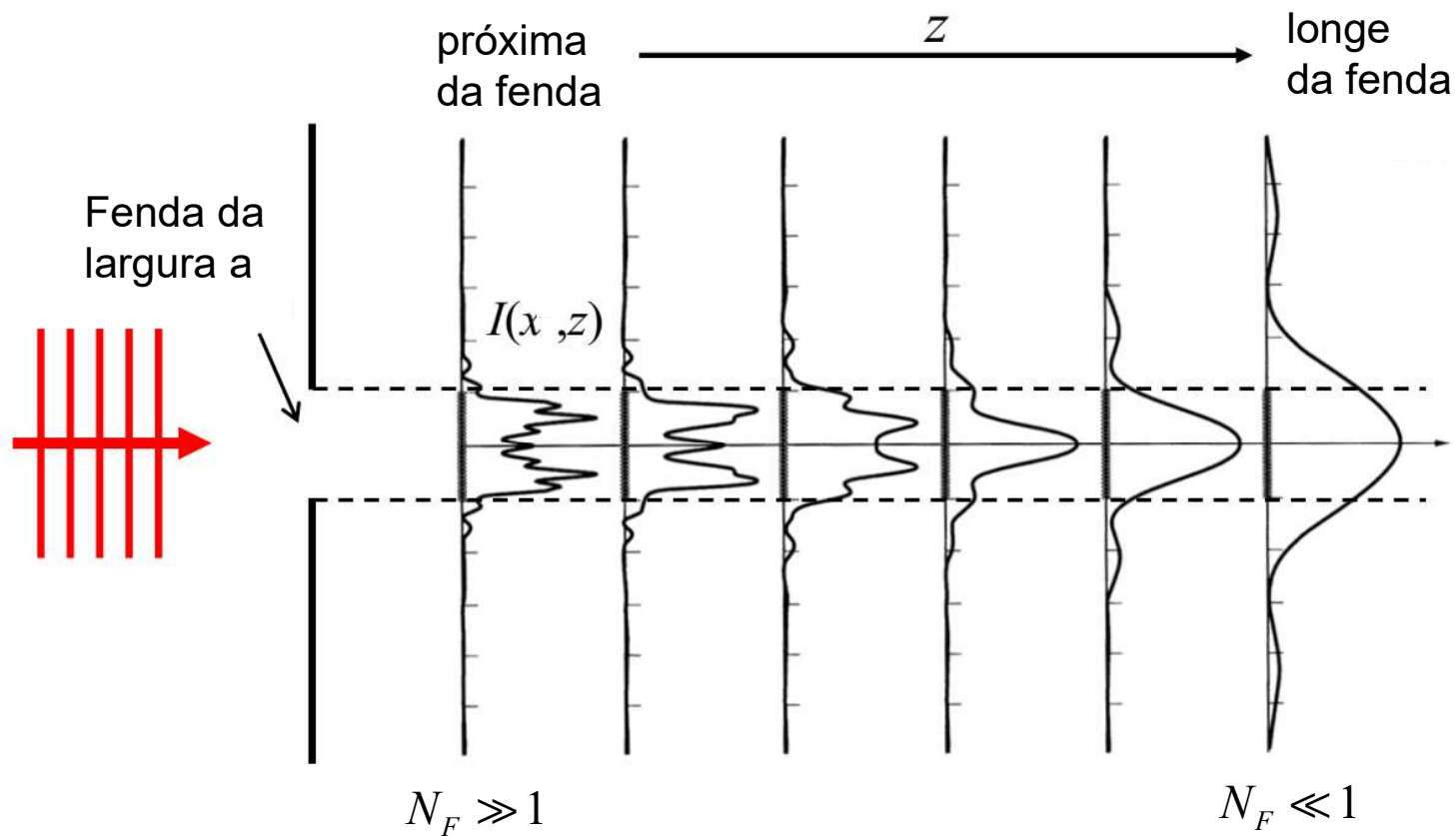
Soma infinita de ondas cilíndricas

O amplitude das ondas cilíndricas  $\sim \frac{1}{\sqrt{z}}$

O amplitude das ondas esféricas  $\sim \frac{1}{z}$

# Difração de uma fenda simples

$$\mathcal{I}(x, z) = N_F \mathcal{I}_0 \left| \int_{-1}^1 \exp \left[ i\pi N_F (u - u')^2 \right] du' \right|^2 \quad u = \frac{2x}{a} \quad N_F \equiv \frac{(a/2)^2}{z\lambda}$$



# Importância do número de Fresnel

$$N_F \equiv \frac{(a/2)^2}{z\lambda}$$

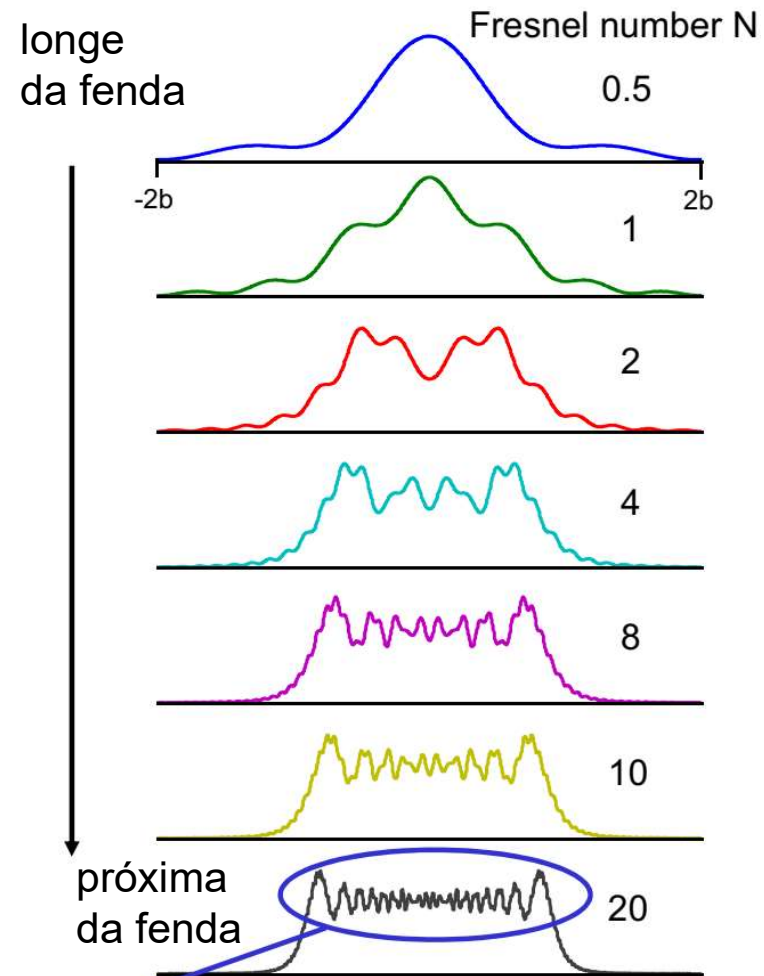
exemplo  $\lambda = 500 \text{ nm}$  luz verde

$$a/2 = 10 \text{ } \mu\text{m} = 20\lambda$$

$$N = 1 \quad @ \quad z = 400\lambda = 0,2\text{mm}$$

$$a/2 = 1 \text{ mm} = 2000\lambda$$

$$N = 1 \quad @ \quad z = 4 \times 10^6 \lambda = 2\text{m}$$



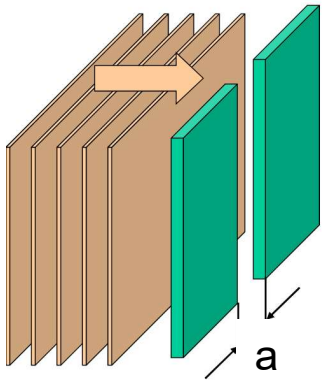
Nº de oscilações =  $N_F$

# Aproximação Fraunhofer $N_F \ll 1$ (campo distante)

$$\mathcal{E}(x, z) = \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} \int_{-a/2}^{a/2} \exp\left[i\frac{\pi}{\lambda z}(x-x')^2\right] dx'$$

$$N_F = \frac{(a/2)^2}{\lambda z} \ll 1$$

Aproximação  
Fraunhofer  
(depende de  $\lambda$ )



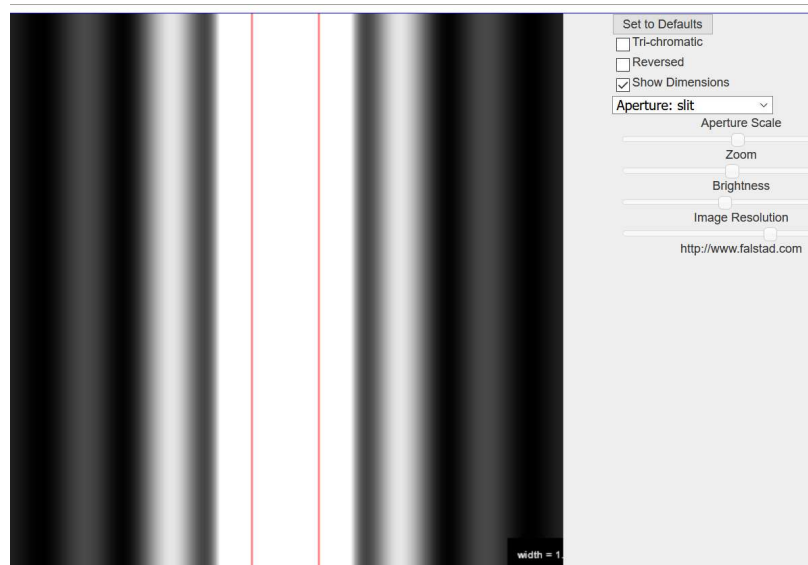
$$e^{i\pi x^2/\lambda z} \int_{-a/2}^{a/2} \exp\left[i\frac{\pi}{\lambda z}(-2xx' + x'^2)\right] du' \quad \left(\frac{x'^2}{\lambda z}\right) \leq \left(\frac{(a/2)^2}{\lambda z}\right) = N_F$$

$$\begin{aligned} e^{i\pi x^2/\lambda z} \int_{-a/2}^{a/2} \exp\left[-i2\pi \frac{xx'}{\lambda z}\right] dx' &= e^{i\pi x^2/\lambda z} \left[ \frac{e^{-i\pi ax/\lambda z} - e^{i\pi ax/\lambda z}}{-i2\pi x/\lambda z} \right] \\ &= e^{i\pi x^2/\lambda z} a \frac{\sin(\pi ax/\lambda z)}{\pi ax/\lambda z} \end{aligned}$$

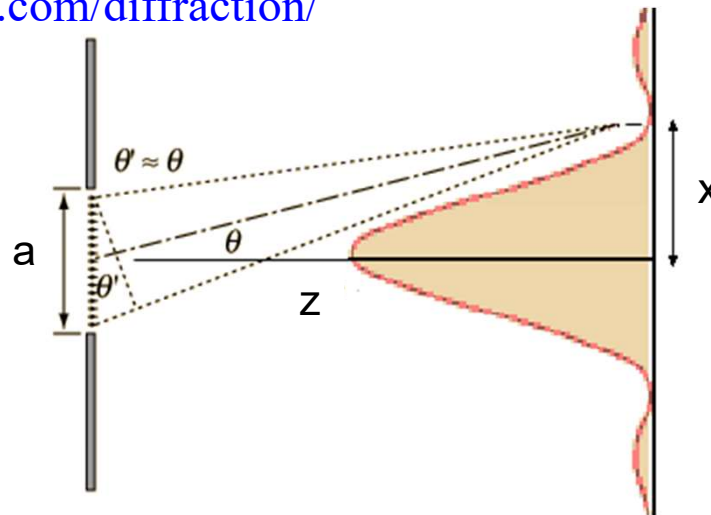
$$\mathcal{E}(x, z) = \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} e^{i\pi x^2/\lambda z} a \left[ \frac{\sin(\pi ax/\lambda z)}{\pi ax/\lambda z} \right]$$

$$\begin{aligned} \mathcal{I}(x, z) &= \mathcal{I}_0 \left( \frac{a^2}{\lambda z} \right) \left[ \frac{\sin(\pi ax/\lambda z)}{\pi ax/\lambda z} \right]^2 \\ &= 4\mathcal{I}_0 N_F \left[ \frac{\sin(4\pi N_F x/a)}{(4\pi N_F x/a)} \right]^2 \end{aligned}$$

# Difração Fenda simples (aproximação Fraunhofer)



<https://www.falstad.com/diffraction/>



$$\mathcal{I}(x, z) = \mathcal{I}_0 \left( \frac{a^2}{\lambda z} \right) \left[ \frac{\sin(\pi a x / \lambda z)}{\pi a x / \lambda z} \right]^2$$

$$\text{sinc}(\xi) = \left[ \frac{\sin(\xi)}{\xi} \right]^2 \quad \lim_{\xi \rightarrow 0} \text{sinc}(\xi) = 1$$

mínimos

$$\mathcal{I}(x, z) = 0 \quad @ \quad \frac{\pi a x_{\min}}{\lambda z} = m\pi$$

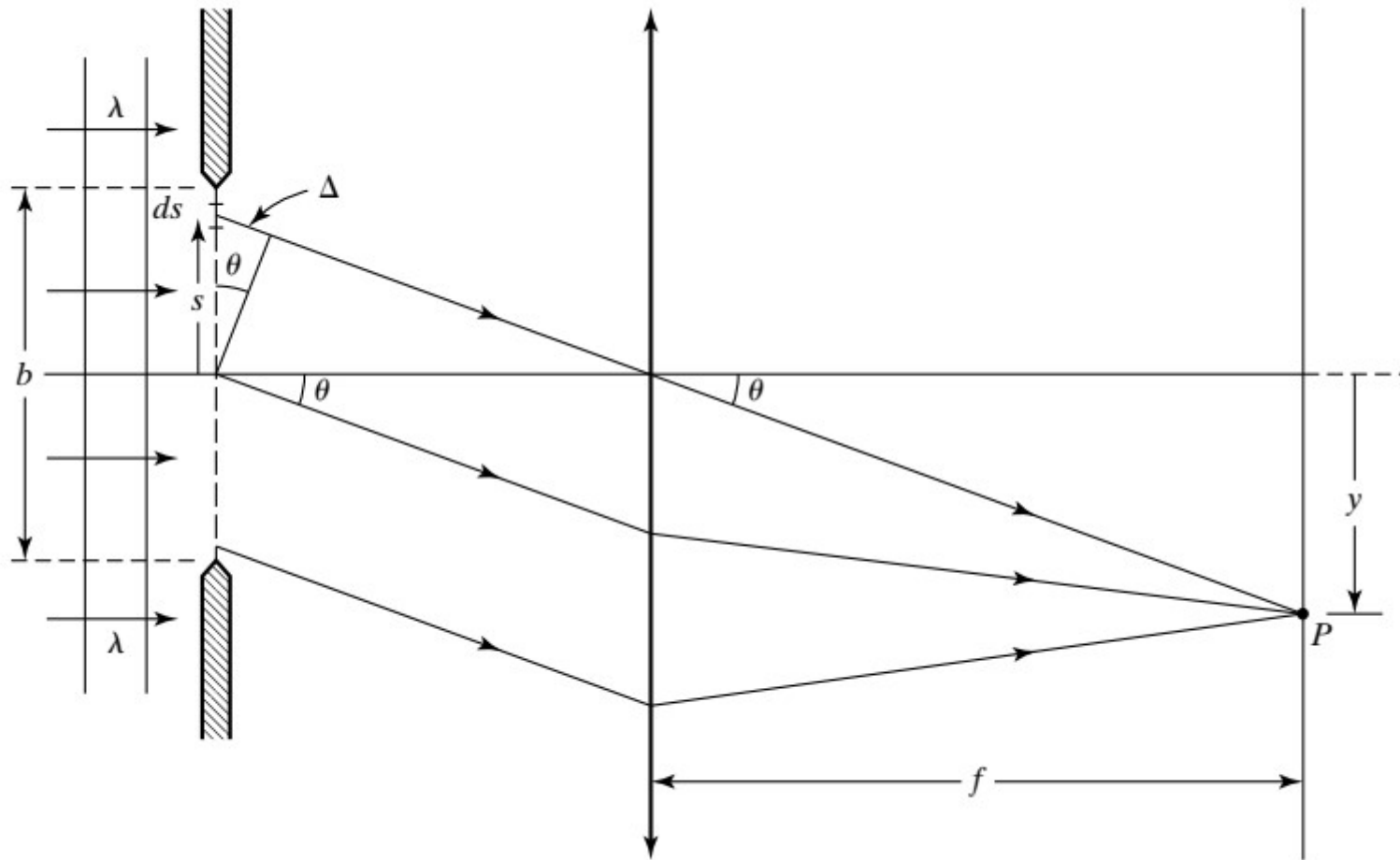
exceto  $m=0$

$$a \frac{x_{\min}}{z} \approx a \sin \theta_{\min} = m\lambda$$

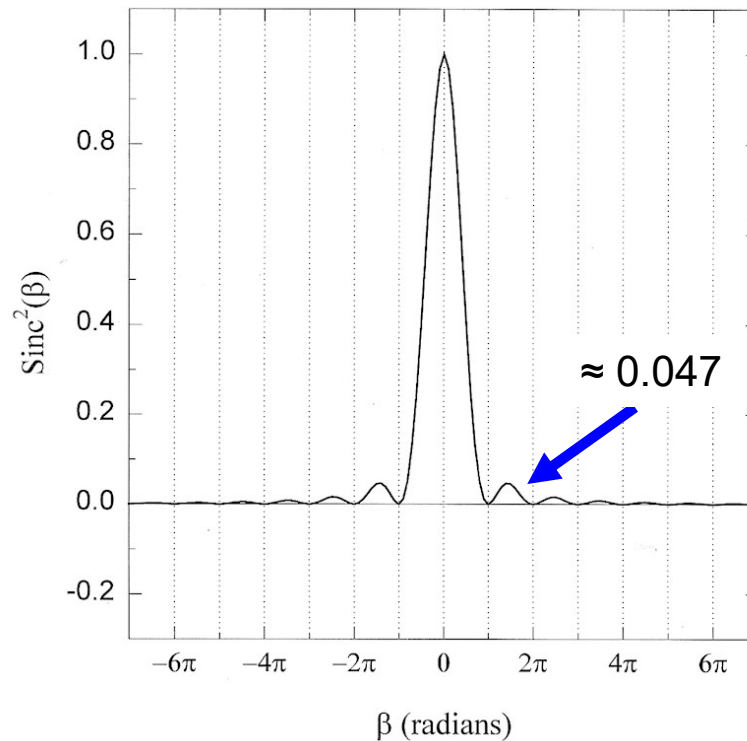
$$\sin \theta_{\min} = \frac{m\lambda}{a}$$

## Uso duma lente para aproximar o infinito...

---

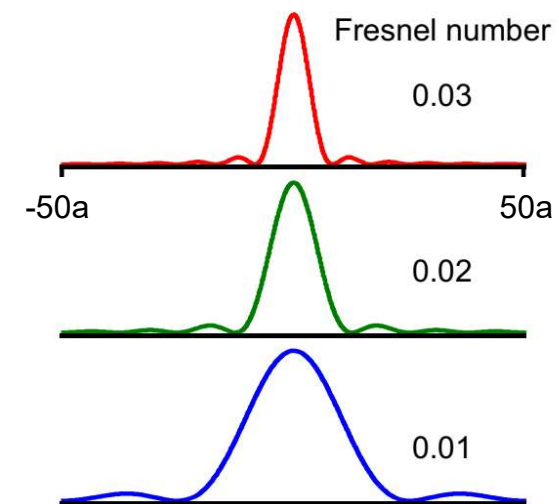


# A função sinc



$$\text{sinc}^2(\beta) = \left[ \frac{\sin(\beta)}{\beta} \right]^2$$

$$N_F \equiv \frac{(a/2)^2}{z\lambda}$$



$$N_F \sim \frac{1}{z}$$

$$\mathcal{I}(x, z) = \mathcal{I}_0 \left( \frac{a^2}{\lambda z} \right) \left[ \frac{\sin(\pi a x / \lambda z)}{\pi a x / \lambda z} \right]^2 = \mathcal{I}_0 4 N_F \text{sinc}^2 \left( \frac{4 \pi N_F x}{a} \right)$$

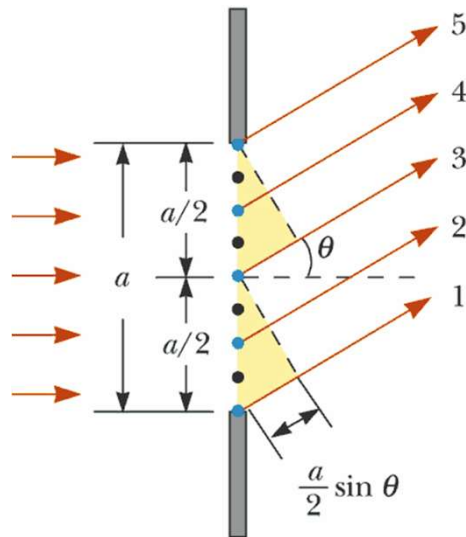
Quando  $z$  aumenta o padrão alarga mas mantém a mesma forma



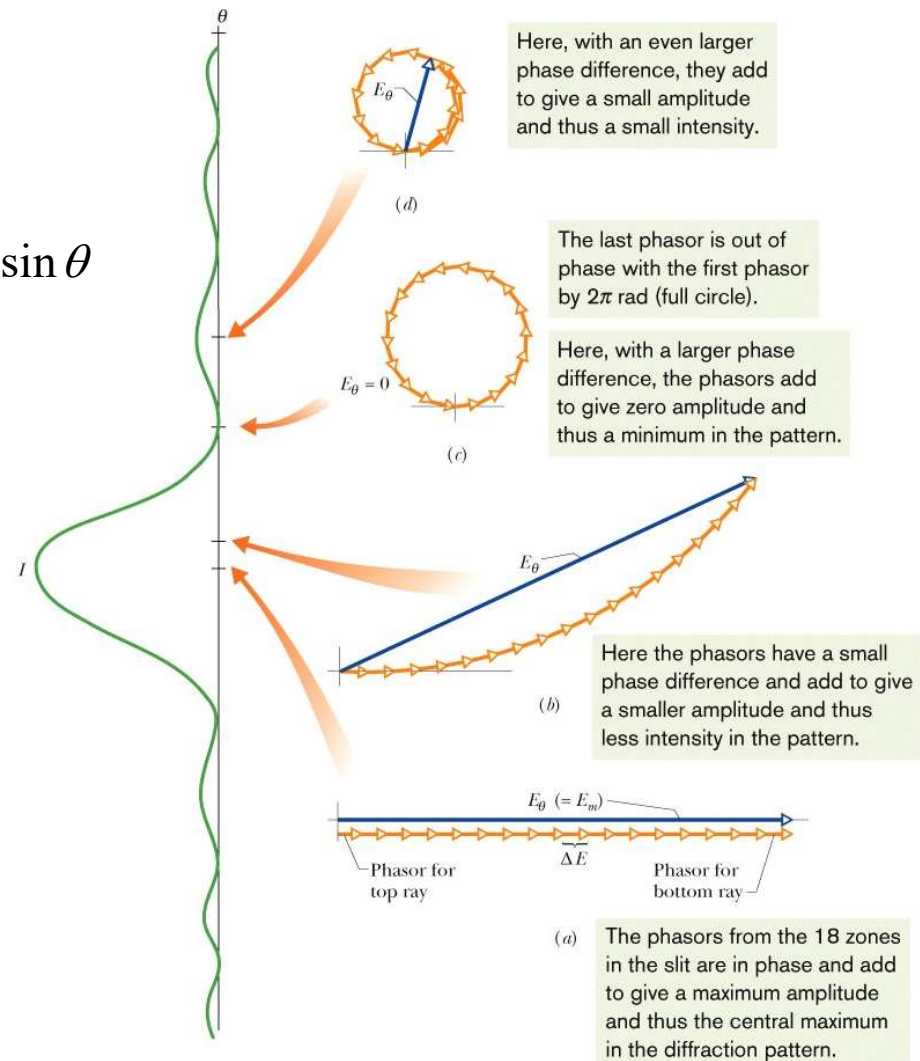
# Interpretação em termos de fasores

$$\mathcal{I}(x, z) = \mathcal{I}_0 \left( \frac{a^2}{\lambda z} \right) \left[ \frac{\sin(\pi a x / \lambda z)}{\pi a x / \lambda z} \right]^2$$

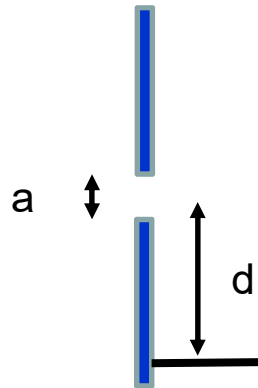
$$\frac{\pi a x}{\lambda z} \approx k \frac{a}{2} \sin \theta$$



© 2006 Brooks/Cole - Thomson



# Padrão duma fenda simples deslocada



$$\mathcal{E}_d(x, y, z) = \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} \int_{-a/2+d}^{a/2+d} \exp\left[ik(x-x')^2 / 2z\right] dx'$$

Integral na  
aproximação Fraunhofer

$$\int_{-a/2+d}^{a/2+d} \exp\left[-i2\pi \frac{xx'}{\lambda z}\right] dx' = e^{-i2\pi dx/\lambda z} \int_{-a/2}^{a/2} \exp\left[-i2\pi \frac{xx''}{\lambda z}\right] dx''$$

igual exceto duma fase adicional

$$\mathcal{E}_d(x, z) = e^{-i2\pi dx/\lambda z} \mathcal{E}(x, z)$$

$$\mathcal{I}(x, z) = \mathcal{I}_0 \left( \frac{a^2}{\lambda z} \right) \left[ \frac{\sin(\pi ax / \lambda z)}{\pi ax / \lambda z} \right]^2$$

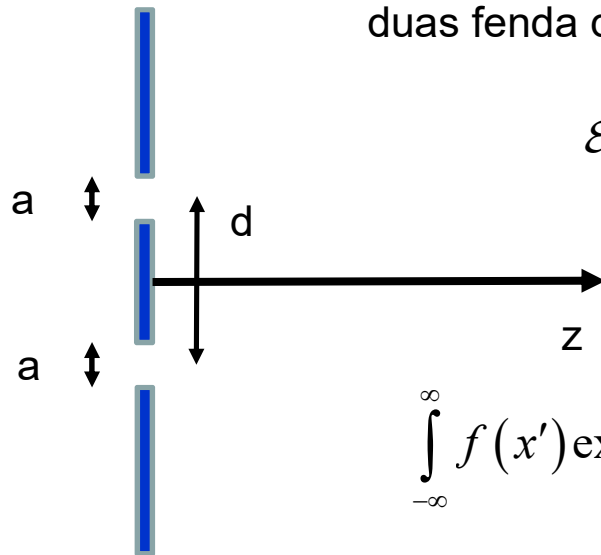
Padrão de difração igual ao padrão não deslocada!

Aproximação Fraunhofer

$$\max \left( \frac{x'^2}{\lambda z} \right) \ll 1$$

implica que a distância de deslocação  $d \ll \sqrt{\lambda z}$

# Dupla Fenda



duas fenda de largura  $a$ , separadas por uma distância  $d$

$$\mathcal{E}_{2\text{fendas}}(x, y, z) = \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} \int_{-\infty}^{\infty} f(x') \exp\left[ik(x-x')^2 / 2z\right] dx'$$

Duas fendas deslocada por  $\pm d/2$

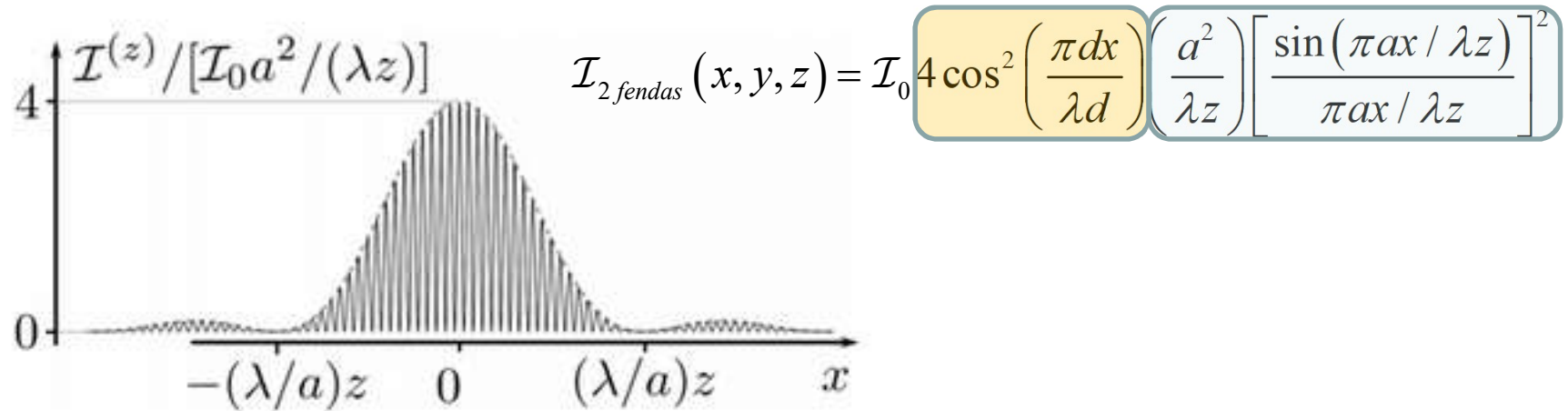
$$\begin{aligned} \int_{-\infty}^{\infty} f(x') \exp\left[-i2\pi \frac{xx'}{\lambda z}\right] dx' &= \left[ e^{-i\pi dx/\lambda z} + e^{i\pi dx/\lambda z} \right] \int_{-a/2}^{a/2} \exp\left[-i2\pi \frac{xx''}{\lambda z}\right] dx'' \\ &= 2 \cos\left(\frac{\pi dx}{\lambda z}\right) e^{i\pi x^2/\lambda z} a \frac{\sin(\pi ax / \lambda z)}{\pi ax / \lambda z} \end{aligned}$$

$$\mathcal{E}_{2\text{fendas}}(x, y, z) = \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} e^{i\pi x^2/\lambda z} 2 \cos\left(\frac{\pi dx}{\lambda z}\right) a \frac{\sin(\pi ax / \lambda z)}{\pi ax / \lambda z}$$

$$\mathcal{I}_{2\text{fendas}}(x, y, z) = 4 \left(\frac{a^2}{\lambda z}\right) \mathcal{I}_0 \cos^2\left(\frac{\pi dx}{\lambda z}\right) \left[\frac{\sin(\pi ax / \lambda z)}{\pi ax / \lambda z}\right]^2$$

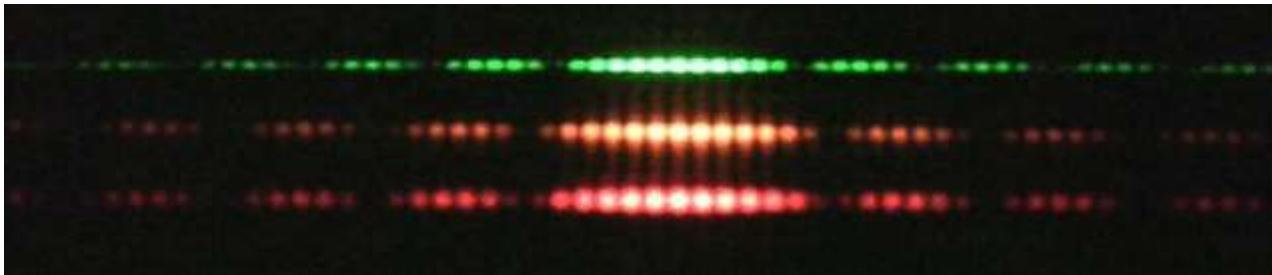
Padrão de 2 fendas multiplicada  
pela padrão de uma fenda  
(teorema de convolução)

# Padrão difração dupla fendas

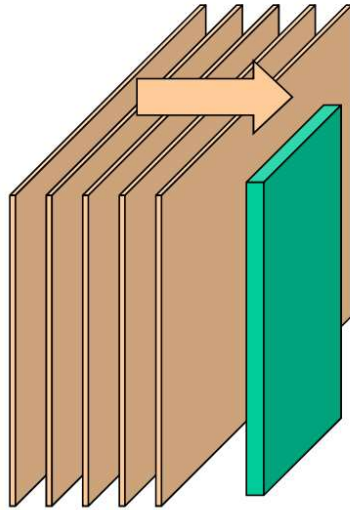


Oscilação rápida devida a interferência das duas fendas

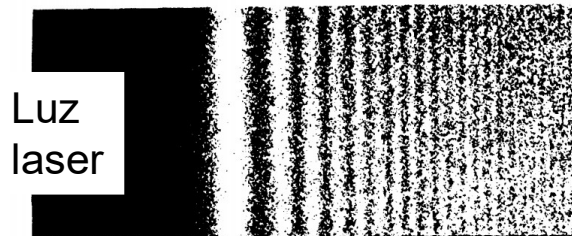
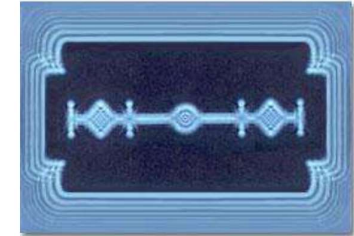
Modulação da amplitude devida a padrão da difração de uma fenda com largura  $a$



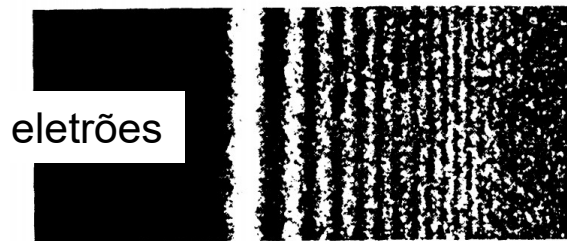
# Difração numa aresta



$$\begin{aligned}\mathcal{E}(x, z) &= \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} \int_{-\infty}^{\infty} f(x') \exp\left[ik(x-x')^2 / 2z\right] dx' \\ &= \frac{\mathcal{E}_0}{\sqrt{i\lambda z}} e^{ikz} \int_0^{\infty} \exp\left[ik(x-x')^2 / 2z\right] dx'\end{aligned}$$

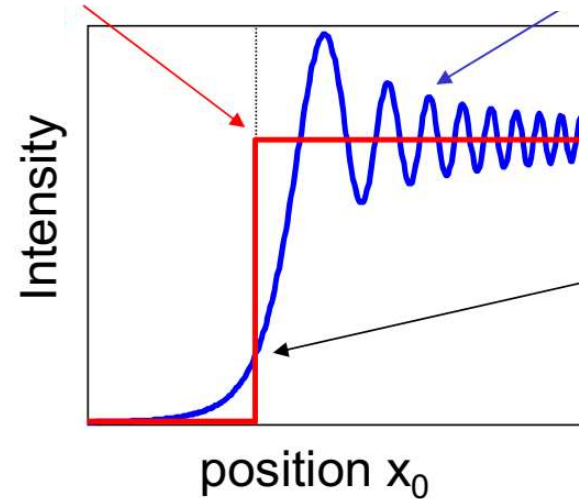


(a)



Sombra  
geométrica

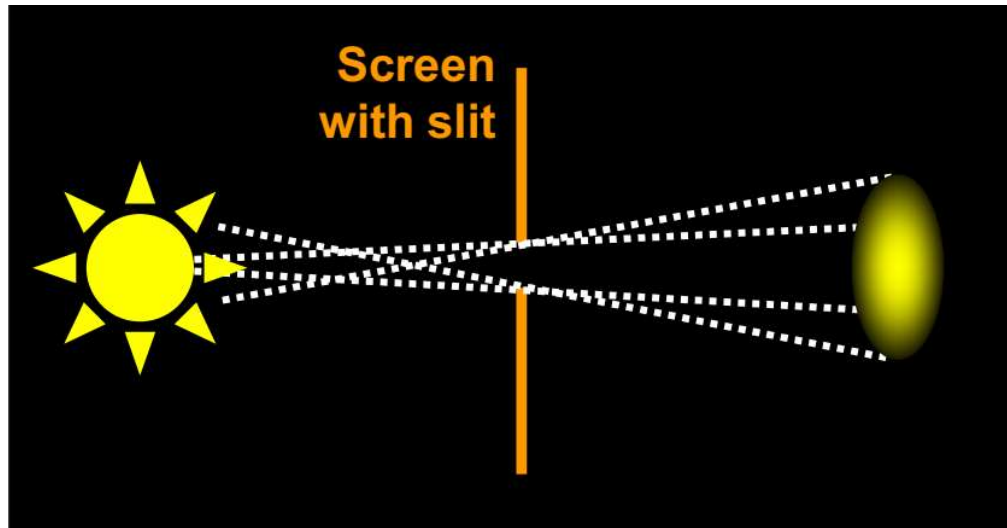
Resultado do integral Fresnel-Huygens



Irradiância  
na aresta é  
 $\frac{1}{4}$  do valor  
no  $x \rightarrow \infty$

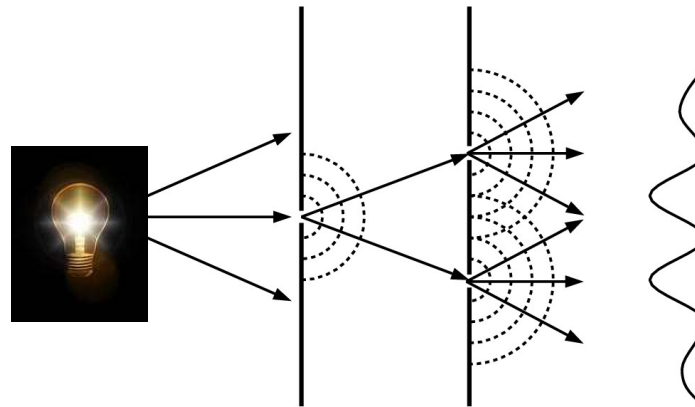
# Porque é raro ver os efeitos de difração com luz ambiente?

Basicamente é um problema com a coerência de fontes extensas



Em princípio, raios esféricos duma fonte pontual produzem efeitos de difração, mas os raios provenientes de outras zonas ofuscam a padrão

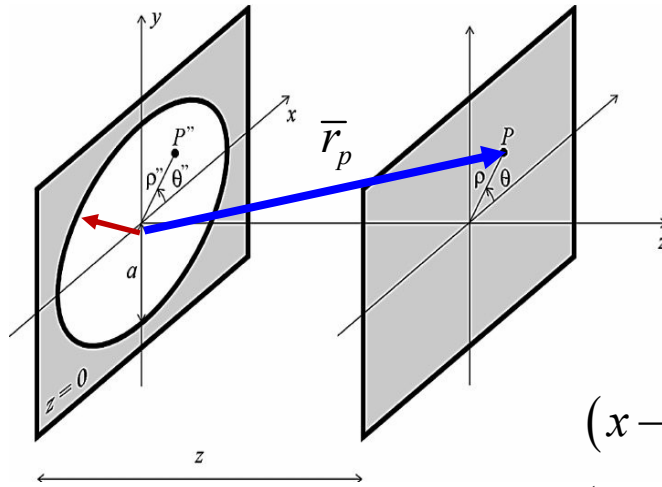
Em geral uma fonte extensa (sol, lâmpada) cria sombras borratadas



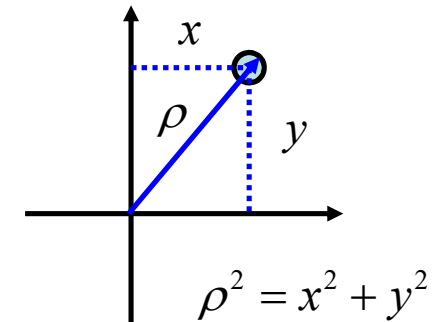
# Integral Fresnel-Huygens com Simetria circular

$$\mathcal{E}(x, y, z) = \frac{\mathcal{E}_0}{i\lambda z} \int_{-\infty}^{\infty} \int f(x', y') e^{ikz} e^{ik[(x-x')^2 + (y-y')^2]/2z} dx' dy'$$

Com simetria circular convêm usar coordenados polares



$$\begin{aligned} x' &= \rho' \cos \theta' & y' &= \rho' \sin \theta' \\ x &= \rho \cos \theta & y &= \rho \sin \theta \end{aligned}$$



$$\bar{r}_p = z + \rho^2 / 2z$$

$$\begin{aligned} (x-x')^2 &= \rho^2 \cos^2 \theta - 2\rho\rho' \cos \theta \cos \theta' + \rho'^2 \cos^2 \theta' \\ (y-y')^2 &= \rho^2 \sin^2 \theta - 2\rho\rho' \sin \theta \sin \theta' + \rho'^2 \sin^2 \theta' \\ \hline (x-x')^2 + (y-y')^2 &= \rho^2 - 2\rho\rho' \cos(\theta - \theta') + \rho'^2 \end{aligned}$$

$$f(\rho') = \begin{cases} 1 & \rho' < R_a \\ 0 & \rho' \geq R_a \end{cases}$$

$$\mathcal{E}(\rho, \theta, z) = \frac{\mathcal{E}_0}{i\lambda z} e^{ik\bar{r}_p} \int_0^{2\pi} d\theta' \int_0^{R_a} \rho' d\rho' \exp \left[ -ik \frac{\rho\rho'}{z} \cos(\theta - \theta') + ik \frac{\rho'^2}{2z} \right]$$

# Abertura circular irradiância no eixo ótico

$$\mathcal{E}(\rho, \theta, z) = \frac{\mathcal{E}_0}{i\lambda z} e^{ik\bar{r}_p} \int_0^{2\pi} d\theta' \int_0^{R_A} \rho' d\rho' \exp \left[ -ik \frac{\rho\rho'}{z} \cos(\theta - \theta') + ik \frac{\rho'^2}{2z} \right]$$

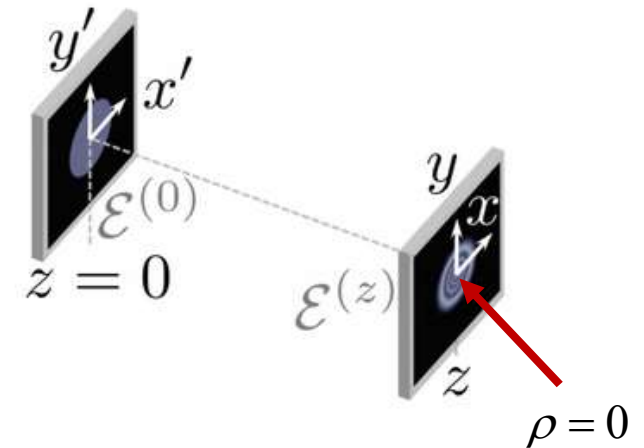
Esta integral é difícil em geral e tem ser resolvida numericamente. No entanto no eixo ótico  $\rho = 0$

$$\mathcal{E}(\rho = 0, z) = \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} 2\pi \int_0^{R_A} \rho' d\rho' \exp \left[ ik \frac{\rho'^2}{2z} \right]$$

$$u' = \frac{ik\rho'^2}{2z} = \frac{i\pi\rho'^2}{\lambda z} \quad \frac{\rho'^2}{2} = \frac{\lambda z}{i2\pi} u \quad \rho' d\rho' = \frac{\lambda z}{i2\pi} du'$$

$$\begin{aligned} \mathcal{E}(\rho = 0, z) &= \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} 2\pi \frac{\lambda z}{i2\pi} \int_0^{i\pi R_A^2/\lambda z} e^{u'} du' = -\mathcal{E}_0 e^{ikz} \left[ e^{i\pi R_A^2/\lambda z} - 1 \right] \\ &= -2i\mathcal{E}_0 e^{ikz} e^{i\pi R_A^2/2\lambda z} \left[ \frac{e^{i\pi R_A^2/2\lambda z} - e^{-i\pi R_A^2/2\lambda z}}{2i} \right] \end{aligned}$$

$$\mathcal{I}(\rho = 0, z) = 4\mathcal{I}_0 \sin^2 \left( \frac{\pi R_a^2}{2\lambda z} \right)$$





# Variação da intensidade no eixo ótico

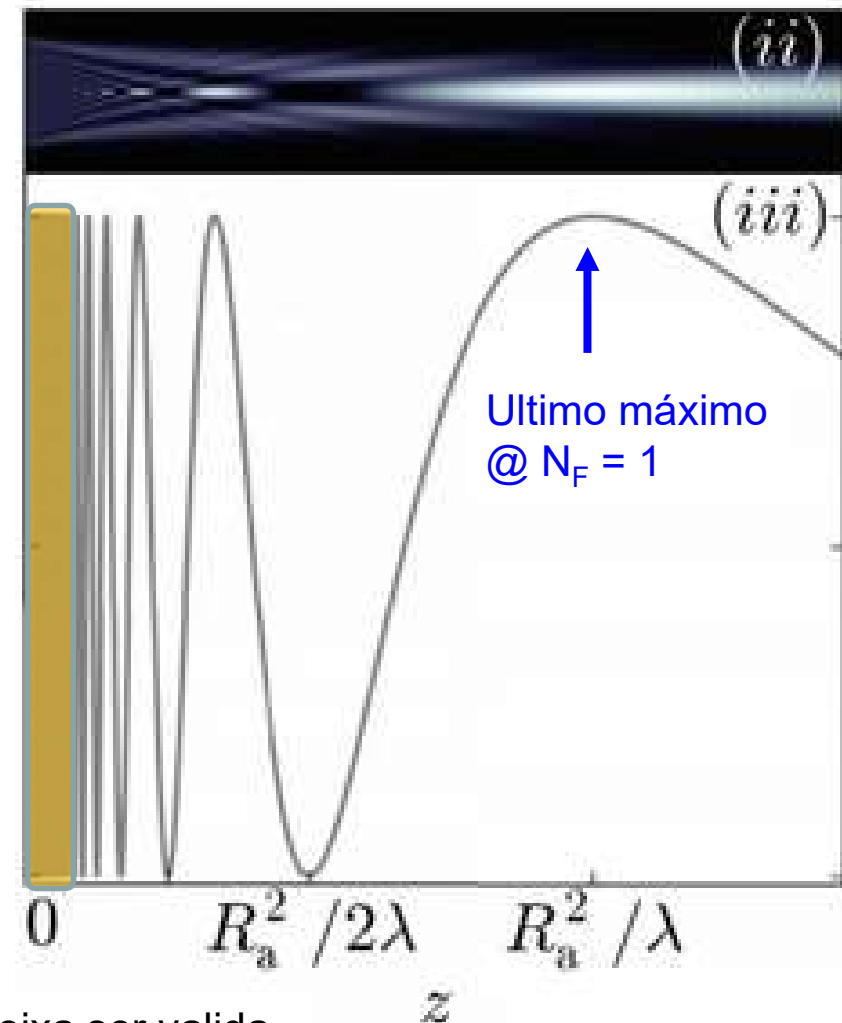
$$\mathcal{I}(\rho = 0, z) = 4\mathcal{I}_0 \sin^2\left(\frac{\pi R_a^2}{2\lambda z}\right)$$

$$N_F = \frac{R_a^2}{\lambda z} \quad \text{Número Fresnel}$$

Quando  $N_F \ll 1$   
no limite paraxial  
o padrão de difração fica mais estável  
e mais simples, tal como aconteceu  
no caso duma fenda simples.



Quando  $z < R_a^2 / \lambda$  a aproximação de Fresnel deixa de ser válida



# Variação da padrão de difração com z

---

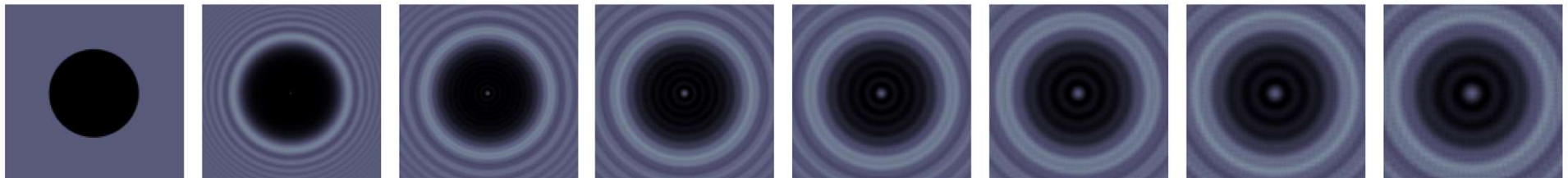
$$\mathcal{I}(\rho, \theta, z) = \mathcal{I}_0 \left| \int_0^{2\pi} d\theta' \int_0^{R_A} \rho' d\rho' \exp \left[ -ik \frac{\rho\rho'}{z} \cos(\theta - \theta') + ik \frac{\rho'^2}{2z} \right] \right|^2$$

Simulação numérica da integral

$z = 0$

Abertura circular

$z = \frac{R_a^2}{\lambda}$

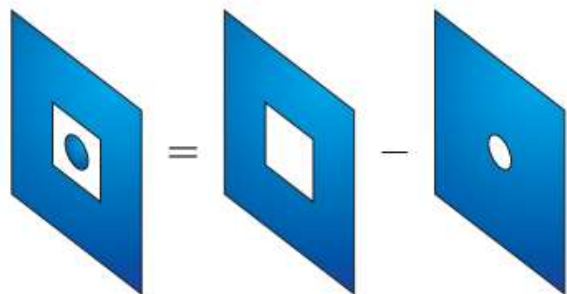


Disco circular

---

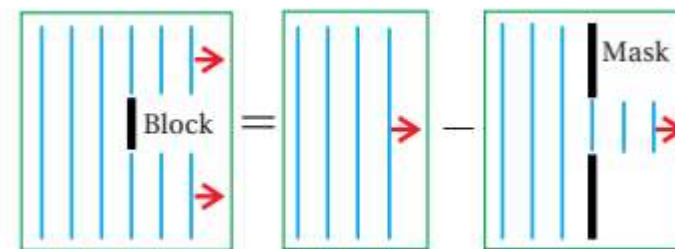
# Princípio de Babinet

O princípio de Babinet é efetivamente o princípio de sobreposição



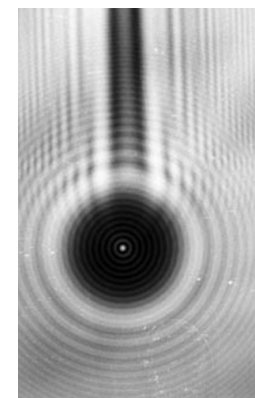
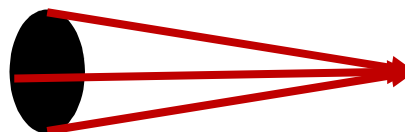
Jaques Babinet  
(1794-1872)

Em particular considere um disco circular  
O campo no eixo ótico é



$$\begin{aligned}\mathcal{E}_{disco}(\rho=0, z) &= \mathcal{E}_{plana}(0, z) - \mathcal{E}_{abertura}(0, z) \\ &= \mathcal{E}_0 e^{ikz} + \mathcal{E}_0 e^{ikz} \left[ e^{i\pi R_a^2 / \lambda z} - 1 \right] \\ &= \mathcal{E}_0 e^{ikz} e^{i\pi R_a^2 / \lambda z}\end{aligned}$$

$$\mathcal{I}_{disco}(\rho=0, z) = \mathcal{I}_0$$



Interferência  
construtiva no  
centro do disco

O spot de  
Poisson/Arago

# Complementaridade

---

No limite Fraunhofer a integral Fresnel de difração é uma transformada Fourier

$$N_F \ll 1$$

$$\begin{aligned}\mathcal{E}(x, y, z) &= \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(x', y') e^{ik[(x-x')^2 + (y-y')^2]/2z} dx' dy' \\ &\Rightarrow \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} e^{ik(x^2+y^2)/2z} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(x', y') e^{-ik[xx' + yy']/z} dx' dy'\end{aligned}$$

Uma abertura complementar (uma que é o inverso da abertura original) da a mesma padrão (exceto no eixo ótico)

$$\begin{aligned}\mathcal{E}_{comp}(x, y, z) &= \frac{\mathcal{E}_0}{i\lambda z} e^{ikz} e^{ik(x^2+y^2)/2z} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} [1 - f(x', y')] e^{-ik[xx' + yy']/z} dx' dy' \\ &= -\mathcal{E}_{original}(x, y, z) + -i\mathcal{E}_0 \lambda z e^{ikz} 2\pi \delta(x) \delta(y)\end{aligned}$$

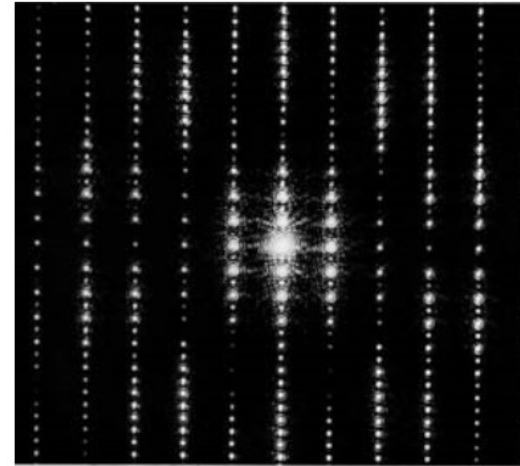
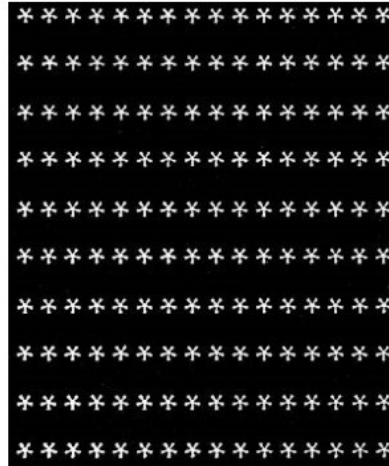
Exceto na origem  $\mathcal{E}_{comp}(x, y, z) = -\mathcal{E}_{original}(x, y, z) \quad \mathcal{I}_{comp}(x, y, z) = \mathcal{I}_{original}(x, y, z)$

---

# Exemplo do principio de Babinet

---

Uma rede  
de buracos



Uma rede  
de anti-buracos

