

# Project : Digital Pulse Oximeter.

Principle:

1). Beer's Law:  $I = I_0 \cdot e^{-\epsilon CL}$

$I_0$ : light intensity entering sample.

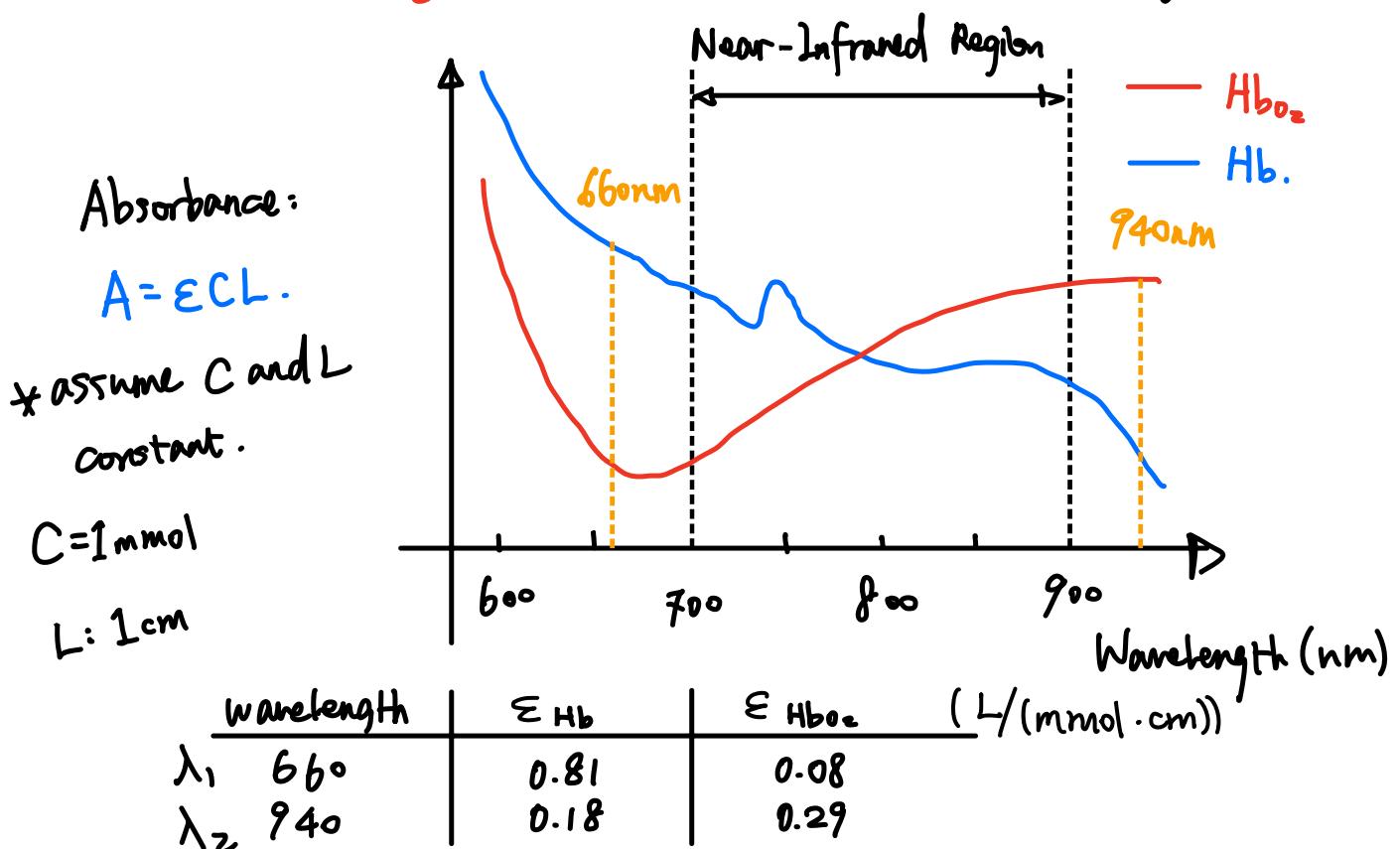
$I$ : light intensity leaving sample.

$\epsilon$ : extinction coefficient

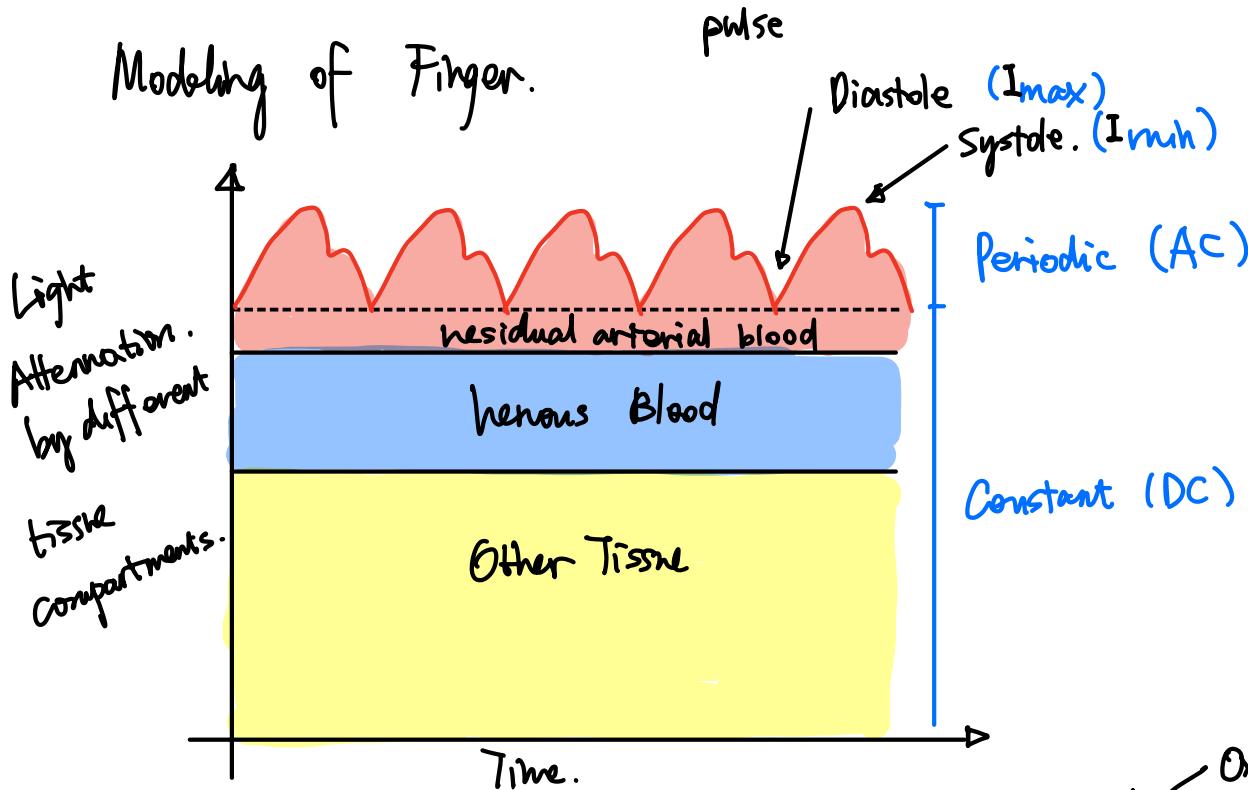
$C$ : sample concentration

$L$ : sample length (depth)

2) Absorbance of Hemoglobin ( $Hb$ ) and Oxygenated Hemoglobin ( $HbO_2$ ) at various wavelength.



# Modeling of Finger.



at systole:

$$I_{min} = I_0 / 0 - \epsilon_{DC} C_{DC} \cdot L_{DC} - (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) L_{max}$$

at diastole:

$$I_{max} = I_0 / 0 - \epsilon_{DC} C_{DC} \cdot L_{DC} - (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) L_{min}$$

ratio:

$$\frac{I_{min}}{I_{max}} = \frac{I_0 / 0 - \epsilon_{DC} C_{DC} \cdot L_{DC} - (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) L_{max}}{I_0 / 0 - \epsilon_{DC} C_{DC} \cdot L_{DC} - (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) L_{min}}$$

$$= 1 / 0 - \cancel{\epsilon_{DC} C_{DC} L_{DC}} - (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2})(L_{max} - L_{min}) + \cancel{\epsilon_{DC} C_{DC} L_{DC}}$$

$$= 1 / 0 - (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) \Delta L$$

$$\Rightarrow \log \frac{I_{min}}{I_{max}} = -(\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) \Delta L$$

$$A = (\epsilon_{Hb} C_{Hb} + \epsilon_{HbO_2} C_{HbO_2}) \Delta L = \log \frac{I_{max}}{I_{min}}$$

$$\text{where } I_{max} = I_{max, AC} + I_{DC} = I_{max} + I_{offset}$$

$$I_{min} = I_{min, AC} + I_{DC} = I_{min} + I_{offset}$$

$$\Rightarrow C_{\text{Hb}} = \frac{A}{\Delta L} - \frac{\epsilon_{\text{HbO}_2} C_{\text{HbO}_2}}{\epsilon_{\text{Hb}}} , \quad C_{\text{HbO}_2} = \frac{A}{\Delta L} - \frac{\epsilon_{\text{Hb}} C_{\text{Hb}}}{\epsilon_{\text{HbO}_2}}$$

at  $\lambda_1$  and  $\lambda_2$  (660 nm and 940 nm to maximize diff)

$$A_{\lambda_1} = (\epsilon_{\text{Hb}, \lambda_1} C_{\text{Hb}} + \epsilon_{\text{HbO}_2, \lambda_1} C_{\text{HbO}_2}) \Delta L$$

$$A_{\lambda_2} = (\epsilon_{\text{Hb}, \lambda_2} C_{\text{Hb}} + \epsilon_{\text{HbO}_2, \lambda_2} C_{\text{HbO}_2}) \Delta L$$

$$\frac{A_{\lambda_1}}{A_{\lambda_2}} = \frac{\epsilon_{\text{Hb}, \lambda_1} C_{\text{Hb}} + \epsilon_{\text{HbO}_2, \lambda_1} C_{\text{HbO}_2}}{\epsilon_{\text{Hb}, \lambda_2} C_{\text{Hb}} + \epsilon_{\text{HbO}_2, \lambda_2} C_{\text{HbO}_2}}$$

$$(\epsilon_{\text{Hb}, \lambda_2} C_{\text{Hb}} + \epsilon_{\text{HbO}_2, \lambda_2} C_{\text{HbO}_2}) A_{\lambda_1} = (\epsilon_{\text{Hb}, \lambda_1} C_{\text{Hb}} + \epsilon_{\text{HbO}_2, \lambda_1} C_{\text{HbO}_2}) A_{\lambda_2}$$

$$C_{\text{Hb}} (\epsilon_{\text{Hb}, \lambda_2} A_{\lambda_1} - \epsilon_{\text{Hb}, \lambda_1} A_{\lambda_2}) = C_{\text{HbO}_2} (\epsilon_{\text{HbO}_2, \lambda_1} A_{\lambda_2} - \epsilon_{\text{HbO}_2, \lambda_2} A_{\lambda_1})$$

$$\Rightarrow C_{\text{Hb}} = C_{\text{HbO}_2} \frac{(\epsilon_{\text{HbO}_2, \lambda_1} A_{\lambda_2} - \epsilon_{\text{HbO}_2, \lambda_2} A_{\lambda_1})}{(\epsilon_{\text{Hb}, \lambda_2} A_{\lambda_1} - \epsilon_{\text{Hb}, \lambda_1} A_{\lambda_2})}$$

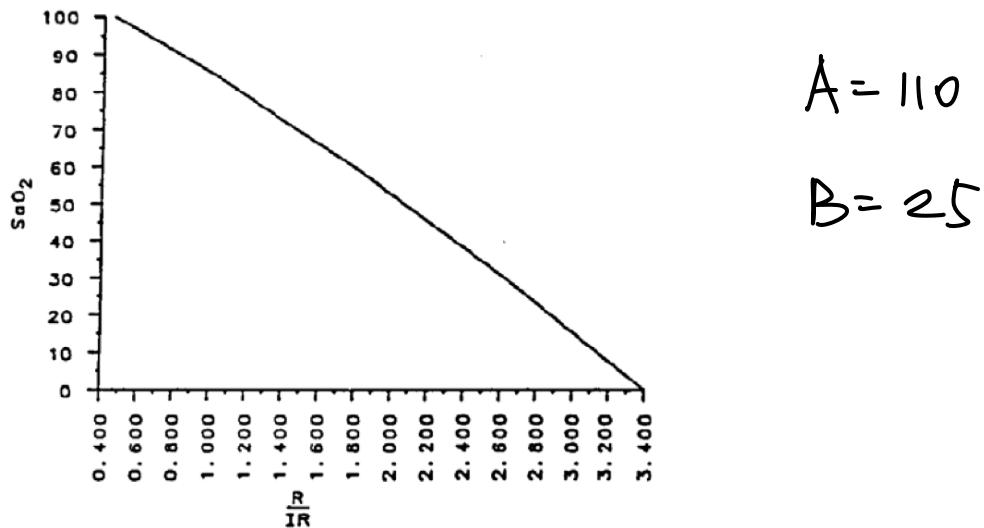
$$SpO_2 = \frac{C_{\text{HbO}_2}}{C_{\text{HbO}_2} + C_{\text{Hb}}} = \frac{\cancel{C_{\text{HbO}_2}}}{\cancel{C_{\text{HbO}_2}} \left( 1 + \frac{(\epsilon_{\text{HbO}_2, \lambda_1} A_{\lambda_2} - \epsilon_{\text{HbO}_2, \lambda_2} A_{\lambda_1})}{(\epsilon_{\text{Hb}, \lambda_2} A_{\lambda_1} - \epsilon_{\text{Hb}, \lambda_1} A_{\lambda_2})} \right)}$$

$$= \frac{(\epsilon_{\text{Hb}, \lambda_2} A_{\lambda_1} - \epsilon_{\text{Hb}, \lambda_1} A_{\lambda_2})}{(\epsilon_{\text{Hb}, \lambda_2} A_{\lambda_1} - \epsilon_{\text{Hb}, \lambda_1} A_{\lambda_2}) + (\epsilon_{\text{HbO}_2, \lambda_1} A_{\lambda_2} - \epsilon_{\text{HbO}_2, \lambda_2} A_{\lambda_1})}$$

or uses Empirically determined relationship between

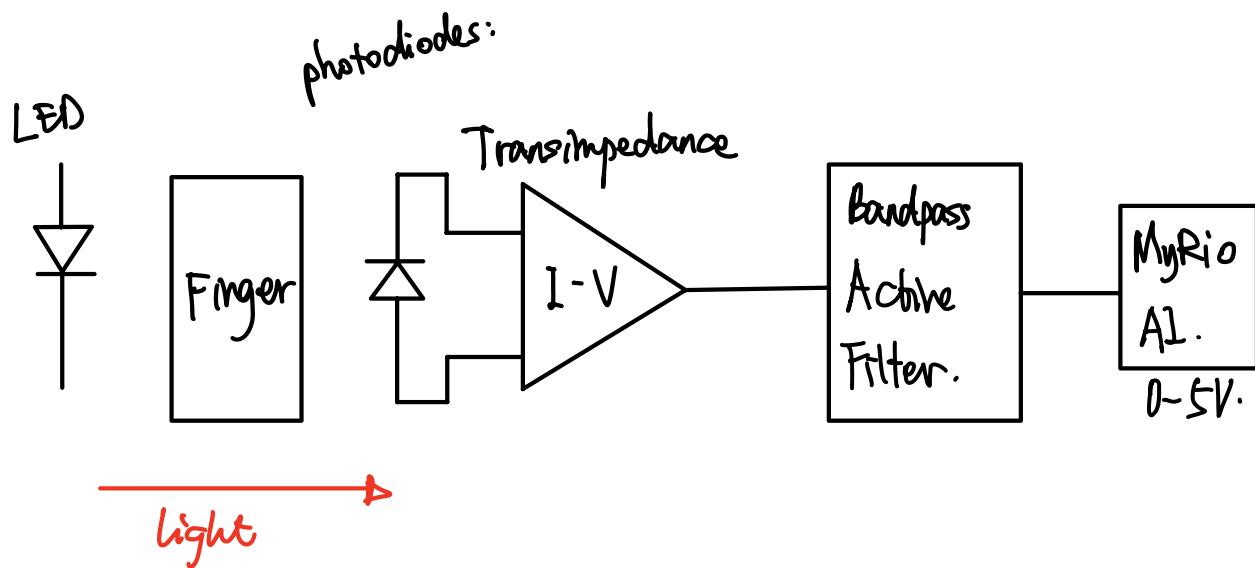
$\text{SpO}_2$  and normalized  $(I_{\max,R} - I_{\min,R}) / (I_{\max,IR} - I_{\min,IR})$

$$\text{SpO}_2 (\%) = A - B \cdot \frac{(I_{\max,R} - I_{\min,R}) / I_{\text{offset},R}}{(I_{\max,IR} - I_{\min,IR}) / I_{\text{offset},IR}}$$



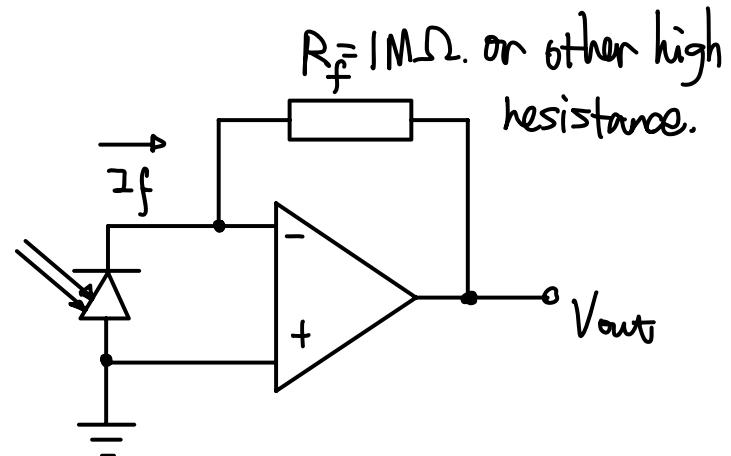
\*final choice of formula depends on how  
easily the DC component of the channel  
readings can be calibrated.

# Theoretical Schematic



- Power.

- Transimpedance Amplifier.



- Measure idle. voltage / finger-inserted voltage .

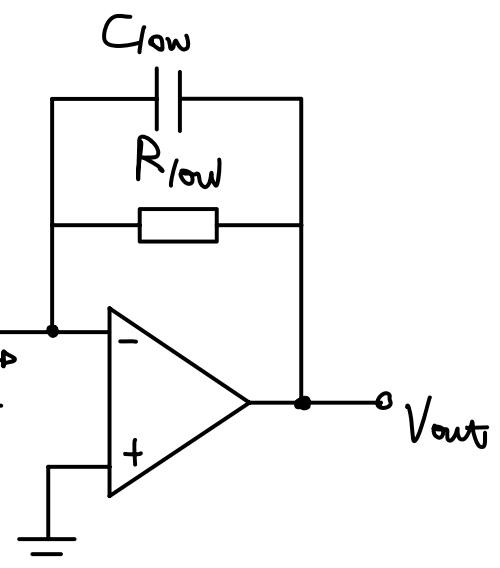
Compare to myRio AI. port.

$$V_{out} = - \mathcal{I}_f R_f .$$

- Bandpass Active Filter



$$\frac{V_{out}}{V_{in}} = \frac{R_{low}}{R_{high}} , f_c = \frac{1}{2\pi R C}$$

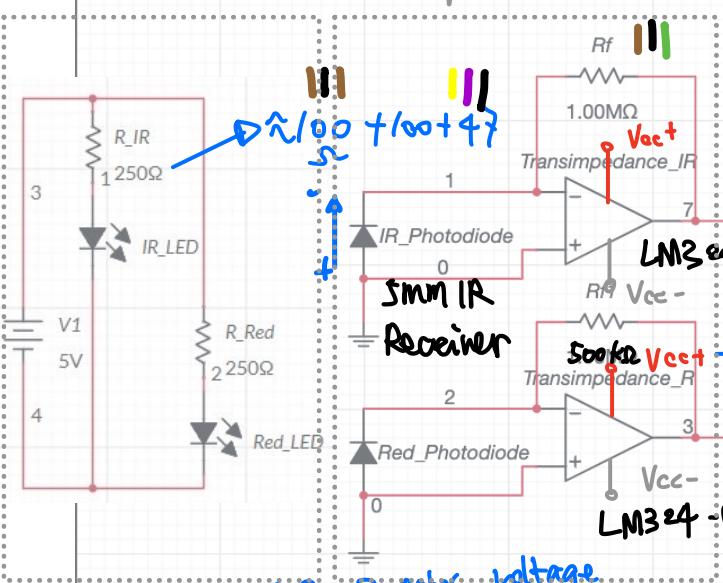


Wiring:

\* color code:  $V_{cc+}$   $V_{cc-}$  GND Signal (Red) Signal ( $\text{IR}$ )

$+5$   $+15$

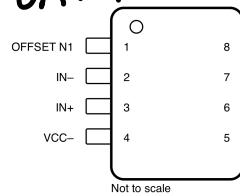
### Transimpedance Stage



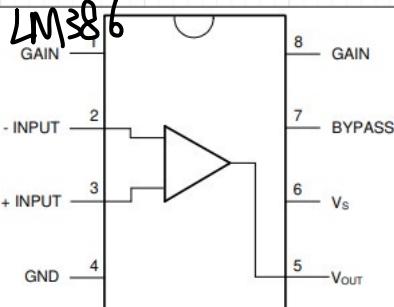
\* 2 DC Supply voltage.

- ① +5V right rail +
- ② +15V left rail +
- ③ -15V right rail -
- ④ GND left rail -

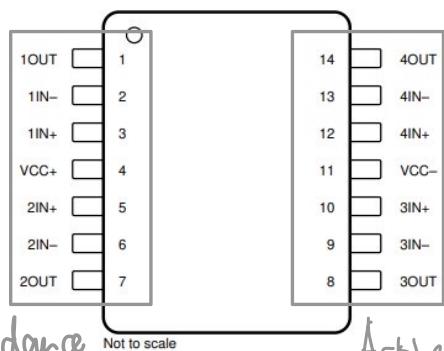
UA741



LM386



LM324



Trans-impedance

Active filter

LM324 Supply Voltage:  $\pm(3,30)\text{V}$

\* common mode voltage  $\frac{1}{2}(\text{sum } \text{IN+}, \text{IN-})$

### Active Filter Stage

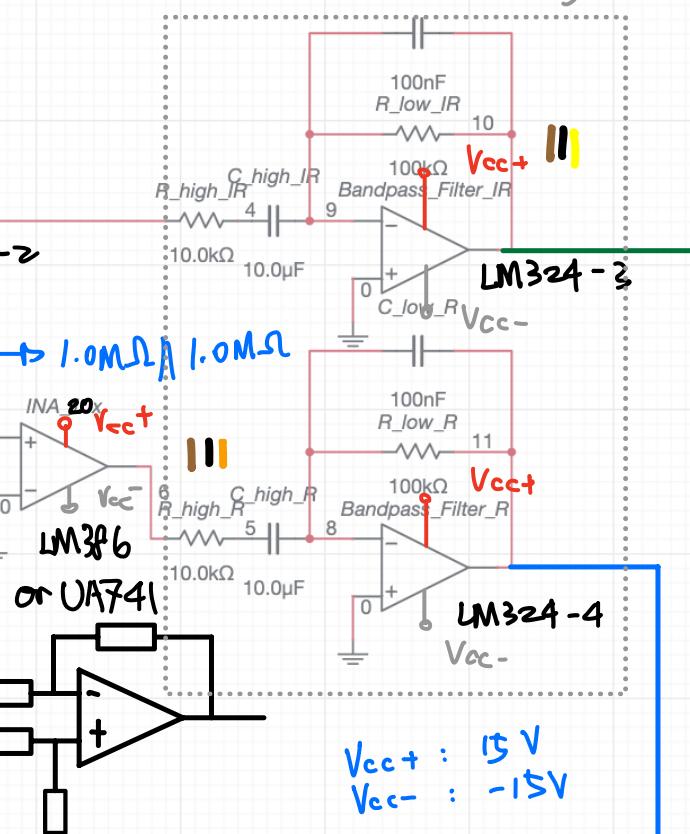
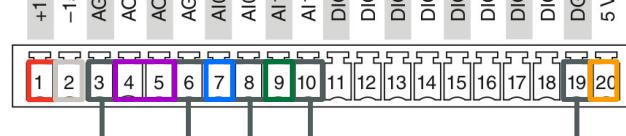
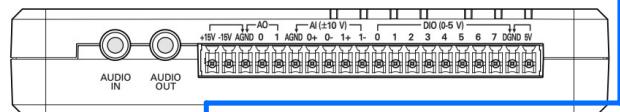


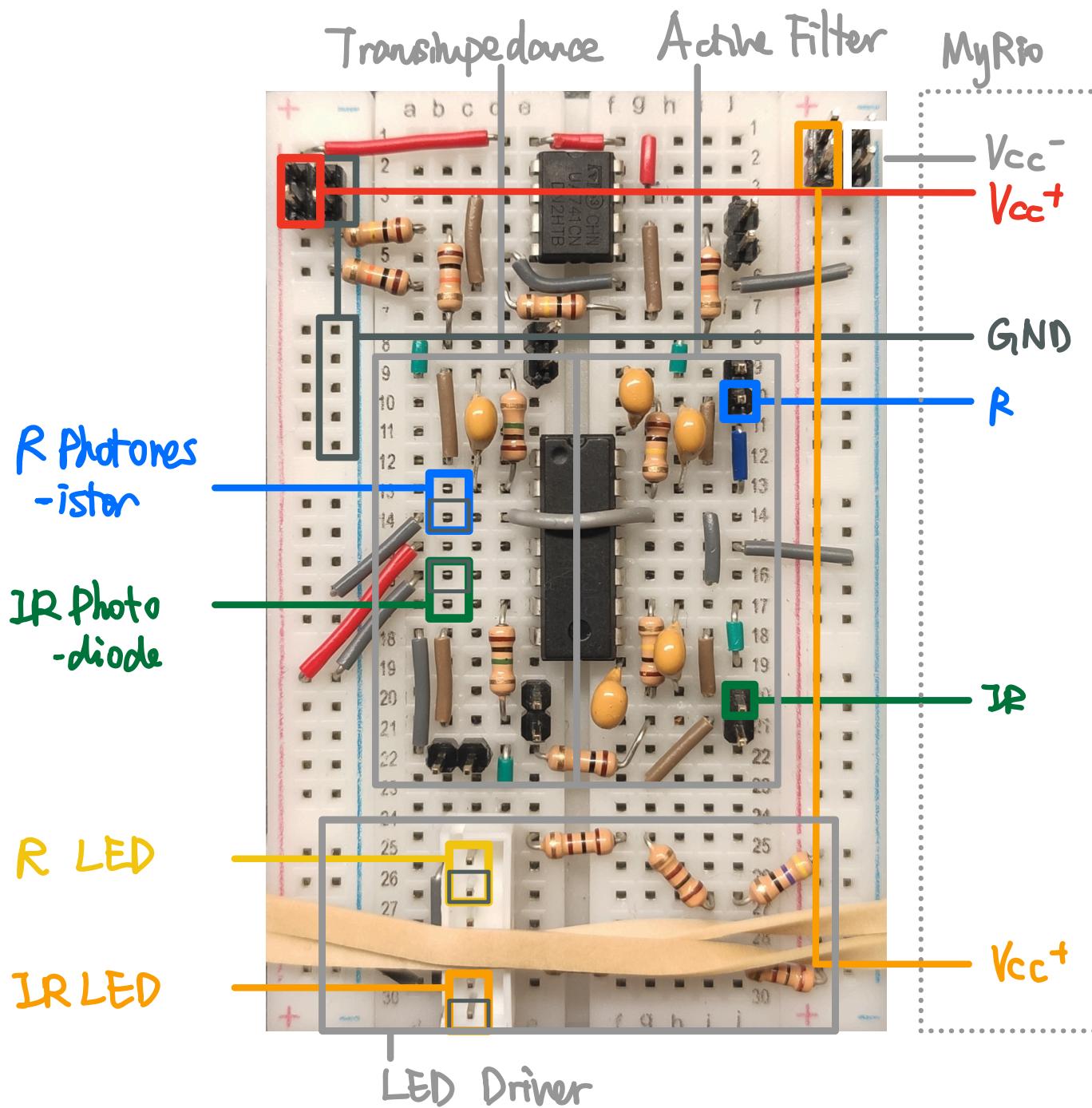
Figure 4. Primary/Secondary Signals on MSP Connector C



$$V_R = V_{A10+} - V_{A10-}$$

$$V_{IR} = V_{A11+} - V_{A11-}$$

# Bread Board Circuit Layout Diagram.



\* added an additional capacitor at R Transimpedance Stage.

+ left room for change Gain of IR Active Filter Stage.

Resistor choice: (based on LM324; LM386 has preset gains)

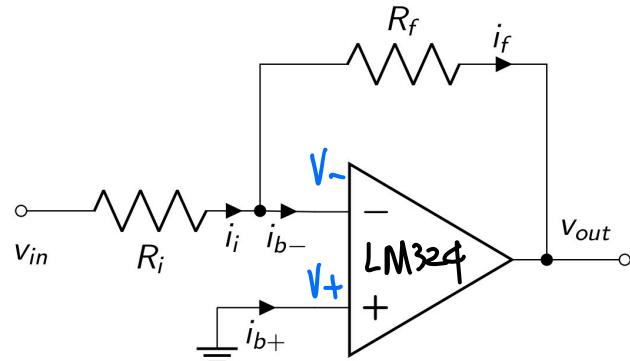
LM324:

- bias current ( $i_b$ )

$$\leq \pm 35 \text{ nA}$$

- input impedance ( $R_{in}$ )

$$= 1 \text{ G}\Omega$$



To avoid signal clipping at A10, let ideal output

$$V_{out,i} = 5V \cdot 90\% = -4.5V$$

and the error tolerance 1%.

In worse case  $V_{out} = (1 - 1\%) \times V_{out,i} = -4.4550V$

assume ideal non-inverting input & virtual short.

$$V_- = V_+ = 0V$$

$$i_f = \frac{V_- - V_{out}}{R_f} = \frac{4.4550V}{R_f}$$

$$V_{in} = -V_{out,i} \cdot \frac{R_i}{R_f} = 4.5V \cdot \frac{R_i}{R_f}$$

$$i_i = \frac{V_{in} - V_-}{R_i} = \frac{V_{in}}{R_i} = \frac{4.5V}{R_f}$$

According to KCL (at - input node):  $i_i = i_{b-} + i_f$

$$i_{b-} = i_i - i_f \quad \text{and} \quad i_{b-} = 35 \text{ nA} = \frac{4.5V - 4.4550V}{R_f}$$

$$\text{so } R_{f,\text{upper}} = \frac{(4.5 - 4.4550)V}{35 \times 10^{-9} A} = 1.3 \times 10^6 \Omega = 1.3 M\Omega$$

- however, the input impedance  $R_{in} = 1 G\Omega$

we want  $R_f \lll R_{in}$

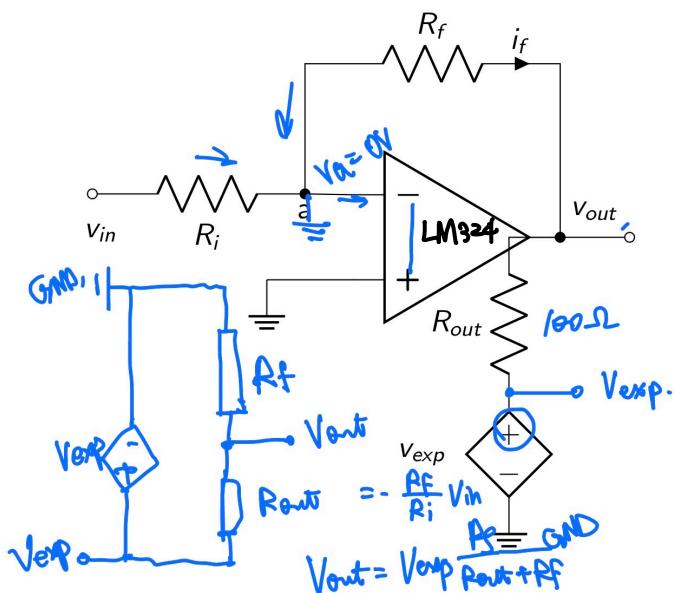
- \* the desired upper bound of  $R_f$  is around  $130 k\Omega$

- output impedance ( $R_{out}$ )

$$= 300 \Omega$$

- output current ( $I_{out}$ )

$$\lesssim -60 \text{ mA}$$



- \* assume input side fully ideal,  $V_a = 0V$

the output impedance  $R_{out}$  forms a voltage divider with  $R_f$

if we would like 99% preserved  $\frac{V_{out}}{V_{exp}}$

$$V_{out} = V_{exp} \cdot \frac{R_f}{R_f + R_{out}} \Rightarrow \frac{R_{f,\text{lower}}}{R_{f,\text{lower}} + 300 \Omega} = 0.99$$

$$\Rightarrow R_{f,\text{lower}} = 29.7 k\Omega$$

Thus for LM324:  $30 k\Omega \leq R_f \leq 130 k\Omega$

# Circuit Characterization.

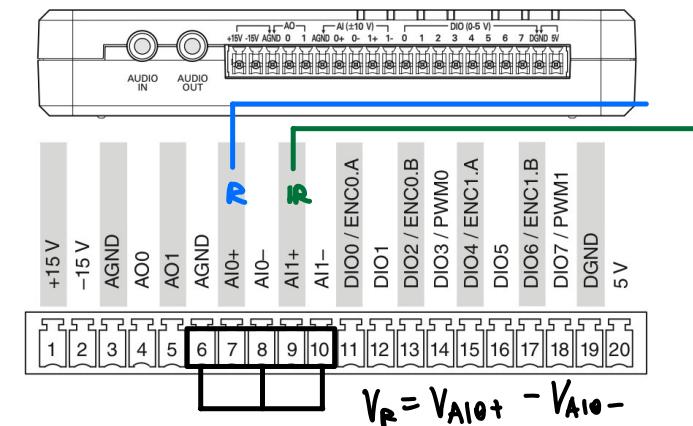
pin layout:

Fgen : offset sine signal.  $\begin{cases} R : C/A01,4 \rightarrow +\text{INPUT}, 3 \\ I/R : C/A00,2 \rightarrow \text{SIN-}, 9 \end{cases}$

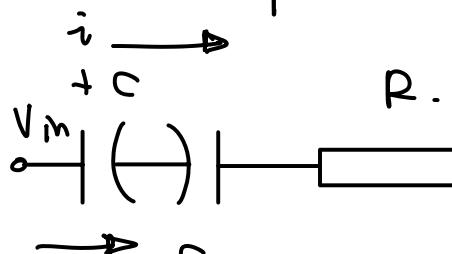
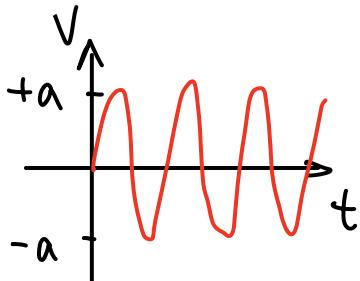
Circuit Output :

amplified & filtered signal  $\begin{cases} R : \text{FOUT}, 14 \rightarrow C/A10^+, 3 \\ I/R : \text{BOUT}, 8 \rightarrow C/A11^+, 5 \end{cases}$

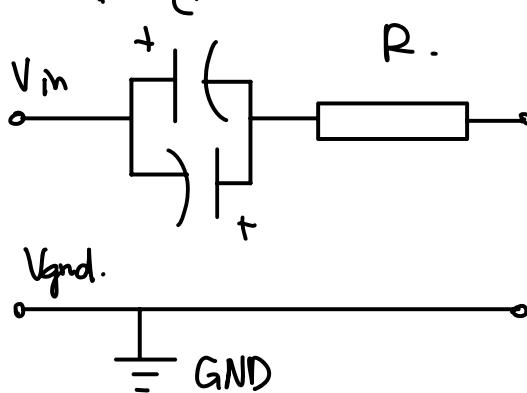
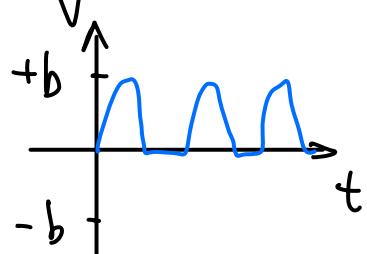
Figure 4. Primary/Secondary Signals on MSP Connector C



- Characterize : Graph vs. Input Frequency



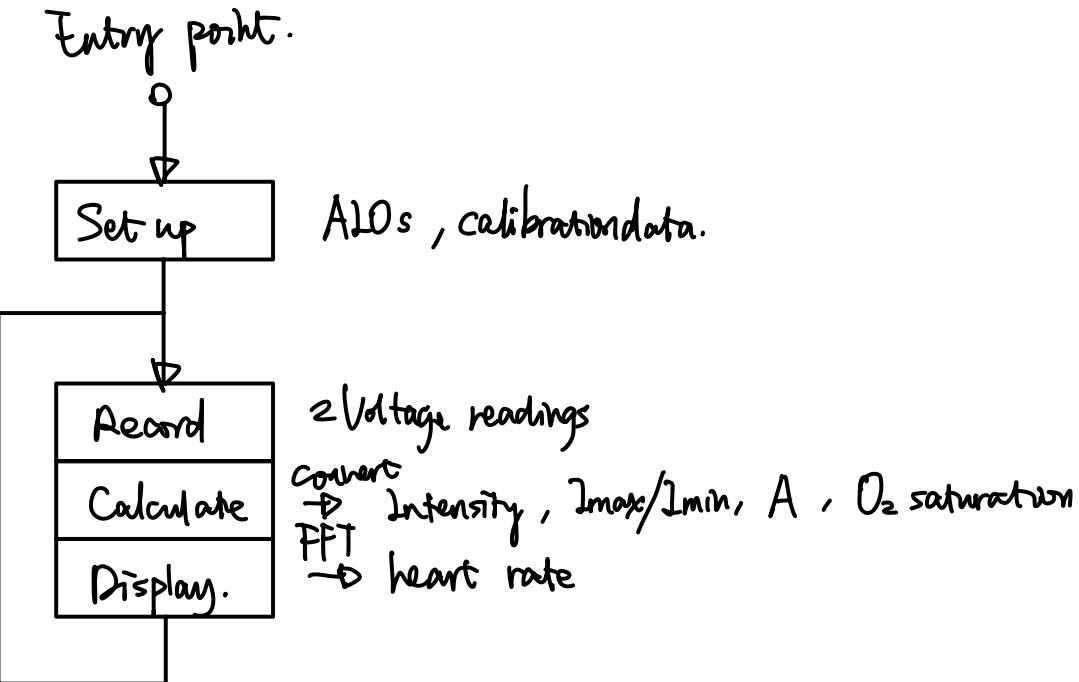
$$V_{IR} = V_{AI1+} - V_{AI1-}$$



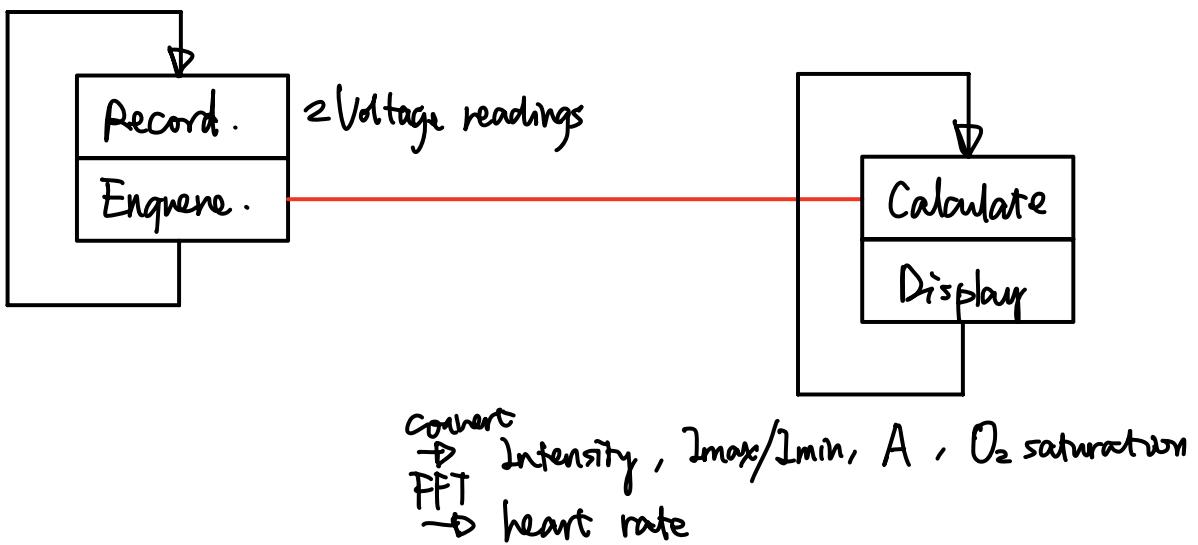
# LabVIEW Program Design:

① Super Loop & Producer consumer loop.

Super Loop: (for proof of concept)

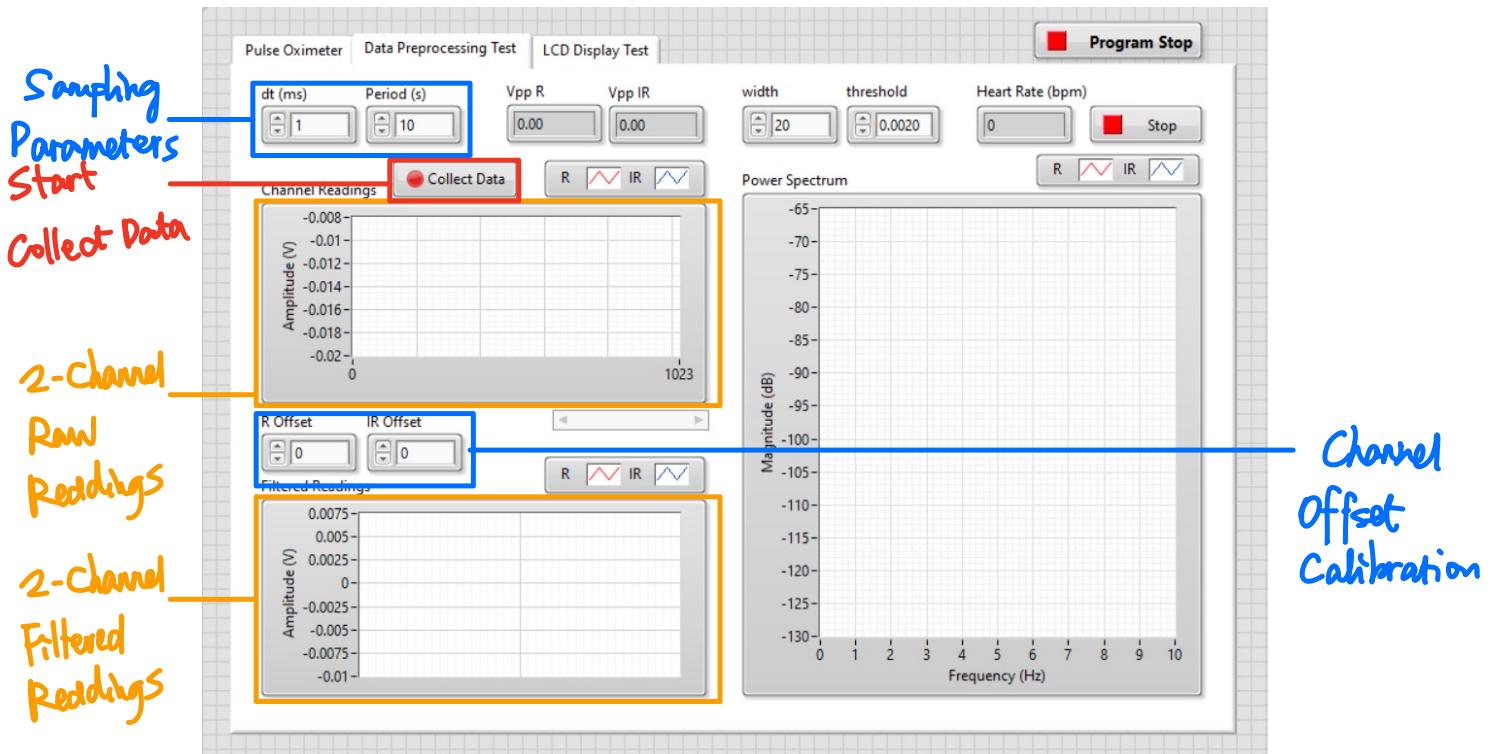
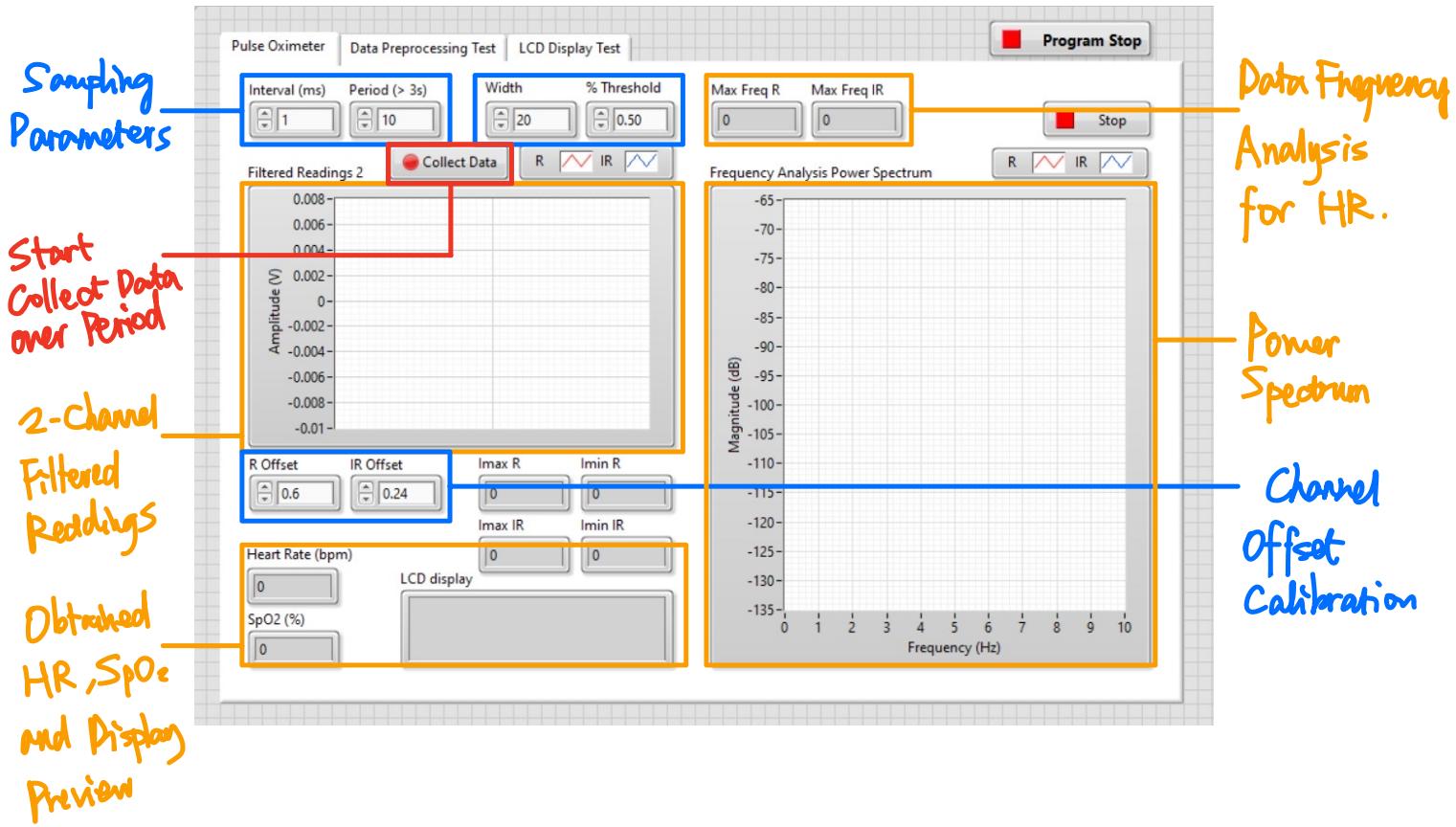


Producer - Consumer Loop: (for future improvements)

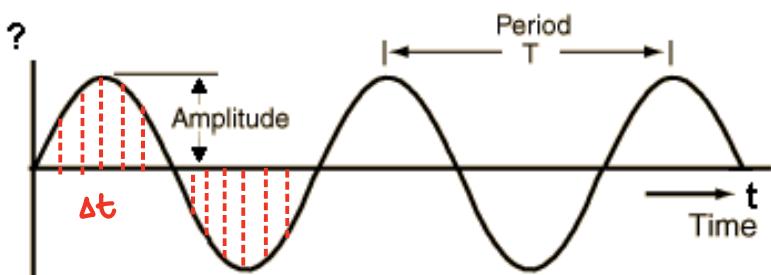
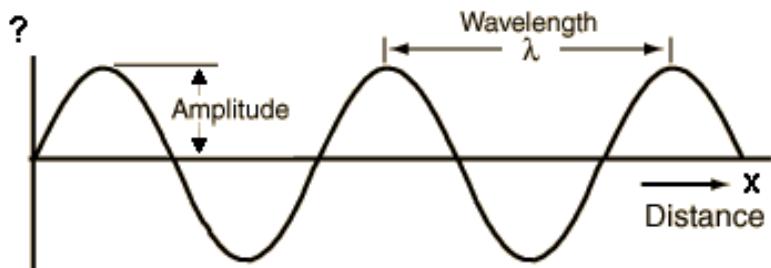


# LabVIEW Front Panel Phenomenon

## ① Pulse Oximeter Tab.



## ② Test Program:

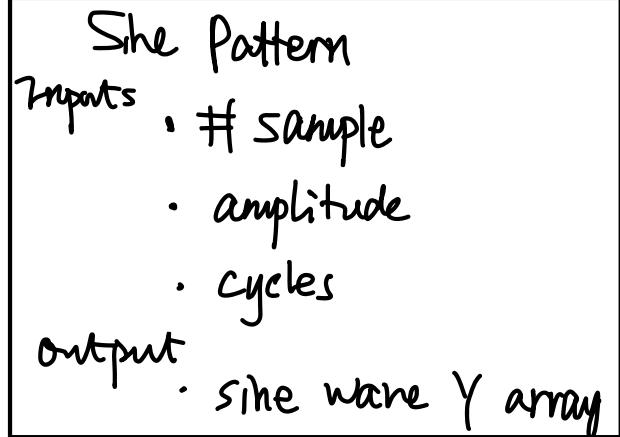
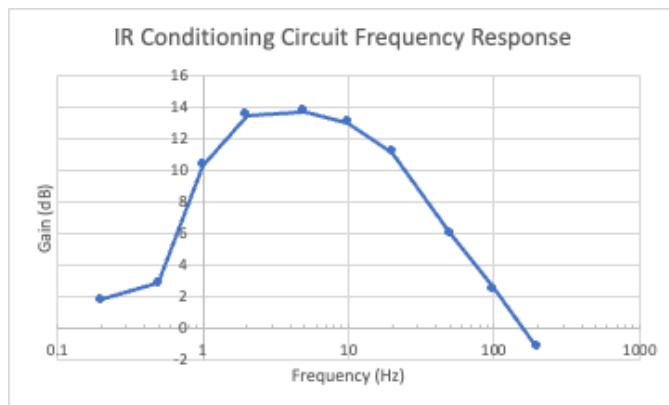
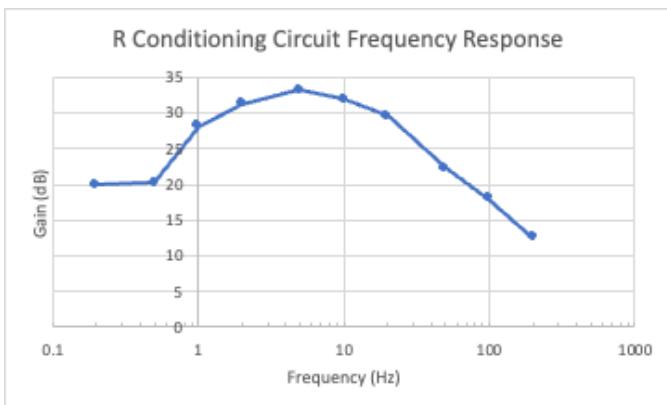


Use Scope & Fgen for NI myRIO.

Freq response data:

R				
Frequency (Hz)	Input (Vpp)	Output (Vpp)	Gain	Gain (dB)
0.2	0.034	0.336	9.882352941	19.89720721
0.5	0.043	0.439	10.20930233	20.17992129
1	0.039	0.996	25.53846154	28.14389463
2	0.039	1.436	36.82051282	31.32179666
5	0.039	1.799	46.12820513	33.27933113
10	0.039	1.548	39.69230769	31.97412699
20	0.039	1.167	29.92307692	29.52012498
50	0.044	0.571	12.97727273	22.26366864
100	0.039	0.312	8	18.06179974
200	0.039	0.166	4.256410256	12.58086962

IR				
Frequency (Hz)	Input (Vpp)	Output (Vpp)	Gain	Gain (dB)
0.2	0.039	0.048	1.230769231	1.803532607
0.5	0.039	0.054	1.384615385	2.826583056
1	0.034	0.112	3.294117647	10.35478211
2	0.034	0.161	4.735294118	13.50693918
5	0.039	0.19	4.871794872	13.75377988
10	0.039	0.175	4.487179487	13.03946883
20	0.039	0.141	3.615384615	11.16309011
50	0.039	0.078	2	6.020599913
100	0.039	0.052	1.333333333	2.498774732
200	0.039	0.034	0.871794872	-1.1917138



$$\text{Period } T . \quad \text{freq } f = \frac{1}{T}$$

Equations:

$$\text{Waveformduration} = \text{Period} \cdot \# \text{of period}.$$

$$\Delta t \cdot \# \text{sample} = T \cdot \# \text{cycle}.$$

$$\Delta t \cdot \# \text{sample/cycle} \cdot \# \text{cycle} = \frac{1}{f} \cdot \# \text{cycle}.$$

$$\Delta t = \frac{1}{f \cdot \# \text{sample/cycle}}$$

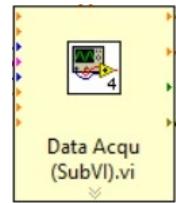
if  $f = 10 \text{ Hz} = 10 \text{ s}^{-1}$ ,  $\# \text{sample/cycle} = 128/\text{cycle}$ .

$$\Delta t = \frac{1}{10 \text{ s}^{-1} \cdot 128} = \frac{1}{1280 \text{ s}^{-1}} = \frac{1}{1280} \text{ s}.$$

### ③ Functional Sub VIs :

#### 1. Data Acquiring :

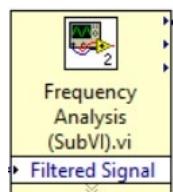
Input : C side A/D, 2 channels



Output : 2 1D arrays containing R, IR  
channel readings.

#### 2. FFT- Frequency Analysis.

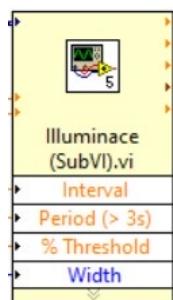
Input : 2-channel filtered signal waveform



Output: 2-channel Power-spectrum

#### 3. Illuminance Calculator

Input: 2-channel filtered signal waveform



Output:  $I_{max, R}$        $I_{min, R}$

$I_{max, IR}$        $I_{min, IR}$ .

## 4. SpO<sub>2</sub> Calculator.

Inputs: ( $I_{max}$ ,  $I_{min}$ ) at  $\lambda_1, \lambda_2$

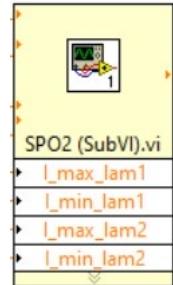
$$A_{\lambda_i} = \log \frac{I_{max, \lambda_i}}{I_{min, \lambda_i}}, \quad \lambda_i, i \in 1, 2$$

wavelength	$\epsilon_{Hb}$	$\epsilon_{HbO_2}$	(L/(mmol · cm))
$\lambda_1 660$	0.81	0.08	
$\lambda_2 940$	0.18	0.29	

$$SpO_2 = \frac{(\epsilon_{Hb, \lambda_2} A_{\lambda_1} - \epsilon_{Hb, \lambda_1} A_{\lambda_2})}{(\epsilon_{Hb, \lambda_2} A_{\lambda_1} - \epsilon_{Hb, \lambda_1} A_{\lambda_2}) + (\epsilon_{HbO_2, \lambda_1} A_{\lambda_2} - \epsilon_{HbO_2, \lambda_2} A_{\lambda_1})}$$

$$SpO_2 (\%) = A - B \cdot \frac{(I_{max, \lambda_1} - I_{min, \lambda_1}) / I_{offset, \lambda_1}}{(I_{max, \lambda_2} - I_{min, \lambda_2}) / I_{offset, \lambda_2}}$$

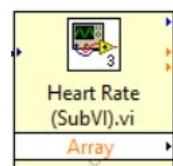
Output: SpO<sub>2</sub>



## 5. Heart Rate Calculator.

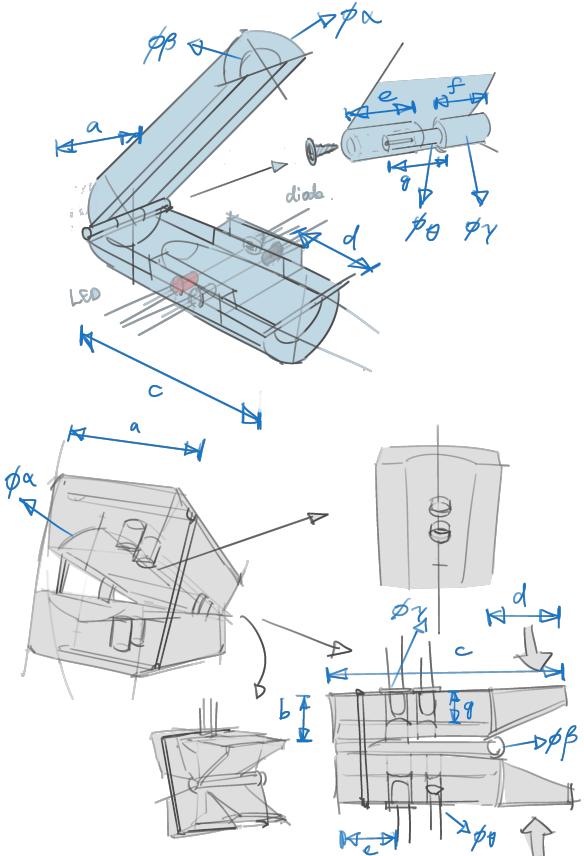
Input: 2-channel power-spectrum

Output: Average Heart Rate (bpm)



# Finger Clip Design.

design 1.

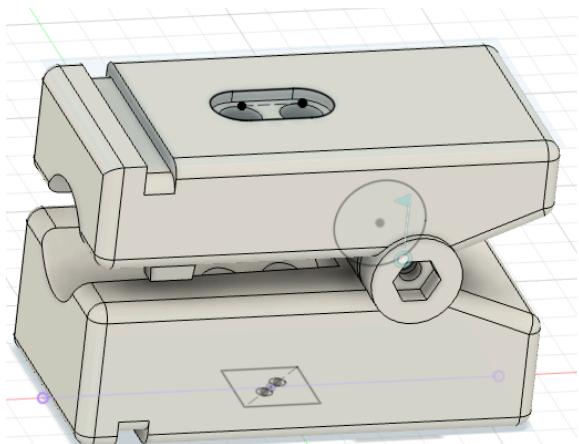


design 2.

# Finger Clip Modeling

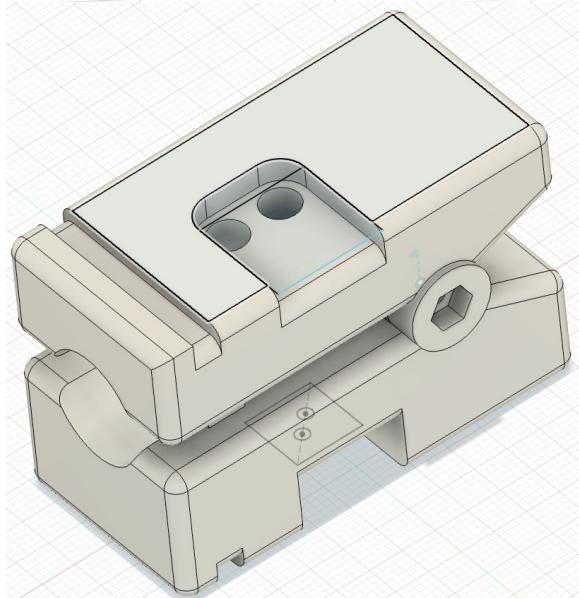
V1.

- ① designed to fit with a M3 bolt & nuts.



V2.

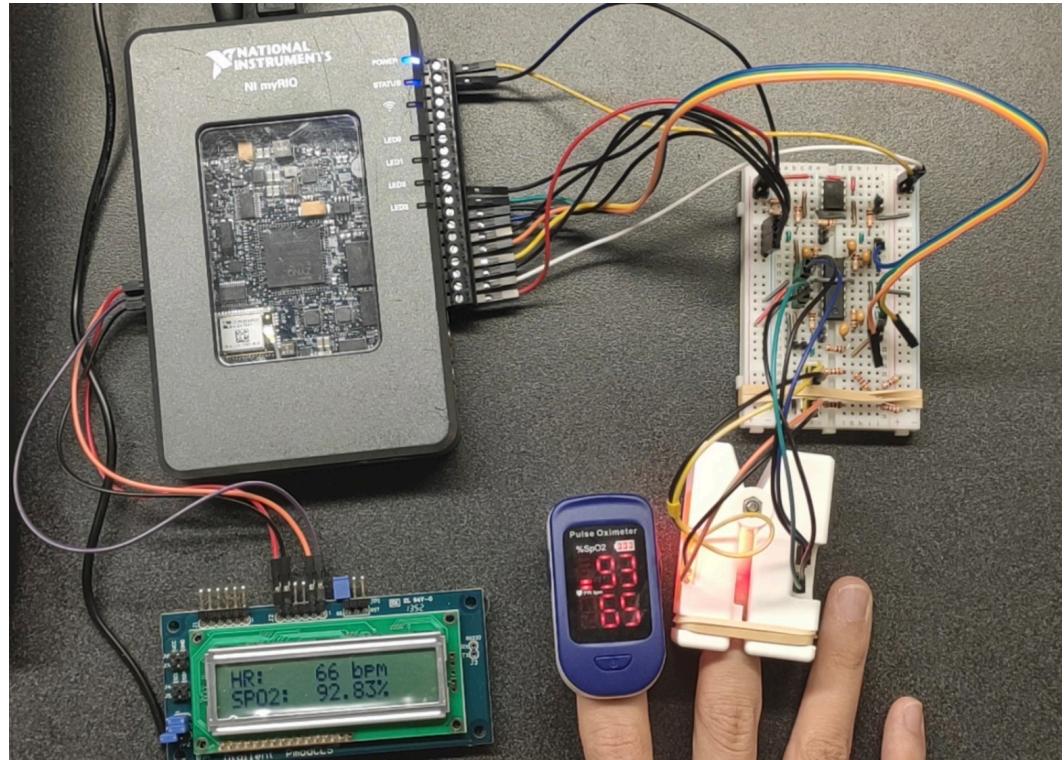
- ② added cable management slots



- ③ adjusted dimensions for 3d printing

## System Preview.

1. readings compared to commercial product after holding breath .30s



2. readings compared to commercial product

