0.1 Electrical subsystem analysis

A diagram of the electrical subsystem is shown in figure 1, assuming that all the phases have the same inductances and resistances. From it, it's possible to obtain expressions for v_{ab}, v_{bc} and v_{ca} (defined as $v_a - v_b$, $v_b - v_c$ and $v_c - v_a$, respectively) [1, p. 457-459]. That, added to the fact that the currents in each phase must sum to zero (Kirchhoff's current law applied at the central node) and assuming that the mutual inductances are negligible, leads to the following equations:

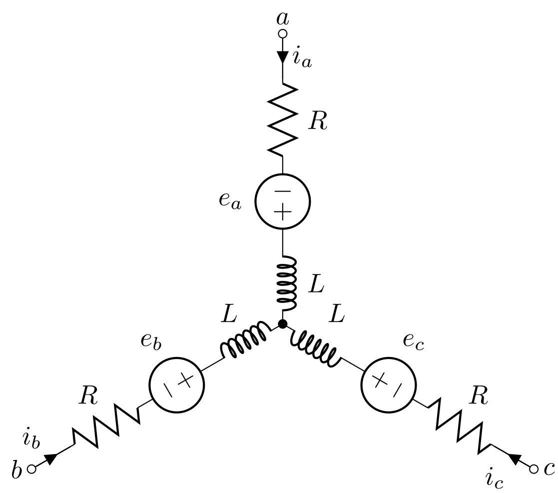

Figure 1: Diagram of the electrical circuit of a three-phase BLDC motor

$$v_{ab} = R(i_a - i_b) + L\frac{d}{dt}(i_a - i_b) + e_a - e_b \tag{1}$$

$$v_{bc} = R(i_a + 2i_b) + L\frac{d}{dt}(i_a + 2i_b) + e_b - e_c \tag{2}$$

$$i_a + i_b + i_c = 0. \tag{3}$$

Additionally, since the back-emfs in each phase are proportional to the angular velocity, we can write them as

$$e_a = \frac{f_a(\theta_e).K_e}{2}.\frac{d\theta_m}{dt} \tag{4}$$

$$e_b = \frac{f_b(\theta_e).K_e}{2}.\frac{d\theta_m}{dt} \tag{5}$$

$$e_c = \frac{f_c(\theta_e).K_e}{2}.\frac{d\theta_m}{dt}. \tag{6}$$

Here, K_e is the motor's back-emf constant and $f_a(\theta_e)$, $f_b(\theta_e)$ and $f_c(\theta_e)$ are the functions that give the intended waveform for the back-emf; θ_m is the rotor's angular position in relation to the stator and θ_e is the electrical angular position, defined as

$$\theta_e = \theta_m.\frac{P}{2}, \tag{7}$$

where P is the motor's number of poles.

Assuming constant a constant air gap in the motor, an analysis of the consumed power of the machine yields the electromagnetic torque expression [1, p. 459]. This can be further simplified by substituting equations 4 through 6 in the result. The final expression is

$$T_e = \frac{K_t}{2}.\Big(f_a(\theta_e).i_a + f_b(\theta_e).i_b + f_c(\theta_e).i_c\Big). \tag{8}$$

Equations 1 through 8 model the dynamic relationship between the electromagnetic torque and the currents, back-emfs and voltages of each phase of the BLDC.

0.2 Mechanical subsystem analysis

A diagram for the mechanical subsystem is illustrated in figure 2 (to improve clarity, the load is not shown in this diagram).

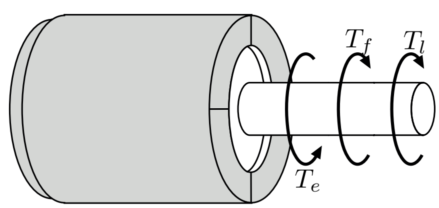

Figure 2: Mechanical subsystem

Applying Newton's second law to the motor's rotor, we obtain the following equation

$$J.\frac{d^2\theta_m}{dt^2} = T_e - T_f - T_l, \tag{9}$$

where J is the motor's rotor inertia, T_f is the resistance torque due to friction and T_l is the torque applied by the load to the rotor.

In order to provide an accurate motor model for a wide range of angular velocities, not only viscous friction must considered in the model. Therefore, T_f is decomposed as viscous friction (referred to as T_{f1}) and Coulomb friction (referred to as T_{f2})

$$T_f = T_{f1} + T_{f2}. \tag{10}$$

Viscous frictions can be calculated with

$$T_{f1} = K_d.\frac{d\theta_m}{dt}, \tag{11}$$

where K_d is the damping constant.

And Coulomb's model of friction [2, p.171] is given by

$$T_{f2} = \begin{cases} -T_k.sign(\frac{d\theta}{dt}) & : \frac{d\theta_m}{dt} \neq 0 \\ -min(T_s, T_e - T_l).sign(T_e - T_l) & : \frac{d\theta_m}{dt} = 0 \end{cases} \quad (12)$$

where T_k is the static friction constant and T_s is the kinetic friction constant.

Analogously to section 0.1, equations 9 through 12 model the dynamic relationship between the electromagnetic torque and the angular position of the rotor. This equations, together with equations 1 through 8, constitute the full mathematical model used to simulate the BLDC.

References

[1] R. Krishnan. *Permanent Magnet Synchronous and Brushless DC Motor Drives*. Boca Raton: CRC/Taylor & Francis, 2010.

[2] Andy Ruina & Rudra Pratap. *Introduction to Statics and Dynamics*. Oxford University Press, 2015.