

# X-RAY INTERFERENCE METHODS OF ELECTRON BEAM DIAGNOSTICS

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## Abstract

Electron beam diagnostics methods based on interference and diffraction of synchrotron radiation (SR) in hard X-ray range will be discussed. Two simple optical schemes providing X-ray interference patterns highly sensitive to transverse size of the emitting electron beam, will be considered. For each scheme, the visibility of fringes in the pattern depends on transverse size of the electron beam. However, the pattern is also determined by the scheme geometry, shape and material of diffracting bodies. Therefore, for correct interpretation of the experimental results, high-accuracy computation of SR emission and propagation in the framework of physical optics should be used. Examples of practical measurements and processing of the results are presented.

## 1 INTRODUCTION

Visible light interference methods have proved to be very efficient for diagnostics of relativistic charged particle beams emitting synchrotron radiation in magnetic fields of accelerators [1-6]. Nevertheless, since 3<sup>rd</sup>-generation SR sources are mainly dedicated for X-rays, the use of X-rays for electron beam diagnostics in these accelerators can be advantageous. Such diagnostics can be based on the same equipment that is used in other experiments; besides, it may offer higher resolution.

A number of X-ray experimental techniques benefiting from high spatial coherence of the SR, e.g. phase-contrast imaging, holography, interferometry, have been developed [7-11]. These techniques require characterisation and “in-place” control of the source coherence, which makes the X-rays based beam diagnostics further important.

This paper considers two very simple diffraction/interference schemes, which can be readily used for beam diagnostics at any X-ray beamline (not necessarily fully dedicated for the diagnostics). One is the well-known Fresnel diffraction at a slit, and the other is a wavefront-splitting interference scheme where a thin fiber is used as an obstacle and phase-shifting object. As different from previous considerations made for isotropic source with finite transverse size [12-14], the current paper takes into account peculiarities of synchrotron (undulator) radiation emitted by an electron beam with finite transverse emittance (i.e., not only with the size, but also with angular divergence).

## 2 BASICS OF THE METHODS

### 2.1 Isotropic Source with Finite Transverse Size

Let us recall that in the case when a source has finite transverse size, and different points of the source emit incoherently, the resulting intensity of the radiation passed through an optical system to a detector plane is obtained by summing up intensities of emission from all points of the source [15]:

$$I(x, y) = \iint I_0(x_s, y_s) B(x_s, y_s) dx_s dy_s, \quad (1)$$

where  $(x, y)$  are transverse coordinates in the detector plane,  $(x_s, y_s)$  transverse coordinates at the source,  $I_0$  intensity from a point source (referenced below as point-source intensity), and  $B$  the source brightness.

For many simple diffraction and interference schemes with a source emitting spherical waves, in small-angle approximation, Eq. (1) is a convolution-type integral, i.e.:

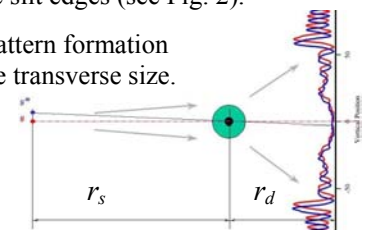
$$I_0(x, y; x_s, y_s) \approx \tilde{I}_0(x - mx_s, y - my_s), \quad (2)$$

where  $m = -r_d/r_s$  is a “magnification” factor, with  $r_s$  being distance from the source to an obstacle, and  $r_d$  distance from the obstacle to the detector (see Fig. 1). We note that this effect is used in pinhole cameras (which are successfully applied for electron beam diagnostics [16]).

If Eq. (2) is valid,  $\tilde{I}_0(x, y)$  is known, and the resulting intensity  $I(x, y)$  is measured to a sufficient accuracy, one can try to reconstruct  $B(x_s, y_s)$  using the Wiener filtering [17] or a regularization technique [18].

The resolution of an optical scheme at the source size measurement depends on the point-source intensity  $\tilde{I}_0(x, y)$ . In the case of Fresnel diffraction at a slit,  $\tilde{I}_0$  possesses fringes with the widths on the order of  $\lambda r_d/a$ , where  $\lambda$  is the radiation wavelength and  $a$  the slit size. This can be compared with the source image size  $\sigma r_d/r_s$ . However, the resolution of this scheme can be much better, because  $\tilde{I}_0$  has also smaller details originating from “interaction” of the slit edges (see Fig. 2).

Figure 1: Interference pattern formation from a source with finite transverse size.



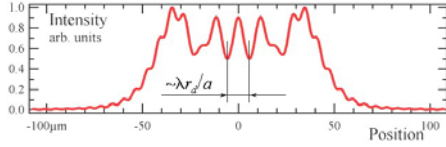


Figure 2: Point-source intensity distribution at the Fresnel diffraction at a slit.

## 2.2 Finite-Emittance Electron Beam

This section describes how a more accurate computation of the SR emitted by an electron beam and propagated through an optical system, can be performed. Such computation allows to verify whether a particular approximation corresponds to realistic experimental conditions, and thus to choose an adequate model and method for processing the experimental results.

Starting from Fourier transformations of the retarded potentials, one can obtain the following expression for the frequency-domain electric field of radiation emitted by a relativistic electron (Gaussian System) [19]:

$$\vec{E} = iek \int_{-\infty}^{+\infty} [\vec{\beta} - \vec{n} [1 + i(kR)^{-1}]] R^{-1} \exp[ik(c\tau + R)] d\tau, \quad (3)$$

where  $k$  is a wave number,  $\vec{\beta} = \vec{\beta}(\tau)$  instant relative velocity of electron,  $\vec{n} = \vec{n}(\tau)$  unit vector directed from instant electron position to an observation point,  $R = R(\tau)$  distance from the electron to the observation point,  $c$  speed of light,  $e$  charge of electron. Eq.(3) describes practically all kinds of single-electron emission in the near- and far-field observation regions. It allows to compute SR electric field at some longitudinal position, e.g. before the first optical element of a beamline. Typically, only transverse components of the electric field (3) need to be considered.

The wavefront propagation through transmission optical elements can be simulated by multiplication of the transverse electric field by a complex transmission function of transverse position, which can take into account attenuation and phase shift of the wave field.

Assuming small angles and distances considerably larger than wavelength, the transverse component of the electric field propagated through a drift space  $\vec{E}_{\perp 2}$  can be computed from the electric field  $\vec{E}_{\perp 1}$  before the drift space by the well-known Huygens-Fresnel principle

$$\vec{E}_{\perp 2} = -ik(2\pi)^{-1} \iint_{\Sigma} \vec{E}_{\perp 1} S^{-1} \exp(ikS) d\Sigma, \quad (4)$$

where  $S$  is a distance from a point on this surface to an observation point. If the integration surface  $\Sigma$  is (a part of) a plane perpendicular to the optical axis, and the observation points belong to another plane perpendicular to the optical axis, then Eq.(4) is a convolution-type integral that can be quickly computed by applying the convolution theorem and 2D FFT.

To obtain intensity distribution of the SR emitted by the finite-emittance electron beam, one needs to sum-up intensities obtained after propagation of electric fields

from individual electrons. In general case, the single-electron intensity  $I_0$  depends on transverse coordinates, angles and energy of the electron  $(x_s, y_s, x'_s, y'_s, E_s)$ , so that the final intensity is derived by integration with respect to all these variables:

$$I(x, y) = \int I_0(x, y; x_s, y_s, x'_s, y'_s, E_s) \times n(x_s, y_s, x'_s, y'_s, E_s) dx_s dy_s dx'_s dy'_s dE_s \quad (5)$$

where  $n$  is particle distribution in the beam phase space.

For different types of SR and different optical schemes, the single-electron intensity  $I_0$  may not strongly depend on some of the phase-space variables. In each particular case, this dependence, as well as the validity of the convolution approximation (e.g. Eq.(2)), can be checked numerically, by making single-electron wavefront propagations for different values of  $(x_s, y_s, x'_s, y'_s, E_s)$ .

When performed for the Fresnel diffraction of undulator radiation (UR) at a slit, this test showed that if angular aperture of the slit is comparable to the opening angle of the single-electron UR, and to the electron beam angular divergence, then the latter can contribute to the final intensity distribution of the diffracted radiation. This contribution is typically smaller than that of the beam transverse size, however it should be taken into account at results processing of the diagnostics measurements.

The numerical methods based on Eqs.(3)-(5) are implemented in the SRW, a physical optics computer code for synchrotron radiation [20].

## 3 MEASUREMENTS

The measurements of Fresnel diffraction and the interference from a fiber were carried out at ID22 beamline of ESRF, using the radiation from a planar undulator (38 periods of 42 mm) at 11 keV photon energy. After the undulator, the radiation was deflected horizontally by a mirror (in order to suppress high-energy part of the UR spectrum), and then passed through a double-crystal monochromator.

In the Fresnel diffraction scheme, a 100  $\mu\text{m}$   $\times$  100  $\mu\text{m}$  rectangular slit was located at 37.6 m distance from the middle of the undulator, and the distance from the slit to detector was 5.5 m.

In another scheme, a cylindrical boron fiber was placed at a distance of 40.6 m from the undulator, and the detector was located at 1.85 m after the fiber. The diameter of the fiber was 100  $\mu\text{m}$ ; the fiber possessed a tungsten core with a diameter of  $\sim$ 15  $\mu\text{m}$ .

The intensity distributions in the two schemes were registered by a 2D coordinate-sensitive detector consisted of a 1  $\mu\text{m}$  thick YAG scintillator coupled by a visible light microscope to a CCD camera. The re-focused CCD pixel size was 0.24  $\mu\text{m}$ , and the resolution, estimated as FWHM size of the point-spread function, was on the order of 1  $\mu\text{m}$ . The intensity distributions registered in the two schemes are shown in Fig. 3 on the left.

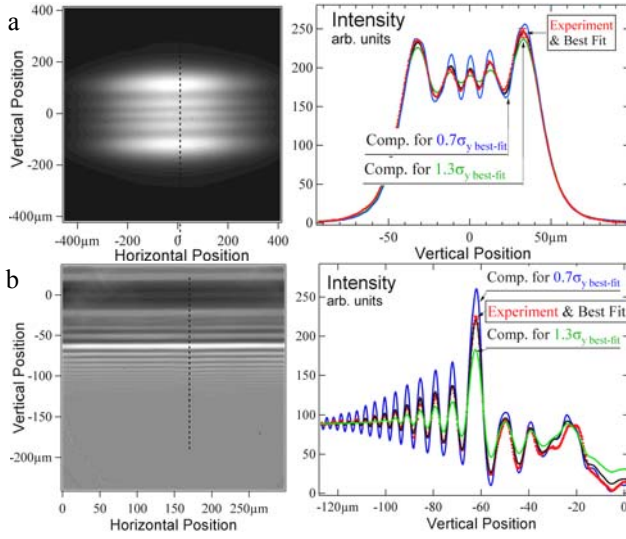


Figure 3: Measured intensity distributions and results of the fitting procedure for the Fresnel diffraction at a slit (a) and interference from a boron fiber (b).

The right-hand plots in Fig. 3 illustrate the fitting of vertical slices of the measured intensity by distributions computed for different values of vertical electron beam emittance  $\varepsilon_y$ , using a numerical procedure based on Eqs. (3)-(5). At the fitting, the vertical beam size and divergence were recalculated for the middle of the straight section via:

$$\sigma_y = (\varepsilon_y \beta_y)^{1/2}; \quad \sigma'_y = (\varepsilon_y / \beta_y)^{1/2}, \quad (6)$$

with the value of the vertical beta function assumed to be known:  $\beta_y = 2.5$  m [21]. The particle distribution in the electron beam was assumed Gaussian over vertical position and angle. The detector point-spread function was approximated by the Gaussian as well.

The vertical RMS beam size value obtained from the Fresnel diffraction measurements is:  $\sigma_y = 22 \pm 4$   $\mu\text{m}$ , and from the interference at the fiber:  $\sigma_y = 24 \pm 5$   $\mu\text{m}$ . These values are larger than the vertical beam size value in the middle of a straight section which follows from the ESRF pinhole camera measurements performed at larger  $\beta_y$  [21]. The most probable reason for this discrepancy is the presence of the mirror and the vertically reflecting crystal monochromator in the optical scheme. These two optical components were not taken into account at processing of the experimental results, however, each of them could reduce the transverse coherence of the wavefront, due to imperfections of the mirror surface and possible contribution of the crystal transfer function, respectively.

## 5 CONCLUSIONS

X-ray diffraction and interference schemes can be used for beam diagnostics in 3<sup>rd</sup>-generation SR sources. The schemes are very simple and can be applied nearly at any X-ray beamline. This diagnostics has very high theoretical resolution: on the order of microns. However, it is also very sensitive to the quality of optics. Therefore,

to avoid systematic errors, transfer functions of the optical elements should be known to a reasonable accuracy; the use of transmission X-ray optics is preferable.

On the other hand, this type of measurements and data processing can be applied to characterize the transverse coherence properties of an entire X-ray beamline, including both the source and the optics in use.

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