

姓名：\_\_\_\_\_

學號：\_\_\_\_\_

- 注意事項：1. 題目卷(第一頁)，以及「Smith chart」，皆要填寫考生姓名與學號；  
2. 考試完畢，請將題目卷、Smith chart、答案卷一併繳回，未繳回的部份，不予計分；  
3. 題目一共六題，每題 20 分，採計個人最高分之五題。

1. (20%) For a transmission line of characteristic impedance  $50 \Omega$ , terminated by a load impedance  $(100 + j100) \Omega$ , find the following quantities by using the provided Smith chart:
- (1) reflection coefficient at the load;
  - (2) SWR on the line;
  - (3) the distance of the first voltage minimum of the standing-wave pattern from the load;
  - (4) the line impedance at  $d = 0.125 \lambda$
  - (5) the line admittance at  $d = 0.125 \lambda$  and
  - (6) the location nearest to the load at which the real part of the line admittance is equal to the line characteristic admittance.
- (Make sure you obtain the answers by using the Smith chart)

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(Solution)

- (1)  $\Gamma_R = 0.62 \angle 29.7^\circ$
- (2)  $\text{SWR} = 4.2656$
- (3)  $0.29 \lambda$
- (4)  $(0.8 - j1.4) \times 50 = 40 - j70$
- (5)  $(0.3 + j0.54) / 50 = 0.006 + j0.0108$
- (6)  $0.22 \lambda$

2. (20%) The input impedance of a lossy line of length 100 m is measured at a frequency of 100 MHz for two cases: with the output short-circuited, it is  $(36 + j48) \Omega$ , and with the output open circuited, it is  $(36 - j48) \Omega$ . Find:
- (1) (5%) the characteristic impedance of the line;
  - (2) (5%) the attenuation constant of the line; and
  - (3) (10%) the phase velocity in the line, assuming its approximate value to be  $2 \times 10^8$  m/s.

(Solution)

$$(1) (5\%) \quad Z_o = \sqrt{\bar{Z}_{in}^s \bar{Z}_{in}^o} = \sqrt{(36 + j48)(36 - j48)} = \sqrt{3600} = 60 \Omega$$

where :

$\bar{Z}_{in}^s$  = Input impedance of short-end transmission line.

$\bar{Z}_{in}^o$  = Input impedance of open-end transmission line.

$$(2) (5\%) \quad \tanh(\bar{\gamma}\ell) = \sqrt{\frac{\bar{Z}_{in}^s}{\bar{Z}_{in}^o}} = \sqrt{\frac{36 + j48}{36 - j48}} = \sqrt{\frac{60\angle 53^\circ}{60\angle -53^\circ}} = 1\angle 53^\circ = 0.6 + j0.8$$

$$\bar{\gamma}\ell = \frac{1}{2} \ln \left( \frac{1.6 + j0.8}{0.4 - j0.8} \right) = \frac{1}{2} \ln \left( \frac{1.789\angle 26.565}{0.894\angle -63.435} \right) = \frac{1}{2} \ln(2\angle 90^\circ)$$

$$= \frac{1}{2} \ln \left( 2e^{j\left(\frac{\pi}{2} + 2n\pi\right)} \right) = \frac{1}{2} \ln(2) + \frac{1}{2} \ln \left( e^{j\left(\frac{\pi}{2} + 2n\pi\right)} \right)$$

$$= \frac{1}{2} \ln(2) + j \left( \frac{\pi}{4} + n\pi \right) \quad n = 0, 1, 2, \dots$$

$$\alpha\ell = \frac{1}{2} \ln(2) \rightarrow \alpha = 3.466 \times 10^{-3} \text{ (Np/m)}$$

$$(3) (10\%) \quad \beta = \frac{1}{\ell} \left( \frac{\pi}{4} + n\pi \right) = \frac{\omega}{v_p} = \frac{2\pi \times 100 \times 10^6}{2 \times 10^8} = \frac{\pi \times 10^8}{10^8} = \pi$$

$$\rightarrow \frac{\pi}{4} + n\pi = \ell\pi = 100\pi \rightarrow n = \frac{1}{\pi} \left( 100\pi - \frac{\pi}{4} \right) = 99.75$$

$$n = 99 \Rightarrow v_p = \frac{\omega}{\beta} = \frac{2\pi \times 100 \times 10^6}{\frac{1}{100} \left( \frac{\pi}{4} + 99\pi \right)} = \frac{2\pi \times 100 \times 10^8}{99.25\pi} = \frac{2 \times 100 \times 10^8}{99.25} = 2.015 \times 10^8 \text{ (m/s)}$$

$$n = 100 \Rightarrow v_p = \frac{\omega}{\beta} = \frac{2\pi \times 100 \times 10^6}{\frac{1}{100} \left( \frac{\pi}{4} + 100\pi \right)} = \frac{2\pi \times 100 \times 10^8}{100.25\pi} = \frac{2 \times 100 \times 10^8}{100.25} = 1.995 \times 10^8 \text{ (m/s)}$$

The latter one is closer to the given value. Therefore,  $n$  is 100, and phase velocity is  $1.995 \times 10^8$  (m/s).

3. (20 %) Consider a parallel-plate waveguide propagating waves in the  $\hat{z}$  direction and filled with a dielectric medium  $(\mu_0, \epsilon_0)$  for  $z < 0$  and  $(\mu_0, 3\epsilon_0)$  for  $z > 0$ . The plate separation is  $2\sqrt{3}\pi(\text{cm})$ , and the operating frequency is  $30/2\pi$  GHz.

(1) (5 %) Consider the  $z < 0$  region, i.e. the waveguide in the absence of the dielectric, which  $\text{TE}_m$  and  $\text{TM}_m$  modes can propagate in this waveguide?

(2) (5 %) Find the oblique incident angles  $\theta_i$  corresponding to each propagating modes in (1).

(3) (5 %) What are the phase and group velocities in the  $\hat{z}$  direction for the  $\text{TM}_2$  mode at the  $z < 0$  region and the operating frequency  $30/2\pi$  GHz?

(4) (5 %) For waves propagating in the  $-\hat{z}$  direction from  $z > 0$  region, for which TE and TM modes be totally reflected at the dielectric boundary?

(Solution) 改分原則：可以參考解答中之分配比例給分，亦或是以一個地方扣一分(或扣等份的分數)之方式計分。

(1) (5 %) Consider the  $z < 0$  region, i.e. the waveguide in the absence of the dielectric, which  $\text{TE}_m$  and  $\text{TM}_m$  modes can propagate in this waveguide?

$$f_c = \frac{m}{2a\sqrt{\mu\epsilon}} = \frac{m}{2 \times 2\sqrt{3}\pi \times 10^{-2} \times \sqrt{\mu_0\epsilon_0}} = \frac{mc}{4\pi\sqrt{3} \times 10^{-2}} \Big|_{c=3 \times 10^8} = \frac{(\sqrt{3})m}{4\pi} \times 10^{10} \text{ Hz} \rightarrow (+1\%)$$

If the operating frequency is  $30/2\pi$  GHz, then

$$m=1, f_c = \frac{(\sqrt{3})}{4\pi} \times 10^{10} \text{ Hz} < f = \frac{3}{2\pi} \times 10^{10} \text{ Hz}; m=2, f_c = \frac{\sqrt{3}}{2\pi} \times 10^{10} \text{ Hz} < f = \frac{3}{2\pi} \times 10^{10} \text{ Hz}$$

$$m=3, f_c = \frac{3\sqrt{3}}{4\pi} \times 10^{10} \text{ Hz} < f = \frac{3}{2\pi} \times 10^{10} \text{ Hz}; m=2, f_c = \frac{\sqrt{3}}{\pi} \times 10^{10} \text{ Hz} > f = \frac{3}{2\pi} \times 10^{10} \text{ Hz}$$

→ Propagation mode:  $m = 1, 2, 3 \rightarrow (+1\%)$

Answer:  $(\text{TE}_1, \text{TE}_2, \text{TE}_3), (\text{TM}_0, \text{TM}_1, \text{TM}_2, \text{TM}_3)$  can propagate. → (+3%)

(Note: There is no  $\text{TE}_0$  mode existing in the parallel plate waveguide.)

(2) (5 %) Find the oblique incident angles  $\theta_i$  corresponding to each propagating modes in (1).

$$\text{Answer: } \theta_i = \cos^{-1}\left(\frac{f_c}{f}\right) = \cos^{-1}\left(\frac{\frac{(\sqrt{3})m}{4\pi} \times 10^{10}}{\frac{3}{2\pi} \times 10^{10}}\right) = \cos^{-1}\left(\frac{m}{2\sqrt{3}}\right), \rightarrow \frac{f_c}{f} = \frac{m}{2\sqrt{3}} \rightarrow (+1\%)$$

Propagation Mode	$\theta_i$
$\text{TM}_0$	$90^\circ \rightarrow (+1\%)$
$\text{TE}_1, \text{TM}_1$	$\theta_i = \cos^{-1}\left(\frac{1}{2\sqrt{3}}\right) = 1.278 \rightarrow (+1\%)$
$\text{TE}_2, \text{TM}_2$	$\theta_i = \cos^{-1}\left(\frac{1}{\sqrt{3}}\right) = 0.9553 \rightarrow (+1\%)$
$\text{TE}_3, \text{TM}_3$	$\theta_i = \cos^{-1}\left(\frac{3}{2\sqrt{3}}\right) = 0.5236 \rightarrow (+1\%)$

- (3) (5 %) What are the phase and group velocities in the  $\hat{z}$  direction for the  $TM_2$  mode at the  $z < 0$  region and the operating frequency  $30/2\pi$  GHz?

Answer:

$$v_{pz} = \frac{v_p}{\sqrt{1 - (f_c/f)^2}} \left| \begin{array}{l} TM_2 \text{ mode} \\ v_p = c = 3 \times 10^8 \\ \frac{f_c}{f} = \frac{m}{2\sqrt{3}}, m=2 \end{array} \right. \rightarrow (+1\%) = \frac{3 \times 10^8}{\sqrt{1 - \left(\frac{1}{\sqrt{3}}\right)^2}} = \frac{3 \times 10^8}{\sqrt{\frac{2}{3}}} = 3.67 \times 10^8 \text{ m/s} \rightarrow (+2\%)$$

$$v_g = v_p \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = 3 \times 10^8 \times \sqrt{\frac{2}{3}} = 2.45 \times 10^8 \rightarrow (+2\%)$$

- (4) (5 %) For waves propagating in the  $-\hat{z}$  direction from  $z > 0$  region, for which TE and TM modes be totally reflected at the dielectric boundary?

Consider the  $z < 0$  region,

$$\begin{array}{ccccccc} z < 0 & \text{---} & | & | & | & | & \text{---} & f \\ & & f(TM_0) & f(TE_1) & f(TE_2) & f(TE_3) & & \\ & & f(TM_1) & f(TM_2) & f(TM_3) & & & \end{array} \rightarrow (+1\%)$$

Consider the  $z > 0$  region,

$$\begin{array}{ccccccccccc} z > 0 & \text{---} & | & | & | & | & | & | & | & | & \text{---} & f \\ & & f(TM_0) & f(TE_1) & f(TE_2) & f(TE_3) & f(TE_4) & f(TE_5) & f(TE_6) & & & \\ & & f(TM_1) & f(TM_2) & f(TM_3) & f(TM_4) & f(TM_5) & f(TM_6) & & & & \end{array} \rightarrow (+1\%)$$

Answer:

( $TE_4, TM_4$ ), ( $TE_5, TM_5$ ), ( $TE_6, TM_6$ ) are reflected.  $\rightarrow (+3\%)$

4. (20 %) The electric field inside a certain dielectric-slab waveguide (where  $\varepsilon = 9\varepsilon_0$ ,  $\mu = \mu_0$  and thickness 3 m) is  $\bar{E}(\bar{r}) = \hat{y}E_0(\sin x)e^{-jz}$  (V/m).

(1) (5 %) Is this a TE or TM mode, why?

(2) (5 %) What is the waveguide wavelength  $\lambda_z$  in meters?

(3) (5 %) What is  $\omega$  in radians/s?

(4) (5 %) Find the effective thickness  $d_{eff}$  of this dielectric-slab waveguide for this mode.

(Solution)

(1) (5 %) Is this a TE or TM mode, why?

Answer:

This is a TE mode because there is no  $\bar{E}(\bar{r})$  in the propagation direction. (i.e.,  $\bar{E}(\bar{r}) = \hat{y}E_y$  only)

(2) (5 %) What is the waveguide wavelength  $\lambda_z$  in meters?

Answer:

$$\bar{E}(\bar{r}) = \hat{y}E_0(\sin x)e^{-jz} \text{ (V / m)} \rightarrow \beta_z = 1m, \rightarrow \lambda_z = \frac{2\pi}{\beta_z} = 2\pi \text{ (m)}$$

(3) (5 %) What is  $\omega$  in radians/s?

Answer:

$$\begin{aligned} \bar{E}(\bar{r}) &= \hat{y}E_0(\sin x)e^{-jz} \text{ (V / m)} \rightarrow \beta_x = 1m, \\ \because \beta_x^2 + \beta_z^2 &= \omega^2 \mu_0 \varepsilon_2 \Big|_{\varepsilon_2=9\varepsilon_0} = 9\omega^2 \mu_0 \varepsilon_0 \\ \rightarrow \omega &= \sqrt{\frac{\beta_x^2 + \beta_z^2}{9\mu_0 \varepsilon_0}} = \frac{\sqrt{2}}{3} \frac{1}{\sqrt{\mu_0 \varepsilon_0}} = \frac{\sqrt{2}}{3} \times 3 \times 10^8 = 1.414 \times 10^8 \text{ (rad/s)} \end{aligned}$$

(4) (5 %) Find the effective thickness  $d_{eff}$  of this dielectric-slab waveguide for this mode.

Answer:

$$\begin{aligned} \beta_{x1}^2 + \beta_z^2 &= \omega^2 \mu_0 \varepsilon_1 \rightarrow -\alpha_{x2}^2 + \beta_z^2 = \omega^2 \mu_0 \varepsilon_2 \Big|_{\varepsilon_2=\varepsilon_0} = \omega^2 \mu_0 \varepsilon_0 \\ \rightarrow \alpha_{x2}^2 &= \beta_z^2 - \omega^2 \mu_0 \varepsilon_0 = 1 - (1.414 \times 10^8)^2 \times \frac{1}{9} \times 10^{-16} = 1 - (1.414)^2 \frac{1}{9} = 1 - \frac{(\sqrt{2})^2}{9} = \frac{7}{9} \\ \rightarrow \alpha_{x2} &= \frac{\sqrt{7}}{3} \\ d_{eff} &= d + \frac{2}{\alpha_{x2}} = 3 + \frac{2 \times 3}{\sqrt{7}} = 5.27 \text{ (m)} \end{aligned}$$

where:

$$\beta_{x1}^2 + \beta_z^2 = \omega^2 \mu_0 \varepsilon_2 \Big|_{\varepsilon_2=9\varepsilon_0} = 9\omega^2 \mu_0 \varepsilon_0 \rightarrow \omega = \sqrt{\frac{\beta_x^2 + \beta_z^2}{9\mu_0 \varepsilon_0}} = 1.414 \times 10^8 \text{ (rad/s)}$$

5. (20 %) Figure 3 shows a rectangular waveguide of height  $a$  and width  $b$ . Consider a wave guided in the  $z$  direction, with  $z$ -dependence of  $e^{-j\beta_z z}$ .

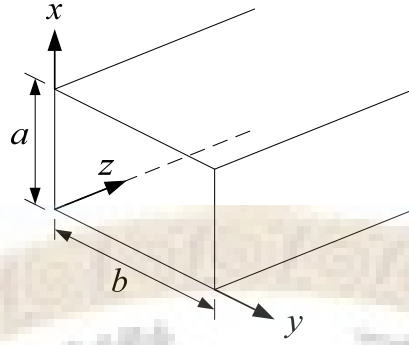


Fig. 5

- (1) (5%) For TE modes with  $E_z = 0$ ,  $H_z \neq 0$ , derive  $E_x$ ,  $E_y$ ,  $H_x$  and  $H_y$  in terms of  $H_z$  from the Faraday's law and the Ampere's law.

Answer:

We conclude that  $E_x, E_y, H_x$  and  $H_y$  in terms of  $\bar{H}_z$  are shown as following,  $\rightarrow (+1\%)$

$$\begin{cases} \bar{E}_x = \frac{j\omega\mu}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial y} \rightarrow (+1\%) \\ \bar{E}_y = -\frac{j\omega\mu}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial x} \rightarrow (+1\%) \end{cases} \quad \begin{cases} \bar{H}_x = j \frac{\beta_z}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial x} \rightarrow (+1\%) \\ \bar{H}_y = j \frac{\beta_z}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial y} \rightarrow (+1\%) \end{cases}$$

(Derivation)

$$\text{Faraday's law: } \nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t} \rightarrow \text{Phasor form: } \nabla \times \bar{E} = -j\omega\mu \bar{H} \rightarrow \begin{vmatrix} \hat{a}_x & -\hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \bar{E}_x & \bar{E}_y & \bar{E}_z \end{vmatrix} = -j\omega\mu \bar{H}$$

$$\hat{a}_x \left( \frac{\partial \bar{E}_z}{\partial y} - \frac{\partial \bar{E}_y}{\partial z} \right) + \hat{a}_y \left( \frac{\partial \bar{E}_x}{\partial z} - \frac{\partial \bar{E}_z}{\partial x} \right) + \hat{a}_z \left( \frac{\partial \bar{E}_y}{\partial x} - \frac{\partial \bar{E}_x}{\partial y} \right) = -j\omega\mu (\hat{a}_x \bar{H}_x + \hat{a}_y \bar{H}_y + \hat{a}_z \bar{H}_z)$$

$$\text{Ampere's law: } \nabla \times \bar{H} = \frac{\partial D}{\partial t} \rightarrow \text{Phasor form: } \nabla \times \bar{H} = j\omega\epsilon \bar{E} \rightarrow \begin{vmatrix} \hat{a}_x & -\hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \bar{H}_x & \bar{H}_y & \bar{H}_z \end{vmatrix} = j\omega\epsilon \bar{E}$$

$$\hat{a}_x \left( \frac{\partial \bar{H}_z}{\partial y} - \frac{\partial \bar{H}_y}{\partial z} \right) + \hat{a}_y \left( \frac{\partial \bar{H}_x}{\partial z} - \frac{\partial \bar{H}_z}{\partial x} \right) + \hat{a}_z \left( \frac{\partial \bar{H}_y}{\partial x} - \frac{\partial \bar{H}_x}{\partial y} \right) = j\omega\epsilon (\hat{a}_x \bar{E}_x + \hat{a}_y \bar{E}_y + \hat{a}_z \bar{E}_z)$$

$$\bar{E}_z = 0, \bar{E}_y = E_y e^{-j\beta_z z} :$$

$$\begin{cases} -\frac{\partial \bar{E}_y}{\partial z} = -j\omega\mu \bar{H}_x \rightarrow j\beta_z \bar{E}_y = -j\omega\mu \bar{H}_x \quad (1.1) \\ \frac{\partial \bar{E}_x}{\partial z} = -j\omega\mu \bar{H}_y \rightarrow j\beta_z \bar{E}_x = j\omega\mu \bar{H}_y \quad (1.2) \\ \frac{\partial \bar{E}_y}{\partial x} - \frac{\partial \bar{E}_x}{\partial y} = -j\omega\mu \bar{H}_z \quad (1.3) \end{cases} \quad \begin{cases} \frac{\partial \bar{H}_z}{\partial y} - \frac{\partial \bar{H}_y}{\partial z} = j\omega\epsilon \bar{E}_x \rightarrow \frac{\partial \bar{H}_z}{\partial y} + j\beta_z \bar{H}_y = j\omega\epsilon \bar{E}_x \quad (1.4) \\ \frac{\partial \bar{H}_x}{\partial z} - \frac{\partial \bar{H}_z}{\partial x} = j\omega\epsilon \bar{E}_y \rightarrow -j\beta_z \bar{H}_x - \frac{\partial \bar{H}_z}{\partial x} = j\omega\epsilon \bar{E}_y \quad (1.5) \\ \frac{\partial \bar{H}_y}{\partial x} - \frac{\partial \bar{H}_x}{\partial y} = j\omega\epsilon \bar{E}_z \rightarrow \frac{\partial \bar{H}_y}{\partial x} - \frac{\partial \bar{H}_x}{\partial y} = 0 \quad (1.6) \end{cases}$$

$$\begin{cases}
(1.4) \rightarrow \bar{H}_y = \frac{1}{j\beta_z} \left( j\omega\varepsilon\bar{E}_x - \frac{\partial\bar{H}_z}{\partial y} \right) \\
(1.2) \rightarrow j\beta_z\bar{E}_x = j\omega\mu\bar{H}_y = \frac{j\omega\mu}{j\beta_z} \left( j\omega\varepsilon\bar{E}_x - \frac{\partial\bar{H}_z}{\partial y} \right) \rightarrow -\beta_z^2\bar{E}_x = j\omega\mu \left( j\omega\varepsilon\bar{E}_x - \frac{\partial\bar{H}_z}{\partial y} \right) \\
\rightarrow -\beta_z^2\bar{E}_x + \omega^2\mu\varepsilon\bar{E}_x = -j\omega\mu \left( \frac{\partial\bar{H}_z}{\partial y} \right) \rightarrow (\beta_z^2 - \beta^2)\bar{E}_x = j\omega\mu \left( \frac{\partial\bar{H}_z}{\partial y} \right) \rightarrow \bar{E}_x = \frac{j\omega\mu}{\beta_z^2 - \beta^2} \frac{\partial\bar{H}_z}{\partial y}
\end{cases}$$

$$\begin{cases}
-\frac{\partial\bar{E}_y}{\partial z} = -j\omega\mu\bar{H}_x \rightarrow j\beta_z\bar{E}_y = -j\omega\mu\bar{H}_x \quad (1.1) & \left\{ \begin{aligned} \frac{\partial\bar{H}_z}{\partial y} - \frac{\partial\bar{H}_y}{\partial z} &= j\omega\varepsilon\bar{E}_x \rightarrow \frac{\partial\bar{H}_z}{\partial y} + j\beta_z\bar{H}_y = j\omega\varepsilon\bar{E}_x \quad (1.4) \\ \frac{\partial\bar{H}_x}{\partial z} - \frac{\partial\bar{H}_z}{\partial x} &= j\omega\varepsilon\bar{E}_y \rightarrow -j\beta_z\bar{H}_x - \frac{\partial\bar{H}_z}{\partial x} = j\omega\varepsilon\bar{E}_y \quad (1.5) \end{aligned} \right. \\
\frac{\partial\bar{E}_x}{\partial z} = -j\omega\mu\bar{H}_y \rightarrow j\beta_z\bar{E}_x = j\omega\mu\bar{H}_y \quad (1.2) & \left\{ \begin{aligned} \frac{\partial\bar{H}_y}{\partial x} - \frac{\partial\bar{H}_x}{\partial y} &= j\omega\varepsilon\bar{E}_z \rightarrow \frac{\partial\bar{H}_y}{\partial x} - \frac{\partial\bar{H}_x}{\partial y} = 0 \quad (1.6) \end{aligned} \right. \\
\frac{\partial\bar{E}_y}{\partial x} - \frac{\partial\bar{E}_x}{\partial y} = -j\omega\mu\bar{H}_z \quad (1.3)
\end{cases}$$

$$\begin{cases}
(1.5) \rightarrow -j\beta_z\bar{H}_x - \frac{\partial\bar{H}_z}{\partial x} = j\omega\varepsilon\bar{E}_y \rightarrow \bar{H}_x = \frac{-1}{j\beta_z} \left( j\omega\varepsilon\bar{E}_y + \frac{\partial\bar{H}_z}{\partial x} \right) \\
(1.1) \rightarrow j\beta_z\bar{E}_y = -j\omega\mu\bar{H}_x = \frac{j\omega\mu}{j\beta_z} \left( j\omega\varepsilon\bar{E}_y + \frac{\partial\bar{H}_z}{\partial x} \right) \rightarrow -\beta_z^2\bar{E}_y = j\omega\mu \left( j\omega\varepsilon\bar{E}_y + \frac{\partial\bar{H}_z}{\partial x} \right) \\
\rightarrow -\beta_z^2\bar{E}_y + \omega^2\mu\varepsilon\bar{E}_y = j\omega\mu \left( \frac{\partial\bar{H}_z}{\partial x} \right) \rightarrow -(\beta_z^2 - \beta^2)\bar{E}_y = j\omega\mu \left( \frac{\partial\bar{H}_z}{\partial x} \right) \rightarrow \bar{E}_y = -\frac{j\omega\mu}{\beta_z^2 - \beta^2} \frac{\partial\bar{H}_z}{\partial x}
\end{cases}$$

$$\begin{cases}
(1.5) \rightarrow \bar{E}_y = \frac{-1}{j\omega\varepsilon} \left( j\beta_z\bar{H}_x + \frac{\partial\bar{H}_z}{\partial x} \right) \\
(1.1) \rightarrow -j\omega\mu\bar{H}_x = j\beta_z\bar{E}_y = \frac{-j\beta_z}{j\omega\varepsilon} \left( j\beta_z\bar{H}_x + \frac{\partial\bar{H}_z}{\partial x} \right) \rightarrow \omega^2\mu\varepsilon\bar{H}_x = -j\beta_z \left( j\beta_z\bar{H}_x + \frac{\partial\bar{H}_z}{\partial x} \right) \\
\rightarrow -(\beta_z^2 - \beta^2)\bar{H}_x = -j\beta_z \frac{\partial\bar{H}_z}{\partial x} \rightarrow \bar{H}_x = j \frac{\beta_z}{\beta_z^2 - \beta^2} \frac{\partial\bar{H}_z}{\partial x}
\end{cases}$$

$$\begin{cases}
(1.4) \rightarrow \bar{E}_x = \frac{1}{j\omega\varepsilon} \left( \frac{\partial\bar{H}_z}{\partial y} + j\beta_z\bar{H}_y \right) \\
(1.2) \rightarrow j\omega\mu\bar{H}_y = j\beta_z\bar{E}_x = \frac{j\beta_z}{j\omega\varepsilon} \left( \frac{\partial\bar{H}_z}{\partial y} + j\beta_z\bar{H}_y \right) \rightarrow -\omega^2\mu\varepsilon\bar{H}_y = j\beta_z \left( \frac{\partial\bar{H}_z}{\partial y} + j\beta_z\bar{H}_y \right) \\
\rightarrow (-\omega^2\mu\varepsilon\bar{H}_y + \beta_z^2)\bar{H}_y = j\beta_z \frac{\partial\bar{H}_z}{\partial y} \rightarrow \bar{H}_y = j \frac{\beta_z}{\beta_z^2 - \beta^2} \frac{\partial\bar{H}_z}{\partial y}
\end{cases}$$



(2) (2%) If the waveguide is made of perfect electric conductor, list the boundary conditions on the four walls,  $x = 0, x = a, y = 0, y = b$ .

Answer:

$$\begin{cases} \bar{E}_x = 0, \forall y = 0, x \in (0, a) \\ \bar{E}_x = 0, \forall y = b, x \in (0, a) \end{cases} \begin{cases} \bar{E}_y = 0, \forall x = 0, y \in (0, b) \\ \bar{E}_y = 0, \forall x = a, y \in (0, b) \end{cases} \rightarrow (+1\%)$$

$$\text{From (1):} \begin{cases} \frac{\partial \bar{H}_z}{\partial y} = 0, \forall y = 0, x \in (0, a) \\ \frac{\partial \bar{H}_z}{\partial y} = 0, \forall y = b, x \in (0, a) \end{cases} \begin{cases} \frac{\partial \bar{H}_z}{\partial x} = 0, \forall x = 0, y \in (0, b) \\ \frac{\partial \bar{H}_z}{\partial x} = 0, \forall x = a, y \in (0, b) \end{cases} \rightarrow (+1\%)$$

(3) (3%) Assume  $H_z(x, y, z) = X(x)Y(y)e^{-j\beta_z z}$ , which satisfies the wave equation  $(\nabla^2 + k^2)H_z(x, y, z) = 0$ , where  $k^2 = \omega^2\mu\epsilon$ . Derive the harmonic equations of  $X(x)$  and  $Y(y)$ , with proper constants  $\beta_x$  and  $\beta_y$ , respectively.

Answer:

$$(\nabla^2 + k^2)H_z(x, y, z) = 0 \rightarrow \left[ \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) + \omega^2\mu\epsilon \right] H_z(x, y, z) = 0, \text{ where: } H_z(x, y, z) = \bar{X}(x)Y(y)e^{-j\beta_z z}$$

$$\rightarrow \bar{X}''(x)\bar{Y}(y) + \bar{X}(x)\bar{Y}''(y) + \omega^2\mu\epsilon\bar{X}(x)\bar{Y}(y) = 0 \rightarrow \frac{\bar{X}''(x)}{\bar{X}(x)} + \frac{\bar{Y}''(y)}{\bar{Y}(y)} = -\omega^2\mu\epsilon$$

$$\rightarrow \frac{\bar{X}''(x)}{\bar{X}(x)} = -\beta_x^2 = \text{constant}, \rightarrow \frac{d^2\bar{X}}{dx^2} = -\beta_x^2\bar{X}(x) \rightarrow \bar{X}(x) = A_1e^{j\beta_x x} + A_2e^{-j\beta_x x}$$

$$\frac{\bar{Y}''(y)}{\bar{Y}(y)} = -\beta_y^2 = \text{constant}, \rightarrow \frac{d^2\bar{Y}}{dy^2} = -\beta_y^2\bar{Y}(y) \rightarrow \bar{Y}(y) = B_1e^{j\beta_y y} + B_2e^{-j\beta_y y}$$

(4) (3%) Use the relations derived in (1) to list the corresponding expressions of  $E_x, E_y, H_x$  and  $H_y$  in terms of the  $H_z$  expression obtained in (3).

Answer:

$$\bar{H}_z(x, y, z) = \bar{X}(x)\bar{Y}(y)e^{-j\beta_z z} = (A_1e^{j\beta_x x} + A_2e^{-j\beta_x x})(B_1e^{j\beta_y y} + B_2e^{-j\beta_y y})e^{-j\beta_z z} \rightarrow (+1\%)$$

$$\text{where: } \bar{X}(x) = A_1e^{j\beta_x x} + A_2e^{-j\beta_x x}, \bar{Y}(y) = B_1e^{j\beta_y y} + B_2e^{-j\beta_y y} \rightarrow (+1\%)$$

$$\begin{cases} \bar{E}_x = \frac{j\omega\mu}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial y} = \frac{-\omega\mu\beta_y}{\beta_z^2 - \beta^2} (A_1e^{j\beta_x x} + A_2e^{-j\beta_x x})(B_1e^{j\beta_y y} - B_2e^{-j\beta_y y})e^{-j\beta_z z} \\ \bar{E}_y = -\frac{j\omega\mu}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial x} = \frac{\omega\mu\beta_x}{\beta_z^2 - \beta^2} (A_1e^{j\beta_x x} - A_2e^{-j\beta_x x})(B_1e^{j\beta_y y} + B_2e^{-j\beta_y y})e^{-j\beta_z z} \\ \bar{H}_x = j\frac{\beta_z}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial x} = -\frac{\beta_z\beta_x}{\beta_z^2 - \beta^2} (A_1e^{j\beta_x x} - A_2e^{-j\beta_x x})(B_1e^{j\beta_y y} + B_2e^{-j\beta_y y})e^{-j\beta_z z} \\ \bar{H}_y = j\frac{\beta_z}{\beta_z^2 - \beta^2} \frac{\partial \bar{H}_z}{\partial y} = -\frac{\beta_z\beta_y}{\beta_z^2 - \beta^2} (A_1e^{j\beta_x x} + A_2e^{-j\beta_x x})(B_1e^{j\beta_y y} - B_2e^{-j\beta_y y})e^{-j\beta_z z} \end{cases} \rightarrow (+1\%)$$



(5) (3%) Impose the boundary conditions listed in (2) upon the expressions of  $E_x, E_y$  in (4) to prove that  $\beta_x = m\pi / a$  and  $\beta_y = n\pi / b$ . List all possible values of  $m$  and  $n$ , and explain why.

Answer:

Boundary condition:

$$\begin{cases} \bar{E}_x = 0, \forall y = 0, x \in (0, a) \\ \bar{E}_x = 0, \forall y = b, x \in (0, a) \end{cases} \quad \begin{cases} \bar{E}_y = 0, \forall x = 0, y \in (0, b) \\ \bar{E}_y = 0, \forall x = a, y \in (0, b) \end{cases}$$

$$\bar{E}_x = \frac{-\omega\mu\beta_y}{\beta_z^2 - \beta^2} (A_1 e^{j\beta_x x} + A_2 e^{-j\beta_x x}) (B_1 e^{j\beta_y y} - B_2 e^{-j\beta_y y}) e^{-j\beta_z z} \dots (5.1)$$

$$\bar{E}_y = \frac{\omega\mu\beta_x}{\beta_z^2 - \beta^2} (A_1 e^{j\beta_x x} - A_2 e^{-j\beta_x x}) (B_1 e^{j\beta_y y} + B_2 e^{-j\beta_y y}) e^{-j\beta_z z} \dots (5.2)$$

$$\because \bar{E}_x = 0, \forall y = 0, x \in (0, a) \rightarrow B_1 - B_2 = 0 \rightarrow B_1 = B_2$$

$$\because \bar{E}_y = 0, \forall x = 0, y \in (0, b) \rightarrow A_1 - A_2 = 0 \rightarrow A_1 = A_2, (c)(js)$$

$$(5.1) \rightarrow \bar{E}_x = \frac{-\omega\mu\beta_y}{\beta_z^2 - \beta^2} A (e^{j\beta_x x} + e^{-j\beta_x x}) (e^{j\beta_y y} - e^{-j\beta_y y}) e^{-j\beta_z z} = \frac{-j\omega\mu\beta_y}{\beta_z^2 - \beta^2} A \cos \beta_x x \cdot \sin \beta_y y \cdot e^{-j\beta_z z}, \dots (5.3)$$

$$(5.2) \rightarrow \bar{E}_y = \frac{\omega\mu\beta_x}{\beta_z^2 - \beta^2} A (e^{j\beta_x x} - e^{-j\beta_x x}) (e^{j\beta_y y} + e^{-j\beta_y y}) e^{-j\beta_z z} = \frac{j\omega\mu\beta_x}{\beta_z^2 - \beta^2} A \cdot \sin \beta_x x \cdot \cos \beta_y y \cdot e^{-j\beta_z z}, \dots (5.4)$$

$$\because \bar{E}_x = 0, \forall y = b, x \in (0, a) \rightarrow (5.3)$$

$$\rightarrow \sin \beta_y b = 0 \rightarrow \beta_y = \frac{n\pi}{b}, n = 0, 1, 2, \dots \left( \because \text{If } \beta_y = \frac{n\pi}{b}, n = 0, 1, 2, \dots, \text{ then } \sin \beta_y b = 0 \right)$$

$$\because \bar{E}_y = 0, \forall x = a, y \in (0, b) \rightarrow (5.4)$$

$$\rightarrow \sin \beta_x a = 0 \rightarrow \beta_x = \frac{m\pi}{a}, m = 0, 1, 2, \dots \left( \because \text{If } \beta_x = \frac{m\pi}{a}, m = 0, 1, 2, \dots, \text{ then } \sin \beta_x a = 0 \right)$$

(6) (4%) Given specific  $m$  and  $n$ , derive the expressions of cutoff frequency  $f_c$ , guided wavelength  $\lambda_g$ , apparent phase velocity  $v_{pz}$  and group velocity  $v_{gz}$ .

Answer:

$$(\nabla^2 + k^2) H_z(x, y, z) = 0 \rightarrow \left[ \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) + \omega^2 \mu \epsilon \right] H_z(x, y, z) = 0, \text{ where } H_z(x, y, z) = \bar{X}(x)Y(y)e^{-j\beta_z z}$$

$$\because \frac{\bar{X}''(x)}{\bar{X}(x)} = -\beta_x^2, \frac{\bar{Y}''(y)}{\bar{Y}(y)} = -\beta_y^2, \rightarrow (-\beta_x^2 - \beta_y^2 + \omega^2 \mu \epsilon) H_z(x, y, z) = 0 \rightarrow \omega^2 \mu \epsilon = \beta_x^2 + \beta_y^2$$

$$\rightarrow f_c = \frac{1}{2\pi\sqrt{\mu\epsilon}} \sqrt{\left( \frac{m\pi}{a} \right)^2 + \left( \frac{n\pi}{b} \right)^2} = \frac{1}{\sqrt{\mu\epsilon}} \sqrt{\left( \frac{m}{2a} \right)^2 + \left( \frac{n}{2b} \right)^2}$$

$$\rightarrow \lambda_c = \frac{v_p}{f_c} = \frac{1}{\sqrt{\mu\epsilon} \cdot f_c} = \left( \sqrt{\left( \frac{m}{2a} \right)^2 + \left( \frac{n}{2b} \right)^2} \right)^{-1}$$

$$\rightarrow \lambda_g = \frac{2\pi}{\beta_z} = \frac{2\pi}{\beta \sin \theta} = \frac{\lambda}{\sqrt{1 - (\lambda/\lambda_c)^2}} = \frac{\lambda}{\sqrt{1 - (f_c/f)^2}}$$

$$\rightarrow v_{pz} = \frac{\omega}{\beta_z} = \frac{\omega}{\beta \sin \theta} = \frac{v_p}{\sqrt{1 - (\lambda/\lambda_c)^2}} = \frac{v_p}{\sqrt{1 - (f_c/f)^2}}$$

$$\rightarrow v_{gz} = \frac{d\omega}{d\beta_z} = \frac{1}{\sqrt{\mu\epsilon}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2}, \text{ where: } \beta_z = \frac{2\pi}{\lambda_g} = \frac{2\pi}{\lambda} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = \omega \sqrt{\mu\epsilon} \sqrt{1 - \left(\frac{f_c}{f}\right)^2}$$

Note: **Problem 6** is in the following page.



6. (20 %) Figure 4 shows a Hertzian dipole of current moment  $\hat{z}I\ell$ , located at the origin. The magnetic

vector potential is derived as  $\bar{A} = \mu \frac{I\ell}{4\pi r} e^{-jkr} (\hat{r} \cos \theta - \hat{\theta} \sin \theta)$ .

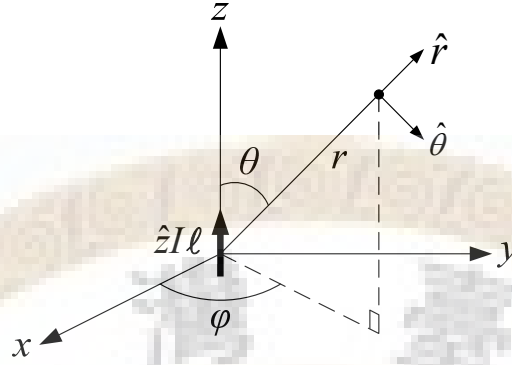


Fig. 4

(1) (4%) Derive the magnetic field by using the relation

$$\bar{H} = \frac{1}{\mu} \nabla \times \bar{A} = \frac{1}{\mu} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{r} & r\hat{\theta} & r \sin \theta \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & rA_\theta & r \sin \theta A_\phi \end{vmatrix}$$

Answer:  $\bar{H} = \hat{\phi} \frac{I\ell}{4\pi} (\sin \theta e^{-jkr}) \left\{ \frac{jk}{r} + \frac{1}{r^2} \right\}$

(Derivation)

$$\bar{A} = \mu \frac{I\ell}{4\pi r} e^{-jkr} (\hat{r} \cos \theta - \hat{\theta} \sin \theta) = \hat{r} A_r + \hat{\theta} A_\theta, \text{ where: } A_\phi = 0$$

$$\begin{aligned} \bar{H} &= \frac{1}{\mu} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{r} & r\hat{\theta} & r \sin \theta \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & rA_\theta & r \sin \theta A_\phi \end{vmatrix} = \frac{1}{\mu} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{r} & r\hat{\theta} & r \sin \theta \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & rA_\theta & 0 \end{vmatrix} \\ &= \frac{1}{\mu} \frac{1}{r^2 \sin \theta} \left[ \hat{r} \left( -r \frac{\partial A_\theta}{\partial \phi} \right) + r\hat{\theta} \left( \frac{\partial A_r}{\partial \phi} \right) + r \sin \theta \hat{\phi} \left( \frac{\partial (rA_\theta)}{\partial r} - \frac{\partial A_r}{\partial \theta} \right) \right] = \frac{1}{\mu} \frac{1}{r^2 \sin \theta} \left[ r \sin \theta \hat{\phi} \left( \frac{\partial (rA_\theta)}{\partial r} - \frac{\partial A_r}{\partial \theta} \right) \right] \\ &= \frac{1}{\mu r} \hat{\phi} \left( \frac{\partial (rA_\theta)}{\partial r} - \frac{\partial A_r}{\partial \theta} \right) = \hat{\phi} \frac{1}{\mu r} \left\{ jk \left( \frac{\mu I\ell}{4\pi} \sin \theta e^{-jkr} \right) + \frac{1}{r} \left( \frac{\mu I\ell}{4\pi} \sin \theta e^{-jkr} \right) \right\} \\ &= \hat{\phi} \frac{1}{\mu} \left( \frac{\mu I\ell}{4\pi} \sin \theta e^{-jkr} \right) \left( \frac{1}{r} \right) \left\{ jk + \frac{1}{r} \right\} = \hat{\phi} \frac{I\ell}{4\pi} (\sin \theta e^{-jkr}) \left\{ \frac{jk}{r} + \frac{1}{r^2} \right\} \end{aligned}$$

where:

$$A_r = \mu \frac{I\ell}{4\pi r} \cos \theta e^{-jkr}, A_\theta = -\mu \frac{I\ell}{4\pi r} \sin \theta e^{-jkr}$$

$$\frac{\partial (rA_\theta)}{\partial r} = -\frac{\partial}{\partial r} \left( \mu \frac{I\ell}{4\pi} \sin \theta e^{-jkr} \right) = -\mu \frac{I\ell}{4\pi} \sin \theta \frac{\partial}{\partial r} (e^{-jkr}) = jk \left( \frac{\mu I\ell}{4\pi} \sin \theta e^{-jkr} \right)$$

$$-\frac{\partial A_r}{\partial \theta} = -\mu \frac{I\ell}{4\pi r} e^{-jkr} \frac{\partial}{\partial \theta} (\cos \theta) = \frac{1}{r} \left( \frac{\mu I\ell}{4\pi} \sin \theta e^{-jkr} \right)$$

(2) (4%) Derive the electric field by applying the Ampere's law to the magnetic field derived in (1) as

$$\bar{E} = \frac{1}{j\omega\epsilon} \nabla \times \bar{H} = \frac{1}{j\omega\epsilon} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{r} & r\hat{\theta} & r \sin \theta \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ H_r & rH_\theta & r \sin \theta H_\phi \end{vmatrix}$$

Answer:

$$\begin{aligned} \bar{H} &= \hat{\phi} \frac{I\ell}{4\pi} (\sin \theta e^{-jkr}) \left\{ \frac{jk}{r} + \frac{1}{r^2} \right\} = \hat{\phi} H_\phi, \text{ where: } H_r = H_\theta = 0, H_\phi = \frac{I\ell}{4\pi} (\sin \theta e^{-jkr}) \left\{ \frac{jk}{r} + \frac{1}{r^2} \right\} \\ \bar{E} &= \frac{1}{j\omega\epsilon} \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{r} & r\hat{\theta} & r \sin \theta \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ 0 & 0 & r \sin \theta H_\phi \end{vmatrix} = \frac{1}{j\omega\epsilon} \frac{1}{r^2 \sin \theta} \left[ \hat{r} \frac{\partial}{\partial \theta} (r \sin \theta H_\phi) - r\hat{\theta} \frac{\partial}{\partial r} (r \sin \theta H_\phi) \right] \\ &= \frac{1}{j\omega\epsilon} \frac{1}{r^2 \sin \theta} \left[ \hat{r} \left( \frac{I\ell}{4\pi} \right) (2 \sin \theta \cos \theta e^{-jkr}) \left\{ jk + \frac{1}{r} \right\} + r\hat{\theta} \left( \frac{I\ell}{4\pi} \right) (\sin^2 \theta) \left\{ -k^2 e^{-jkr} + \frac{jk}{r} e^{-jkr} + \frac{1}{r^2} e^{-jkr} \right\} \right] \\ &= \left( \frac{I\ell}{4\pi} \right) \frac{1}{j\omega\epsilon} \frac{1}{\sin \theta} \frac{1}{r^2} \left[ \hat{r} 2 \cos \theta (\sin \theta e^{-jkr}) \left\{ jk + \frac{1}{r} \right\} + \hat{\theta} \sin \theta (\sin \theta e^{-jkr}) r \left( -k^2 + \frac{jk}{r} + \frac{1}{r^2} \right) \right] \\ &= \frac{I\ell}{4\pi} \frac{1}{j\omega\epsilon} \frac{\sin \theta e^{-jkr}}{\sin \theta} \frac{1}{r^2} \left[ \hat{r} 2 \cos \theta \left( jk + \frac{1}{r} \right) + \hat{\theta} \sin \theta \left( -k^2 r + jk + \frac{1}{r} \right) \right] \\ &= \frac{I\ell}{4\pi} \frac{e^{-jkr}}{j\omega\epsilon} \left[ \hat{r} 2 \cos \theta \left( \frac{jk}{r^2} + \frac{1}{r^3} \right) + \hat{\theta} \sin \theta \left( -\frac{k^2}{r} + \frac{jk}{r^2} + \frac{1}{r^3} \right) \right] \end{aligned}$$

where:

$$\begin{aligned} r \sin \theta H_\phi &= (r \sin \theta) \frac{I\ell}{4\pi} (\sin \theta e^{-jkr}) \left\{ \frac{jk}{r} + \frac{1}{r^2} \right\} = \frac{I\ell}{4\pi} (\sin^2 \theta e^{-jkr}) \left\{ jk + \frac{1}{r} \right\} \\ \frac{\partial}{\partial \theta} (r \sin \theta H_\phi) &= \frac{I\ell}{4\pi} \left( jk + \frac{1}{r} \right) e^{-jkr} \frac{\partial}{\partial \theta} (\sin^2 \theta) = \frac{I\ell}{4\pi} (2 \sin \theta \cos \theta e^{-jkr}) \left\{ jk + \frac{1}{r} \right\} \\ \frac{\partial}{\partial r} (r \sin \theta H_\phi) &= \frac{I\ell}{4\pi} (\sin^2 \theta) \frac{\partial}{\partial r} \left\{ jk e^{-jkr} + \frac{e^{-jkr}}{r} \right\} = \frac{I\ell}{4\pi} (\sin^2 \theta) \left\{ k^2 e^{-jkr} - \frac{jk}{r} e^{-jkr} - \frac{1}{r^2} e^{-jkr} \right\} \end{aligned}$$

(3) (2%) In the far-field region,  $kr \gg 1$ ; by keeping only the terms with  $(1/r)$ -dependence and neglecting all the higher-order terms, write down the approximate expression of the electric field derived in (2).

Answer:

$$\bar{E} = \frac{I\ell}{4\pi} \frac{e^{-jkr}}{j\omega\epsilon} \left[ \hat{r} 2 \cos \theta \left( \frac{jk}{r^2} + \frac{1}{r^3} \right) + \hat{\theta} \sin \theta \left( -\frac{k^2}{r} + \frac{jk}{r^2} + \frac{1}{r^3} \right) \right]_{r \gg 1} \approx -\hat{\theta} \frac{I\ell}{4\pi r} \left( \frac{k^2}{j\omega\epsilon} \right) (\sin \theta e^{-jkr})$$

(4) (3%) Calculate the time-averaged Poynting vector  $\langle \bar{P} \rangle = \frac{1}{2} \text{Re} \{ \bar{E} \times \bar{H}^* \}$  in the far-field region.

Answer:

In the far-field region,  $kr \gg 1$

$$\bar{E} \approx -\hat{\theta} \frac{I\ell}{4\pi r} \left( \frac{k^2}{j\omega\epsilon} \right) (\sin \theta e^{-jkr}), \bar{H} = \hat{\phi} \frac{I\ell}{4\pi} (\sin \theta e^{-jkr}) \left\{ \frac{jk}{r} + \frac{1}{r^2} \right\} \approx \hat{\phi} \frac{I\ell}{4\pi r} (jk) (\sin \theta e^{-jkr})$$

$$\langle P \rangle = \frac{1}{2} \text{Re} \{ \bar{E} \times \bar{H}^* \} = \hat{r} \frac{1}{2} \left( \frac{I\ell \sin \theta}{4\pi r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right)$$

where:

$$\begin{aligned} \bar{E} \times \bar{H}^* &= \left[ -\hat{\theta} \frac{I\ell}{4\pi r} \left( \frac{k^2}{j\omega\epsilon} \right) (\sin \theta e^{-jkr}) \right] \times \left[ \hat{\phi} \frac{I\ell}{4\pi r} (jk) (\sin \theta e^{-jkr}) \right]^* \\ &= -\hat{\theta} \times \hat{\phi} \left[ \left( \frac{I\ell \sin \theta}{4\pi r} \right) \left( \frac{k^2}{j\omega\epsilon} \right) (e^{-jkr}) \right] \left[ \left( \frac{I\ell \sin \theta}{4\pi r} \right) (jk)^* (e^{-jkr})^* \right] \\ &= -\hat{r} \left( \frac{I\ell \sin \theta}{4\pi r} \right)^2 \left( \frac{k^2}{j\omega\epsilon} \right) (-jk) = \hat{r} \left( \frac{I\ell \sin \theta}{4\pi r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \end{aligned}$$

(5) (3%) Integrate  $\langle \bar{P} \rangle$  derived in (4) over a spherical surface of radius  $r$ , centered at the origin, to

derive the time-averaged total radiated power,  $\langle P_{\text{rad}} \rangle$ . Note that an infinitesimal area on the spherical

surface is  $d\bar{a} = \hat{r} r^2 \sin \theta d\theta d\phi$ .

Answer:

$$\begin{aligned} \langle P_{\text{rad}} \rangle &= \int_S \langle P \rangle \cdot d\bar{a} = \int_{\phi=0}^{\phi=2\pi} \int_{\theta=0}^{\theta=\pi} \langle P \rangle r^2 \sin \theta d\theta d\phi = \frac{1}{2} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \int_{\phi=0}^{\phi=2\pi} \int_{\theta=0}^{\theta=\pi} \left( \frac{\sin \theta}{r} \right)^2 r^2 \sin \theta d\theta d\phi \\ &= \frac{1}{2} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \int_{\phi=0}^{\phi=2\pi} \int_{\theta=0}^{\theta=\pi} \sin^3 \theta d\theta d\phi = \frac{1}{2} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) 2\pi \int_{\theta=0}^{\theta=\pi} \frac{1}{4} (3 \sin \theta - \sin 3\theta) d\theta d\phi \\ &= \frac{\pi}{4} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \int_{\theta=0}^{\theta=\pi} (3 \sin \theta - \sin 3\theta) d\theta = \frac{\pi}{4} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \left( -3 \cos \theta \Big|_{\theta=0}^{\theta=\pi} + \frac{1}{3} \cos 3\theta \Big|_{\theta=0}^{\theta=\pi} \right) \\ &= \frac{\pi}{4} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \left[ -3(-1-1) + \frac{1}{3}(-1-1) \right] = \frac{\pi}{4} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \left( 6 - \frac{2}{3} \right) = \frac{\pi}{4} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \left( \frac{16}{3} \right) \\ &= \frac{4\pi}{3} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) = \frac{(I\ell)^2}{12\pi} \left( \frac{k^3}{\omega\epsilon} \right) \end{aligned}$$

where:

$$\langle P \rangle = \frac{1}{2} \text{Re} \{ \bar{E} \times \bar{H}^* \} = \hat{r} \frac{1}{2} \left( \frac{I\ell \sin \theta}{4\pi r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) = \hat{r} \frac{1}{2} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{\sin \theta}{r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right),$$

$$d\bar{a} = \hat{r} r^2 \sin \theta d\theta d\phi$$

$$\sin 3\theta = 3 \sin \theta - 4 \sin^3 \theta \rightarrow \sin^3 \theta = \frac{1}{4} (3 \sin \theta - \sin 3\theta)$$

(6) (2%) Let  $\langle P_{\text{rad}} \rangle = \frac{1}{2} R_{\text{rad}} I^2$ , derive the expression of  $R_{\text{rad}}$ .

Answer:

$$\langle P_{\text{rad}} \rangle = \frac{(I\ell)^2}{12\pi} \left( \frac{k^3}{\omega\epsilon} \right) = \frac{1}{2} I^2 \frac{(\ell)^2}{6\pi} \left( \frac{k^3}{\omega\epsilon} \right) = \frac{1}{2} R_{\text{rad}} I^2 \rightarrow R_{\text{rad}} = \frac{(\ell)^2}{6\pi} \left( \frac{k^3}{\omega\epsilon} \right)$$

(7) (2%) Define the directivity as  $D = \frac{|\langle \bar{P} \rangle|_{\text{max}}}{\langle P_{\text{rad}} \rangle / 4\pi}$ . Find the directivity of a Hertzian dipole.

Answer:

$$D = \frac{|\langle \bar{P} \rangle|_{\text{max}}}{\langle P_{\text{rad}} \rangle / 4\pi} = \frac{1}{2} \left( \frac{I\ell}{4\pi r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \bigg/ \left[ -\frac{(I\ell)^2}{12\pi} \left( \frac{k^3}{\omega\epsilon} \right) \left( \frac{1}{4\pi} \right) \right] = \frac{1}{2} \left( \frac{I\ell}{4\pi r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right) \bigg/ \left[ -\frac{(I\ell)^2}{48\pi^2} \left( \frac{k^3}{\omega\epsilon} \right) \right]$$

$$= \frac{1}{2} \left( \frac{1}{4\pi r} \right)^2 \bigg/ \left[ \frac{1}{48\pi^2} \right] = \frac{1}{2} \frac{1}{(4\pi r)^2} 48\pi^2 = \frac{3}{2} \frac{16\pi^2}{(4\pi r)^2} = \frac{3}{2r^2}$$

where:

$$\langle P \rangle = -\hat{r} \frac{1}{2} \left( \frac{I\ell}{4\pi} \right)^2 \left( \frac{\sin \theta}{r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right), \rightarrow |\langle P \rangle|_{\text{max}} = \frac{1}{2} \left( \frac{I\ell}{4\pi r} \right)^2 \left( \frac{k^3}{\omega\epsilon} \right)$$

$$\langle P_{\text{rad}} \rangle = -\frac{(I\ell)^2}{12\pi} \left( \frac{k^3}{\omega\epsilon} \right)$$

Note: There is some flaw in the definition of directivity  $D$ . It should be  $D = \frac{|\langle \bar{P} \rangle|_{\text{max}}}{\langle P_{\text{rad}} \rangle / (4\pi r^2)}$ . Because of

this indiscretion, the solution of  $D = \frac{3}{2r^2}$  and  $D = \frac{3}{2r^2}$  would both be considered as correct answers

although  $D = \frac{3}{2r^2}$  does not coincide with the physical meaning of directivity.

Useful formulas: One could refer to the useful formulas as shown in the followings.

$$\lambda_c = \frac{2a}{m}, \quad f_c = \frac{m}{2a\sqrt{\mu\epsilon}}$$

$$\lambda_g = \frac{2\pi}{\beta_z} = \frac{2\pi}{\beta \sin \theta} = \frac{\lambda}{\sqrt{1 - (\lambda/\lambda_c)^2}} = \frac{\lambda}{\sqrt{1 - (f_c/f)^2}},$$

$$v_{pz} = \frac{\omega}{\beta_z} = \frac{\omega}{\beta \sin \theta} = \frac{v_p}{\sqrt{1 - (\lambda/\lambda_c)^2}} = \frac{v_p}{\sqrt{1 - (f_c/f)^2}}$$

$$v_{pz} = \frac{\omega}{\beta_z}; \frac{1}{v_g} = \frac{d\beta_z}{d\omega}; v_g = \frac{\omega_B - \omega_A}{\beta_{zB} - \beta_{zA}}$$

$$\tan\left(\frac{\pi d \sqrt{\epsilon_{r1}}}{\lambda_0} \cos \theta_i - \frac{m\pi}{2}\right) = \frac{\sqrt{\sin^2 \theta_i - (\epsilon_2/\epsilon_1)}}{\cos \theta_i}, m = 0, 1, 2, \dots$$

$$\begin{cases} \beta_{x1}^2 + \beta_z^2 = \omega^2 \mu_0 \epsilon_1 \\ -\alpha_{x2}^2 + \beta_z^2 = \omega^2 \mu_0 \epsilon_2 \end{cases}, \rightarrow \frac{\alpha_{x2}}{\beta_{x1}} = \sqrt{\frac{\omega^2 \mu_0 (\epsilon_1 - \epsilon_2)}{\beta_{x1}^2} - 1}$$

$$\tan\left(\beta_{x1} \frac{d}{2}\right) = \sqrt{\frac{\omega^2 \mu_0 (\epsilon_1 - \epsilon_2)}{\beta_{x1}^2} - 1}, \quad \tan\left(\beta_{x1} \frac{d}{2} \cos \theta_i\right) = \sqrt{\frac{\omega^2 \mu_0 (\epsilon_1 - \epsilon_2)}{\omega^2 \mu_0 \epsilon_1 \cos^2 \theta_i} - 1}$$

$$\tan\left(\frac{\pi d \sqrt{\epsilon_{r1}}}{\lambda_0} \cos \theta_i\right) = \frac{\sqrt{\sin^2 \theta_i - (\epsilon_2/\epsilon_1)}}{\cos \theta_i}, \quad \tan[f(\theta_i)] = \begin{cases} g(\theta_i), & m = 0, 2, 4, \dots \\ \frac{-1}{g(\theta_i)}, & m = 1, 3, 5, \dots \end{cases}$$

$$f_c = \frac{mc}{2d\sqrt{\epsilon_{r1} - \epsilon_{r2}}}, m = 0, 1, 2, \dots; \quad f_c = \frac{1}{2\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$\lambda_g = \frac{\lambda}{\sqrt{1 - (f_c/f)^2}}, \quad v_{pz} = \frac{1}{\sqrt{\mu\epsilon} \cdot \sqrt{1 - (f_c/f)^2}}$$