

Chapter 6 z-Transform



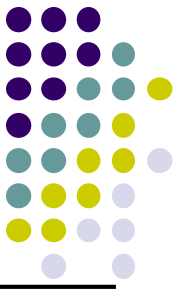
Part A: z-Transform

**Part B: The Inverse z-Transform
and z-Transform Theorems**

Part C: Convolution(卷积)

Part D: The Transfer Function

6.7 The Transfer Function



- **The convolution sum description of an LTI discrete-time system with an impulse response $h[n]$ is given by**

$$y[n] = \sum_{k=-\infty}^{\infty} h[k]x[n-k]$$

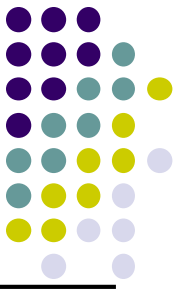
6.7 The Transfer Function



- Taking the z -transforms of both sides we get

$$\begin{aligned} Y(z) &= \sum_{n=-\infty}^{\infty} y[n]z^{-n} = \sum_{n=-\infty}^{\infty} \left(\sum_{k=-\infty}^{\infty} h[k]x[n-k] \right) z^{-n} \\ &= \sum_{k=-\infty}^{\infty} h[k] \left(\sum_{n=-\infty}^{\infty} \underline{x[n-k]} z^{-n} \right) \quad \text{变量代换} \\ &= \sum_{k=-\infty}^{\infty} h[k] \left(\sum_{l=-\infty}^{\infty} \underline{x[l]} z^{-(l+k)} \right) \end{aligned}$$

6.7 The Transfer Function



Or,
$$Y(z) = \sum_{k=-\infty}^{\infty} h[k] \underbrace{\left(\sum_{\ell=-\infty}^{\infty} x[\ell] z^{-\ell} \right)}_{X(z)} z^{-k}$$

Therefore,

$$Y(z) = \underbrace{\left(\sum_{k=-\infty}^{\infty} h[k] z^{-k} \right)}_{H(z)} X(z)$$

Thus, $Y(z) = H(z)X(z)$

6.7.1 Definition

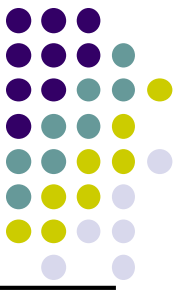


- **Transfer function or the system function**

$$H(z) = \frac{Y(z)}{X(z)}$$

$$H(z) = \sum_{n=-\infty}^{\infty} h[n]z^{-n}$$

6.7.2 Transfer Function Expression



- Consider an LTI discrete-time system characterized by a difference equation

$$\sum_{k=0}^N d_k y[n-k] = \sum_{k=0}^M p_k x[n-k]$$

- Its transfer function is obtained by taking the z -transform of both sides of the above equation
- Thus

$$H(z) = \frac{\sum_{k=0}^M p_k z^{-k}}{\sum_{k=0}^N d_k z^{-k}}$$

6.7.2 Transfer Function Expression

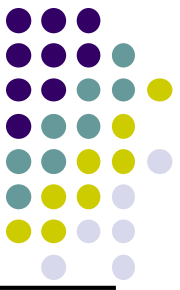


- Or, equivalently as

$$H(z) = z^{(N-M)} \frac{\sum_{k=0}^M p_k z^{M-k}}{\sum_{k=0}^N d_k z^{N-k}}$$

- An alternate form of the transfer function is given by

$$H(z) = \frac{p_0}{d_0} \cdot \frac{\prod_{k=1}^M (1 - \xi_k z^{-1})}{\prod_{k=1}^N (1 - \lambda_k z^{-1})}$$



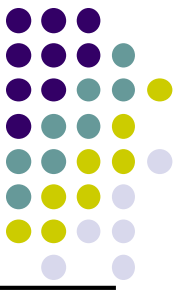
IIR数字滤波器传递函数的表达式

- For a **causal** IIR digital filter, the impulse response is a **causal** sequence.
- The ROC of the causal transfer function

$$H(z) = \frac{p_0}{d_0} z^{(N-M)} \frac{\prod_{k=1}^M (z - \xi_k)}{\prod_{k=1}^N (z - \lambda_k)}$$

is thus **exterior to a circle** going through the pole furthest from the origin

- Thus the ROC is given by $|z| > \max_k |\lambda_k|$



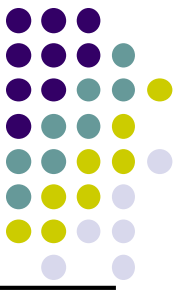
IIR数字滤波器传递函数的表达式

- **Example** - A **causal** LTI IIR digital filter is described by a constant coefficient difference equation given by

$$y[n]=x[n-1]-1.2x[n-2]+x[n-3]+1.3y[n-1]-1.04y[n-2]+0.222y[n-3]$$

- Its transfer function is therefore given by

$$H(z) = \frac{z^{-1} - 1.2z^{-2} + z^{-3}}{1 - 1.3z^{-1} + 1.04z^{-2} - 0.222z^{-3}}$$



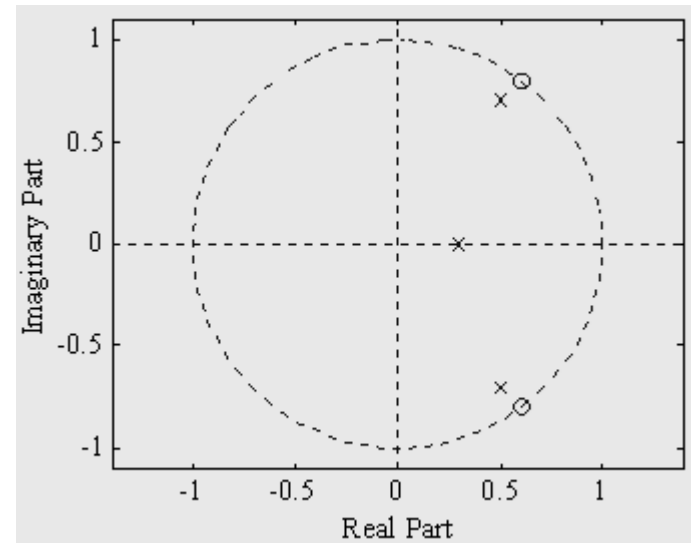
IIR数字滤波器传递函数的表达式

- **Alternate forms:**

$$\begin{aligned} H(z) &= \frac{z^2 - 1.2z + 1}{z^3 - 1.3z^2 + 1.04z - 0.222} \\ &= \frac{(z - 0.6 + j0.8)(z - 0.6 - j0.8)}{(z - 0.3)(z - 0.5 + j0.7)(z - 0.5 - j0.7)} \end{aligned}$$

- **Note: Poles farthest from $z=0$ have a magnitude $\sqrt{0.74}$**

ROC: $|z| > \sqrt{0.74}$





FIR数字滤波器传递函数的表达式

- FIR数字滤波器的卷积和方程可表达为

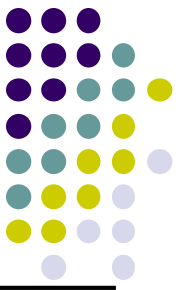
$$y[n] = \sum_{k=N_1}^{N_2} h[k]x[n-k] \quad N_1 < N_2$$

$$\sum_{k=0}^N d_k y[n-k] = \sum_{k=0}^M p_k x[n-k], d_0 = 1, d_k = 0, k = 1, \dots, N$$

- FIR数字滤波器的传递函数可表达为

$$H(z) = \sum_{n=N_1}^{N_2} h[n]z^{-n} = \sum_{k=N_1}^{N_2} p_k z^{-k}$$

- 注意，因果FIR滤波器的 $H(z)$ 的所有极点均在 z 平面的原点处。因此， $H(z)$ 的收敛域在除了 $z=0$ 之外的整个 z 平面上。



FIR数字滤波器传递函数的表达式

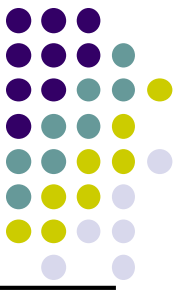
- **Example** - Consider the M -point moving-average FIR filter with an impulse response

$$h[n] = \begin{cases} 1/M, & 0 \leq n \leq M-1 \\ 0, & \text{otherwise} \end{cases}$$

- Its transfer function is then given by

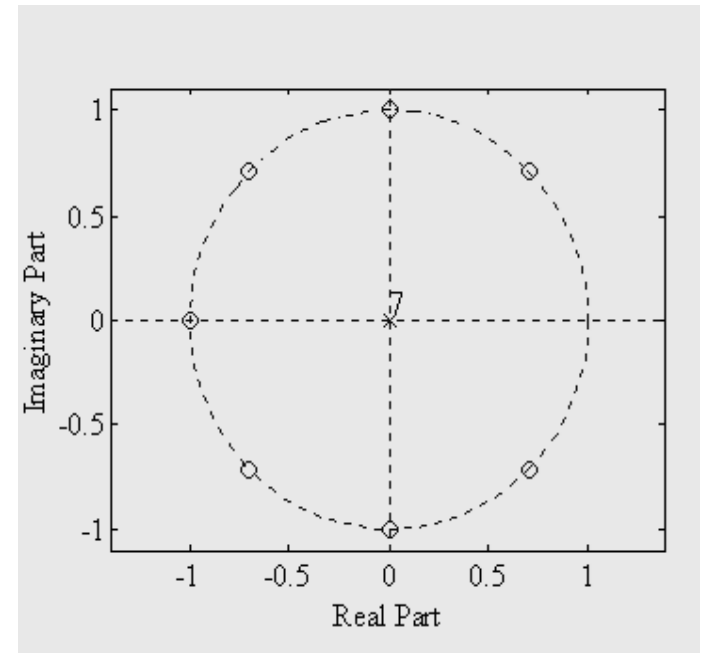
$$H(z) = \frac{1}{M} \sum_{n=0}^{M-1} z^{-n} = \frac{1 - z^{-M}}{M(1 - z^{-1})} = \frac{z^M - 1}{M[z^{M-1}(z - 1)]}$$

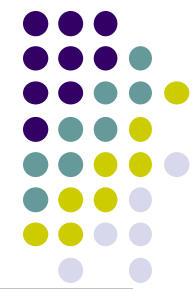
FIR数字滤波器传递函数的表达式



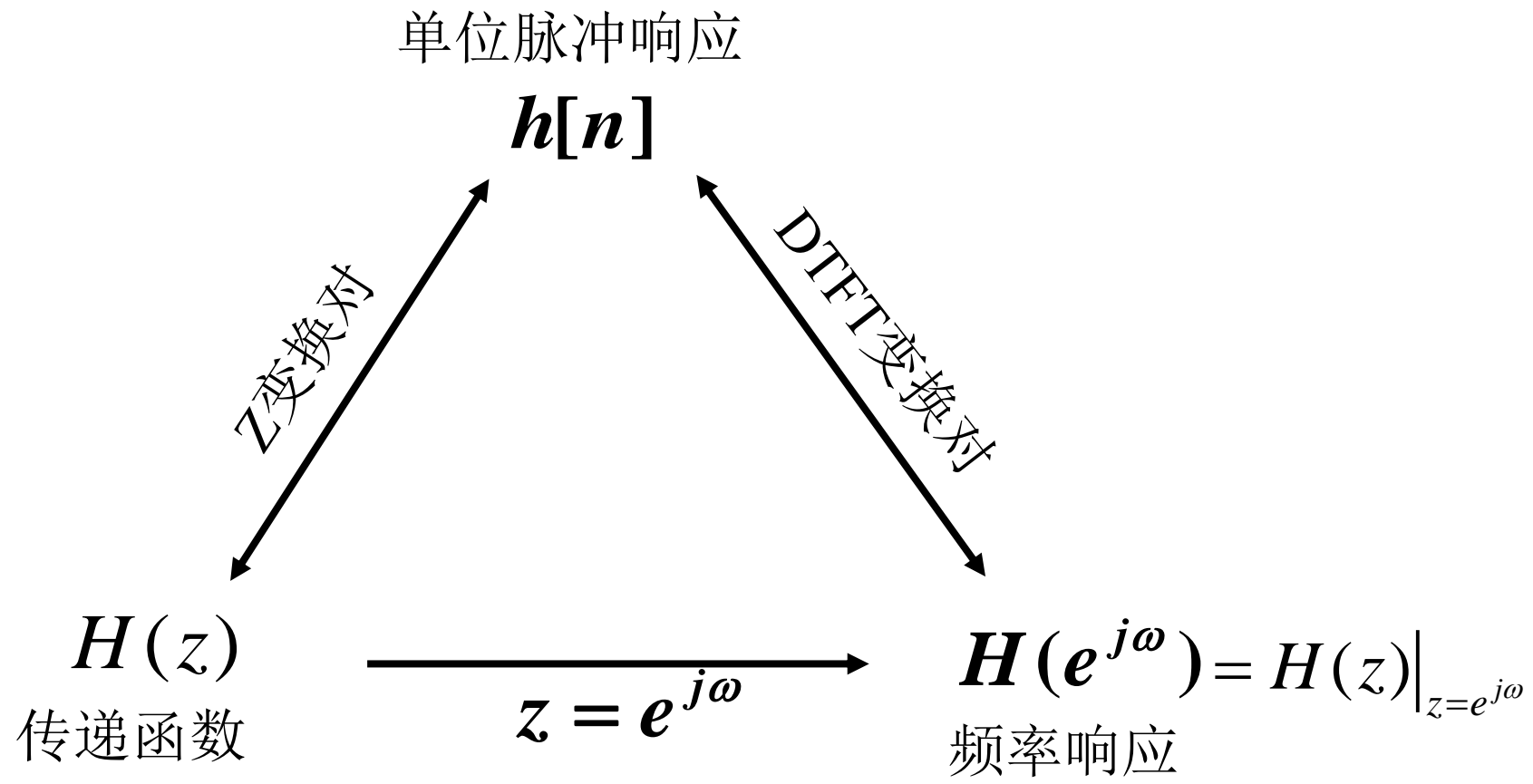
- **M zeros on the unit circle at $z = e^{j2\pi k/M}$, $0 \leq k \leq M-1$**
- **M-1 poles at $z = 0$ and 1 pole at $z = 1$**
- **The pole at $z = 1$ exactly cancels the zero at $z = 1$**
- **The ROC is the entire z-plane except $z = 0$**

$M = 8$

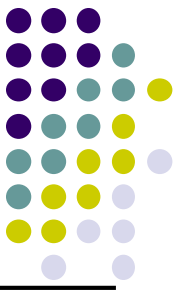




从传递函数得到频率响应



6.7.3 Frequency Response from Transfer Function



- For a **stable** rational transfer function in the form

$$H(z) = \frac{p_0}{d_0} z^{(N-M)} \frac{\prod_{k=1}^M (z - \xi_k)}{\prod_{k=1}^N (z - \lambda_k)}$$

the factored form of the frequency response is given by

$$H(e^{j\omega}) = \frac{p_0}{d_0} e^{j\omega(N-M)} \frac{\prod_{k=1}^M (e^{j\omega} - \xi_k)}{\prod_{k=1}^N (e^{j\omega} - \lambda_k)}$$

6.7.3 Frequency Response from Transfer Function



- The **magnitude function** is given by

$$|H(e^{j\omega})| = \left| \frac{p_0}{d_0} \right| e^{j\omega(N-M)} \frac{\prod_{k=1}^M |e^{j\omega} - \xi_k|}{\prod_{k=1}^N |e^{j\omega} - \lambda_k|} = \left| \frac{p_0}{d_0} \right| \frac{\prod_{k=1}^M |e^{j\omega} - \xi_k|}{\prod_{k=1}^N |e^{j\omega} - \lambda_k|}$$

- The **phase response** for a rational transfer function is of the form

$$\arg H(e^{j\omega}) = \arg(p_0/d_0) + \omega(N-M) + \sum_{k=1}^M \arg(e^{j\omega} - \xi_k) - \sum_{k=1}^N \arg(e^{j\omega} - \lambda_k)$$

6.7.4 Geometric Interpretation of Frequency Response Computation

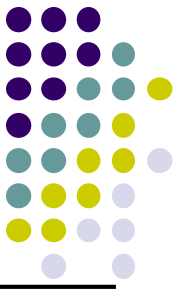


- The factored form of the frequency response

$$H(e^{j\omega}) = \frac{p_0}{d_0} e^{j\omega(N-M)} \frac{\prod_{k=1}^M (e^{j\omega} - \xi_k)}{\prod_{k=1}^N (e^{j\omega} - \lambda_k)}$$

is convenient to develop a **geometric interpretation** of the frequency response computation from the pole-zero plot as ω varies from 0 to 2π on the unit circle

6.7.4 Geometric Interpretation of Frequency Response Computation



- The geometric interpretation can be used to obtain a **sketch** of the response as a function of the frequency
- A typical factor in the factored form of the frequency response is given by

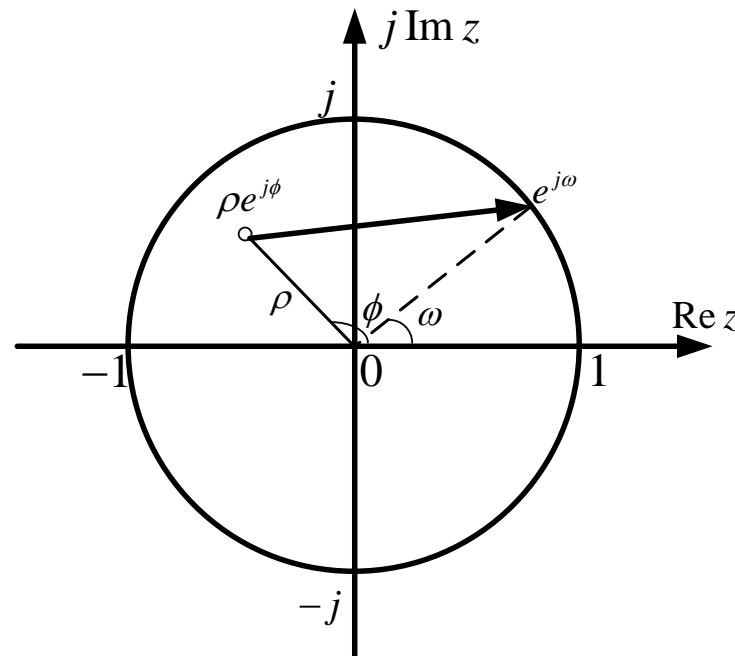
$$(e^{j\omega} - \rho e^{j\Phi})$$

where $\rho e^{j\Phi}$ is a zero if it is zero factor or is a pole if it is a pole factor

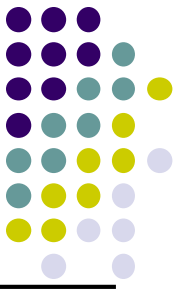
6.7.4 Geometric Interpretation of Frequency Response Computation



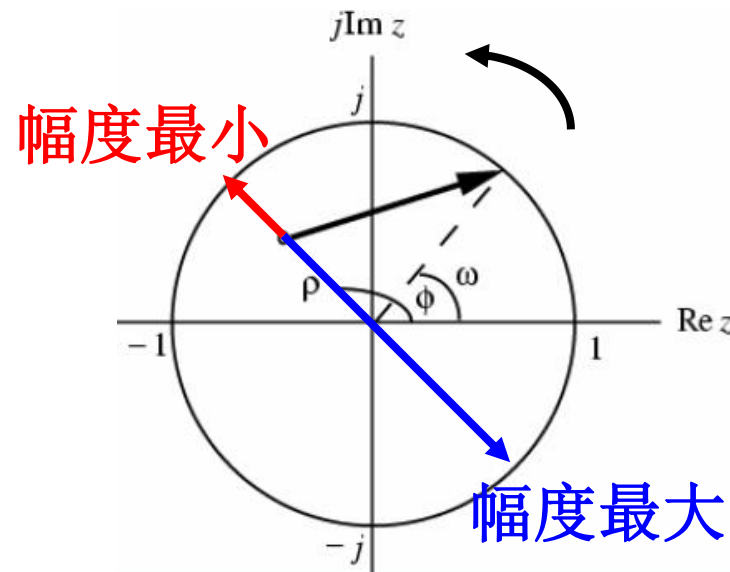
- As shown below in the z -plane the factor $(e^{j\omega} - \rho e^{j\phi})$ represents a vector starting at the point $z = \rho e^{j\phi}$ and ending on the unit circle at $z = e^{j\omega}$



6.7.4 Geometric Interpretation of Frequency Response Computation



- As ω is varied from 0 to 2π , the tip of the vector moves counterclockwise (逆时针) from the point $z = 1$ tracing the unit circle and back to the point $z = 1$



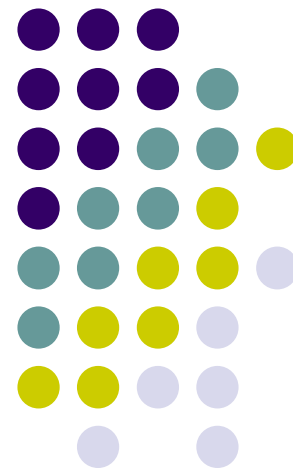
6.7.4 Geometric Interpretation of Frequency Response Computation



- To highly **attenuate** signal components in a specified frequency range, we need to place zeros very close to or on the unit circle in this range (零点——谷值)
- Likewise, to highly **emphasize** signal components in a specified frequency range, we need to place poles very close to or on the unit circle in this range (极点——峰值)

Question:

- 1、极点的位置对系统的稳定性会有影响吗？
- 2、系统在Z域的稳定性条件是什么？



6.7.5 Stability Condition in Terms of the Pole Locations



- A causal LTI digital filter is BIBO stable if and only if its impulse response $h[n]$ is absolutely summable, i.e.,

$$S = \sum_{n=-\infty}^{\infty} |h[n]| < \infty$$

- An FIR digital filter with bounded impulse response is always stable
- On the other hand, an IIR filter may be unstable if not designed properly

6.7.5 Stability Condition in Terms of the Pole Locations



- The ROC of the z -transform $H(z)$ of the impulse response sequence $h[n]$ is defined by values of $|z| = r$ for which $h[n]r^{-n}$ is absolutely summable

$$H(z) = \sum_{n=-\infty}^{\infty} h[n]z^{-n} \stackrel{z=re^{j\omega}}{=} \sum_{n=-\infty}^{\infty} h[n]r^{-n}e^{-j\omega n}$$

$$S' = \sum_{n=-\infty}^{\infty} |h[n]r^{-n}e^{-j\omega n}| = \sum_{n=-\infty}^{\infty} |h[n]r^{-n}| < \infty$$

$$\stackrel{|r|=1}{\Rightarrow} \sum_{n=-\infty}^{\infty} |h[n]r^{-n}| = \sum_{n=-\infty}^{\infty} |h[n]| < \infty$$

BIBO stable

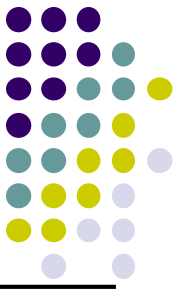
6.7.5 Stability Condition in Terms of the Pole Locations



- Thus, if the ROC **includes the unit circle** $|z| = 1$, then the digital filter is **stable**, and vice versa
- This in turn implies that the DTFT $H(e^{j\omega})$ of $\{h[n]\}$ exists
- Now, if the ROC of the z -transform $H(z)$ includes the unit circle, then

$$H(e^{j\omega}) = H(z) \Big|_{z=e^{j\omega}}$$

6.7.5 Stability Condition in Terms of the Pole Locations



- Consider the **causal** IIR digital filter with a rational transfer function $H(z)$ given by

$$H(z) = \frac{\sum_{k=0}^M p_k z^{-k}}{\sum_{k=0}^N d_k z^{-k}}$$

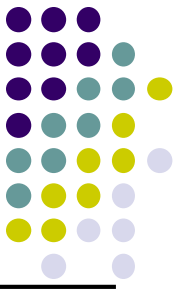
- Its impulse response $\{h[n]\}$ is a **right-sided** sequence
- The ROC of $H(z)$ is exterior to a circle going through the pole furthest from $z = 0$

6.7.5 Stability Condition in Terms of the Pole Locations



- For a **stable and causal** digital filter for which $h[n]$ is a right-sided sequence, the ROC will include the unit circle and entire z-plane including the point $z=\infty$
- Conclusion: **All poles** of a **causal stable** transfer function $H(z)$ must be **strictly inside the unit circle**.

6.7.5 Stability Condition in Terms of the Pole Locations



- Example - The factored form of

$$H(z) = \frac{1}{1 - 1.845z^{-1} + 0.850856z^{-2}}$$

is

$$H(z) = \frac{1}{(1 - 0.902z^{-1})(1 - 0.943z^{-1})}$$

which has a real pole at $z = 0.902$ and a real pole at $z = 0.943$

- Since both poles are inside the unit circle, $H(z)$ is BIBO stable

6.7.5 Stability Condition in Terms of the Pole Locations



- **Example** - The factored form of

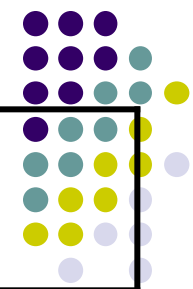
$$\hat{H}(z) = \frac{1}{1 - 1.85z^{-1} + 0.85z^{-2}}$$

is

$$\hat{H}(z) = \frac{1}{(1 - z^{-1})(1 - 0.85z^{-1})}$$

which has a real pole on the unit circle at $z = 1$ and the other pole inside the unit circle

- Since one pole is not inside the unit circle, $H(z)$ is unstable



系统	时域条件	Z域条件
因果	$h(n) \equiv 0 \ (n < 0)$	ROC: $R_1 < Z \leq \infty$
稳定	$\sum_{n=-\infty}^{\infty} h(n) < \infty$	ROC: 包含单位圆
因果 稳定	所有极点全在单位圆内部	

Homework

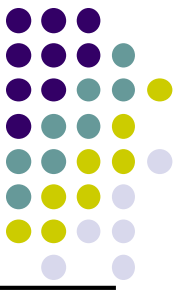


- **Problems: 6.2(a,b), 6.5, 6.7, 6.8(a)(i,iv), 6.13(a), 6.42, 6.44, 6.81**
- **Matlab Exercises: M6.1(a), M6.5**

Consider a LTI *causal* system whose I/O difference equation is $y(n) = \frac{5}{2}y(n-1) - y(n-2) + x(n-1)$



- 1) Compute the transform function.
- 2) Determine the corresponding pole/zero pattern and the ROC.
- 3) Compute the impulse response.
- 4) It is easy to know this system is not stable. Determine another stable (but anticausal) system satisfying the same I/O difference equation.



Solution:

$$\text{a) } H(z) = \frac{z^{-1}}{1 - \frac{5}{2}z^{-1} + z^{-2}} = \frac{z^{-1}}{(1 - 2z^{-1})(1 - \frac{1}{2}z^{-1})}$$

b) zeroes: $z=0$;

poles: $z=2, z=1/2$;

ROC: $|z|>2$

$$\text{c) } H(z) = \frac{\frac{2}{3}}{1 - 2z^{-1}} + \frac{-\frac{2}{3}}{1 - \frac{1}{2}z^{-1}}$$
$$h[n] = \frac{2}{3} 2^n \mu[n] - \frac{2}{3} \left(\frac{1}{2}\right)^n \mu[n]$$



d) ROC: $1/2 < |z| < 2$,

$$h[n] = -\frac{2}{3} 2^n \mu[-n - 1] - \frac{2}{3} \left(\frac{1}{2}\right)^n \mu[n]$$