# EATEX Workshop Fall 2020

# Jack Leightcap<sup>12</sup>

<sup>1</sup>IEEE - nuieeeofficers@gmail.com

<sup>2</sup>Wireless Club - nuwirelessclub@gmail.com

October 5, 2020



# What is LATEX?

- A plain-text method of document preparation and typesetting
- Compiled into a document format (PDF, DVI, etc.)
- Started as an academic tool for mathematicians and computer scientists (Discrete, Algo!)
- Expansive set of packages on CTAN



Figure: The LATEX Project Logo, CC BY 4.0

# Comparison of LATEX to Graphical Editors

### **WYSIWYG**

- "Interpreted"
- Allows ambiguity
- More speed than control
- Platform-dependent
- Directly understood
- Combined composition and formatting

### WYSIWYT

- Compiled
- Unambiguous (pedantic)
- More control than speed
- Portable
- Layer of Abstraction
- Seperated composition and formatting

#### 4.2 Voltage Division

Using the series resistors construction from 4.1,

$$\frac{V_1}{V_s} = \frac{i_s R_1}{i_s R_{123}} = \frac{R_1}{R_{123}}$$

#### Voltage Division

For a resistor  $R_i$  where  $1 \le i \le n$  in series with resistors  $R_1 \dots R_n$  contributing to an equivalent resistance  $R_{i0}$ , the ratio of the total voltage across  $R_i$ ,

$$\frac{V_i}{V_c} = \frac{R_i}{\sum_{i=1}^{n} R_i}$$

#### 4.3 Resistors in Parallel



The three resistors  $R_1$   $R_2$  and  $R_3$  can be simplified into an equivalent resistor  $R_{123}$  just using Ohm's Law and KCL,

$$i_s = \frac{V_s}{R_1} + \frac{V_s}{R_2} + \frac{V_s}{R_3} = \frac{V_s}{R_{123}}$$

#### Resistors in Parallel

For resistors  $R_1 \dots R_n$ , the equivalent resistance  $R_{rs}$ .

$$\frac{1}{R_{eq}} = \sum_{i=1}^{n} \frac{1}{R}$$

Note that  $R_{eq} < R_i \forall i$ .

#### 4.4 Current Division

Using the parallel resistors construction from 4.3,

$$\frac{i_1}{i_s} = \frac{\frac{V_s}{R_1}}{\frac{V_s}{R_{12}}}$$

#### Lecture 5

#### Current Division

For a resistor  $R_t$  where  $1 \le i \le n$  in parallel with resistors  $R_1 ... R_n$  contributing to an equivalent resistance  $R_{to}$ , the ratio of the total current across  $R_t$ .

$$\frac{i_i}{i_r} = \frac{1}{R_1 \sum_{i=1}^{n} \frac{1}{L_i}}$$

#### 5 Lecture #5

#### 5.1 Voltage Division and Loading

A voltage divider has already been covered in the context of resistors in series, but

#### Loading Resistor

What if an addition resistor (called the Louding resistor) is placed in parallel to a voltage divider?



To understand the behavior of this circuit, the three cases  $R_L=0$ ,  $R_L=\infty$ , and  $R_L=l$   $(0 < l < \infty)$  show the general behaviour and the boundary cases. In the context of a voltage divider, the voltage across  $R_L$  shows the useful output voltage of the circuit.

Case 1: 
$$R_L = 0$$

$$\Delta V_L = 0$$

Here, there is a short across  $R_L$ , all of the current bypasses  $R_3$  and moves along the path of no resistance.  $R_L$  is functionally equivalent to a wire, which does not have any voltage drop.

Case 2: 
$$R_1 = \infty$$

$$\Delta V_L = \frac{x}{x+y}V_S$$

With an extremely large resistance along the branch  $R_L$ , this reduced to the base case for a voltage divider, functionally only containing  $R_s$  and  $R_g$ .

#### Case 3: $R_L = l$

For the general case,

$$\Delta V_L = \frac{y \parallel l}{x + (y \parallel l)} V_S = \frac{\left(\frac{1}{y} + \frac{1}{t}\right)^{-1}}{x + \left(\frac{1}{y} + \frac{1}{t}\right)^{-1}} V_S$$

**EECE 2150** 

#### Math 2321 Final

JACK LEIGHTCAP

#### Chapter 1 Dot & Cross Product:

$$\vec{u} \cdot \vec{v} = \sum_{i=1}^{n} u_i v_i$$

$$|\vec{u} \cdot \vec{v}| = |\vec{u}| |\vec{v}| \cos(\theta)$$

$$\vec{u} \times \vec{v} = \begin{vmatrix} i & j & k \\ u_1 & u_2 & u_3 \\ \vdots & \vdots & \vdots \\ v_2 & v_2 & v_3 \end{vmatrix}$$

$$\vec{u} \times \vec{v} = \begin{vmatrix} u_1 & u_2 & u_3 \\ v_1 & v_2 & v_3 \end{vmatrix}$$
  $|\vec{u} \times \vec{v}| = |\vec{u}| |\vec{v}| \sin(\theta)$ 
Cross products returns normal vector

Area of proviled group  $|\vec{u} \times \vec{v}| = Area of triangle |\vec{b}| |\vec{u} \times \vec{v}|$ 

Area of parallelogram  $|\vec{u} \times \vec{v}| \rightarrow \text{Area of triangle } \frac{1}{2} |\vec{u} \times \vec{v}|$ Volume of parallelepiped  $\begin{vmatrix} u_1 & u_2 & u_3 \\ v_1 & v_2 & v_3 \\ w_1 & w_2 & w_2 \end{vmatrix}$ 

 $\nabla f(x_1, x_2, \dots, x_n) = (f_{x_1}, f_{x_2}, \dots, f_{x_n})$ Gradient vector returns normal vector

#### Chapter 2

Linearization: In  $\mathbb{R}^2$ , f(x) at a, f(x) - f(a) = f'(a)(x - a). Using gradient,

$$L(\underline{x}) - f(\underline{a}) = \vec{\nabla} f(\underline{a}) \cdot (\underline{x} - \underline{a})$$

For a point b close to a,  $f(b) \simeq L(b)$ 

#### Multivariable Chain Rule:

$$\frac{d\!f}{dt} = \frac{\partial f}{\partial x}\frac{dx}{dt} + \frac{\partial f}{\partial y}\frac{dy}{dt} + \frac{\partial f}{\partial z}\frac{dz}{dt} = \vec{\nabla} f \cdot \left(\frac{dx}{dt}, \frac{dy}{dy}, \frac{dz}{dy}\right)$$

Evaluating at a point  $t = t_0$ , need to find corresponding point  $t = t_0 \implies (x, u, z) = (a, b, c),$ 

$$\boxed{\frac{df}{dt}\big|_{t=t_0} = \vec{\nabla} f(a,b,c) \cdot \left(\frac{dx}{dt}\big|_{t=t_0}, \frac{dy}{dt}\big|_{t=t_0}, \frac{dz}{dt}\big|_{t=t_0}\right)}$$

#### Directional Derivative:

Derivative in direction of unit vector  $\vec{u}$  at point p,

$$D_{\vec{u}}f(\underline{p}) = \vec{\nabla}f(\underline{p}) \cdot \vec{u}$$

direction 
$$\vec{\nabla} f(\underline{p})$$
 magnitude  $|\vec{\nabla} f(\underline{p})|$   
direction  $-\vec{\nabla} f(\underline{p})$  magnitude  $-|\vec{\nabla} f(\underline{p})|$ 

#### Local Regular Parametrization: For parametrization $\vec{r}(u, v)$ at point $(u_p, v_0)$ , local regular if

For parametrization 
$$F(u, v)$$
 at point  $(u_o, v_0)$ , local regular if  
 $\vec{v}_o(u_o, v_0) \times \vec{v}_o(u_o, v_0) \neq \vec{0}$ 

$$z = f(x, y)$$
,  $\vec{r}(y, y) = (y, y, f(y, y))$  local results

$$\vec{r}(u, v) = (u, v, f(u, v))$$
 local regular.

$$\vec{r}(u, v) = (u, v, f(u, v))$$
 local regular.

#### Hessian Matrix:

$$D(x,y) = \begin{vmatrix} f_{xx} & f_{xy} \\ f_{yx} & f_{yy} \end{vmatrix} = f_{xx}f_{yy} - f_{xy}^2$$
At a point  $(a,b)$ ,

D(a, b) > 0 $f_{xx}(a, b)$  or  $f_{yy}(a, b) > 0$ local minimum  $f_{xx}(a, b)$  or  $f_{yy}(a, b) < 0$ D(a, b) > 0D(a, b) < 0saddle point

#### Extrema:

Given a function f optimized over restriction function g, if restriction has interior. Interior critical points: points (a, b) such that  $\nabla f(a, b) = 0$ 

Boundary critical points: Traditional method: eliminate variable from f using a. Break up the boundary into sections parametrized by one variable. This reduces to finding extrema of one variable functions,

where the endpoints must be considered. Lagrange Multipliers:  $\nabla f = \lambda \nabla g$ , system in addition to g.

#### Chapter 3

Coordinate Conversions

(x, y, z)	$(r, \theta, z)$	(x, y, z)	$(\rho, \theta, \phi)$
æ	$r\cos(\theta)$	x	$\rho \cos(\theta) \sin(\phi)$
y	$r \sin(\theta)$	y	$\rho \sin(\theta) \sin(\phi)$
2	z	z	$\rho \cos(\phi)$
$x^{2} + y^{2}$	r <sup>2</sup>	$x^2 + y^2 + z^2$	$\rho^2$
dV	$rdrdzd\theta$	dV	$\rho^2 \sin(\phi) d\rho d\phi d\theta$
Polar is c	ylindrical coord	linates where $z = 0$	and without dz.

#### Iterated Integrals:

$$\begin{split} \operatorname{Area} &= \iint_{D} dA & \operatorname{Mass} &= \iint_{D} \delta(x, y, y, y, z) \\ \operatorname{Volume} &= \iiint_{E} dV & \operatorname{Mass} &= \iiint_{E} \delta(x, y, y, y, z) \\ \end{split}$$

where  $\delta$  are density per unit area / unit volume Surface Area:

Surface parametrized by  $\vec{r}(u, v)$ , then at point  $(u_0, v_0)$  $\vec{r}_{\nu}(u_0, v_0)$  and  $\vec{r}_{\nu}(u_0, v_0)$  linearly independent tangent vectors.

$$dS = |\vec{r}_u(u_0, v_0) \times \vec{r}_v(u_0, v_0)| dudv$$
 Integrating over surface  $D$ ,

Surface Area = 
$$\iint_{D} |\vec{r}_{u}(u_{0}, v_{0}) \times \vec{r}_{v}(u_{0}, v_{0})| du dv$$

#### If z = f(x, y), then $\vec{r}(u, v) = (u, v, f(u, v))$ . Surface Area = $\iint \sqrt{f_x^2 + f_y^2 + 1} dxdy$

### Chapter 4

### Gradient Operator, Divergence, Curl:

$$\vec{\nabla} = \left(\frac{\partial}{\partial x_1}, \frac{\partial}{\partial x_2}, \cdots\right)$$
 div $(\vec{F}) = \vec{\nabla} \cdot \vec{F}$  curl $(\vec{F}) = \vec{\nabla} \times \vec{F}$   
2D curl: for  $\vec{F} = (P, Q)$ , then z component of curl is named  
curl\_- $(\vec{F}) = Q_- - P_-$ 

#### Line Integrals:

In a force field  $\vec{F} = (P, O)$ , a curve C parametrized by  $\vec{\tau}(u)$ where  $u_0 \le u \le u_1$ , then the work is

$$W = \int_C \vec{F} \cdot d\vec{r} = \int_{u_0}^{u_1} \vec{F}(\vec{r}(u)) \cdot \vec{r'}(u) du$$

#### Green's Theorem:

For a closed curve  $\partial R$  that bounds the region R,

$$\boxed{\int_{\partial R} \vec{F} \cdot d\vec{r} = \iint_{R} Q_{x} - P_{y} dA}$$

If the curve C can be closed by a simple line segment L, then  $C^* = C + L$  where  $C^*$  is the concatenation of  $\tilde{C}$  and L that encloses the region D. Then,

$$\int_C \vec{F} \cdot d\vec{r} = \int_{C^*} \vec{F} \cdot d\vec{r} - \int_L \vec{F} \cdot d\vec{r}$$
 Green's Theorem can be applied to  $C^*$ , and  $L$  can be split,

$$\int \vec{F} \cdot d\vec{r} = \iint Q_x - P_y dA - \int P dx + Q dy$$

$$\int_{C} F \cdot d\vec{r} = \iint_{D} Q_{x} - P_{y}dA - \int_{L} Pdx + Qdy$$

$$- \text{For simple line segments, } dx \text{ or } dy \text{ are } 0, \text{ and } x \text{ or } y \text{ constants.}$$

### Flux Integral:

For a region 
$$D$$
, parametrized by  $\vec{r}(u, v)$  over the domain  $R$ ,  
Flux =  $\iint_{-} \vec{F} \cdot \vec{n} dS = \iint_{-} \vec{F}(\vec{r}(u, v)) \cdot (\vec{r}_u(u, v) \times \vec{r}_v(u, v)) du dv$ 

#### Divergence Theorem: Mass = $\iint \delta(x, y)dA$ For a closed surface $\partial E$ that bounds the solid region E,

Flux = 
$$\iint_{\partial E} \vec{F} \cdot \vec{n} dS = \iiint_{E} \vec{\nabla} \cdot \vec{F} dV$$

Similarly to Green's Theorem, if D can be closed by a simple surface E, then  $D^* = D \cup E$  is the union of D and E that encloses the solid region F. E must have a normal vector such that  $D^*$  is oriented outward

$$\iint_{D} \vec{F} \cdot \vec{n} dS = \iint_{D^{*}} \vec{F} \cdot \vec{n} dS - \iint_{E} \vec{F} \cdot \vec{n} dS$$

The Divergence Theorem can be applied to  $D^*$ 

$$\iint_{D} \vec{F} \cdot \vec{n} dS = \iiint_{F} \vec{\nabla} \cdot \vec{F} dV - \iint_{E} \vec{F} \cdot \vec{n} dS$$

For a simple surface E,  $\vec{n}$  points along an axis

### Stokes' Theorem:

$$\left[\int_{\partial R} \vec{F} \cdot d\vec{r} = \iint_{R} (\vec{\nabla} \times \vec{F}) \cdot \vec{n} dS\right]$$
Stokes' Theorem is a generalization of Green's Theorem where

Stokes' Theorem simplifies problems where R shares a boundary with a simpler shape of a compatible orientation.

5/10

# How to use LATEX

## Windows

# Mac OS

MiKTeX

MacTeX

TeX Live

## Other

- Editors: vim and vimtex, emacs and AUCTeX
- IDE: VSCode and LaTeX Workshop
- Online: Overleaf (what we'll be using today)

# Typesetting a Basic Document: Document Classes

- All documents must include a \documentclass{CLASS}.
- A set of defaults for specific use cases
- \documentclass[12pt, letterpaper]{article}, size 12 font article
- report, longer documents, dissertation
- beamer, what made these slides

# Typesetting a Basic Document: Environments

- \begin{F00} must be matched with \end{F00}, and everything between is in the F00 environment.
- document: a...document!
- itemize: this kind of bullet point list
- center: horizontally centered
- tabular: tables
- can define custom environments

# Typesetting Math

Time for a practical example, over to Overleaf!

# Helpful Tools

### General:

- Overleaf has extensive documentation
- Detexify remembering LATEX commands is hard

# Packages:

- siunitx: anything with units
- circuitikz: circuit diagrams
- minted: syntax highlighted code blocks
- amsmath, amssymb: extended math support