

1. The 7-V zener diode in the circuit of Fig. 1 is specified to have  $V_Z = 7V$  at  $I_Z = 5mA$ ,  $r_Z = 20\Omega$ , and  $I_{ZK} = 0.2mA$ . The supply voltage  $V^+$  is nominally 10V but can vary by  $\pm 1V$ .

(a) What is the maximum current the zener diode conducts in this design? What is the output voltage of the circuit and the power dissipation of the zener diode under this condition? (9 points)

X (b) What is the minimum value of  $R_L$  for which the diode still operates in the breakdown region? (4 points)

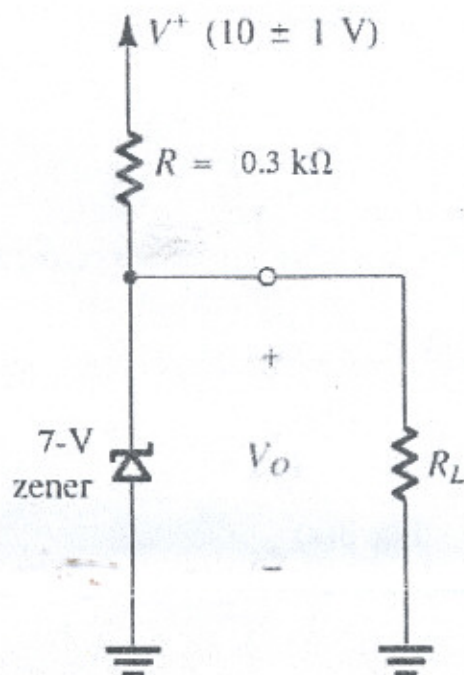


Fig. 1

2. For a Si pn junction operating at 300K, the electron concentration in p-Si is  $10^3/cm^3$ , and the hole concentration in n-Si is  $10^4/cm^3$ .

X (a) Use  $n_i = 1.5 \times 10^{10}/cm^3$  to find the built-in voltage. (Hint:  $V_O = V_T \ln (N_A N_D / n_i^2)$  and  $V_T = 25mV$ ). (3 points)

X (b) Which side (p side or n side) has larger depletion width? Indicate the polarity of the charge stored in the depletion region of this side. What is the ratio of p-side width to n-side width? (3 points)

3. A is an ideal OP AMP with output saturation voltages at  $\pm 4V$ ,  $R_1=10\text{ K}\Omega$ ,  $R_2=500\text{ K}\Omega$ ,  $C=1\text{ nF}$ ,  $V_{OS}=10\text{ mV}$ ,  $v_s(t)$  is shown in Fig.3(b).

- Find  $v_o$  at  $t=0^-$ . (4 points)
- Find the max. value of  $t_1$  such that the OP AMP doesn't enter saturation state. (5 points)
- Under the condition of (2), plot the output waveform  $v_o(t)$  for  $0^+ \leq t < \infty$ . (4 points)
- If, in addition to  $V_{OS}$ , there are bias currents  $I_{B1}=I_{B2}=5\text{ }\mu\text{A}$ , flowing INTO the (+) and (-) input terminals of A. Repeat (a) and (b). (6 points)

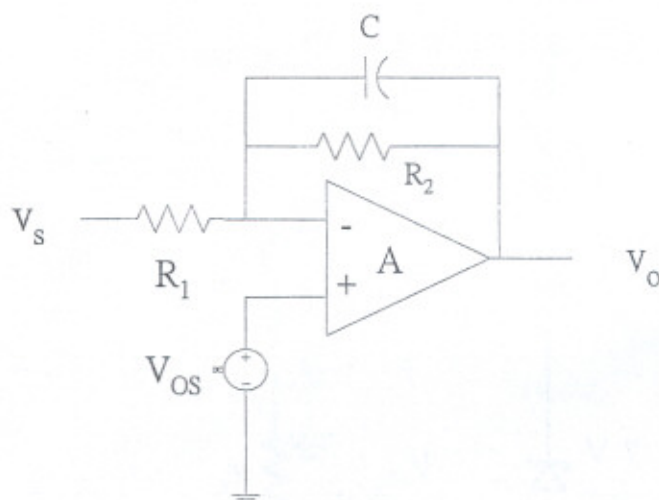


Fig. 3(a)

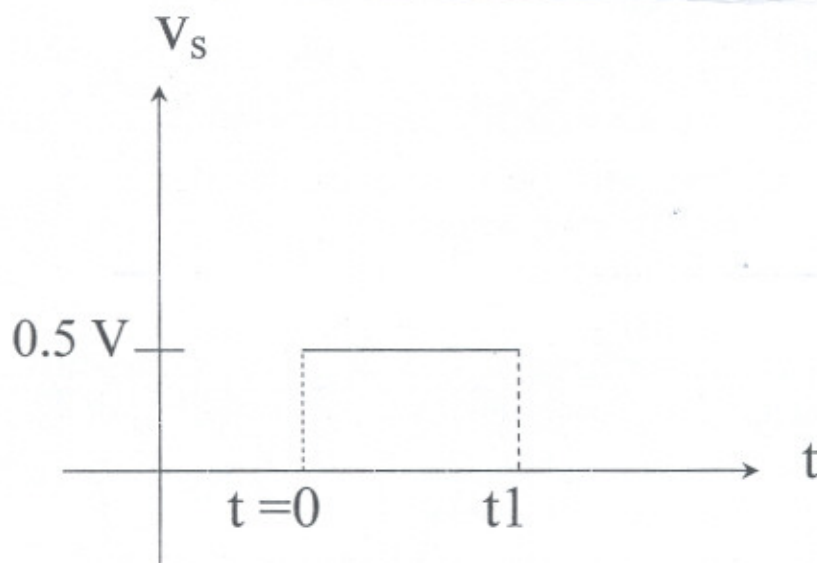


Fig. 3(b)

- Find the value of  $V_O$  using constant-voltage-drop model with  $V_D=0.7V$ . (10 points)
  - Assuming a  $\pm 10\%$  variation in all of the three power supplies, find the maximum voltage variation (in volt) at the output  $V_O$  with  $V_T=25\text{ mV}$  and  $n=2$ . (9 points)

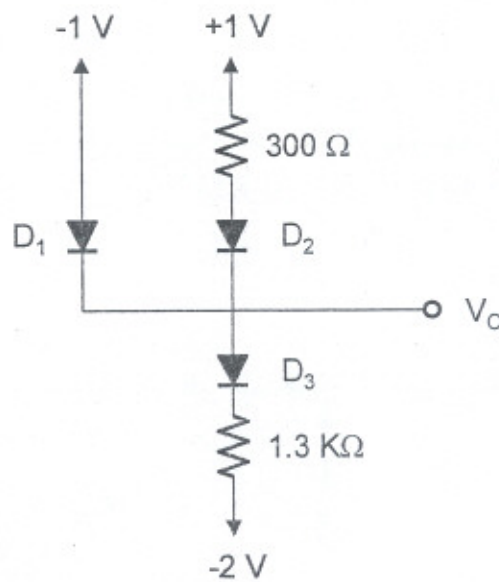


Fig. 4

5. For the circuit shown in the figure below, assuming  $A_1$  and  $A_2$  are ideal Op AMPs and  $R_a=R_b=R_c=R_d=R_1=R_2=R$ .

- ✓ (a) Find the voltage gain  $V_o/(V_{I1}-V_{I2})$ . (5 points)
- ✓ (b) What is the input impedance seen by  $V_{I1}$  and  $V_{I2}$ ? (2 points)
- ✓ (c) If  $V_{I1}=V_{I2}=V_x$ , find  $V_o/V_x$ . (2 points)
- ✓ (d) What is the CMRR (common-mode rejection ratio) of the circuit? (2 points)
- (e) If resistor mismatch exists such that  $R_a=R_b=R_d=R$ ,  $R_c=R+\Delta R$  (assuming  $\Delta R \ll R$ ), derive an expression for the circuit CMRR. (5 points)
- (f) From (e), what is the CMRR value (in dB) if  $R_x=R$  and  $\Delta R=0.01R$ . (2 points)

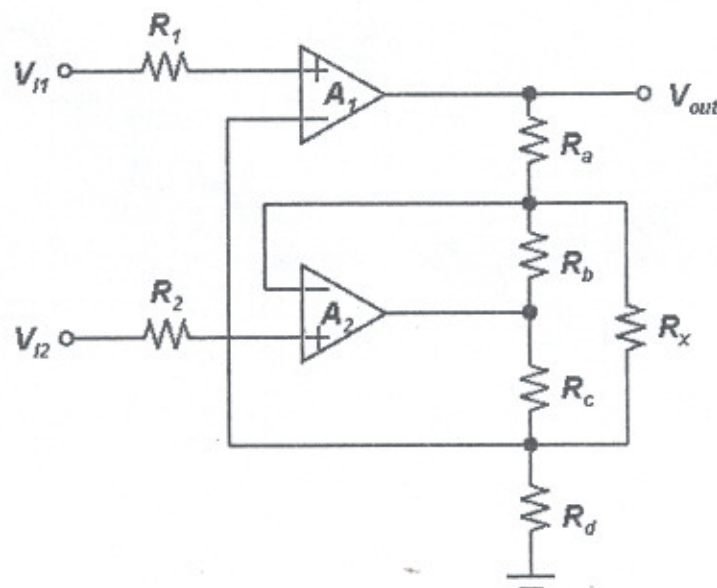


Fig. 5



6. In the circuit shown in Fig. 6,  $D_1$  is a large-area high-current diode whose reverse leakage is high and independent of applied voltage while  $D_2$  is a much smaller, low-current diode for which  $n=1$ . At an ambient temperature of  $20^\circ\text{C}$ , resistor  $R_1$  is adjusted to make  $V_{R1}=V_2=520\text{mV}$ . Subsequent measurement indicates that  $R_1$  is  $520\text{K}\Omega$ . Find the saturation current of  $D_2$ . What do you expect the voltages  $V_{R1}$  and  $V_2$  to become at  $0^\circ\text{C}$  and at  $40^\circ\text{C}$ ? (13 points)

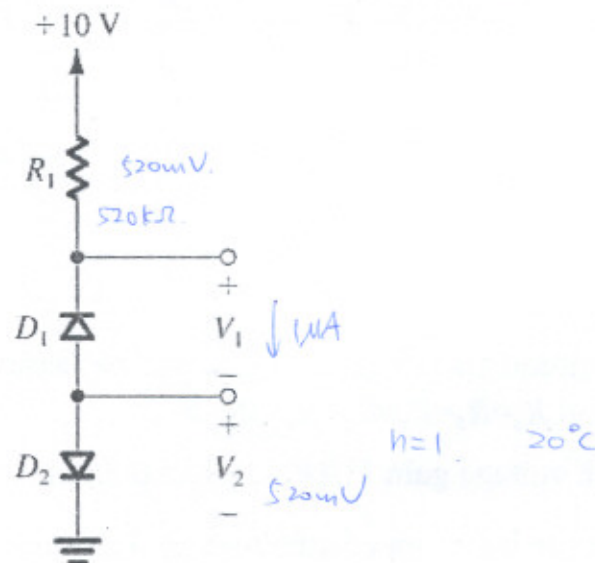


Fig. 6

7. The circuit in Fig. 7 implements a complementary output rectifier. Sketch and clearly label the waveforms of  $V_o^+$  and  $V_o^-$ . Assume a  $0.7\text{-V}$  drop across each conducting diode. If the magnitude of the average of each output is to be  $15\text{ V}$ , find the required amplitude of the sine wave across the entire secondary winding. What is the PIV of each diode? (12 points)

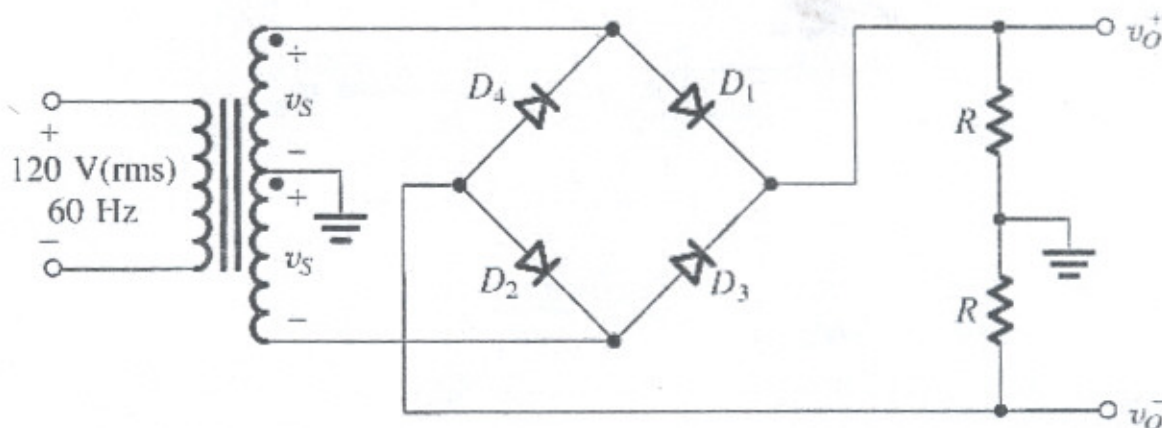
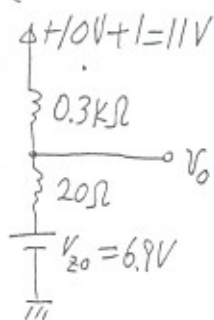


Fig. 7

1. (a)



因为  $V_z = 7V$  @  $I_z = 5mA$

故  $r_z = 20\Omega \cdot 5mA + V_{zo}$ ;  $V_{zo} = 6.9V$

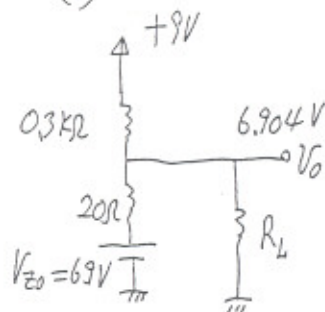
最大电流在负载  $R_L = \infty$ , 且  $V^+ = 10+1V$  时发生

故  $I_z = \frac{11V - 6.9V}{0.32k\Omega} = 12.8mA$  (1)

$V_o = 12.8mA \cdot 20\Omega + 6.9V = 7.156V$  (2)

$P_D = V_o \cdot I_z = 91.6mW$  (3)

(b)



Zener 维持在 breakdown 时之最低电流为  $I_{zk} = 0.2mA$

故  $V_z = 6.9 + 20\Omega \cdot 0.2mA = 6.904V$

若取  $V^+ = 9V$   $I_R = \frac{9 - 6.904}{0.3k\Omega} = \frac{2.096V}{0.3k\Omega} = 6.99mA$

$R_L = \frac{6.904}{6.99 - 0.2} = 1.017k\Omega$  --- Ans. (4)

若取  $V^+ = 11V$   $I_R = \frac{11 - 6.904}{0.3k\Omega} = \frac{4.096V}{0.3k\Omega} = 0.01365A$

$R_L = \frac{6.904}{13.65 - 0.2} = 513\Omega$  ... 此值更小, 但要考虑在

$V^+$  所有变动之下都可以维持在 breakdown 故取  $R_L = 1.017k\Omega$  方为正确.

2. (a)

p-Si  $n = \frac{10^{13}}{N_A}$ ;  $p = \frac{n_i^2}{n} = \frac{2.25 \cdot 10^{-20}}{10^{13}} = 2.25 \cdot 10^{-17}/cm^3 N_A$

n-Si  $p = \frac{10^{16}}{N_D}$ ;  $n = \frac{n_i^2}{p} = \frac{2.25 \cdot 10^{-20}}{10^{16}} = 2.25 \cdot 10^{-16}/cm^3 N_D$

$0.025 \ln \frac{10^{13} \cdot 10^{16}}{(1.5 \cdot 10^{10})^2}$

$V_o = 25mV \cdot \ln \frac{2.25 \cdot 10^{17} \cdot 2.25 \cdot 10^{16}}{(1.5 \cdot 10^{10})^2} = 25mV \cdot \ln 2.25 \cdot 10^{13} = 0.969V$

(b)

n-side  $N_D$  比较低故 n-side depletion region 较宽.

n-side depletion region 内之 charge 为 positive (正 charge)

(p-side width / (n-side width)) = 1/10 与掺杂浓度成反比.



3. A is an ideal OP AMP with output saturation voltages at  $\pm 4V$ ,  $R_1=10\text{ K}\Omega$ ,  $R_2=500\text{ K}\Omega$ ,  $C=1\text{ nF}$ ,  $V_{OS}=10\text{ mV}$ ,  $v_s(t)$  is shown in Fig.3(b).

- Find  $v_o$  at  $t=0^-$ . (4 points)  $V_{OS} (\frac{V_s}{R_1})$   $0.51\text{ V}$
- Find the max. value of  $t_1$  such that the OP AMP doesn't enter saturation state. (5 points)
- Under the condition of (2), plot the output waveform  $v_o(t)$  for  $0^+ \leq t < \infty$ . (4 points)
- If, in addition to  $V_{OS}$ , there are bias currents  $I_{B1}=I_{B2}=5\text{ }\mu\text{A}$ , flowing INTO the (+) and (-) input terminals of A. Repeat (a) and (b). (6 points)

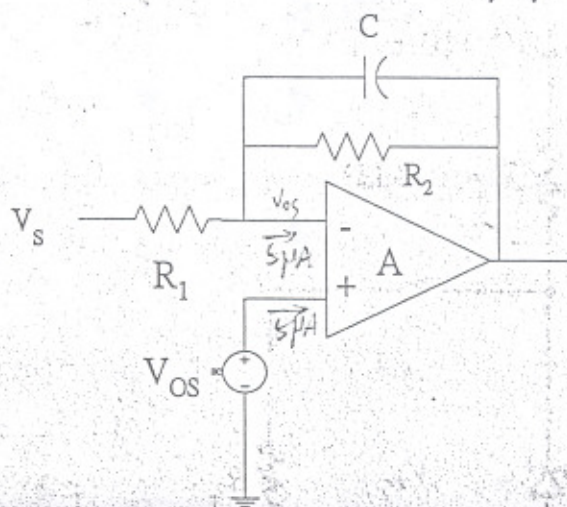


Fig. 3(a)

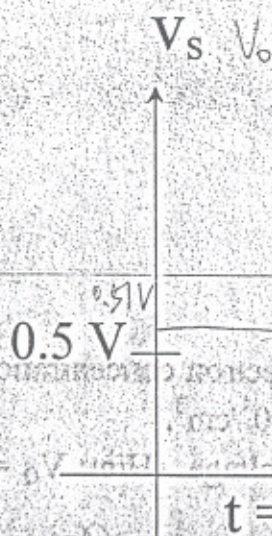


Fig. 3(b)

- Find the value of  $V_O$  using constant-voltage-drop model with  $V_D=0.7V$ . (10 points)
- Assuming a  $\pm 10\%$  variation in all of the three power supplies, find the maximum voltage variation (in volt) at the output  $V_O$  with  $V_T=25\text{ mV}$  and  $n=2$ . (9 points)

$$2.5\text{ V} + 0.51\text{ V} = 3.01\text{ V}$$

$$0.5\text{ ms} \ln \frac{25}{19.99} = 0.1645\text{ ms}$$

$$\frac{V_s - V_{OS}}{R_1} + \frac{V_o - V_{OS}}{R_2} + C \frac{d}{dt}(V_o - V_{OS}) = 0$$

$$\frac{dV_o}{dt} + \frac{V_o}{R_2 C} = \left(\frac{1}{R_1} - \frac{1}{R_2}\right) \frac{V_s}{C} - \frac{V_{OS}}{R_2 C}$$

$$\tau = 0.5\text{ ms}$$

$$V_o = -24.49 + 25e^{-\frac{t}{\tau}} \geq -4$$

$$e^{-\frac{t}{\tau}} \geq \frac{-0.49}{25} \rightarrow 2.5$$

$$t \leq \tau \ln \frac{25}{20.49} \rightarrow 2.5$$

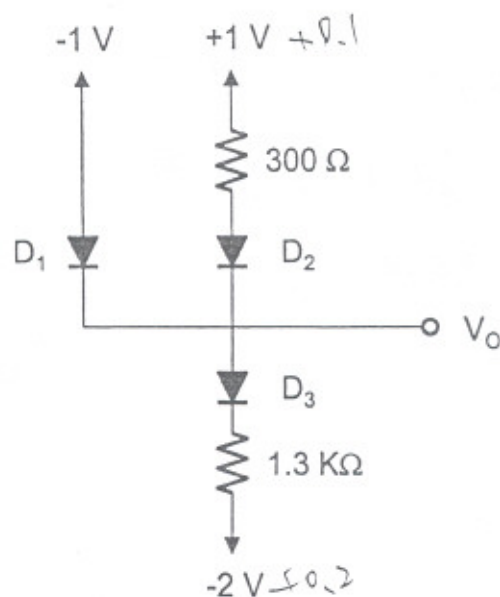
$$t_1 = 0.5\text{ ms} - 0.489 = 99.47\text{ }\mu\text{s}$$

$$0.12\text{ V}$$



# 2004 Midterm

- (a) Find the value of  $V_O$  utilizing constant-voltage-drop model with  $V_D = 0.7V$ . (10 pt)  
 (b) Assuming a  $\pm 10\%$  variation in all of the three power supplies, find the maximum voltage variation (in volt) at the output  $V_O$  with  $V_T = 25 \text{ mV}$  and  $n = 2$ . (9 pt)



$D_1$  off.  $D_2, D_3$  on  $\rightarrow V_O = 0V$

$$I_{D1} = I_{D2} = 1 \text{ mA}$$

$$\pm 0.1V$$

$$300\Omega$$

$$50\Omega$$

$$50\Omega$$

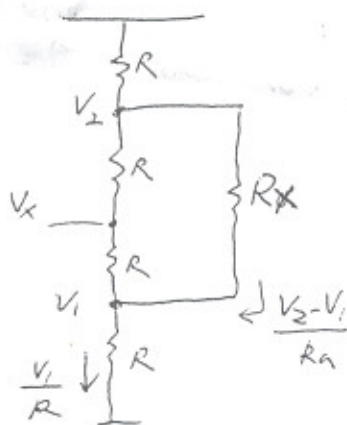
$$1.3K\Omega$$

$$\pm 0.2V$$

$$r_{d1} = r_{d2} = \frac{2 \times 25}{1} = 50\Omega$$

$$\Delta V_O = \pm \left( \frac{1350}{1700} \times 0.1 + \frac{350}{1700} \times 0.2 \right)$$

$$= \pm 0.12V \quad (0.1206)$$



$$V_x = \left( \frac{V_1}{R} - \frac{V_2 - V_1}{R_x} \right) \cdot R + V_1 = 2V_1 + \frac{V_2 - V_1}{R_x} \cdot R$$

$$V_0 = V_2 + R \cdot \left( \frac{V_2 - V_x}{R} + \frac{V_2 - V_1}{R_x} \right)$$

$$= V_2 + \frac{V_2 - V_1}{R_x} \cdot R + (V_2 - 2V_1 + \frac{V_2 - V_1}{R_x} \cdot R)$$

$$= 2V_2 - 2V_1 + 2 \frac{R}{R_x} (V_2 - V_1)$$

$$= (V_2 - V_1) \cdot \left( 2 + \frac{2R}{R_x} \right)$$

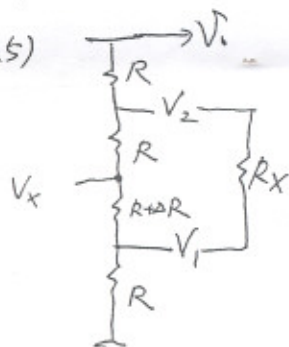
$$\Rightarrow \frac{V_0}{V_1 - V_2} = - \left( 2 + \frac{2R}{R_x} \right)$$

b (2)  $\infty, \infty$

c (3) 0

d (4)  $\infty$

e (5)



$$V_x = V_1 + \frac{V_1}{R} (R + \Delta R) = 2V_1 + V_1 \frac{\Delta R}{R}$$

$$V_0 = V_2 + \frac{V_2 - V_x}{R} \cdot R = 2V_2 - 2V_1 + V_1 \frac{\Delta R}{R}$$

$$V_x = \left( \frac{V_1}{R} - \frac{V_2 - V_1}{R_x} \right) \cdot (R + \Delta R) + V_1 = 2V_1 + V_1 \frac{\Delta R}{R} - \frac{V_2 - V_1}{R_x} (R + \Delta R)$$

$$V_0 = V_2 + R \left( \frac{V_2 - V_x}{R} + \frac{V_2 - V_1}{R_x} \right)$$

$$= V_2 + \frac{V_2 - V_1}{R_x} \cdot R + V_2 - 2V_1 - V_1 \frac{\Delta R}{R} + \frac{V_2 - V_1}{R_x} (R + \Delta R)$$

$$= 2V_2 - 2V_1 + \frac{V_2 - V_1}{R_x} \cdot R + \frac{V_2 - V_1}{R_x} R + \frac{V_1 - V_2}{R_x} \Delta R - V_1 \frac{\Delta R}{R}$$

$$\Rightarrow \frac{V_0}{V_1 - V_2} = \frac{2(V_2 - V_1) \left( 2 + \frac{2R + \Delta R}{R_x} \right)}{V_1 - V_2} \Rightarrow \frac{V_0}{V_1 - V_2} = - \left( 2 + \frac{2R + \Delta R}{R_x} \right) \quad (\text{Assume } \Delta R \ll R)$$

for  $V_1 = V_2 = V_{cm}$ ,

$$V_x = V_{cm} + \frac{V_{cm}}{R} (R + \Delta R) = 2V_{cm} + V_{cm} \frac{\Delta R}{R}$$

$$V_1 = V_{cm} + \frac{V_{cm} - V_x}{R} \cdot R = 2V_{cm} - V_x = V_{cm} \frac{\Delta R}{R}$$

$$\Rightarrow \frac{V_0}{V_{cm}} = \frac{\Delta R}{R} \Rightarrow CMRR \approx \left| \frac{2 + \frac{2R + \Delta R}{R_x}}{\frac{\Delta R}{R}} \right|$$

46)  $R_x = R, \Delta R = 0.01R$

$$CMRR = \frac{4}{0.01} = 400 = 46 \text{ dB}$$