

1. (a) For the circuit in Fig. 1, find the close loop gain  $L(j\omega)$ , the frequency for zero phase, and the condition for oscillation. (15%)
- (b) Given that  $R_1 = R_2 = R_3 = 10 \text{ k}\Omega$  and  $C_1 = C_2 = C_3 = 10 \text{ nF}$  in Fig. 1, find the oscillation frequency. (5%)
- (c) What is the phase and frequency relation between the waveforms at  $V_A$  and  $V_B$ ? (5%)

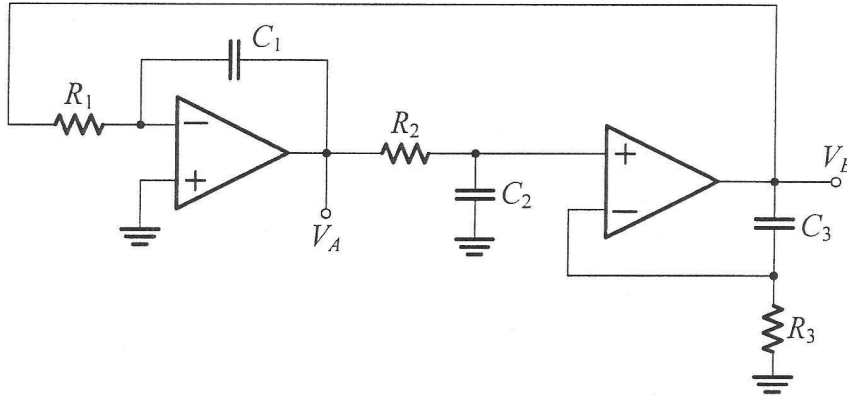


Fig. 1

2. For the circuit shown in Fig. 2,  $A_1$  and  $A_2$  are ideal op amps with an output voltage ranging from 0 to  $V_{DD}$ . The op-amp output will be at either 0 or  $V_{DD}$  if saturated. The input signal,  $V_{in}$ , is a DC voltage.
  - (1) If  $R_1 = 2R_2$ ,  $R_3 = R_4$ , plot the waveforms for signal  $V_a$  and  $V_b$  (please denote key parameters). (12%)
  - (2) If  $R_1 = 2R_2$ ,  $R_3 = R_4$ , what are the period and duty cycle for signal  $V_a$ ? (8%)
  - (3) If you use this circuit to generate a 20% duty-cycle square wave, how would you choose the resistors (i.e. ratios between  $R_1$ ,  $R_2$ , and  $R_3$ ,  $R_4$ )? (5%)

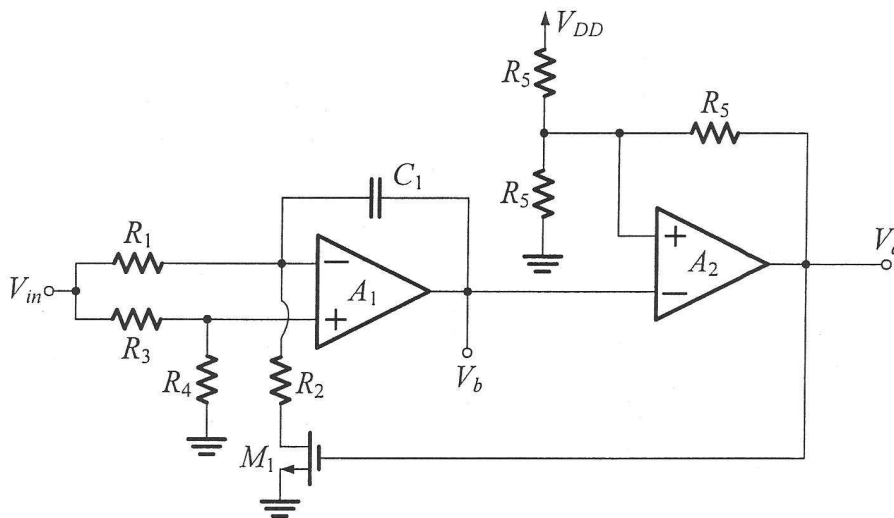


Fig. 2

3. (25%) Derive the relationship between  $v_O$  and  $v_I$  for the circuit shown in Fig. 3 which functions as a logarithmic amplifier by applying  $I_S$  and  $n$  as the diode parameters and  $V_T$  as the thermal voltage. Since the output voltage is proportional to the logarithm of the input voltage, the circuit is known as a logarithmic amplifier. Such amplifiers find application in situations where it is desired to compress the signal range.

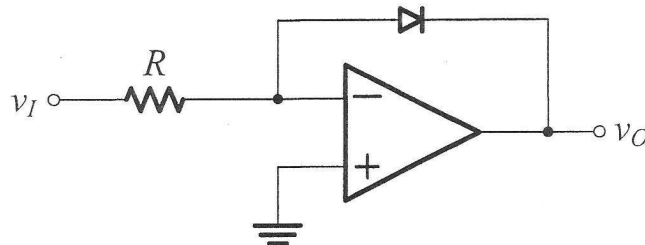


Fig. 3

4. Consider the circuit in Fig. 4(a). Neglect the on resistance of the inverters and other parasitic capacitances. The inverters have switching threshold of  $V_{DD}/2$ .
- (a) Sketch the steady-state waveforms of  $V_A$ ,  $V_B$ ,  $V_C$ , and  $V_D$  and mark important points. (6 %) Does the circuit oscillate? If so, determine the oscillation period. (3 %)
- (b) Now two ideal diodes  $D_1$ ,  $D_2$  are added to node  $A$  as shown in Fig. 4(b). Repeat part (a). (4 %) (3 %)
- (c) For the circuit in Fig. 4(c), repeat part (a). Diode  $D_3$  is ideal. (4 %) (3 %) What kind of damage would the devices possibly suffer from? (2 %)

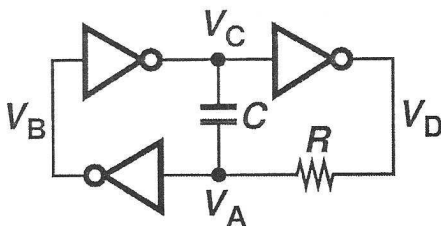


Fig. 4(a)

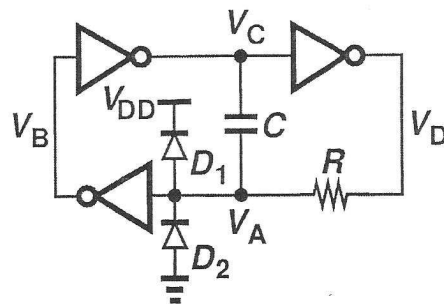


Fig. 4(b)

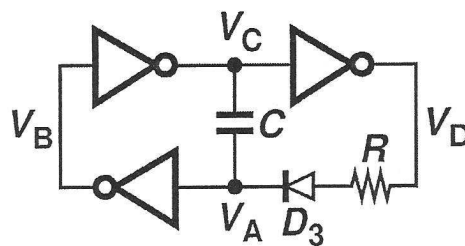


Fig. 4(c)

$$V_{+, \text{com2}} = V_B \cdot \frac{R_3}{R_3 + \frac{1}{j\omega C_3}}$$

$$V_A = V_{+, \text{com2}} + I_{C_2} R_2 = V_B \cdot \frac{R_3}{R_3 + \frac{1}{j\omega C_3}} \cdot [1 + j\omega R_2 C_2]$$

$$V_X = -V_A \cdot j\omega C_1 \cdot R_1 = -V_B \cdot \frac{R_3}{R_3 + \frac{1}{j\omega C_3}} \cdot [1 + j\omega R_2 C_2] j\omega R_1 C_1$$

(The cutopen mode)

$$\frac{V_X}{V_B} = \frac{-j\omega R_3 C_3 [1 + j\omega R_2 C_2] j\omega R_1 C_1}{1 + j\omega R_3 C_3} = \frac{j\omega^3 R_1 C_1 R_2 C_2 R_3 C_3 + \omega^2 R_1 C_1 R_3 C_3}{1 + j\omega R_3 C_3}$$

$$= \frac{\omega^2 R_1 C_1 R_3 C_3 + \omega^4 R_1 C_1 R_2 C_2 R_3^2 C_3^2 + j(\omega^3 R_1 C_1 R_2 C_2 R_3 C_3 - \omega^3 R_1 C_1 R_3^2 C_3^2)}{1 + \omega^2 R_3^2 C_3^2}$$

要 oscillates, 虛部 = 0.  $\Rightarrow R_2 C_2 = R_3 C_3$

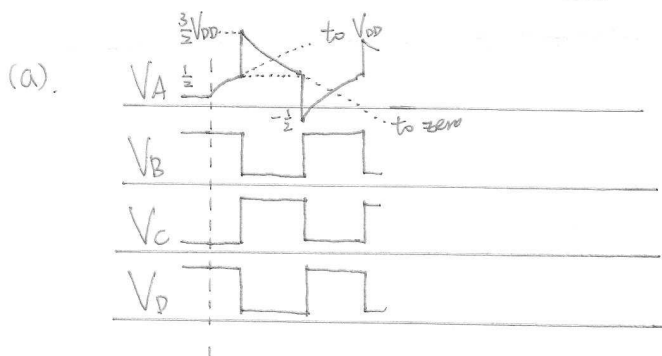
gain = 1  $\Rightarrow \omega_0 = \frac{1}{\sqrt{R_1 C_1 R_2 C_2}}$

$$= \frac{\omega^2 R_1 C_1 R_2 C_2 (1 + \omega^2 R_3^2 C_3^2)}{1 + \omega^2 R_3^2 C_3^2}$$

$$\frac{V_A}{V_B} = \left(\frac{V_X}{V_B}\right) \div (-j\omega R_1 C_1) = \frac{\omega^2 R_1 C_1 R_2 C_2}{-j\omega R_1 C_1} = j\omega R_2 C_2$$

for the case,  $V_A$  is  $90^\circ$  ahead  $V_B$ ,  $f_A = f_B$  頻率相同.

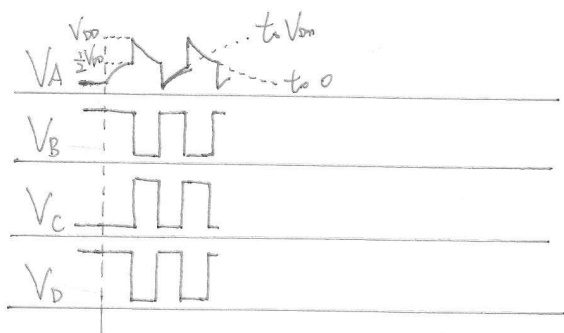
4.  $V_A$  通過  $R$  進行充放電 (與  $V_B$ )



$$V_A(t) \text{ at falling} = \frac{3}{2} V_{DD} e^{-t/\tau_c}$$

$$V_A(t) \text{ at rising} = V_{DD} - \frac{3}{2} V_{DD} e^{-t/\tau_c}$$

$$\text{period} = 2RC \ln 3.$$

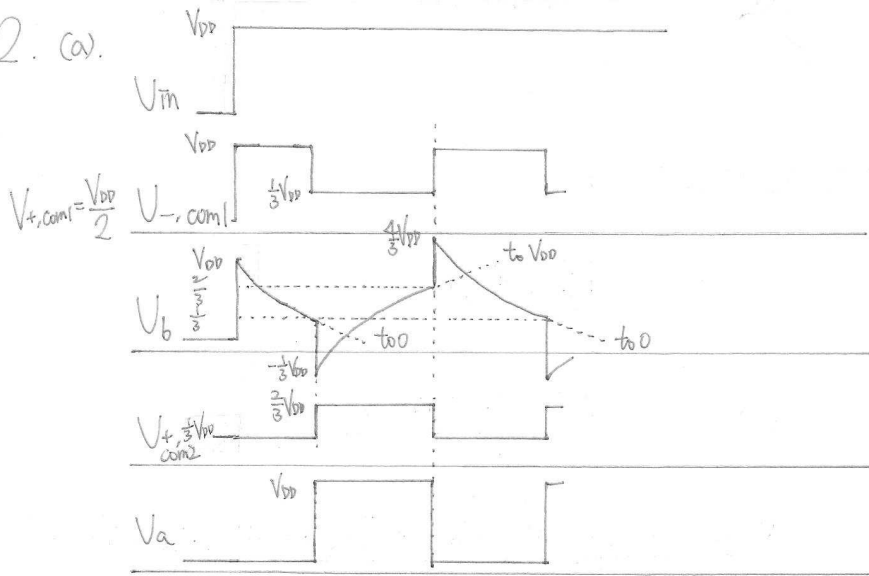


$$V_A(t) \text{ at falling} = V_{DD} e^{-t/\tau_c}$$

$$V_A(t) \text{ at rising} = V_{DD} - V_{DD} e^{-t/\tau_c}$$

$$\text{period} = 2RC \ln 2$$

2. (a).

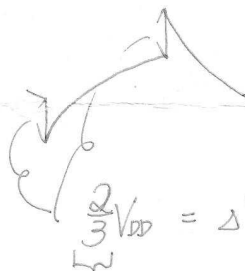


(b).  $V_b(t)$  at falling =  $\frac{4}{3} V_{DD} e^{-t/R_1 C_1}$  terminal:  $\frac{1}{3} V_{DD} \Rightarrow T_f = R_1 C_1 \ln 4$

$V_b(t)$  at rising =  $V_{DD} - \frac{4}{3} V_{DD} e^{-t/R_1 C_1}$  terminal:  $\frac{2}{3} V_{DD} \Rightarrow T_r = R_1 C_1 \ln 4$

duty cycle =  $R_1 C_1 \ln 4$ , period =  $2 R_1 C_1 \ln 4$ .

(c). wish a  $\frac{1}{5} R_1 C_1 \ln 4$  duty cycle.



$$\frac{2}{3} V_{DD} = \Delta V_{-, com1} = V_{DD} - \frac{R_2}{R_1 + R_2} V_{DD}$$

The magnitude =  $\frac{R_1}{R_1 + R_2}$

$$V_b(t) \text{ at rising} = V_{DD} - \left(1 + \frac{1}{3} - \frac{R_1}{R_1 + R_2}\right) V_{DD} e^{-t/R_1 C_1}$$

at rising end:  $\frac{2}{3} V_{DD} = V_{DD} - \left(1 + \frac{1}{3} - \frac{R_1}{R_1 + R_2}\right) V_{DD} e^{-t/R_1 C_1}$

$$+\frac{1}{3} = \left(\frac{4}{3} - \frac{k}{k+1}\right) e^{-t/R_1 C_1}$$

duty cycle =  $R_1 C_1 \ln \left(1 + 3 \frac{1}{k+1}\right)$ .

$$1 - 3 \frac{1}{k+1} = 4^{-\frac{1}{5}} \Rightarrow k = 8.38944.$$