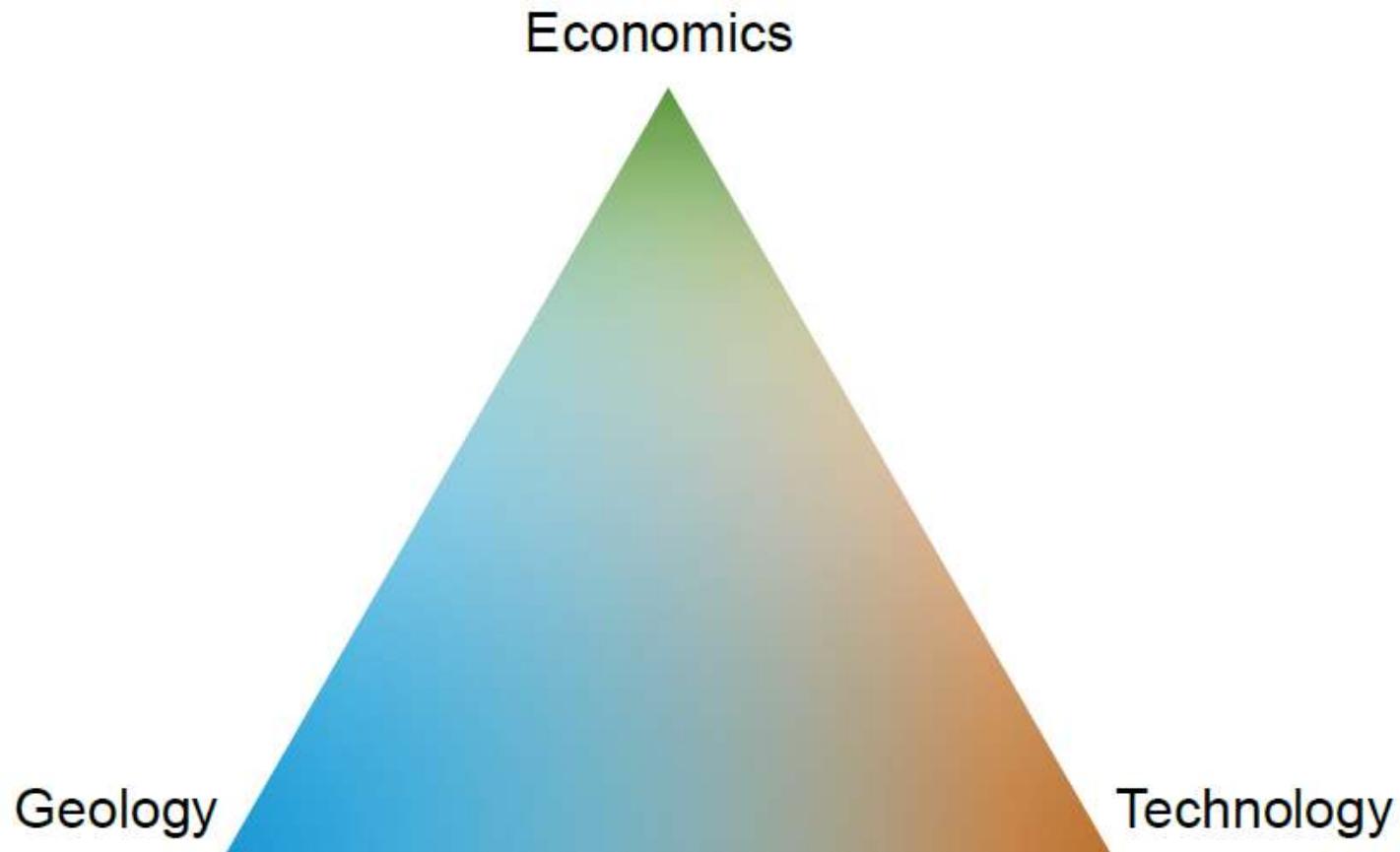


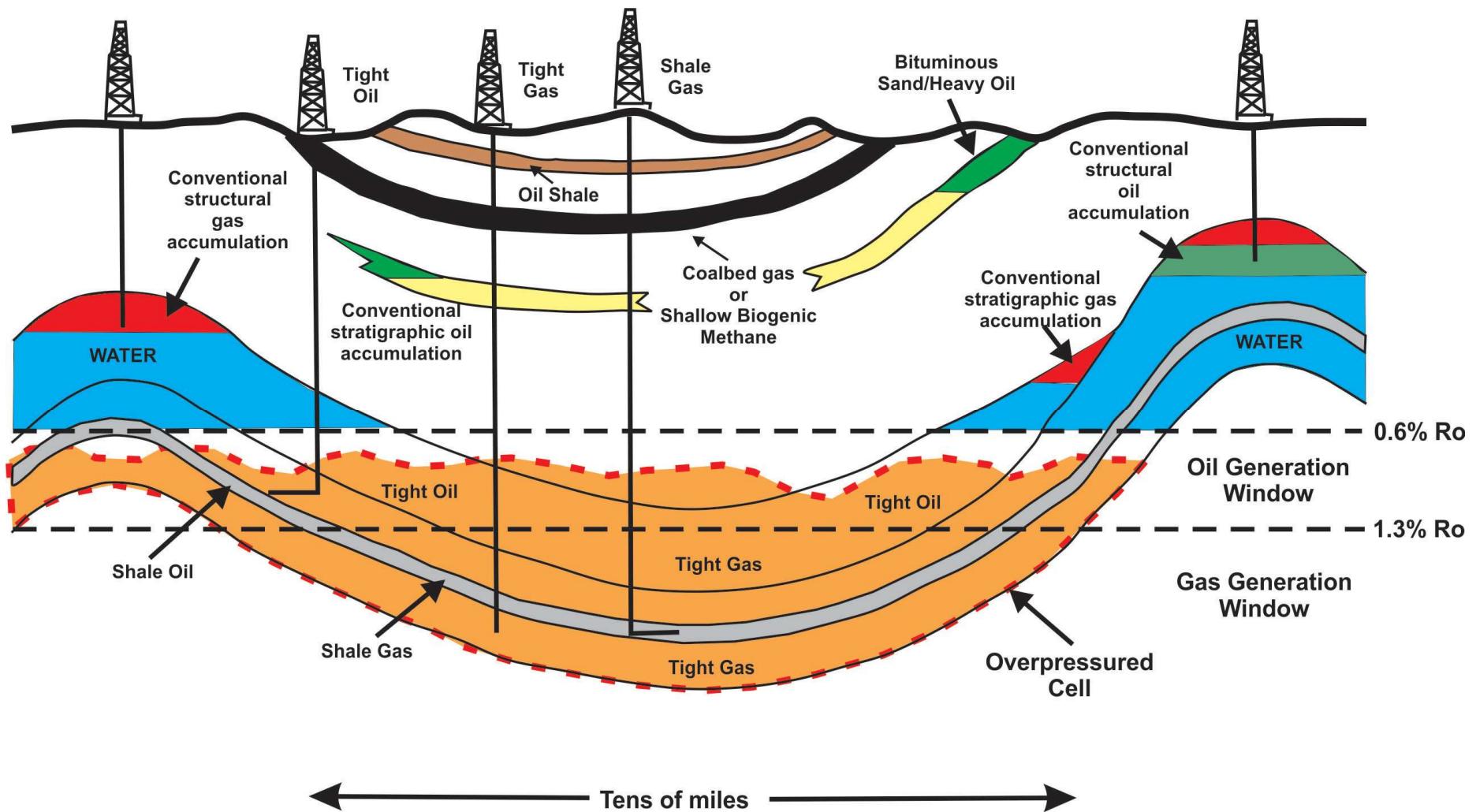
Denver Basin Overview

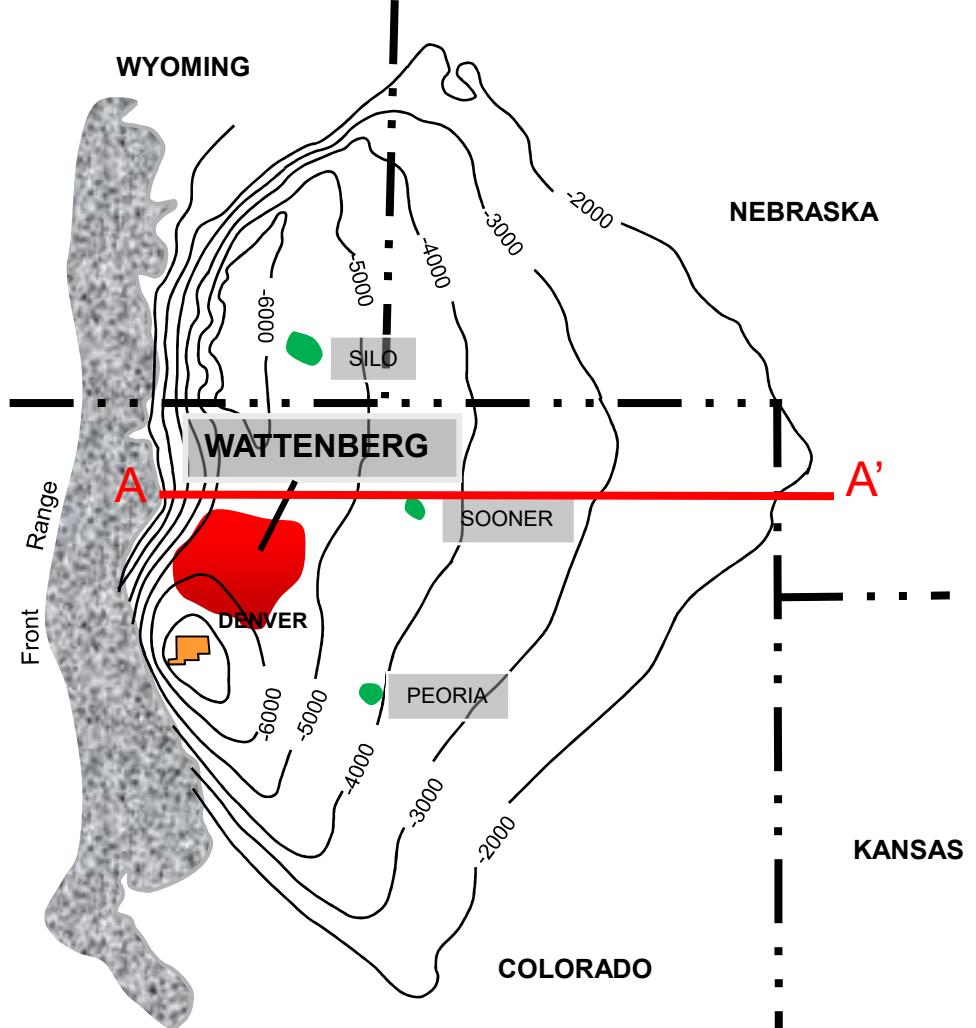
Dr. Steve Sonnenberg

Three Main Drivers of Oil and Natural Gas Production And Resource Estimates

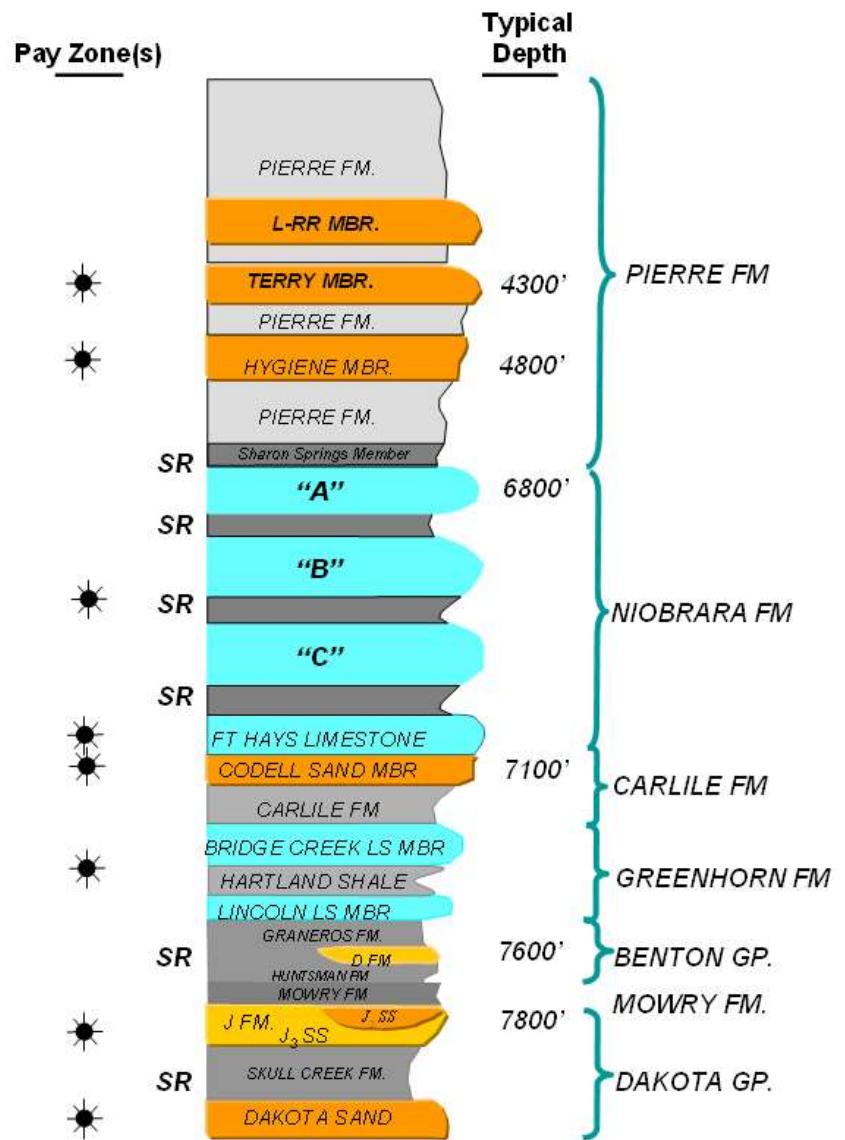


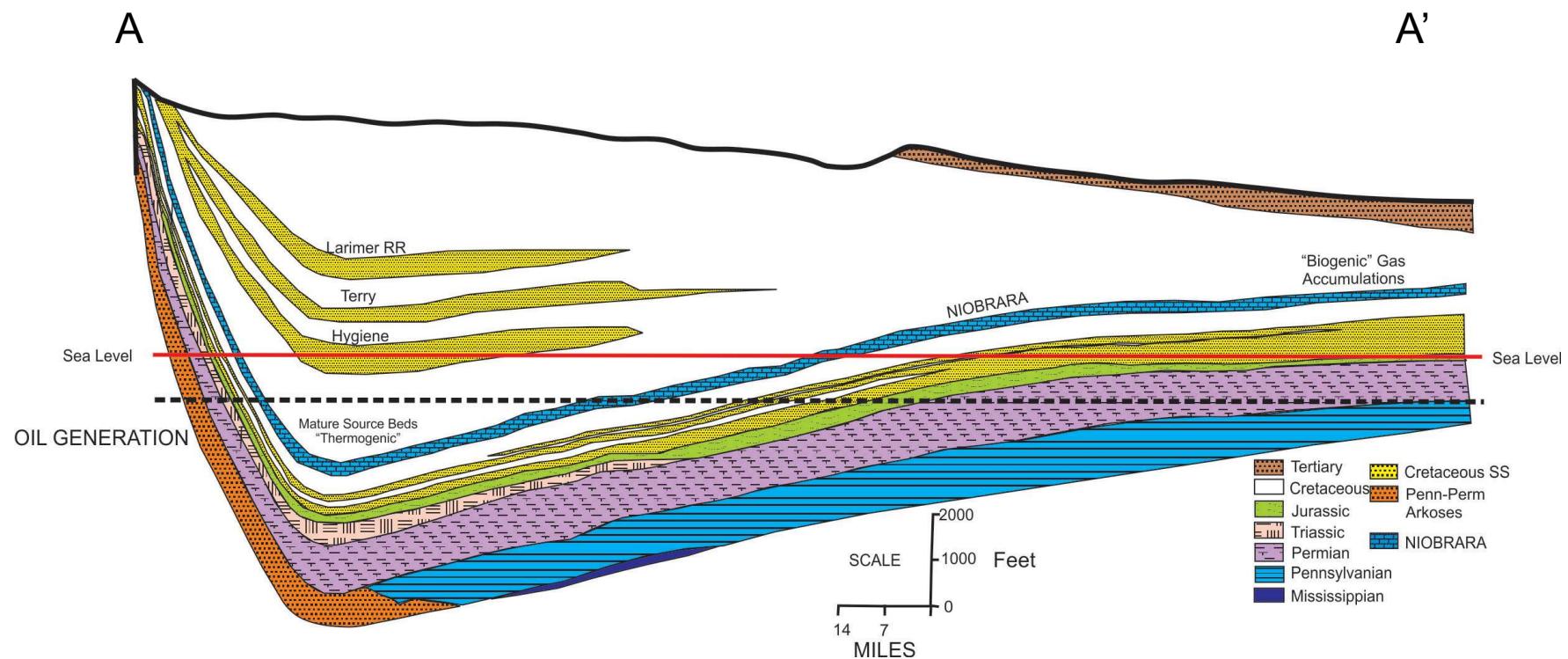
Conventional and Unconventional Traps



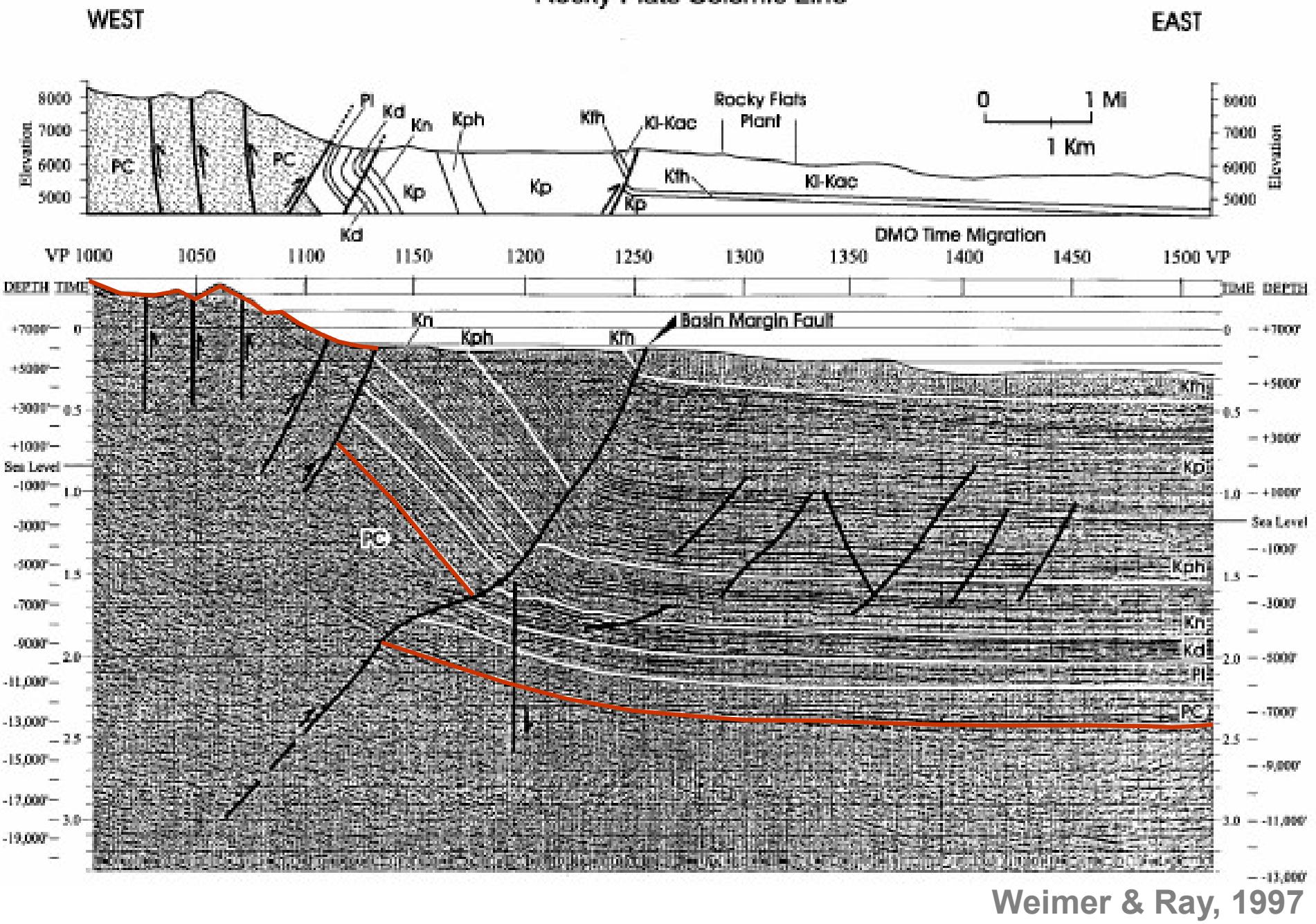


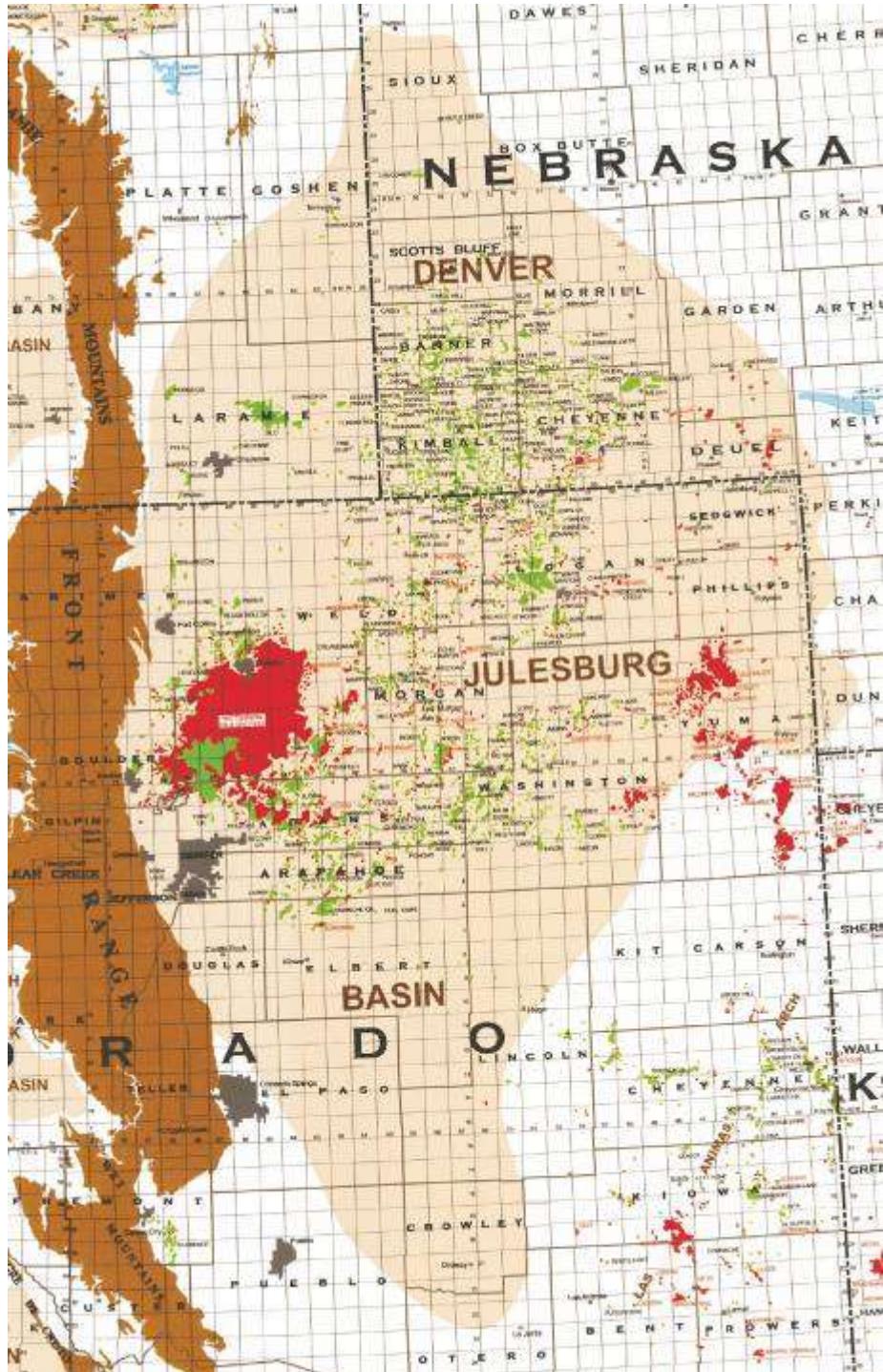
Structure Base Pennsylvanian
After Martin, 1965





Rocky Flats Seismic Line





Denver Basin

- Asymmetric Basin
- 60,000 mi²
- Up to 13,000 ft deep
- Majority of Production from Cretaceous reservoirs

- First oil-1862: Oil spring near Canon City; ~ 1 BOPD

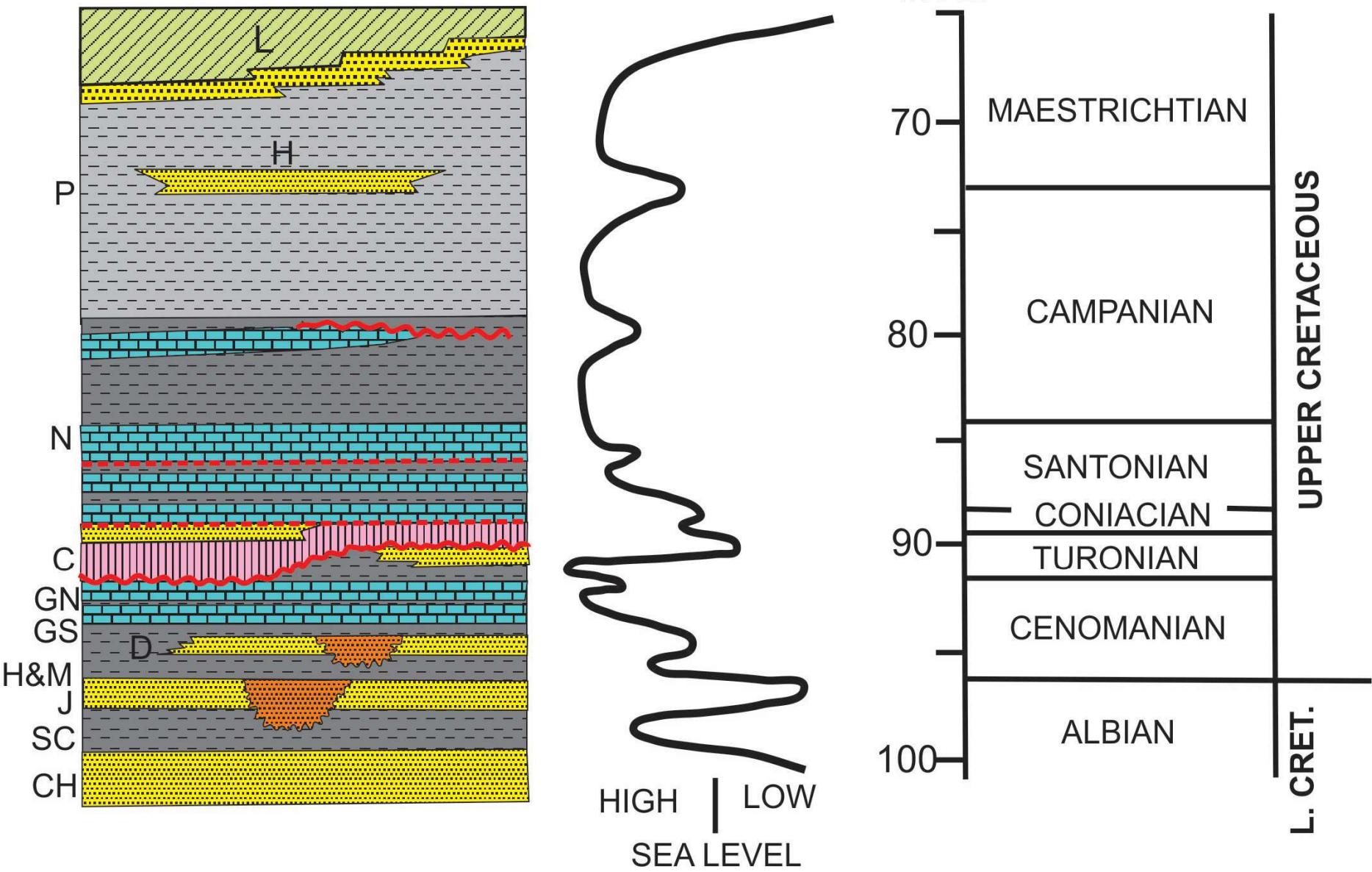
• First oil well-1876:

- Cassidy & Canfield drilled well to 1445 ft and hit oil
- Florence Canon City Field has produced > 15 million BO
- Fracture Pierre shale bottom of Canon City Embayment

• Boulder Oil Field:

- 1901
- Fracture Pierre Shale

- 1949-- Discovery in Nebraska: Ohio Oil Company 225 BOPD

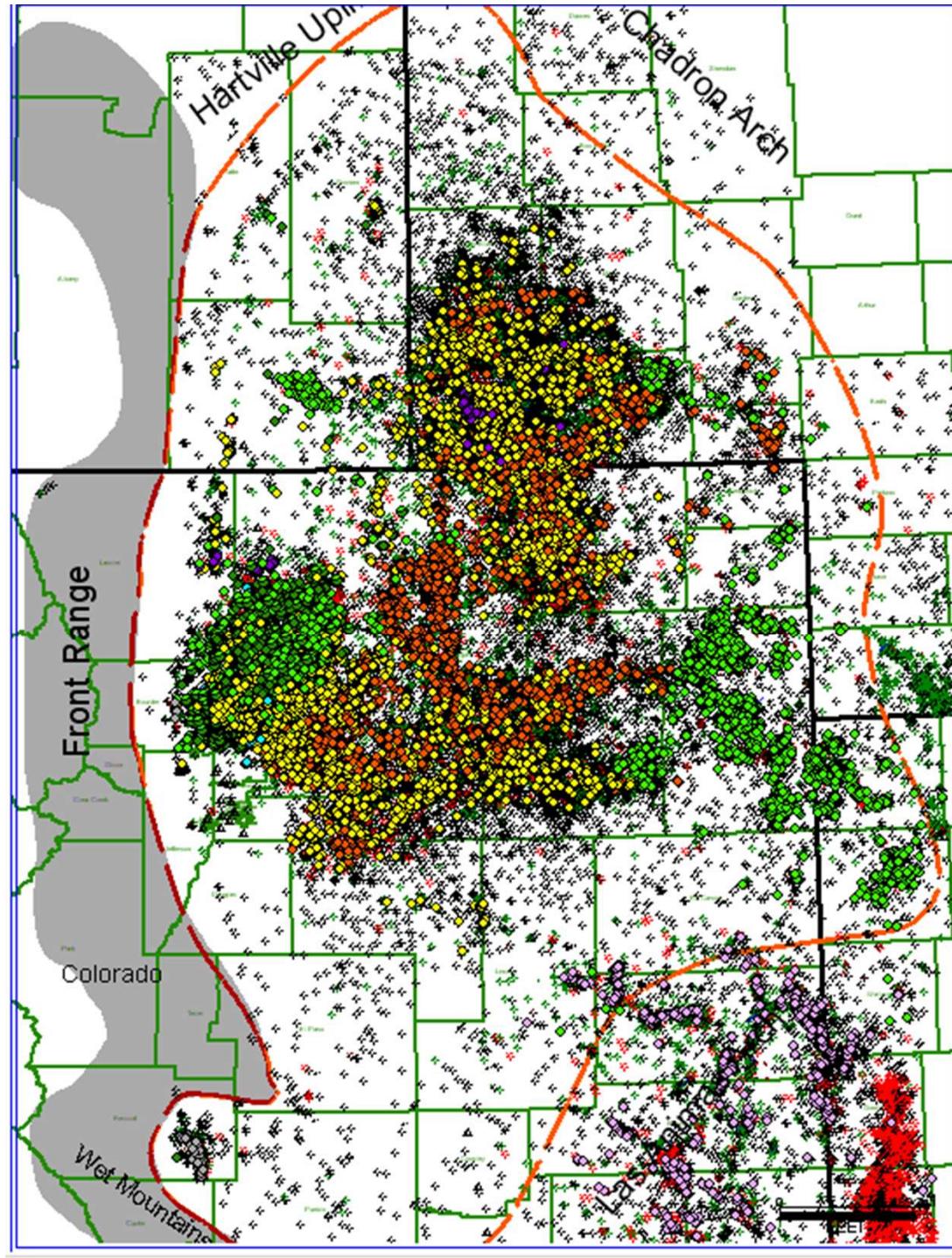


OIL CREEK

SITE OF THE FIRST OIL WELL IN THE WEST
SECOND PLACE IN THE UNITED STATES TO
PRODUCE PETROLEUM FROM THE WELLS.

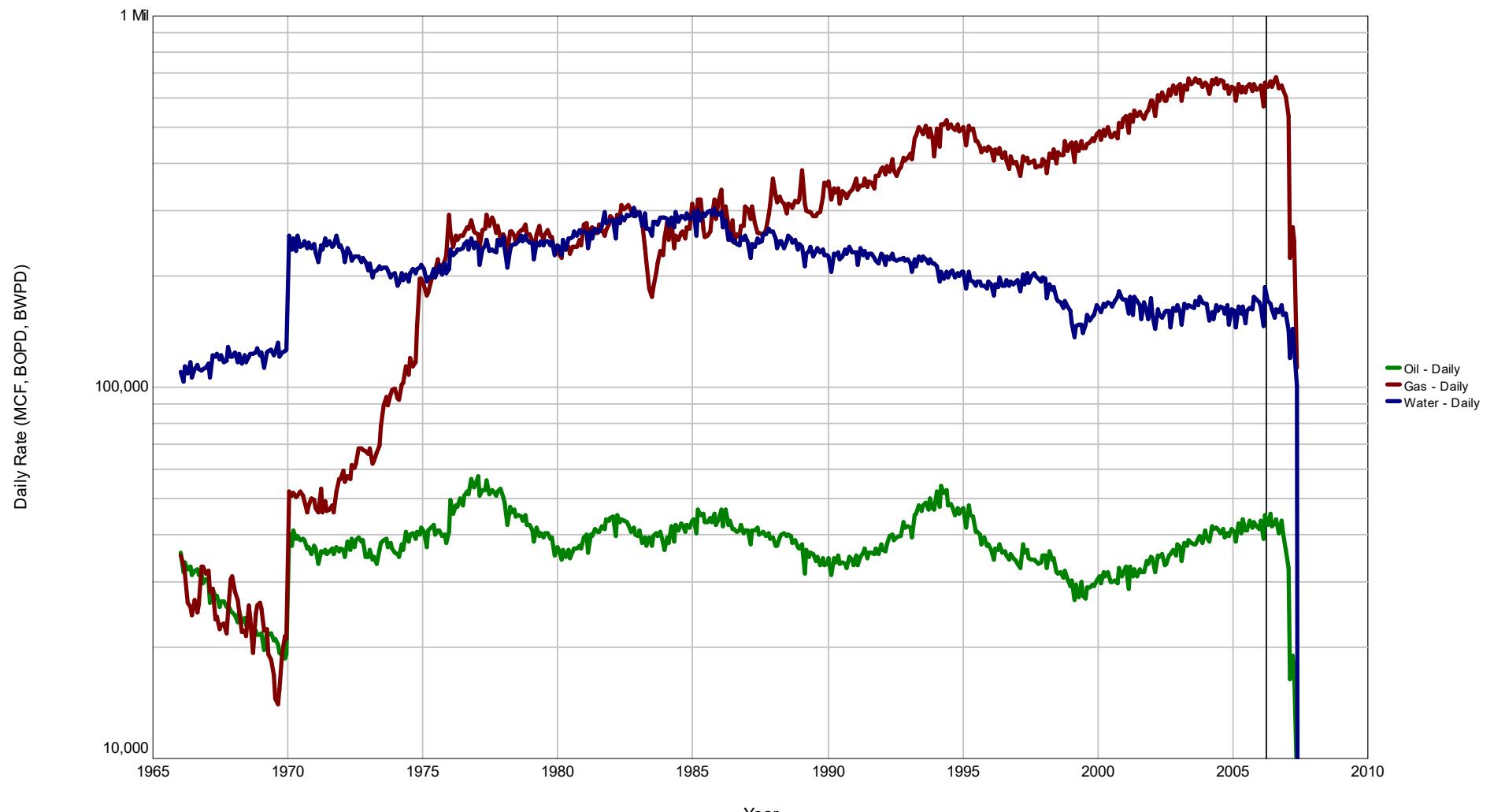
In 1862, just across the stream from this point, A. M. Cassidy drilled an oil well fifty feet deep. By February, 1863, production was one barrel a day. Later, several thousand gallons of petroleum were produced by primitive methods, and kerosene and lubricating oil were shipped by ox-team as far as Denver & Santa Fe.

Cassidy's success led to the finding of Colorado's first real oil field, about seven miles south of here. This field, known as the Florence Pool, was discovered in 1876 by Isaac Canfield. It subsequently was operated for about seventy years by Continental Oil Company and its predecessors. The field still produces a small amount of petroleum.

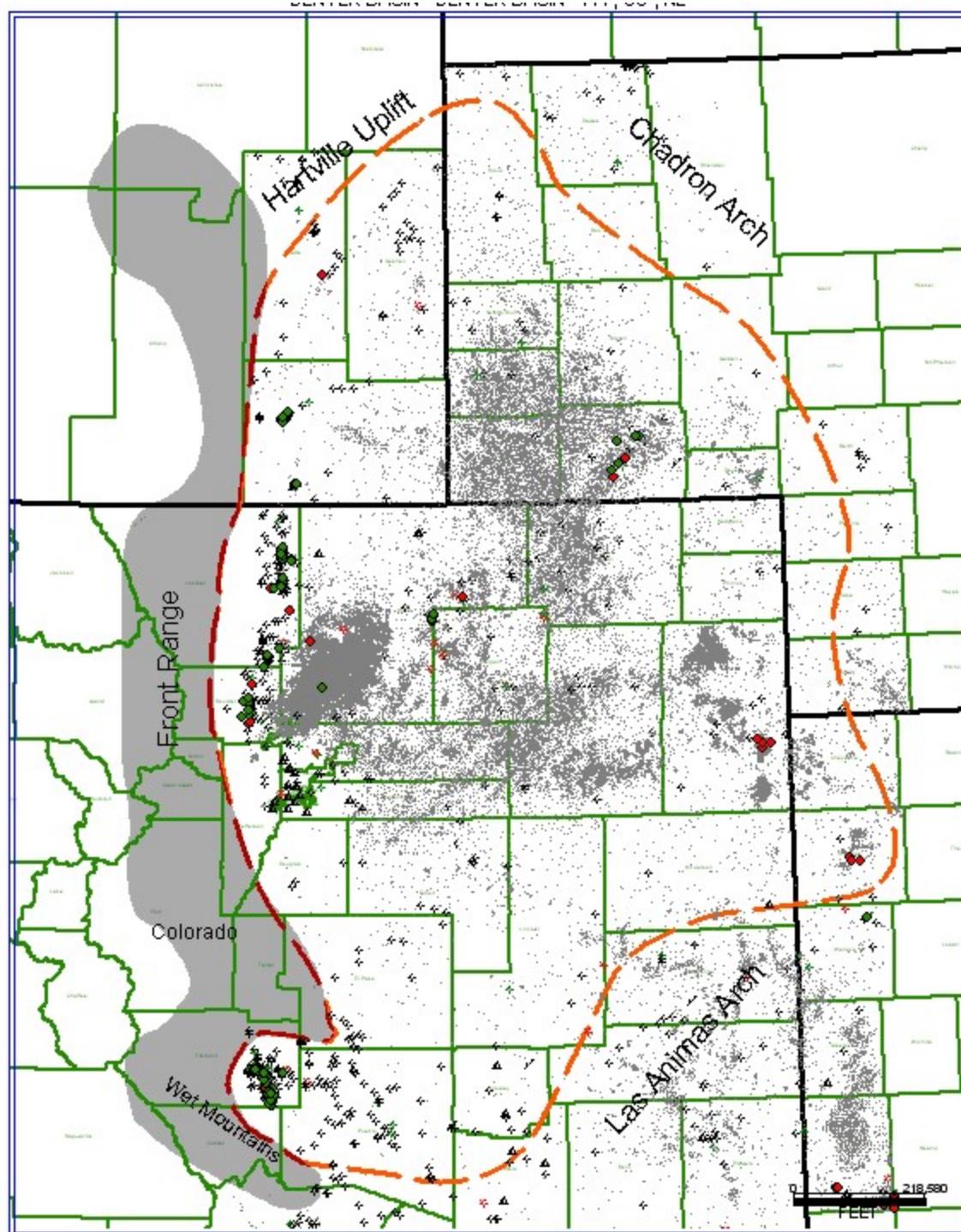


- Pierre Shale
- Sussex Shannon
- Niobrara
- Codell
- D Sand
- J Sand
- Lyons, Wolfcamp
- Morrow

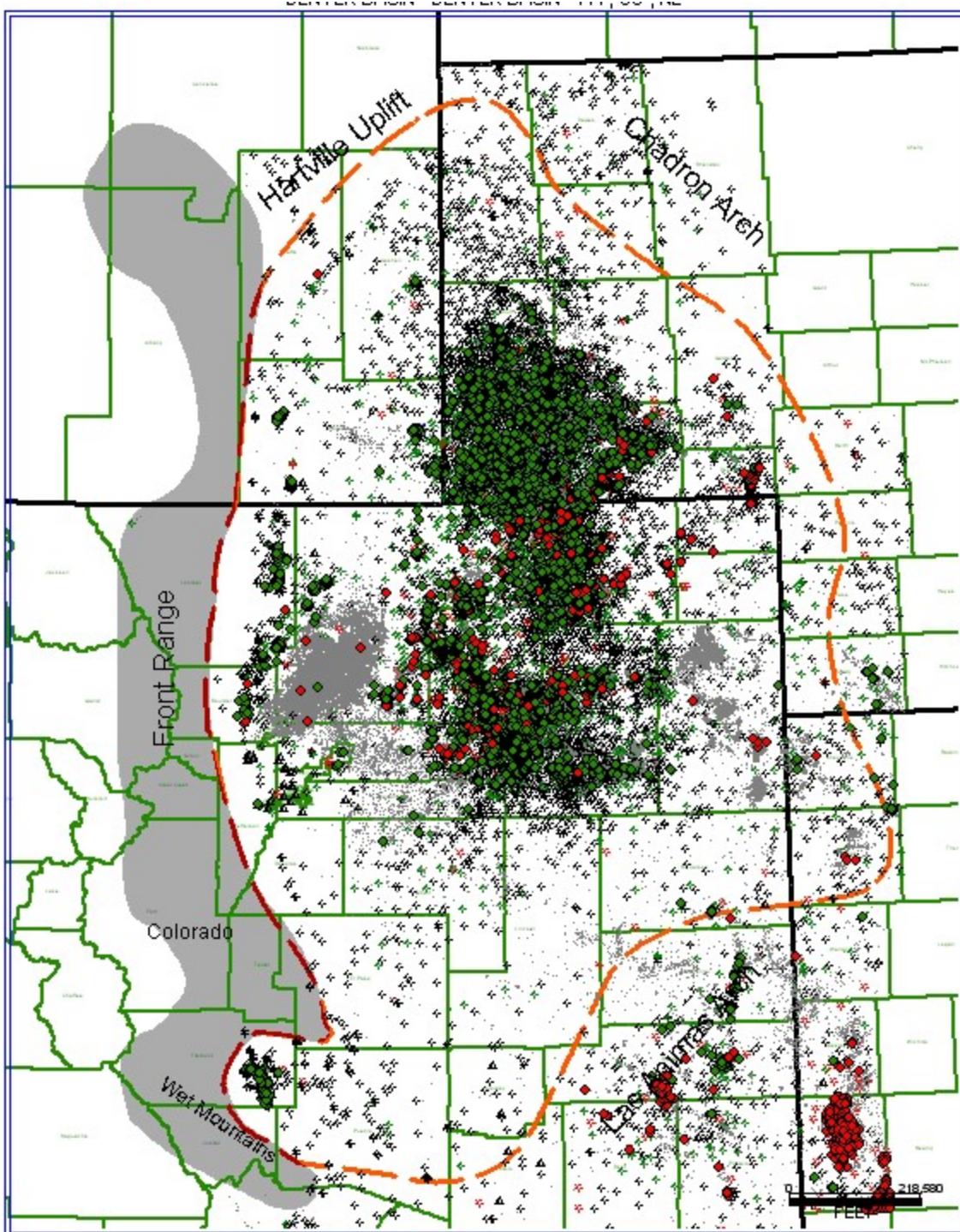
DJ Basin Historical Production



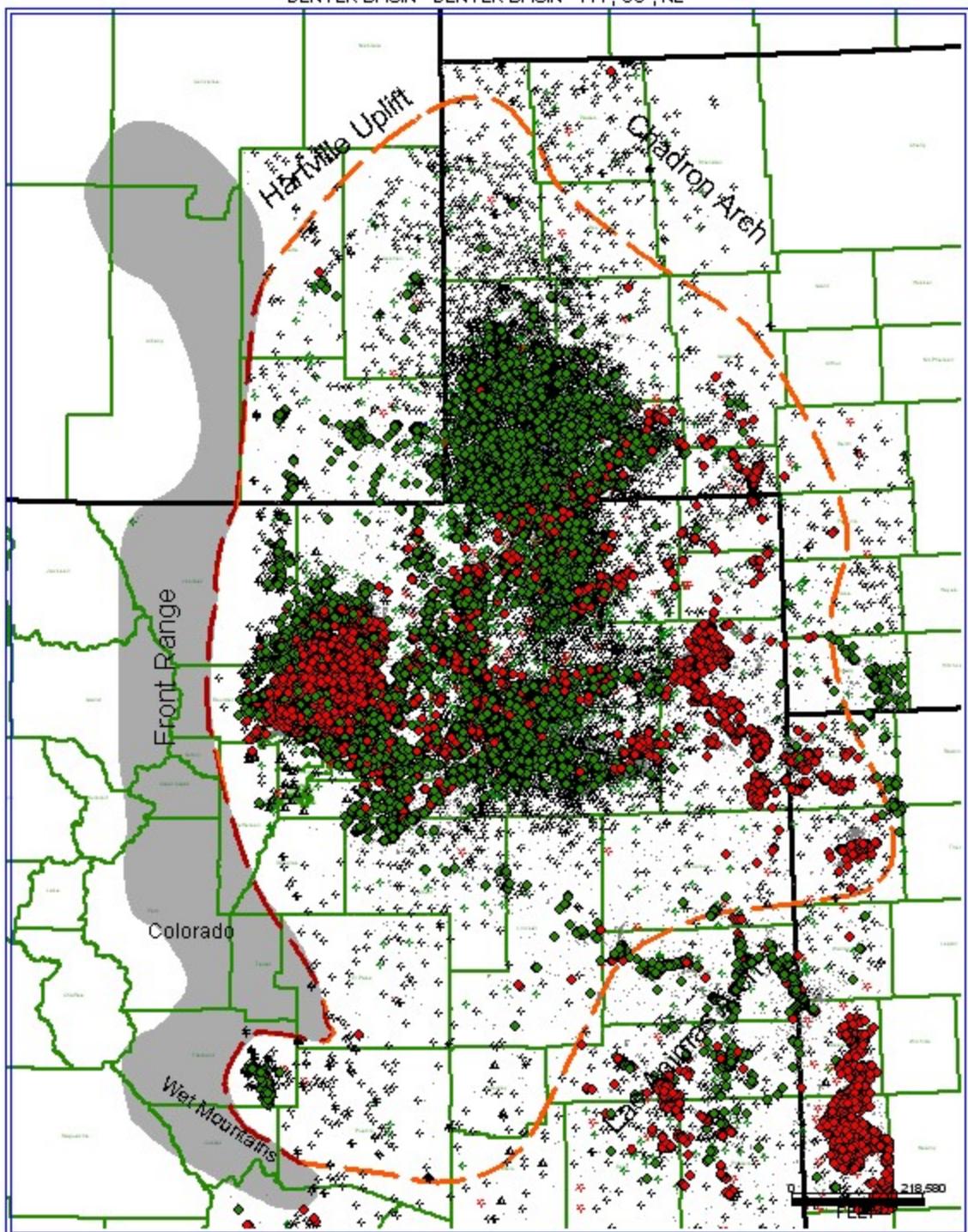
Current Production: > 600 MMCFGD; > 40,000 BOPD



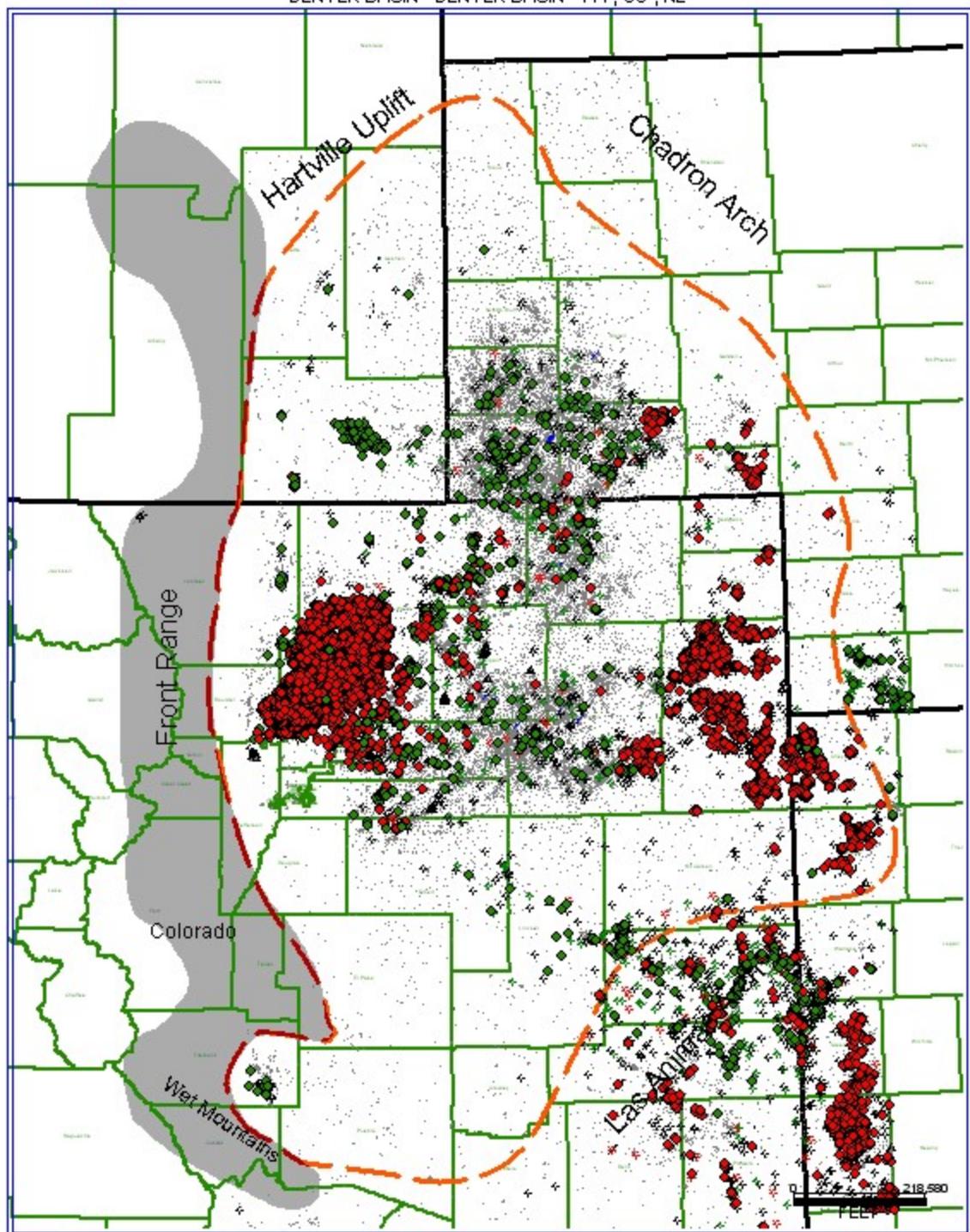
Wells 1850-1950



Wells 1850-1970

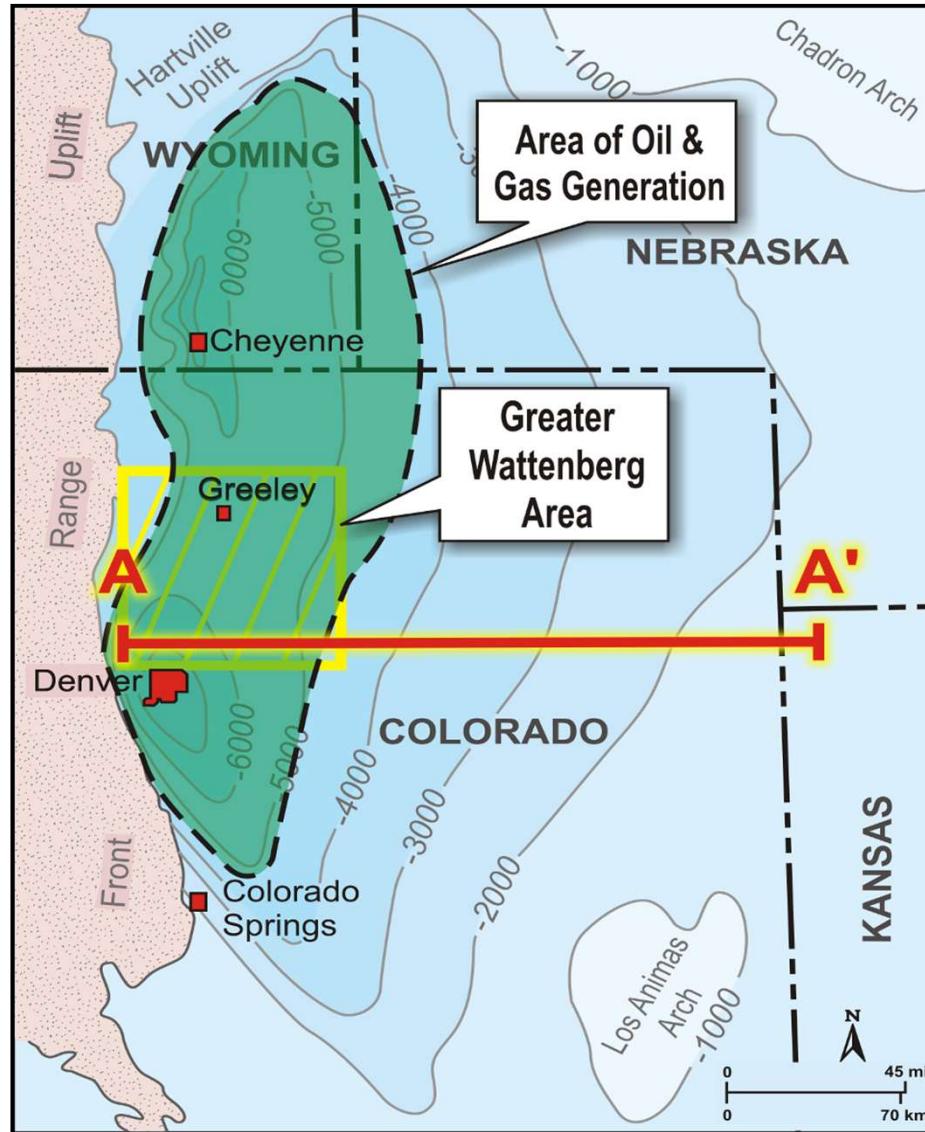


Wells 1850-1990



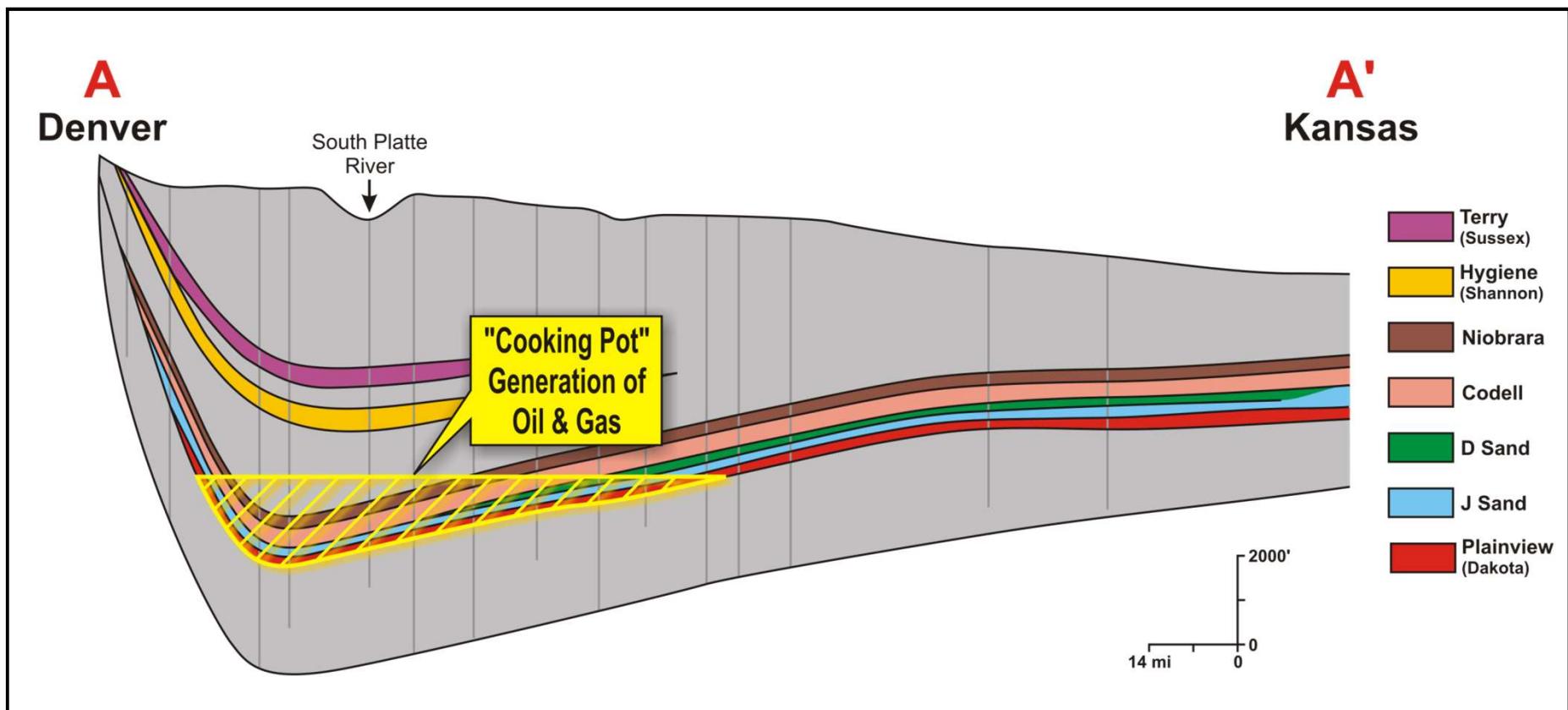
Wells 1990-2007

Deep Basin Petroleum Generation Structure Map (Top PC)

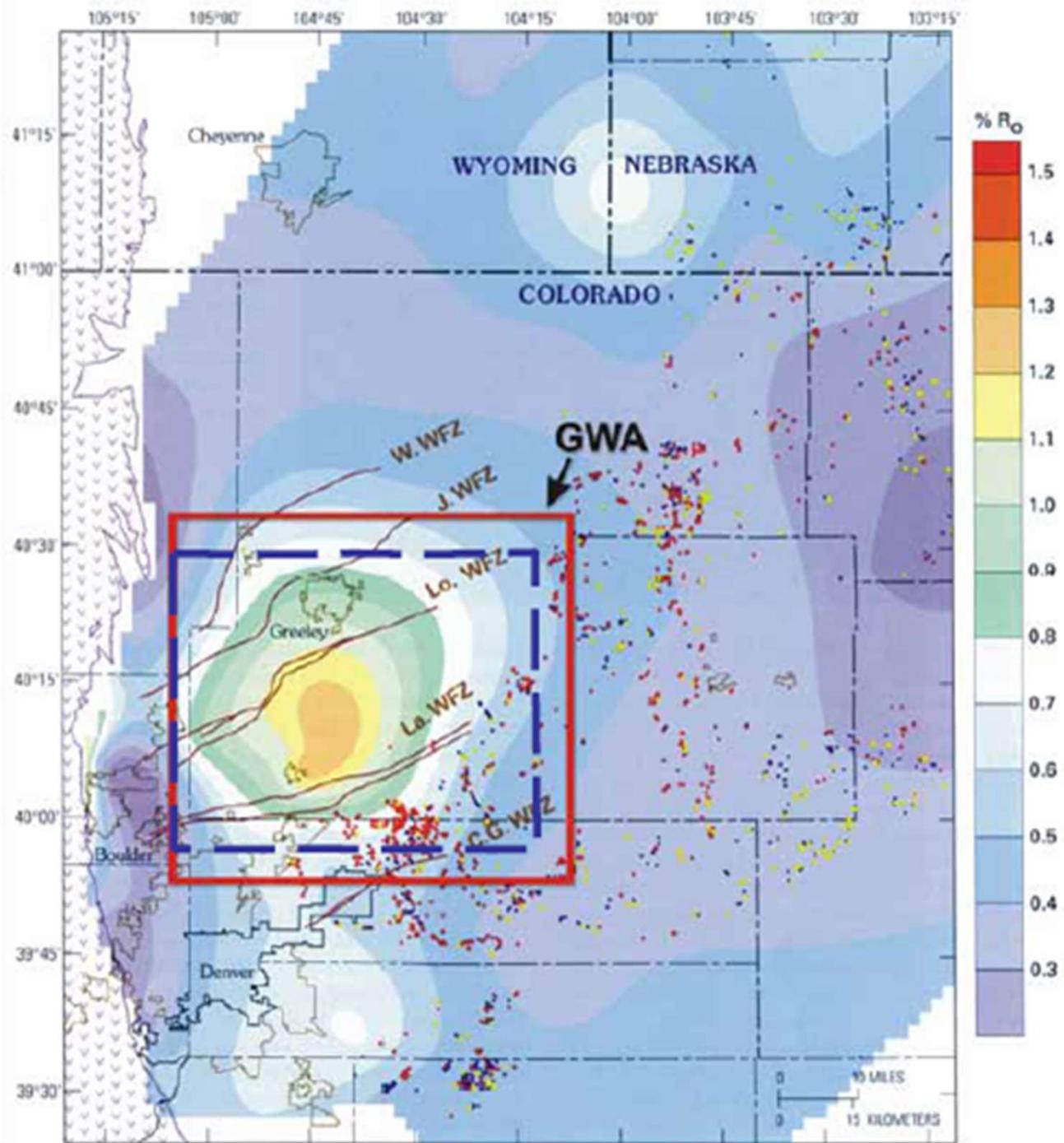


Weimer, 1996

Structural Cross Section of the Denver Basin



Weimer, 1996



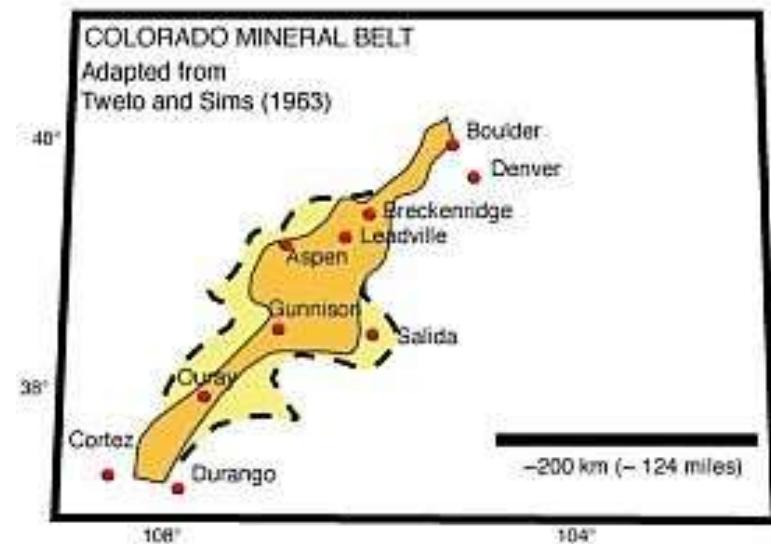
The Wattenberg Geothermal Anomaly

**Vitrinite Reflectance
Values, %Ro**

Higley & Cox, 2005

Wattenberg Thermal Anomaly

- Related to igneous masses in basement (?)
- Located where CMB intersects Denver Basin
- Direct temperature measurements
- Ro values
- GORs



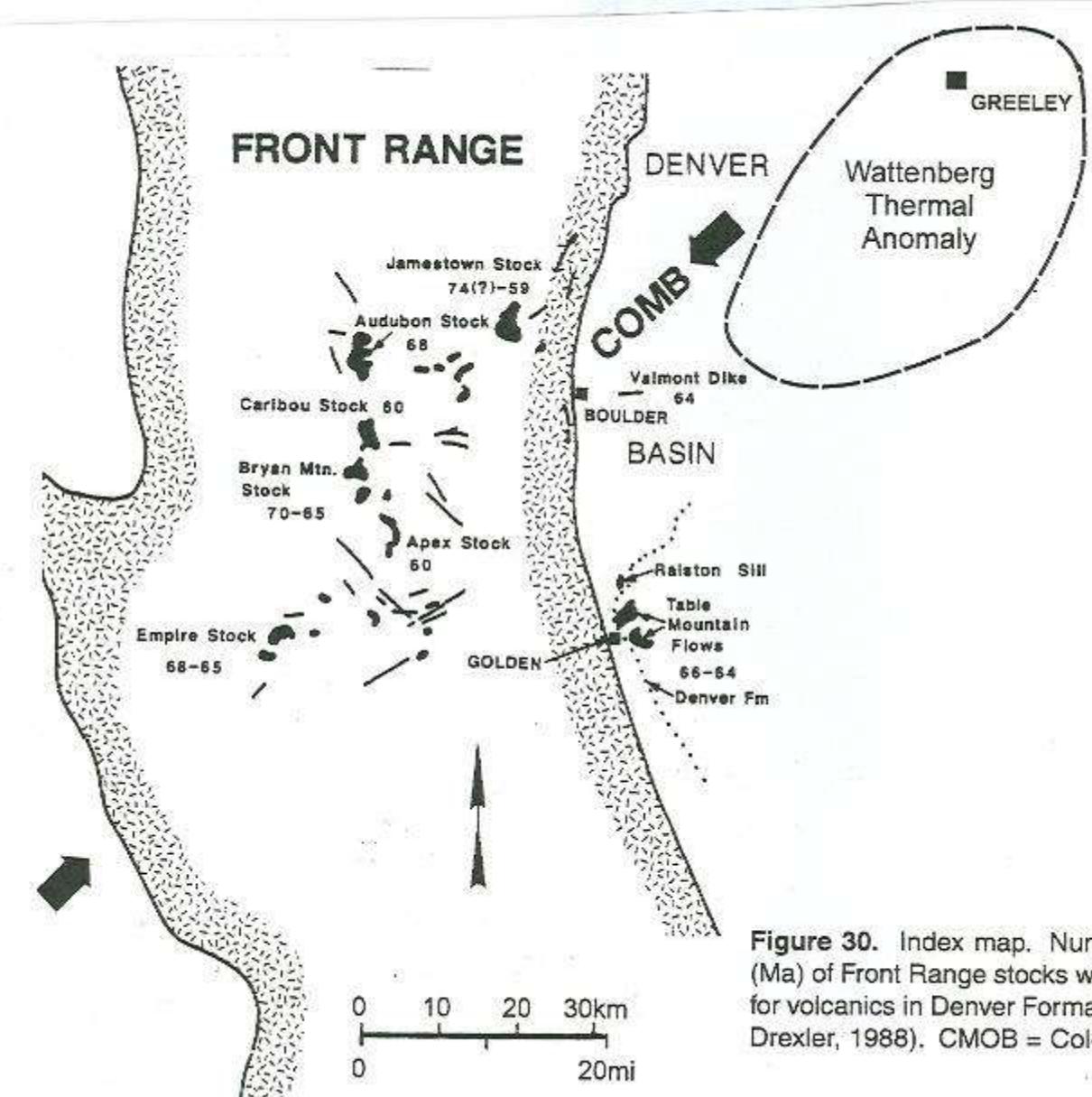
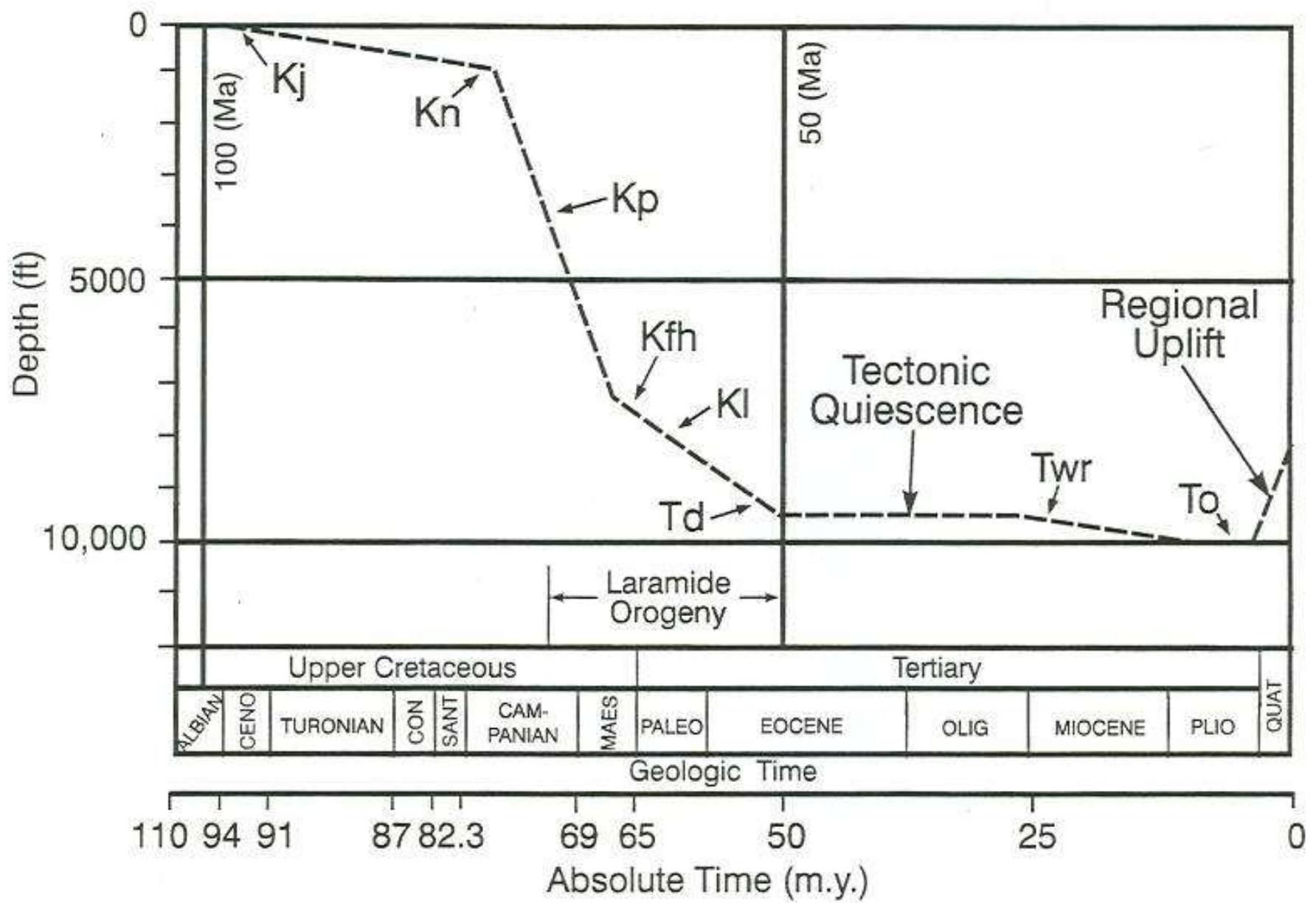


Figure 30. Index map. Numbers represent ages (Ma) of Front Range stocks which could be sources for volcanics in Denver Formation (from Larson and Drexler, 1988). CMOB = Colorado Mineral Belt.

Weimer, 1995

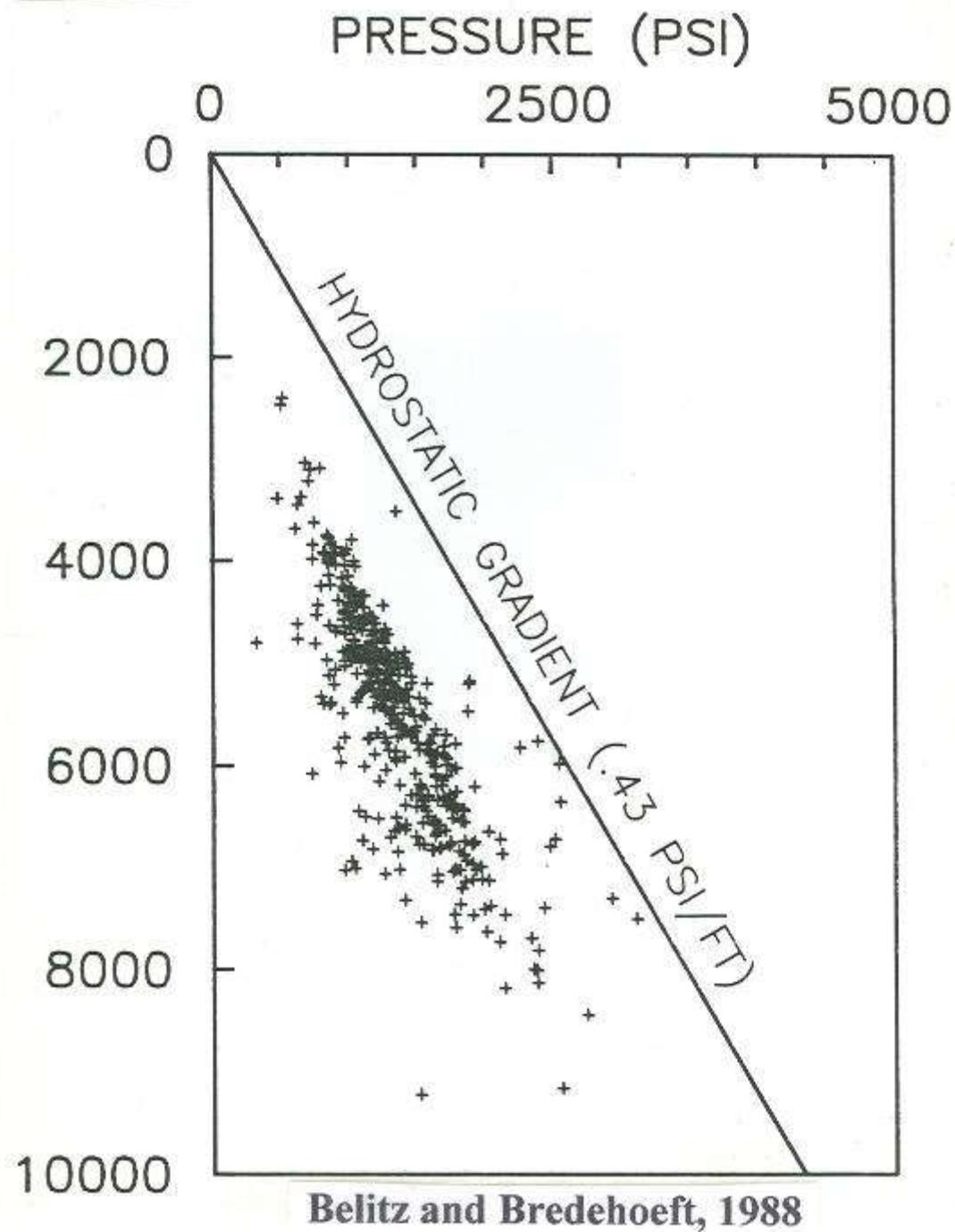
Wattenberg Thermal Anomaly

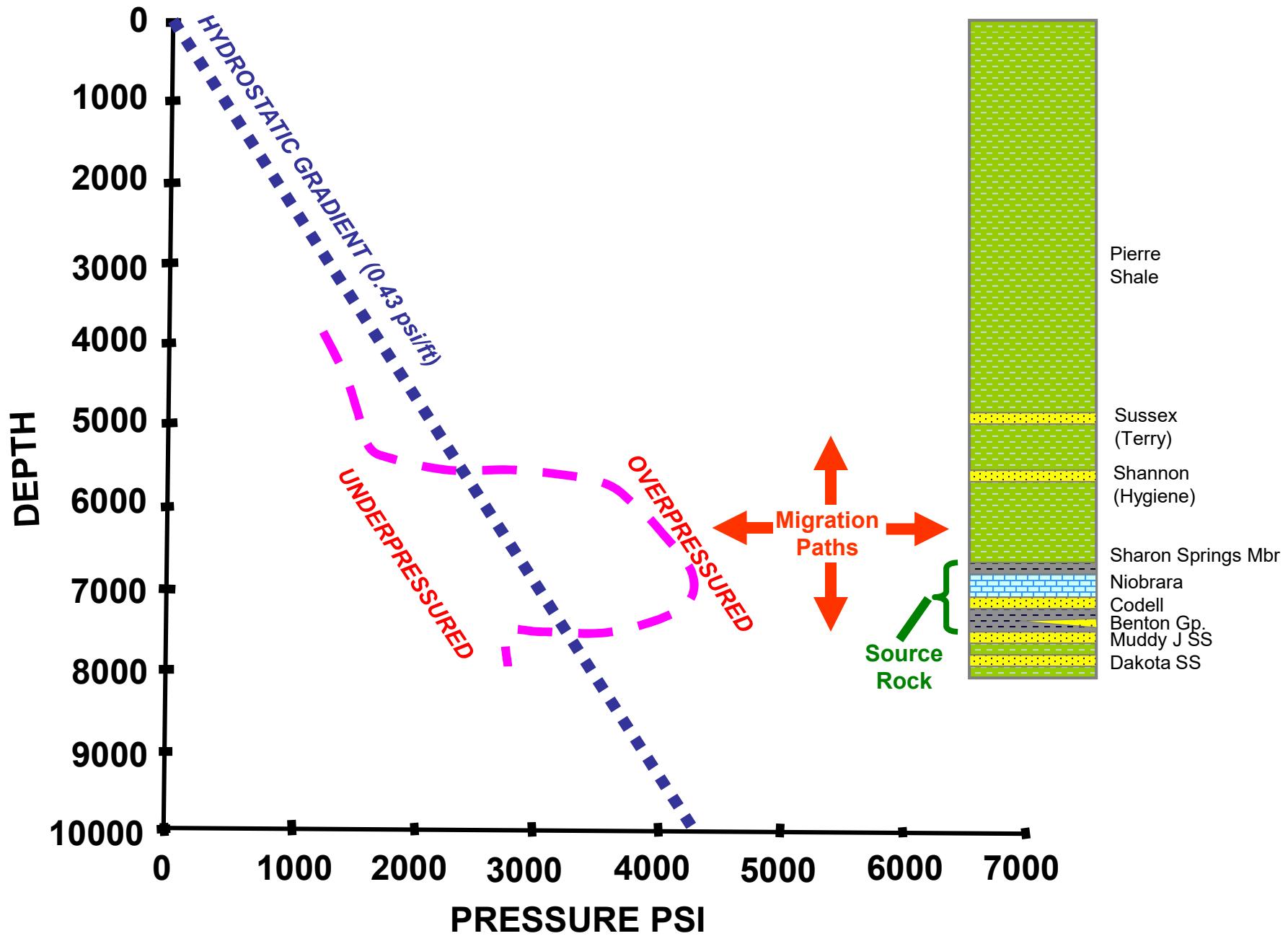
- ◆ Related to igneous masses in basement
- ◆ Located where CMD intersects Denver basin
- ◆ Direct temperature measurements
- ◆ Ro values
- ◆ GORs



Subsidence profile Muddy (J) Sandstone

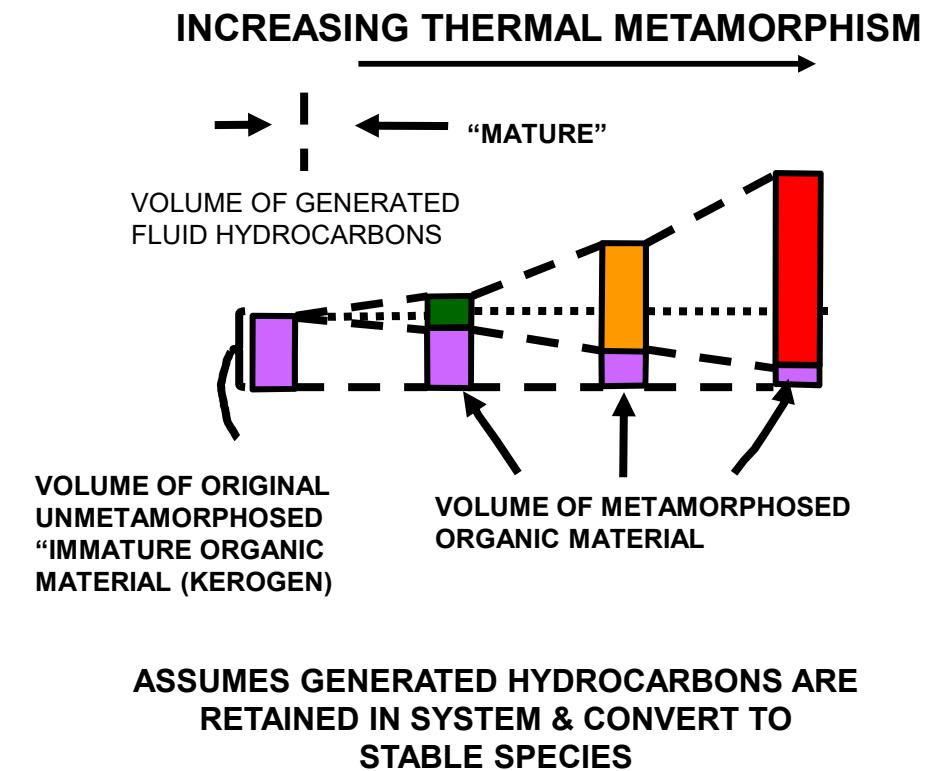
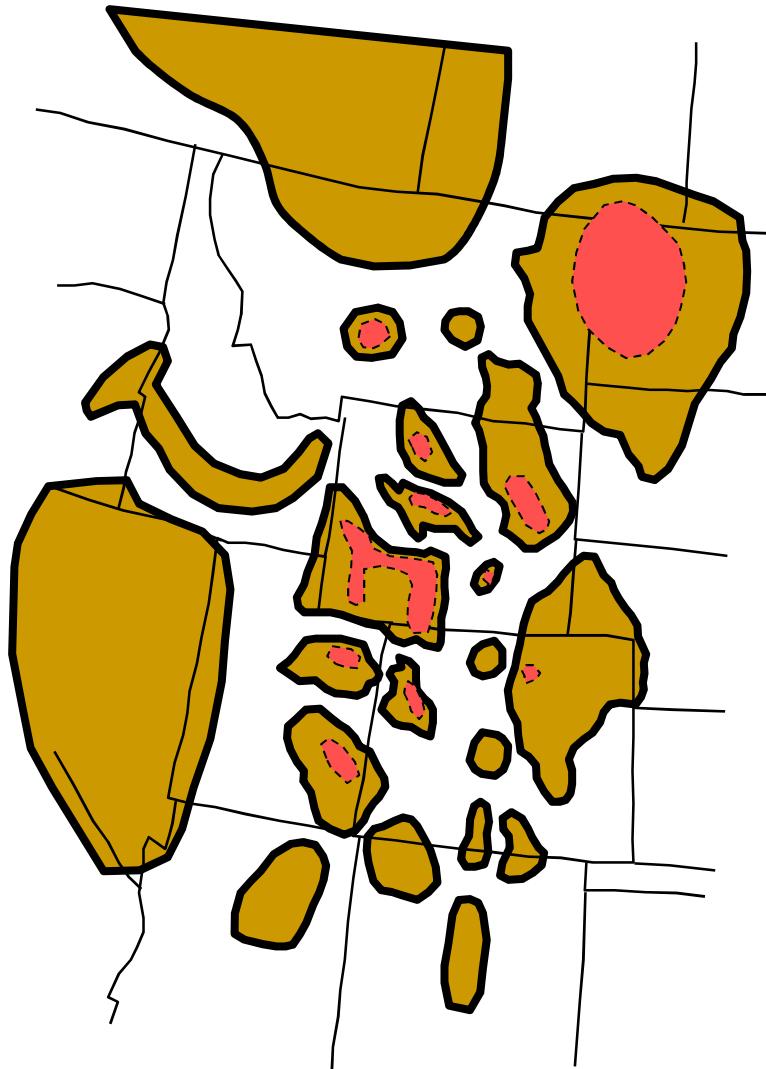
Weimer, 1995



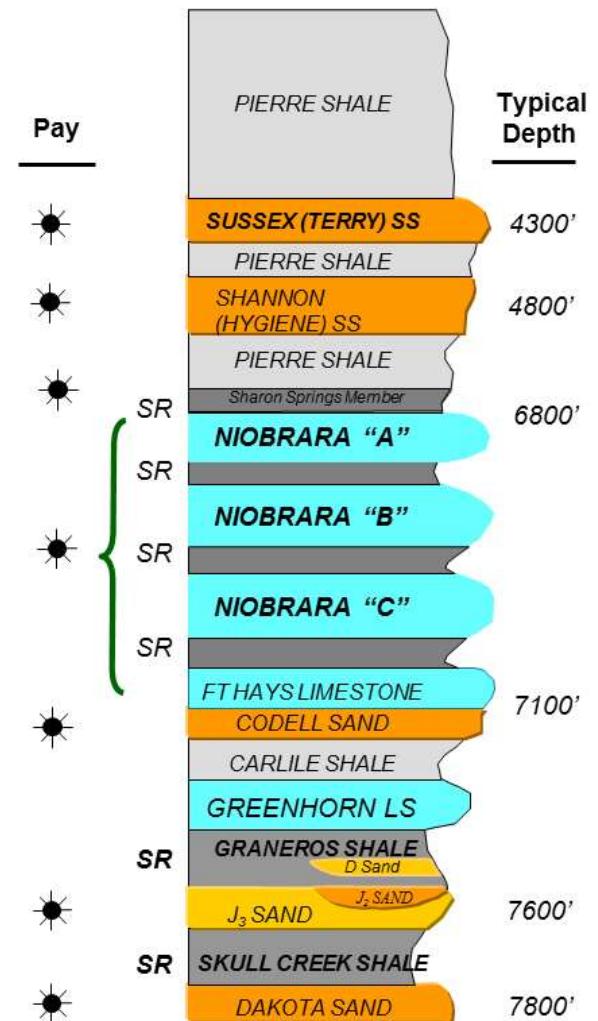
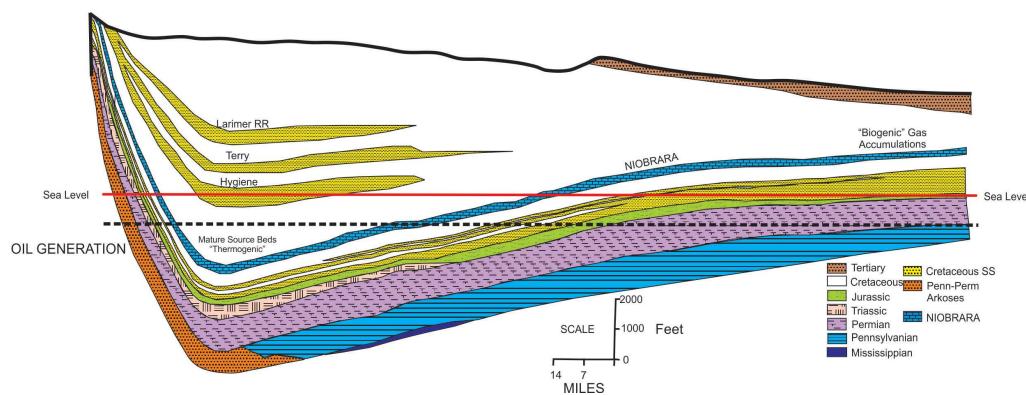
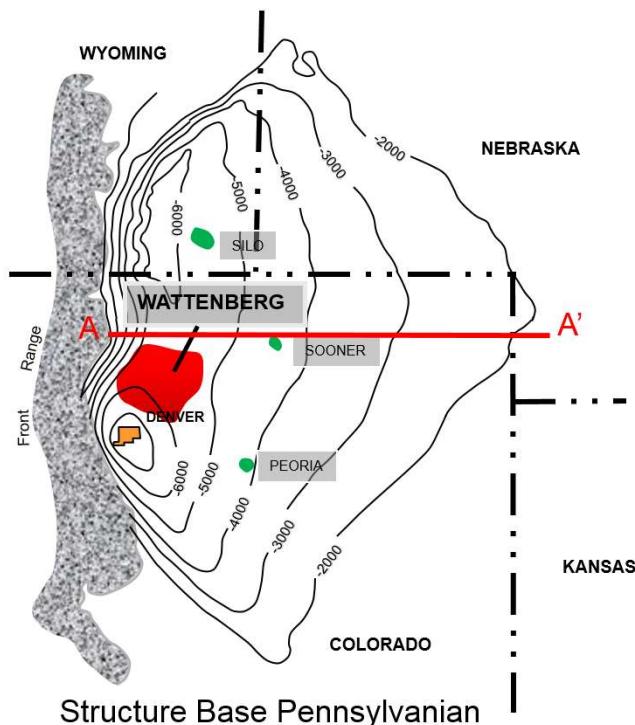


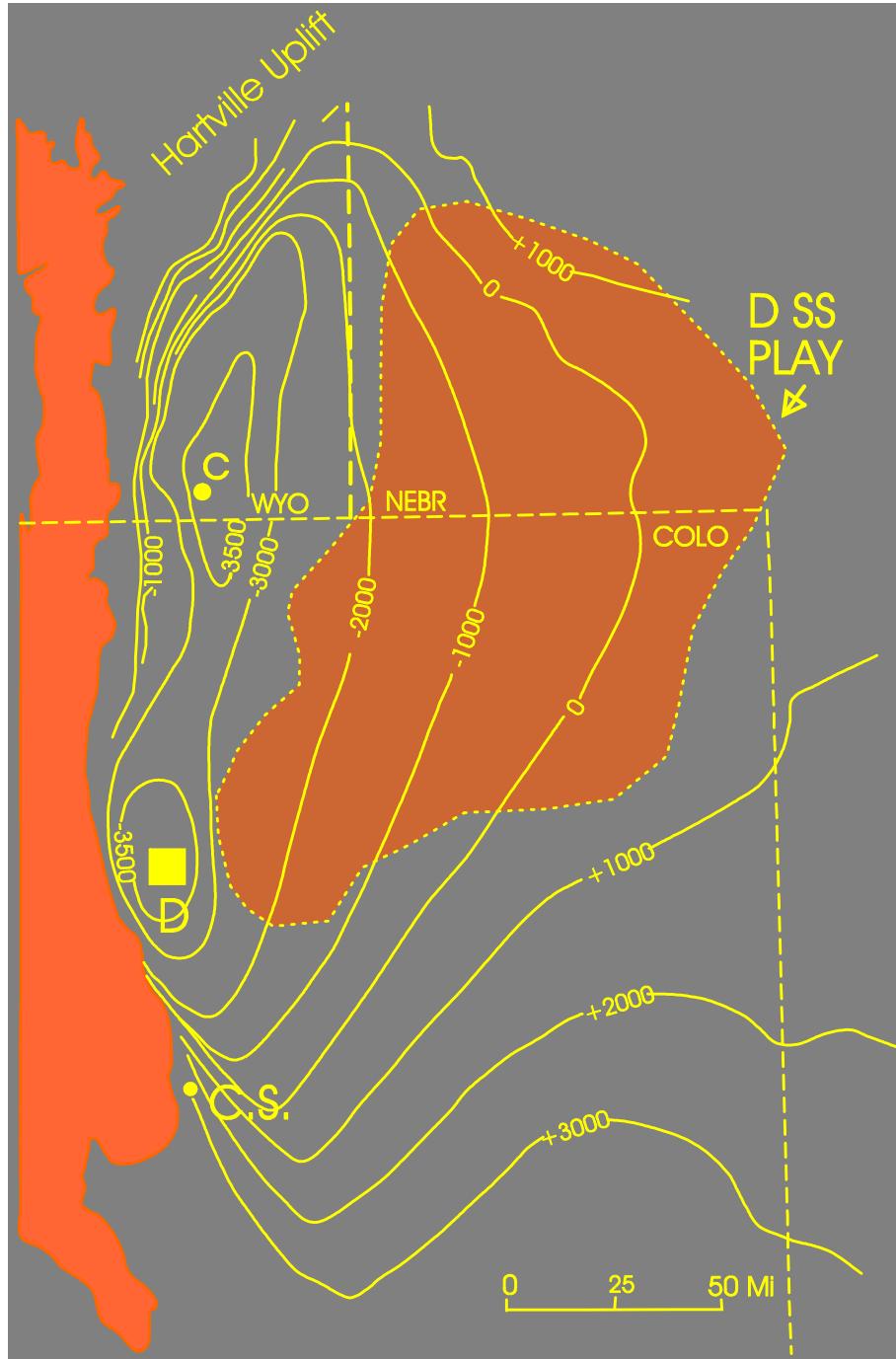
Weimer, 1995

Overpressuring in Rockies Basins



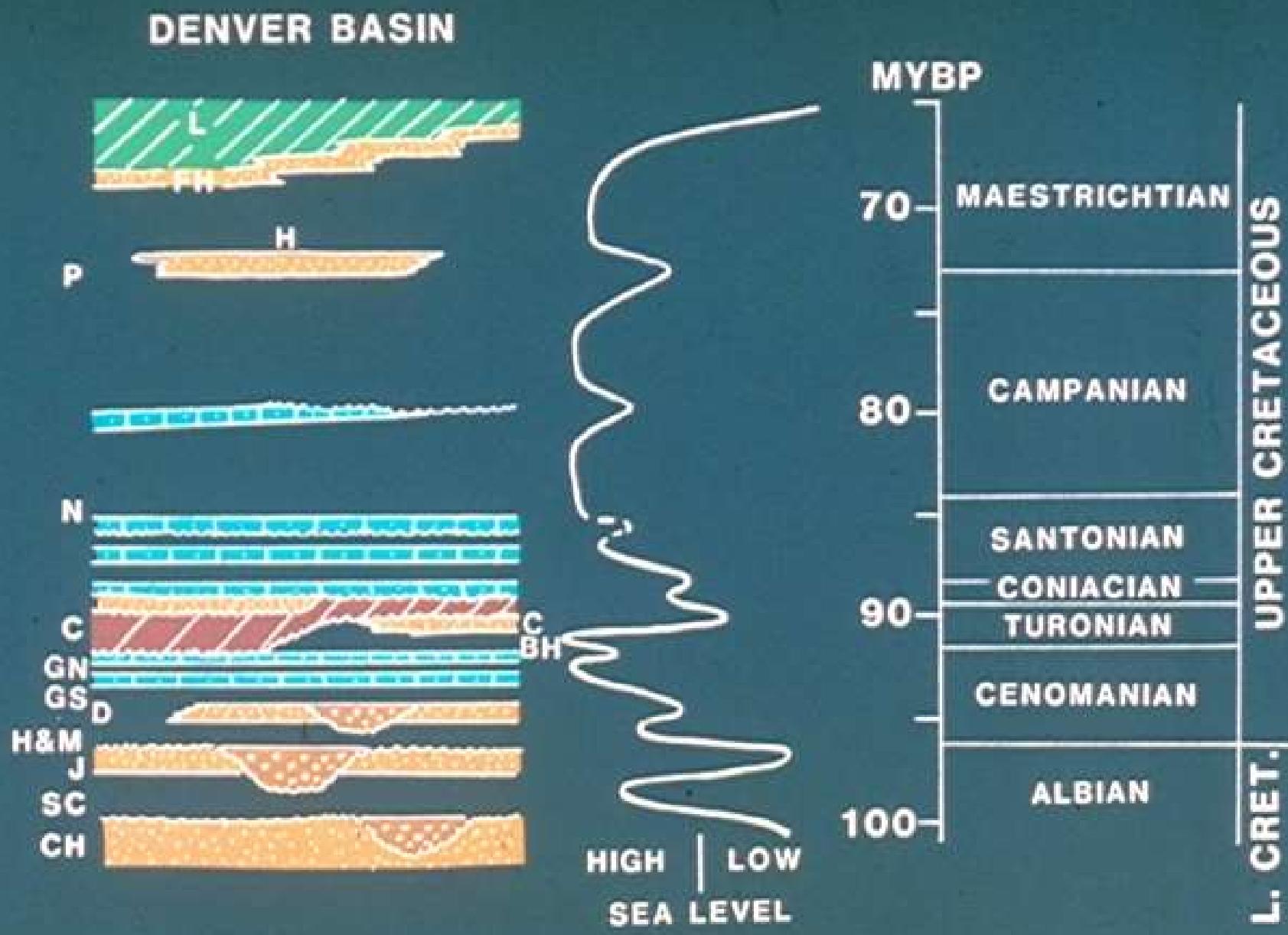
The D Sandstone

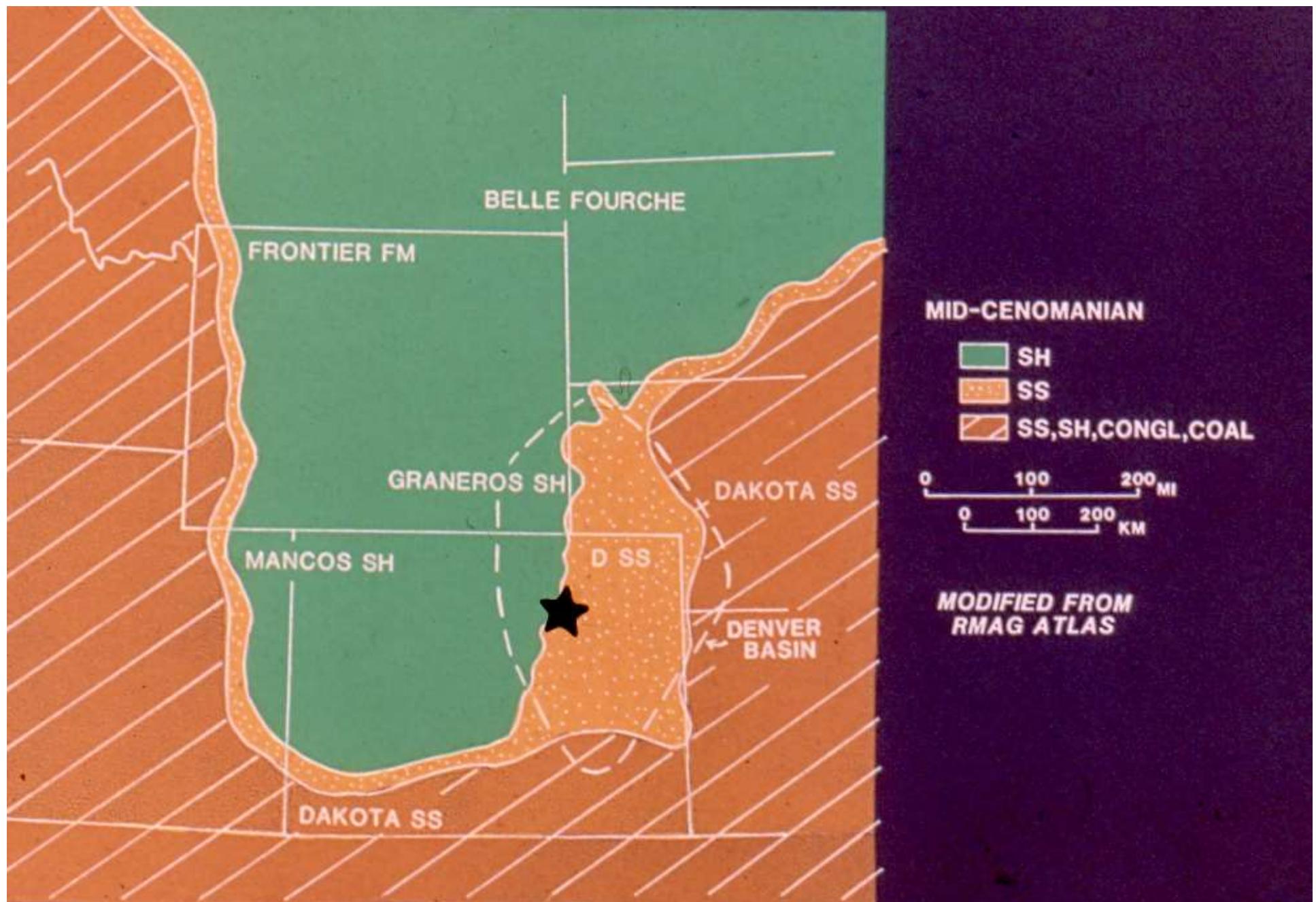


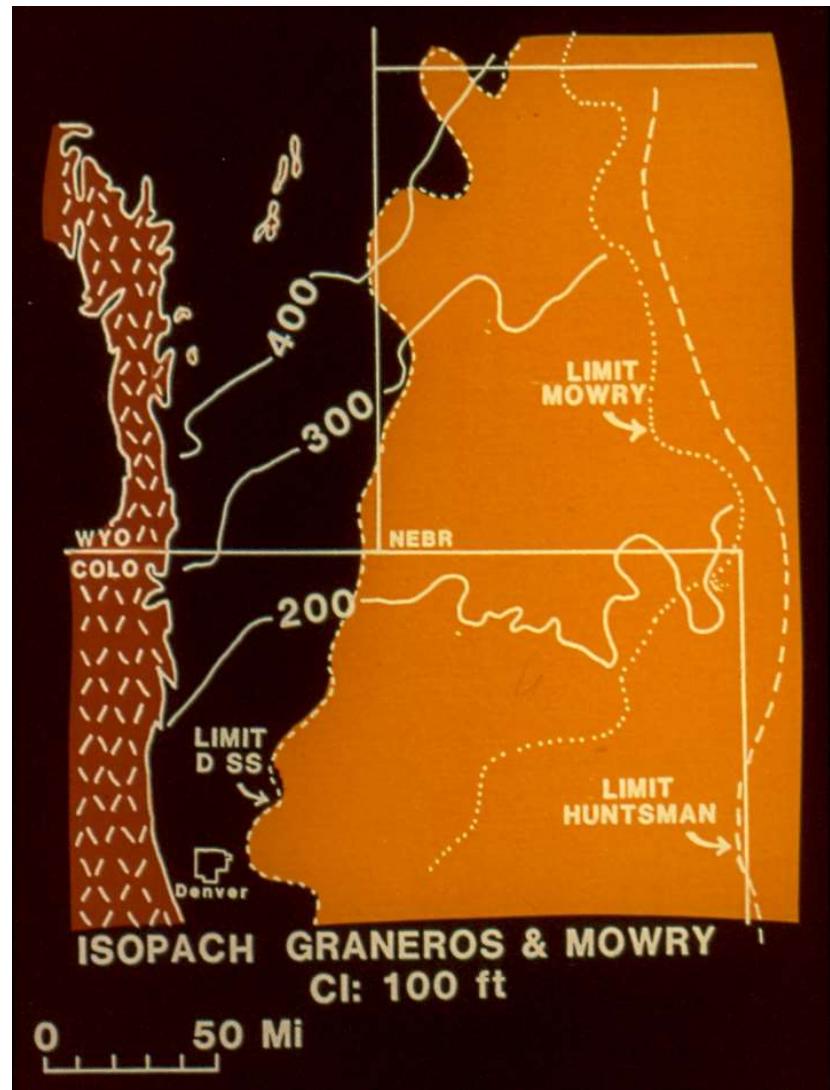
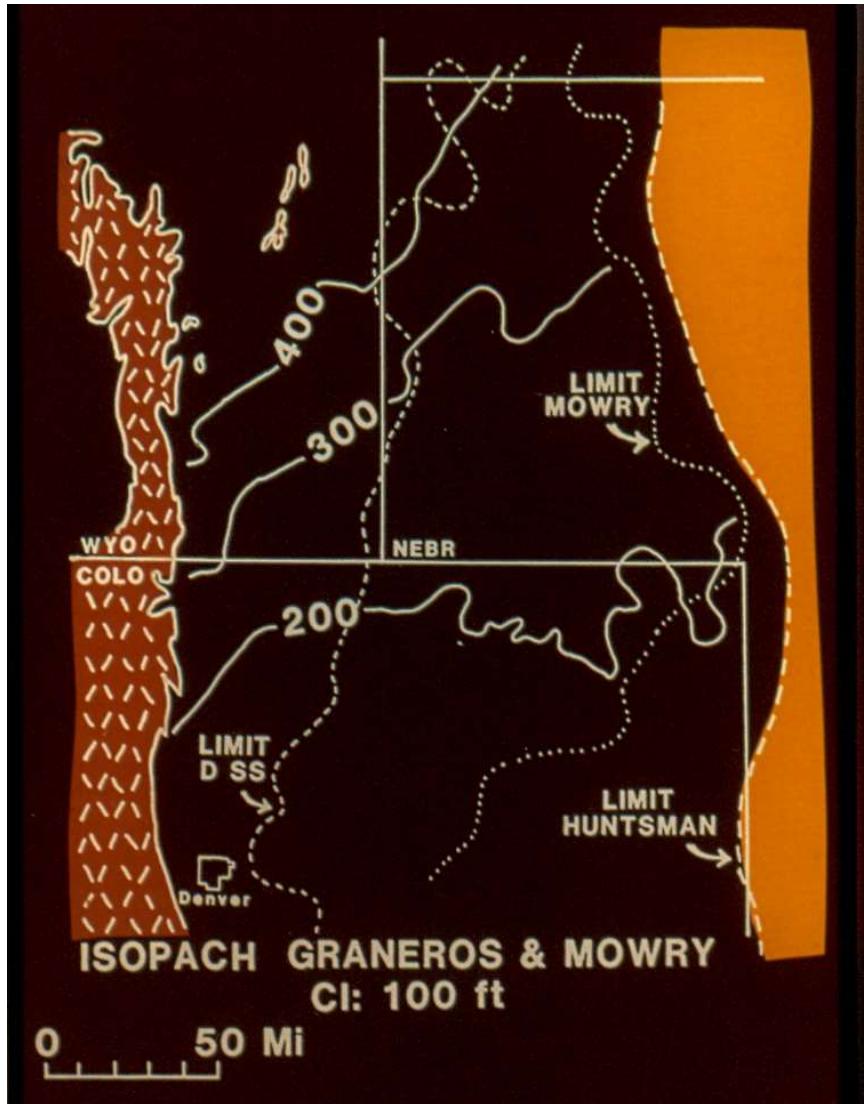


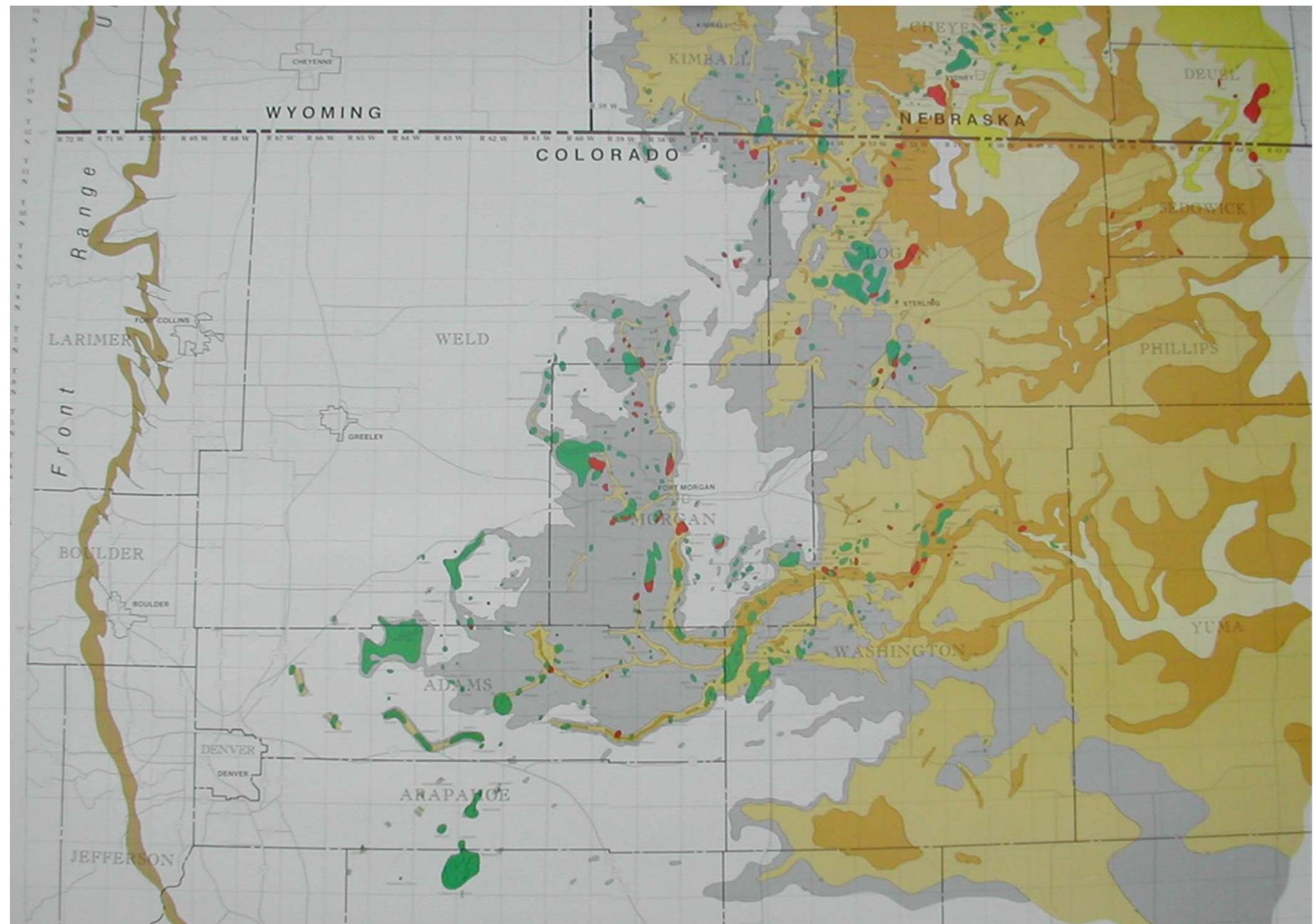
D SS PLAY

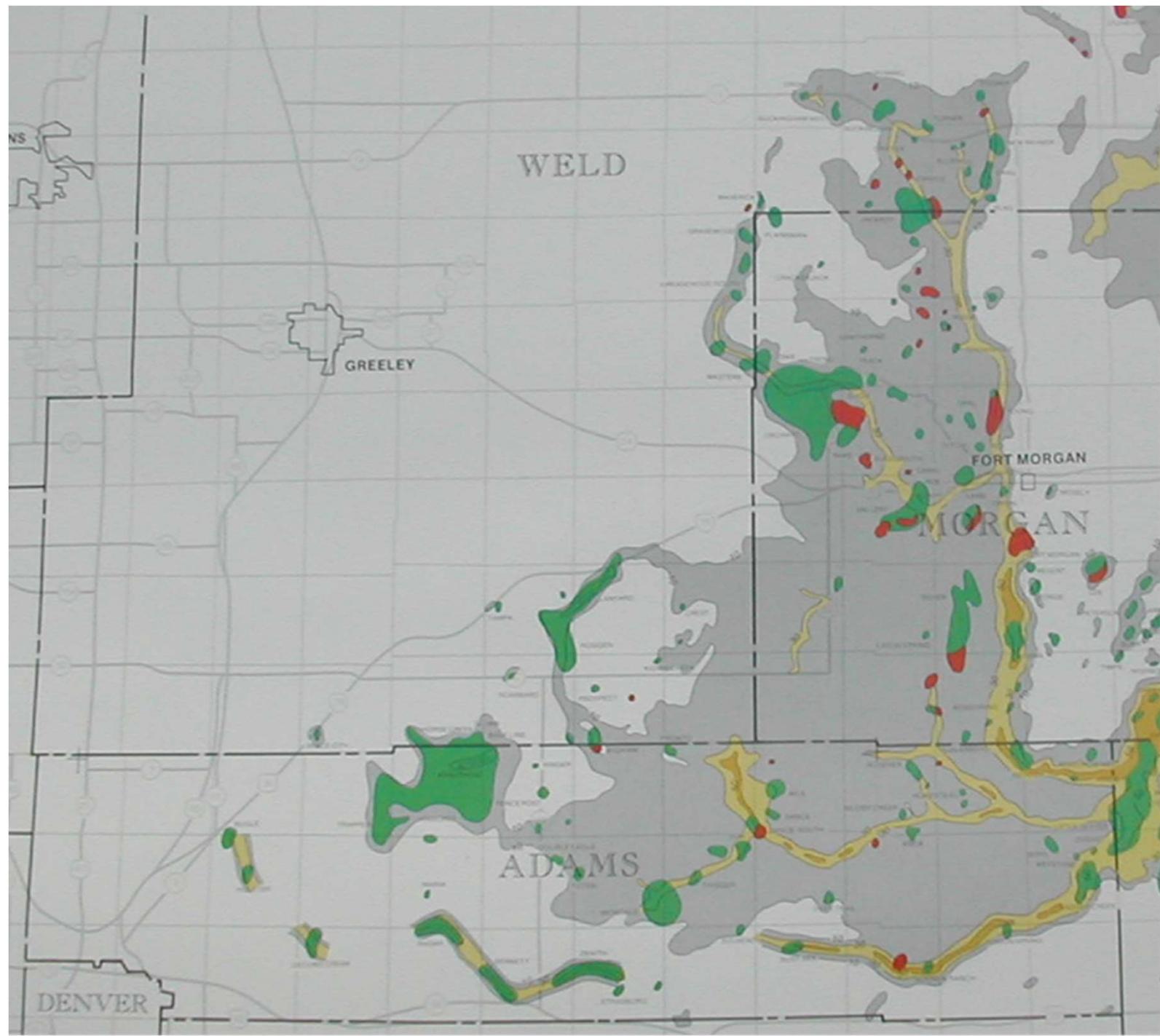
- Good reserves
- Shallow depth
- Low drilling costs
- Multiple pay areas
- Secondary recoveries











Graneros-D(!) Petroleum System

- Reservoirs: D Sandstone
- Source Beds: Graneros
- Seals: Graneros, Huntsman, tight D laterally
- Carrier Beds: D, fracture systems
- Migration: downward into D

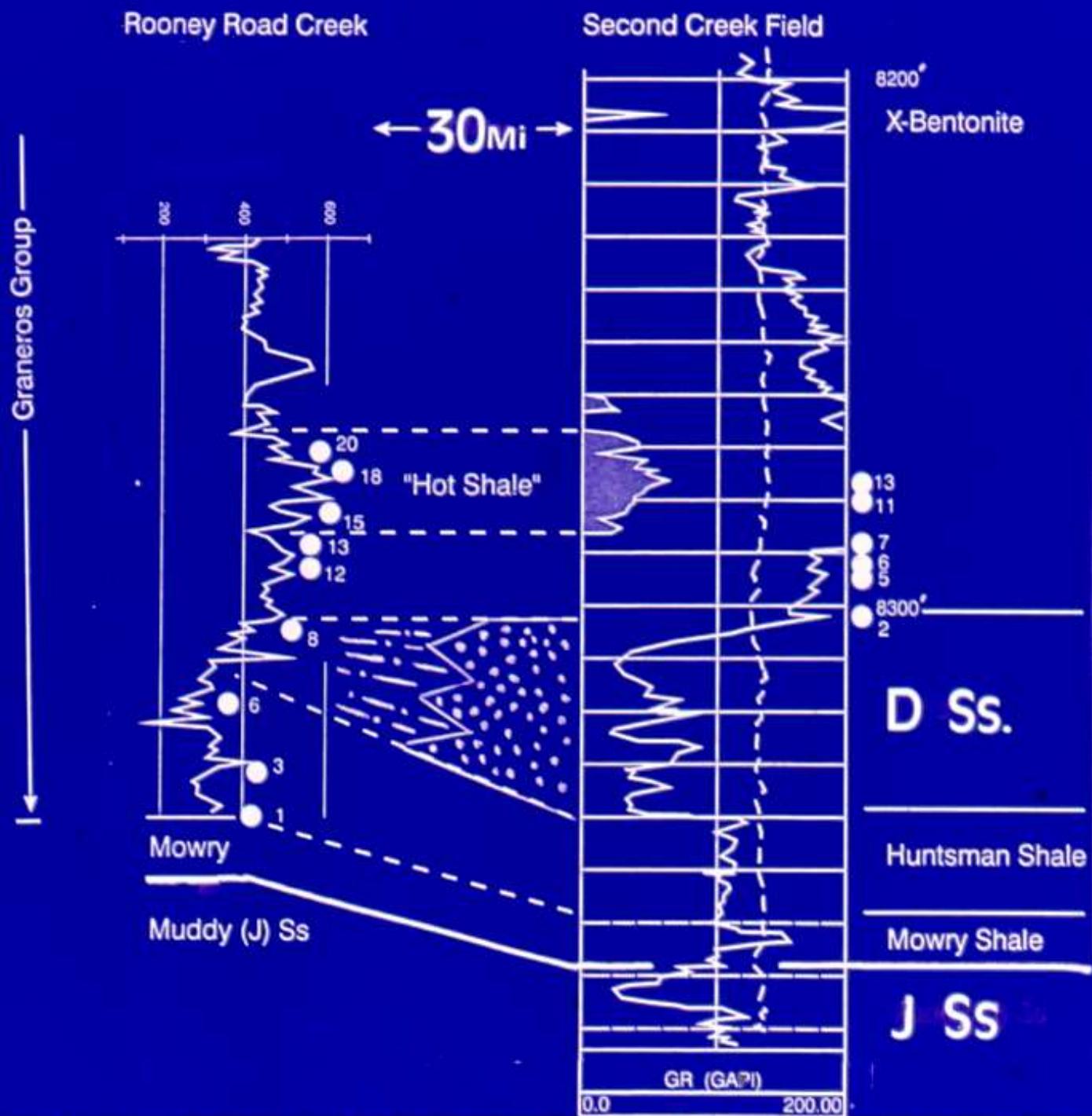


Table 1. Rooney Road, Graneros Shale Section; organic geochemistry analyses (from Pietraszek-Mattner, 1995).

Sample	Location (ft.)	Tmax Deg C	TOC wt%	S1 mg/g	S2 mg/g	S3 mg/g	HI	OI	Reactive Carbon	Transformation Ratio	Facies
AMC 20	70	426	4.61	0.3	24.13	0.5	523	11	53	0.01	
AMC 18	68	428	5.26	0.41	28.92	0.14	550	3	55.8	0.01	C
AMC 15	61	419	4.62	0.2	11.75	1.13	254	24	25.9	0.02	
AMC 13	53	429	3.36	0.12	8.46	1.82	252	54	25.5	0.01	
AMC 12	50	428	2.81	0.08	6.29	1.02	22	36	22.7	0.01	B
AMC 8	39	423	2.84	0.11	4.82	0.61	170	21	17.4	0.02	
AMC 6	24	429	1.53	0.05	0.35	1.1	23	72	2.6	0.13	
AMC 3	9	424	0.95	0.05	0.25	0.92	26	97	3.2	0.17	A
AMC 1	0	428	2.13	0.08	1.44	1.07	68	50	7.1	0.05	

From Pietraszek-Mattner, 1995.

TOC = Total Organic (wt%); S1 = Free Hydrocarbons (mg/g); S2 = Pyrolyzable Hydrocarbons (mg/g);

S3 = CO₂ released during pyrolysis (mg/g); HI = Hydrogen index = [(S2%/TOC) x 100]; OI = Oxygen Index = [(S3%/TOC) x 100];

Reactive Carbon = [10 x (S1+S2)%TOC]; Transformation Ratio = S1/(S1+S2)

Table 2. Bass Box Elder Farm 6-32 Graneros core (SW SE Sec. 6, T. 3 S., R. 65 W.; organic geochemistry analyses (from Pietraszek-Mattner, 1995).

Sample	Core Depth	Log Depth	Tmax Deg. C	TOC wt%	S1 mg/g	S2 mg/g	S3 mg/g	HI	OI	Reactive Carbon	Transformation Ratio	Facies
BEF 13	8285	8277	445	4.42	2.7	10.46	0.15	237	3	29.8	0.21	C
BEF 11	8288	8280	441	3.77	2.44	8.99	0.15	238	4	30.3	0.21	
BEF 7	8296	8288	447	2.93	1.74	5.61	0.19	191	6	25.1	0.24	
BEF 6	8299.5	8291.5	447	3.13	1.94	6.68	0.15	213	5	27.5	0.23	B
BEF 5	8302	8294	448	2.05	1.06	3.08	0.06	150	3	20.2	0.26	
BEF 2	8309.5	8301.5	451	1.28	0.3	1.82	0.09	64	7	8.8	0.14	A

From Pietraszek-Mattner, 1995.

TOC = Total Organic (wt%); S1 = Free Hydrocarbons (mg/g); S2 = Pyrolyzable Hydrocarbons (mg/g);

S3 = CO₂ released during pyrolysis (mg/g); HI = Hydrogen index = [(S2%/TOC) x 100]; OI = Oxygen Index = [(S3%/TOC) x 100];

Reactive Carbon = [10 x (S1+S2)%TOC]; Transformation Ratio = S1/(S1+S2)

Weimer, 1995

Tectonics & Sedimentation

- Fault movement controlled location of valleys
 - 90° turns in valley
 - anomalous thickness of D-Huntsman
 - 2-D & 3-D seismic
- Structural Inversion

Seals and Traps

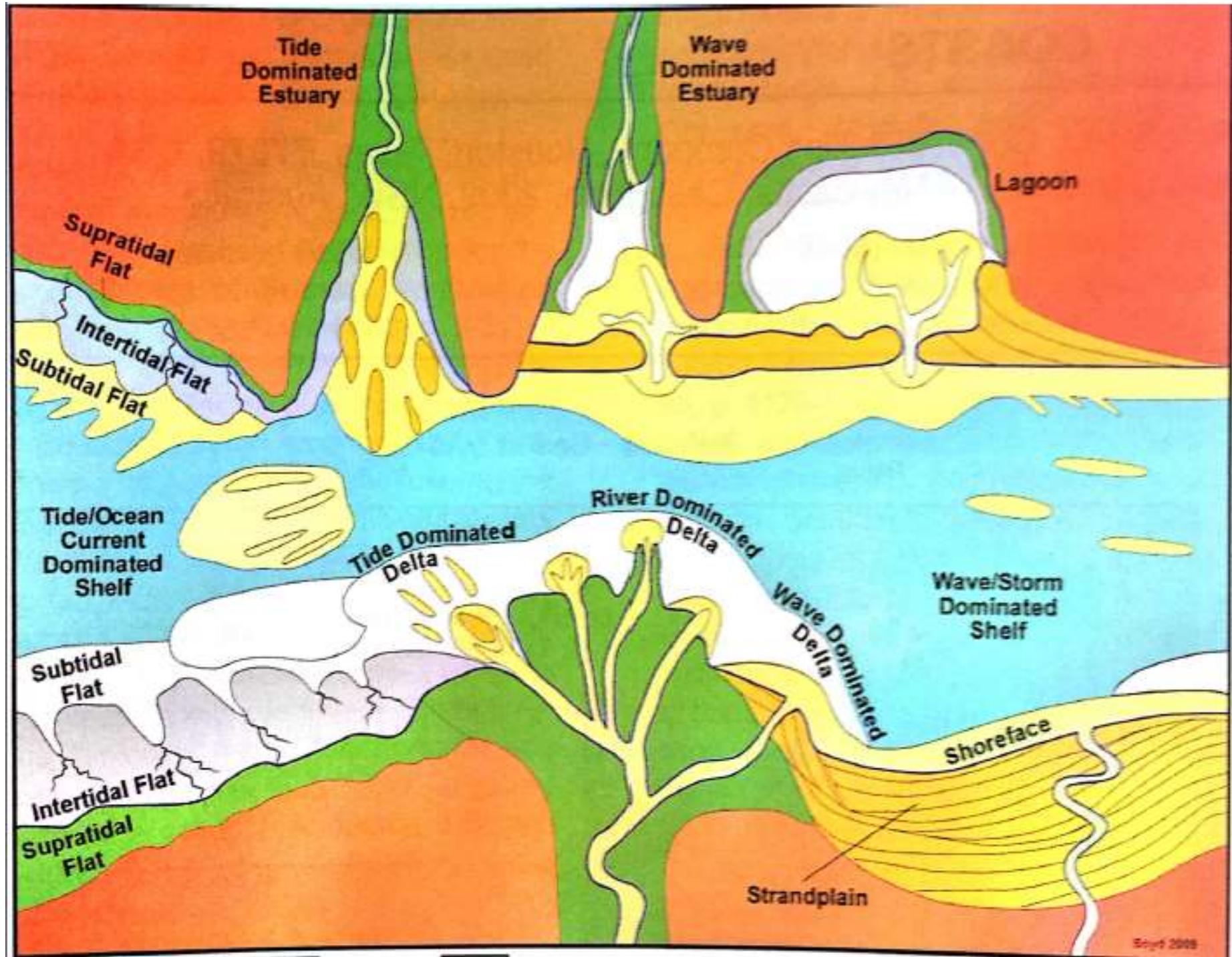
- ◆ Facies changes (capillarity)
- ◆ Faults
- ◆ Clay plugs within channel sandstones
- ◆ Diagenesis
- ◆ Unconformities
- ◆ Anticlines, noses, etc.
- ◆ Combination

D Sweet Spots

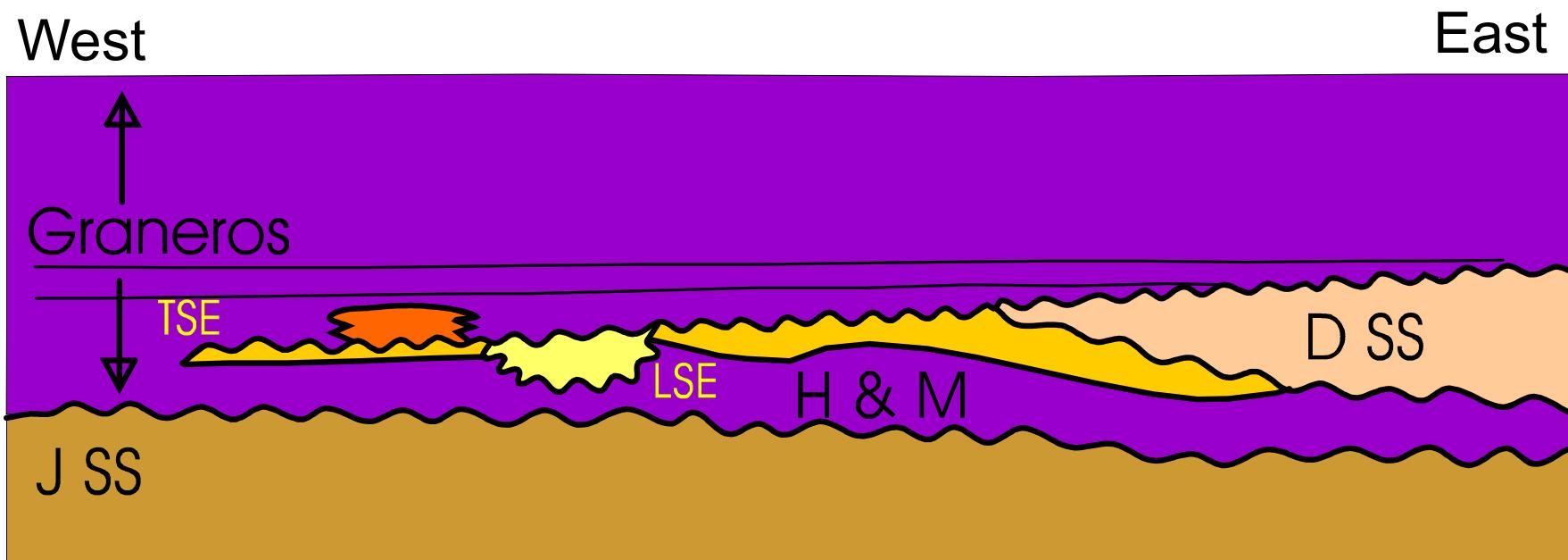
- ◆ EOD
 - Valley fills, distributary channels, transgressive marine ss
- ◆ Fracturing
 - Related to folding, faulting, regional stress field

D Production

- ◆ Valley fills
- ◆ Low-stand deltaic
- ◆ Transgressive Marine
- ◆ Regional regressive



D Sandstone Sequence Stratigraphy

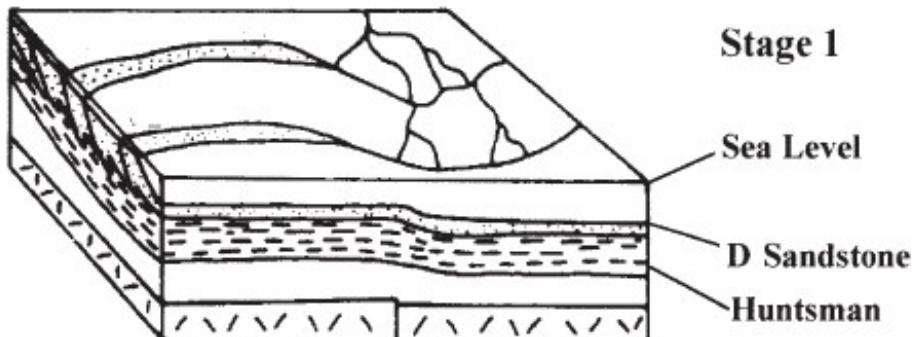


D Valley Fills

- Regional incisement into Huntsman
- 1/4 to 1/2 mi wide
- 30 to 50 ft thick
- Fluvial to estuarine
- Examples: Zenith, Sooner, Lanyard fields

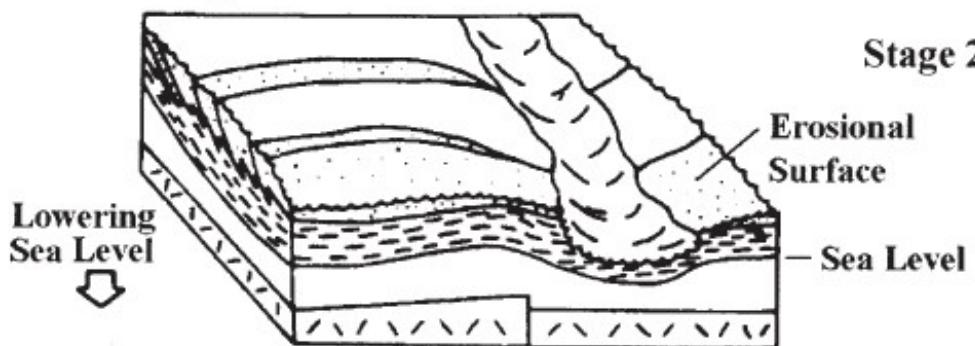
(B)

Regional Regressive Deposition



Drainage Affected by Paleo Faults

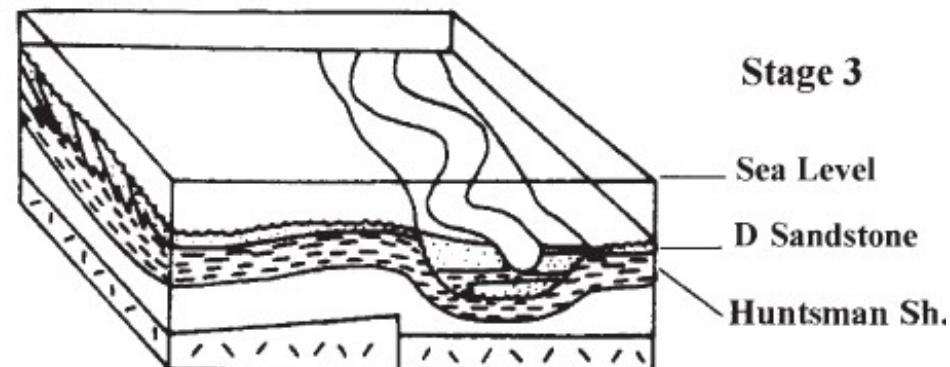
Valley Incision



Stage 2

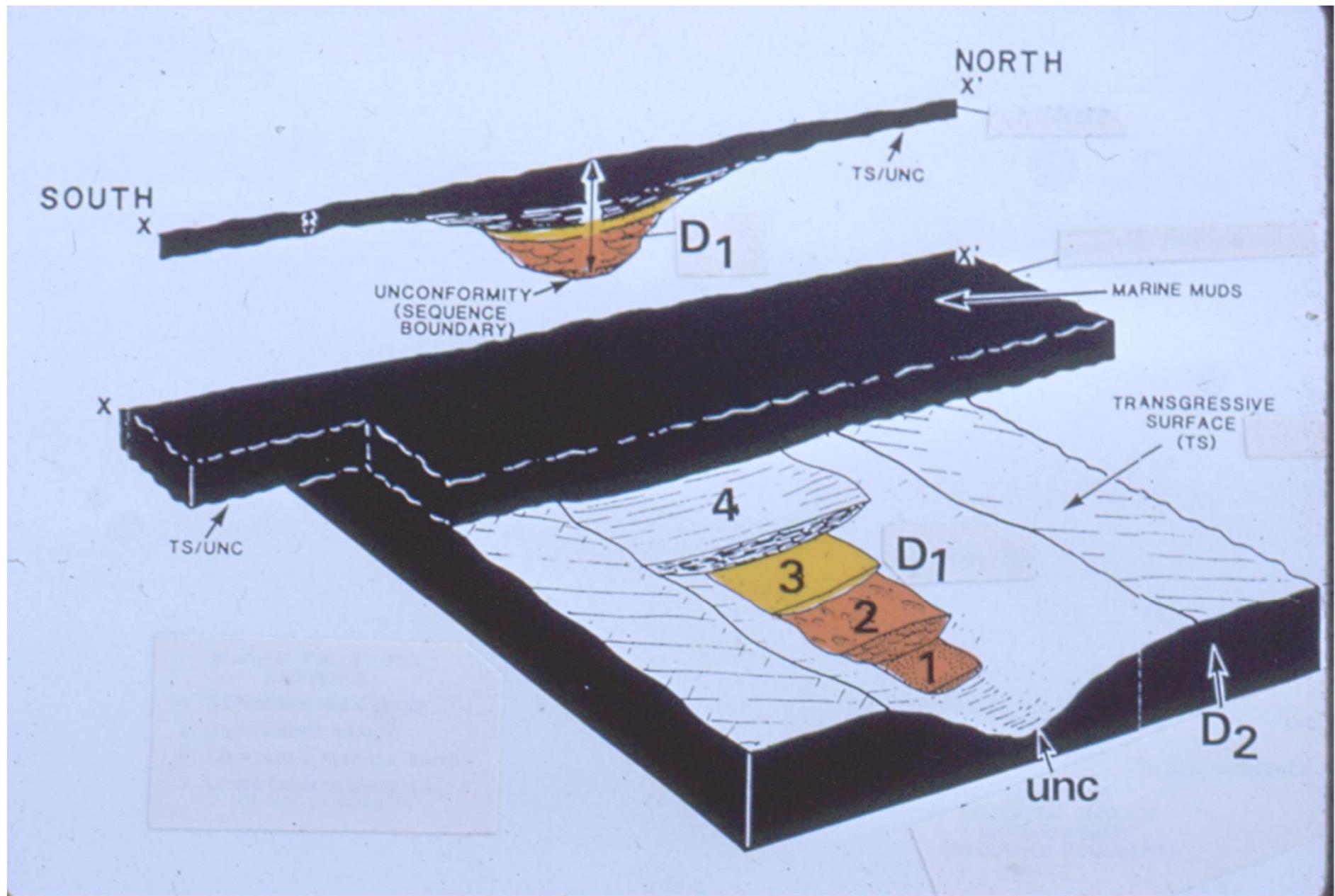
Lowering
Sea Level

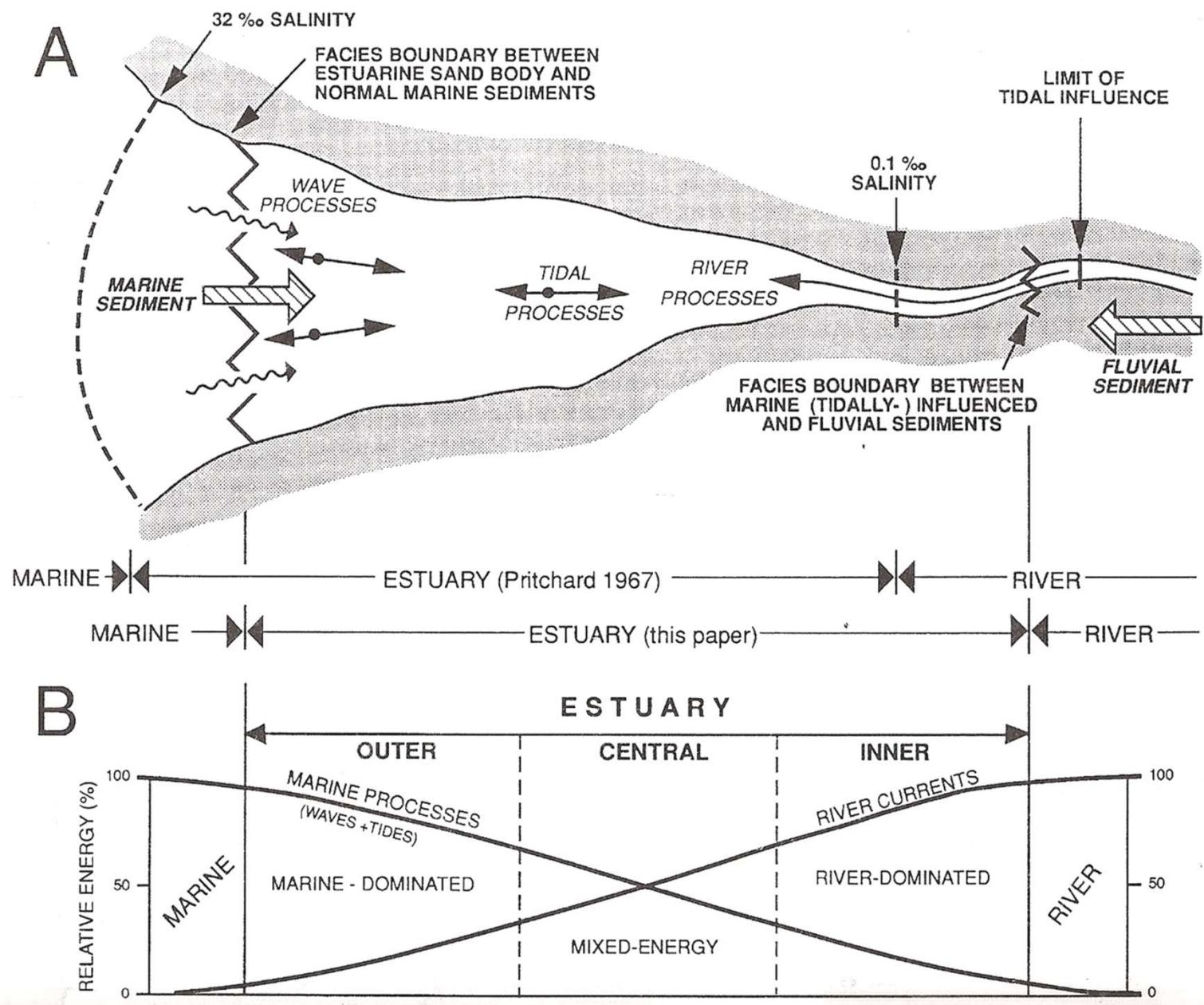
Filling of Valleys and Estuaries
Rising Sea
Level



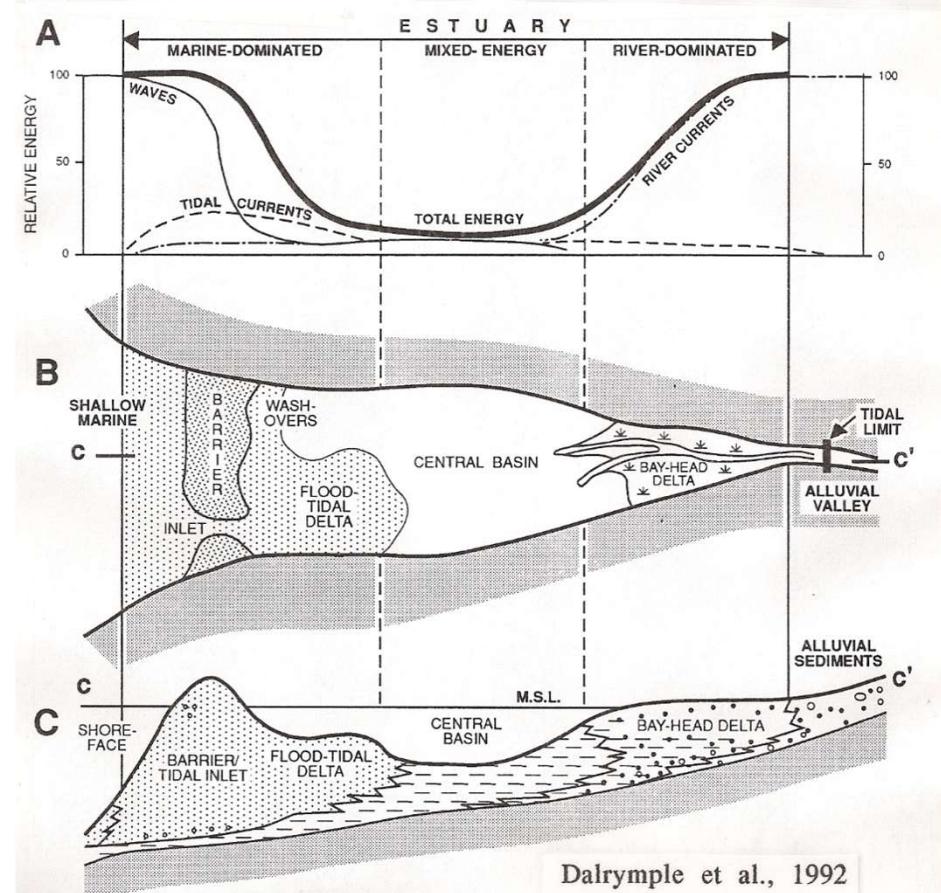
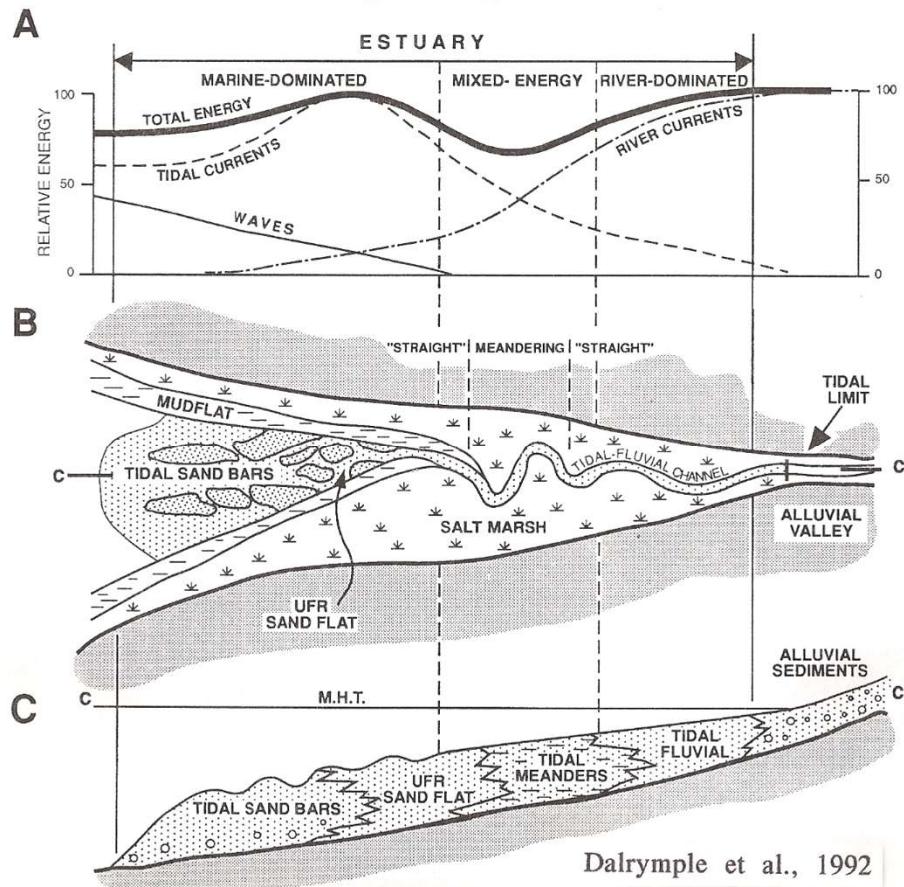
Stage 3

Sea Level
D Sandstone
Huntsman Sh.



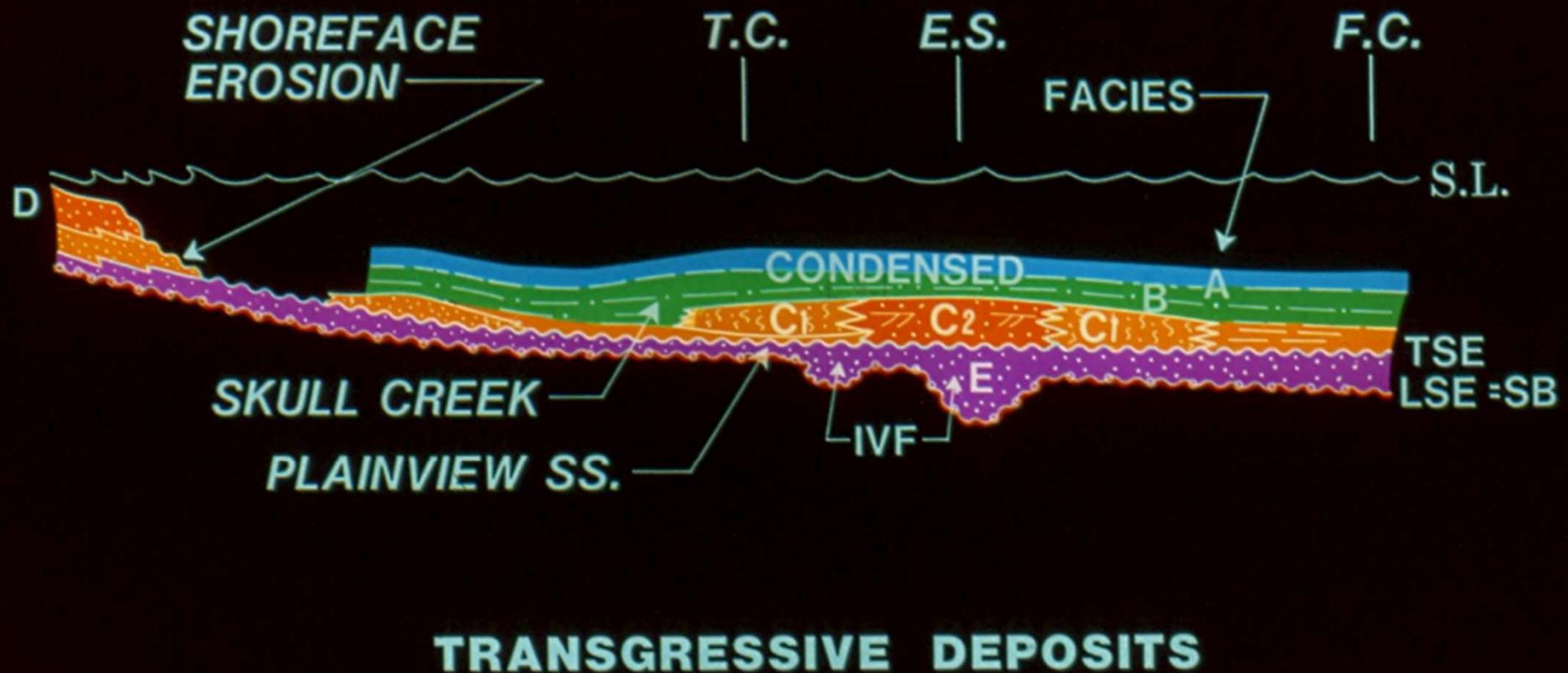


Dalrymple et al., 1992



D Transgressive

- Above TSE
- < 20 ft thick
- Up to 6 miles long 2 miles wide
- Located near terminus of VFs
- Examples: Dragoon, Comanche Crk., Irondale fields



Low Stand Delta

- Prod. from distributary channel >> delta front
- Occur at distal end of VFs
- Little or no incisement into Huntsman
- Narrow and thin
- Fracturing is important
- Examples: Krauthead Field area

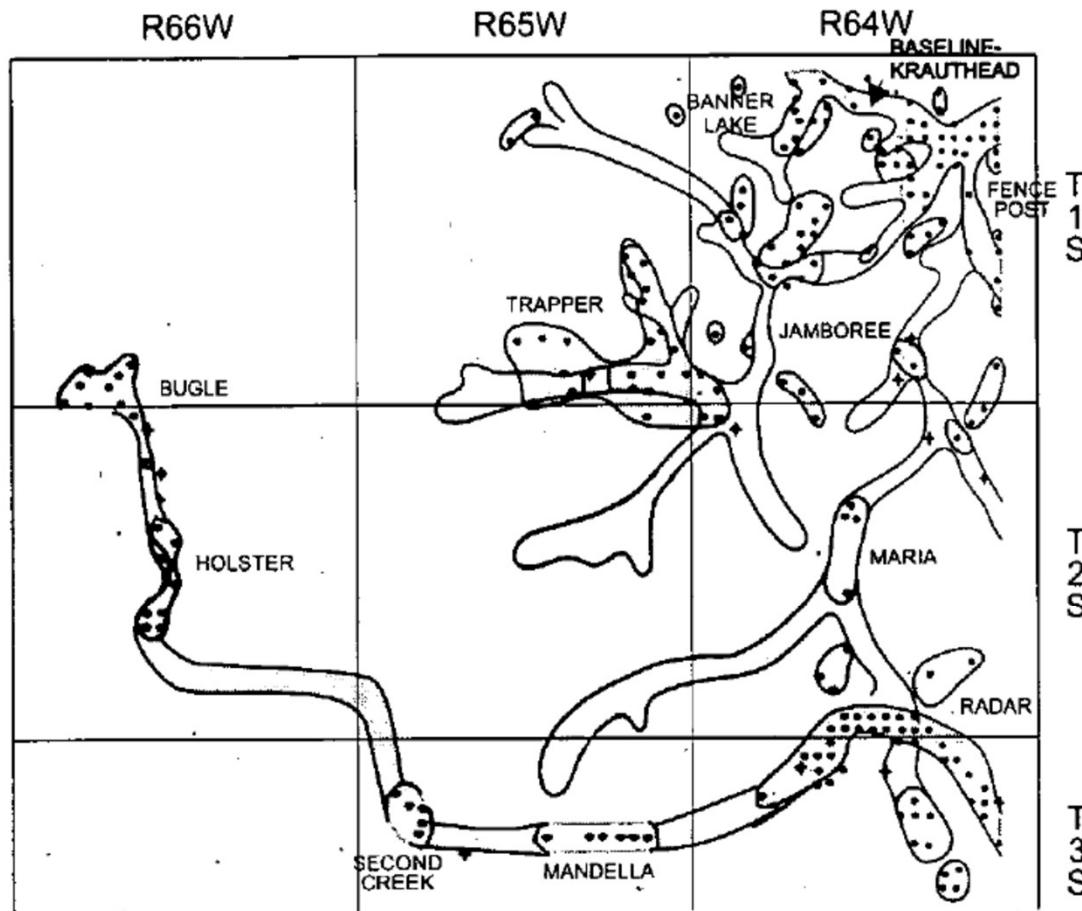


Figure 18. Oil wells producing from D-1 and D-2 sandstones. Syndepositional faults control thicknesses of valley fill in D-1 Sandstone and abrupt changes in trends (refer to Figure 16).

Waterfloods

D Waterfloods

- Historically poor recovery & high gas saturation at depletion
- Reservoir heterogeneity & management
- Successful floods
 - Injection by reservoir compartment
 - Unconventional pattern

Poor Waterflood Performance

- Complex reservoir compartmentalization
- Preferential directions of fluid flow, related to original depositional heterogeneity
- Rapid lateral facies changes
- Completion practices

D Waterfloods

- Notorious for poor response during waterflooding
- Primary recovery factors average 15.9%
- Average incremental 1.8% under waterflood

Table 2. Recovery Data for Fields in Vicinity of Sooner Unit*

Field Name	Township, Range	Area (acres)	OOIP (Mbbl)	Primary EUR Mbbl/ % OOIP	Waterflood Incremental/% OOIP	Recovery Factor Total (%)
Bijou	T4-5N, R59-60W	1180	7410	1400/18.9	170/2.2	21.1
Bijou, West	T4N, R60W	1320	7540	1198/15.9	13/0.2	16.1
Buckingham	T8N, R58W	480	2740	389/14.2	0	14.2
Greasewood	T6N, R61W	240	1235	248/20.0	19/1.5	21.5
Jackpot	T6-7N, R59W	1440	5515	1381/25.0	381/6.9	31.9
Masters	T5N, R60W	360	4070	335/08.2	19/0.5	8.7
Orchard, East	T4N, R60W	360	1237	301/24.3	7/0.6	24.9
Orchard, West	T4N, R60W	200	766	132/17.2	0	17.2
Roggen, NW	T2N, R63W	200	1462	204/14.0	37/2.5	16.5
Roggen, SE	T2N, R63W	1050	6267	496/07.9	56/0.9	8.8
Total		6830	38,242	6084/15.9	702/1.8	17.5

*Data from Sippel, 1996.

Montgomery, 1997

Table 1. Reservoir Rock and Fluid Data, Sooner Unit*

Average Depth	6300 ft
Maximum Gross	55 ft
Average Net	17 ft
Permeability to Air	21 md
Dykstra-Parsons Coefficient	0.74
Oil Gravity	41° API
Oil Viscosity	0.36 cp
Mobility Ratio	0.30

*Data courtesy Mark Sippel Engineering, Inc.

Montgomery, 1997

Dykstra-Parsons Coefficient: common descriptor of reservoir heterogeneity values 0 to 1. It measures reservoir uniformity by the dispersion or scatter of permeability values. A homogeneous reservoir has a permeability variation that approaches zero, while an extremely heterogeneous reservoir would have a permeability variation approaching one. The coefficient is expressed as follow: $V = (k_{50} - k_{84.1}) / k_{50}$ V: coefficient of Permeability Variation k₅₀: Permeability mean k_{84.1}: Permeability mean plus a standard deviation

Mobility ratio: ratio of the permeability of the formation to a fluid, divided by the fluid viscosity
 $\lambda = k/\mu$ where λ = mobility, md/cp; k = effective permeability, md; μ = fluid viscosity, cp

Mobility ratio in a waterflood is defined as the mobility of the displacing fluid divided by the mobility of the displaced fluid: $M = (k_{rw}/\mu_w) / (k_{ro}/\mu_o)$

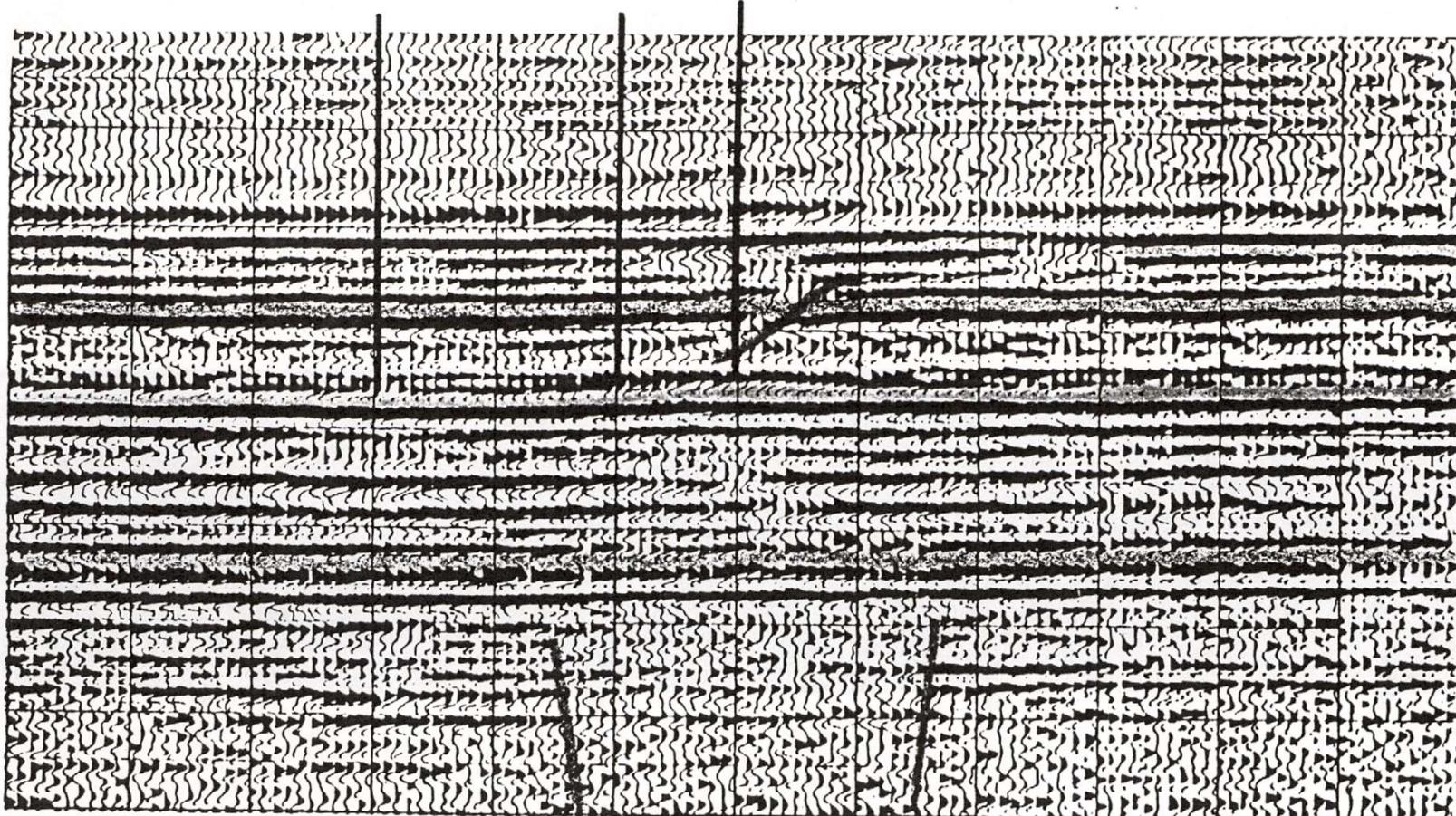
Reservoir Management

- Reservoir compartments
 - Pressure surveys, production history, etc.
- Infill drilling locations (prod + inj)
- Realignment of injection wells
- Controlling injection by operational compartments (pressure data & water-cut information)

Seismic

T-2781

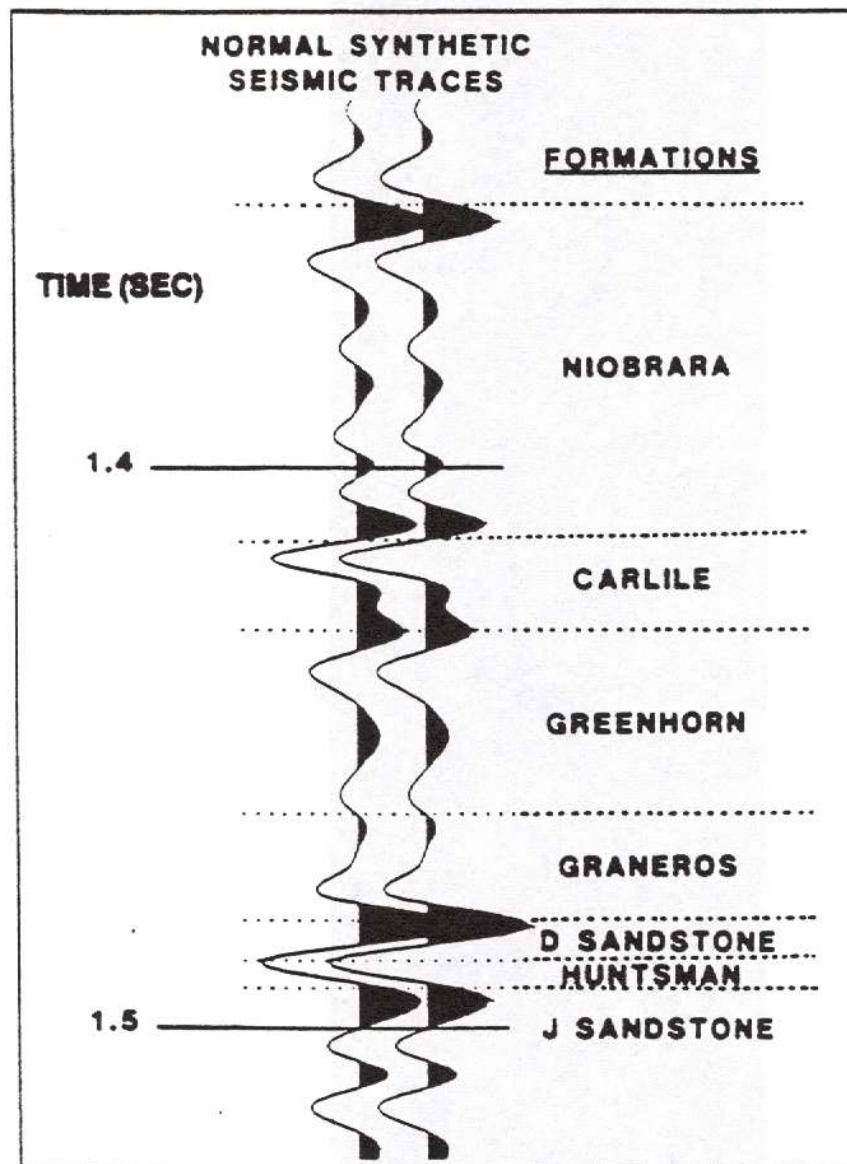
MASTERS FIELD



Line B - Final Stack

Figure 37.

(63)



Normal synthetic seismic traces made from sonic log from Amoco 2 Champlin 287 (NW1/4 SW1/4 Sec. 17, T. 3 S., R. 62 W.). Dashed lines denote formation boundaries. The synthetic illustrates the response expected on seismic from a 52-ft thick D Sandstone (from Sonnenberg, 1987).

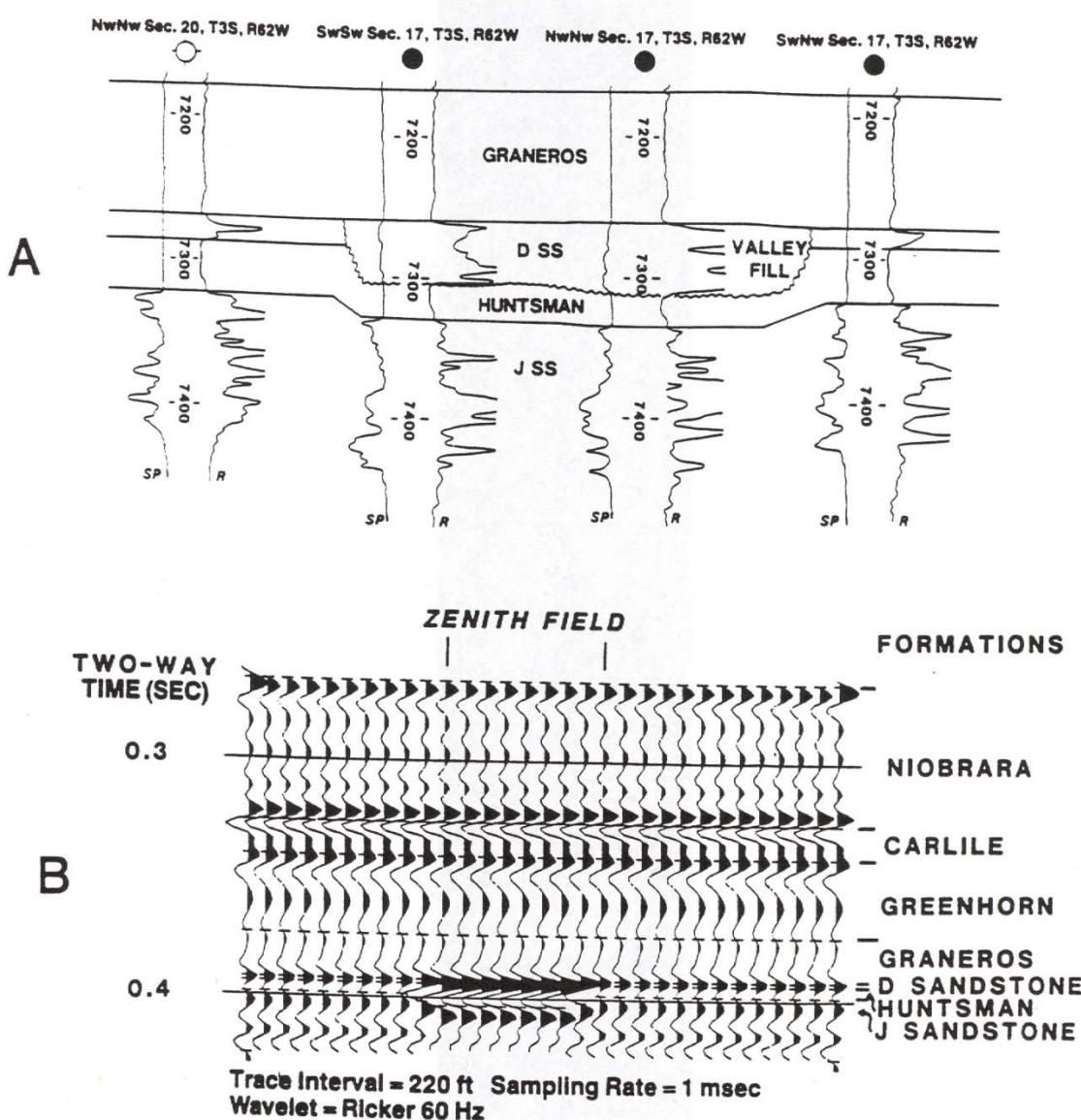
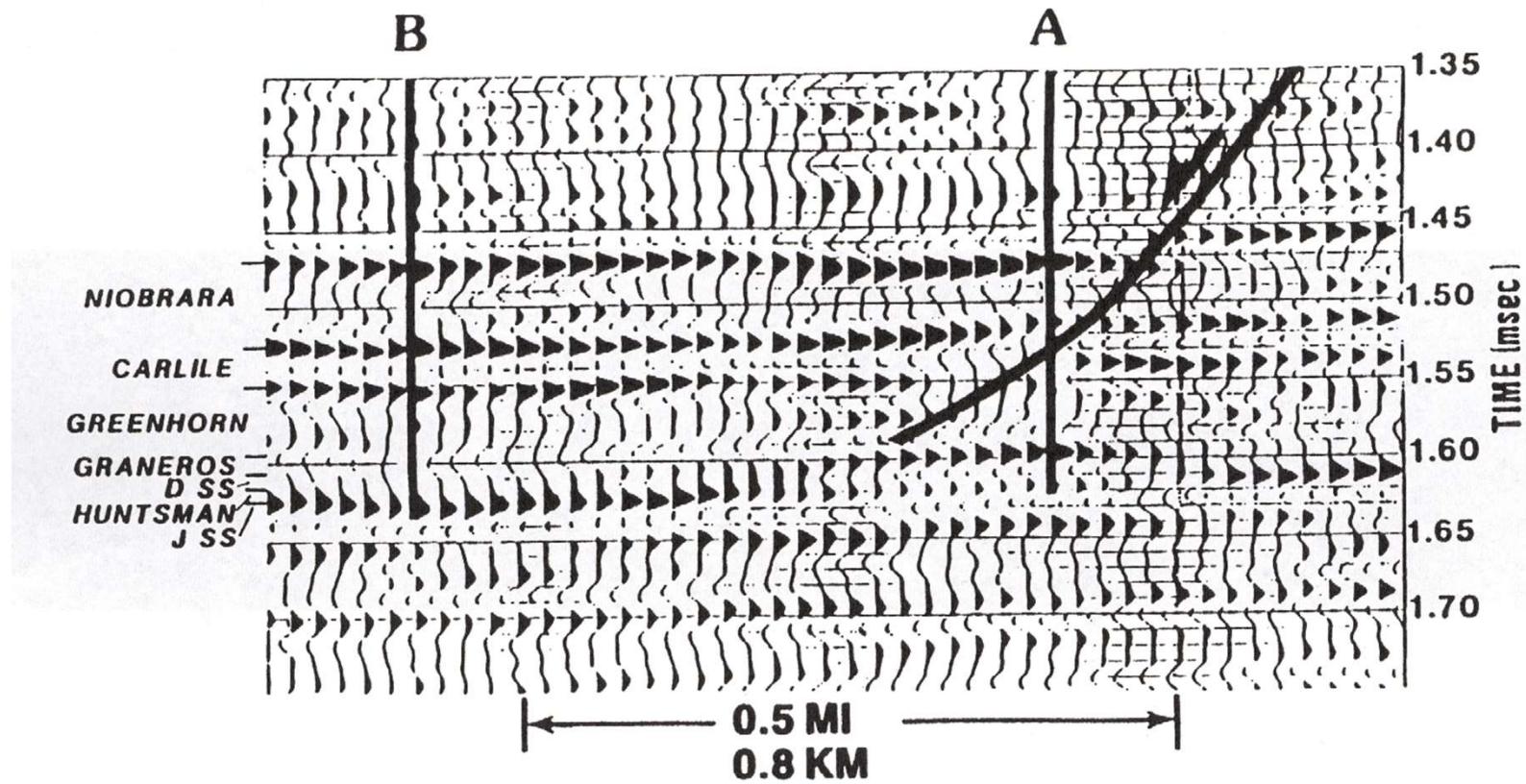
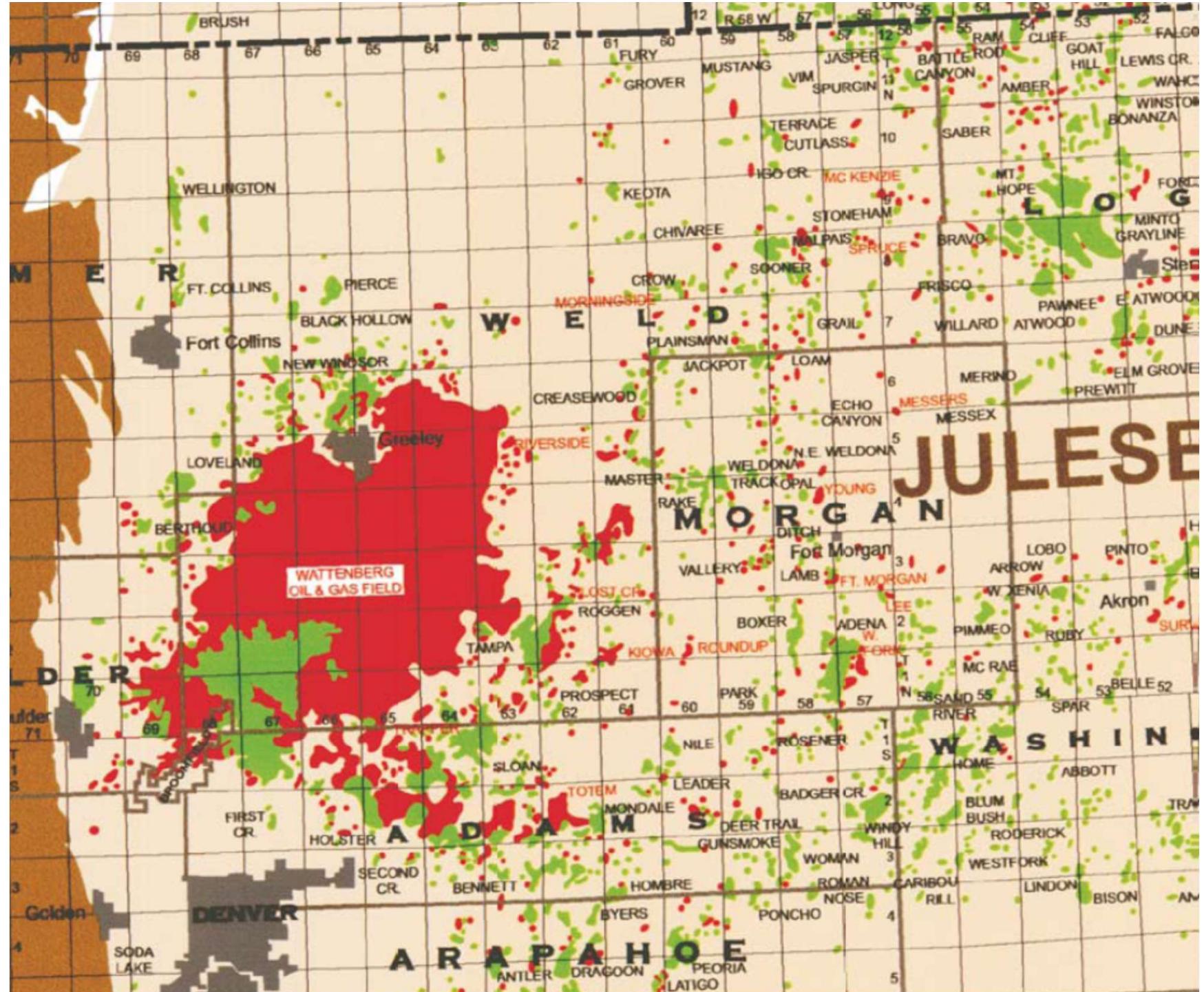


Figure 9. Two-dimensional geologic (a) and normal polarity seismic model (b) across Zenith field. Dashed lines denote formation boundaries. The thickness of the D Sandstone was varied from 10 to 52 ft back to 10 ft across the model to reflect the presence of the valley-fill deposits (from Sonnenberg, 1987).



Seismic line over a portion of Zenith field. Line is perpendicular to D valley fill deposits. Thicknesses of the D Sandstone in wells A and B are 58 ft and 16 ft, respectively. Note listric fault does not penetrate D Sandstone level (from Sonnenberg, 1987).

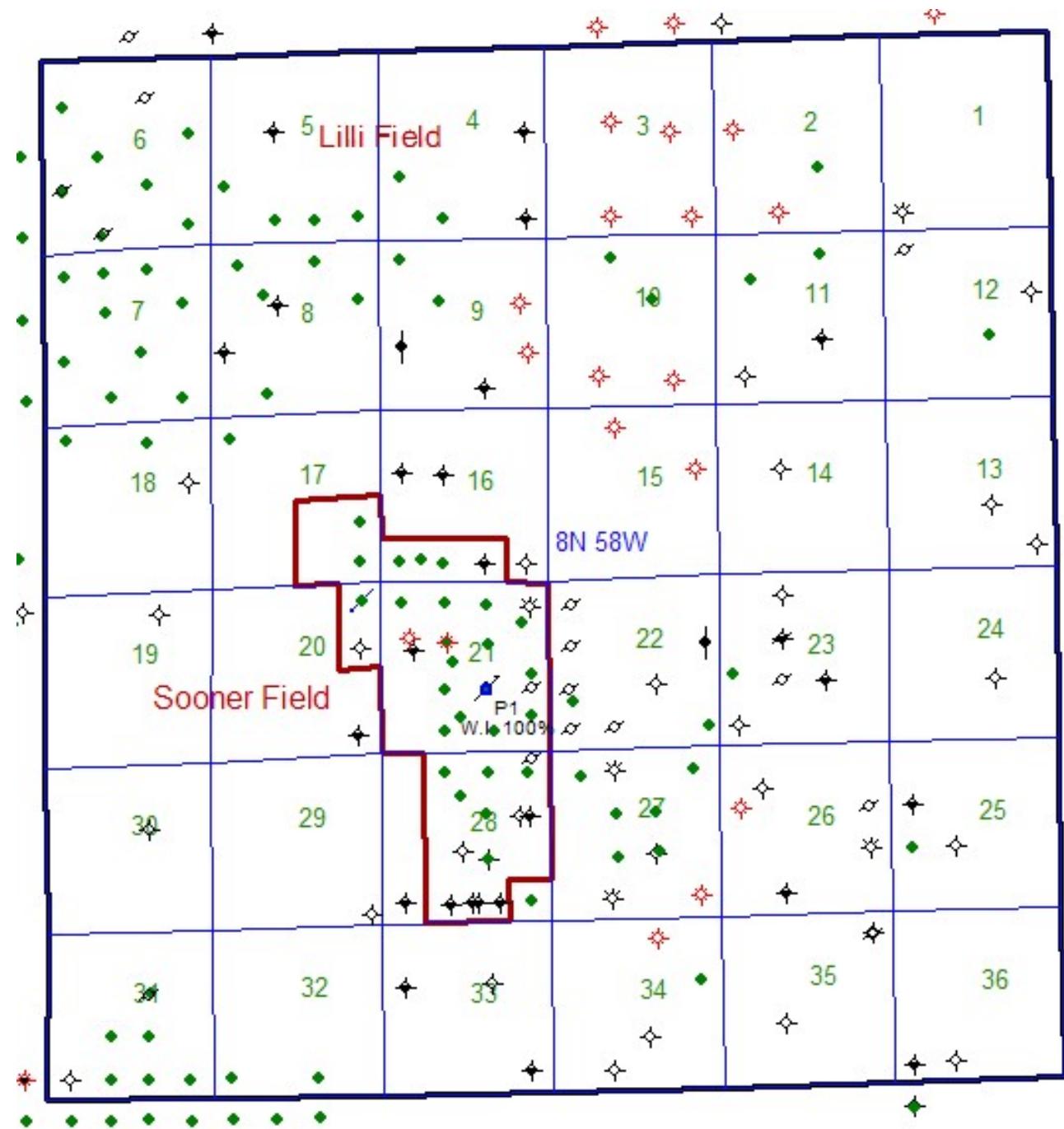


Sooner Field

- Disc. 1985, W.F. 1992
- Depth - 6300 ft
- 40 - ac pattern
- Gross thickness 55 ft; net pay 17 ft
- Fluvial to estuarine V-F ss
- Cum Prod: 1.8 MMBO, 7.1 BCF

Sooner Field

- Original oil-in-place: 6,900,000 STB
- Original Solution Gas: 3,500,000 MCFG
- Cum. To Unitization 10/1/88: 772,000 STB
- Cum to 2/1/93: 1,102,000 STB
- Predicted Primary Recovery: 980,000 STB
- Primary Recovery Factor: 14.2%



Sooner Field 3-D Survey

- October 1992
- 7.7 mi²

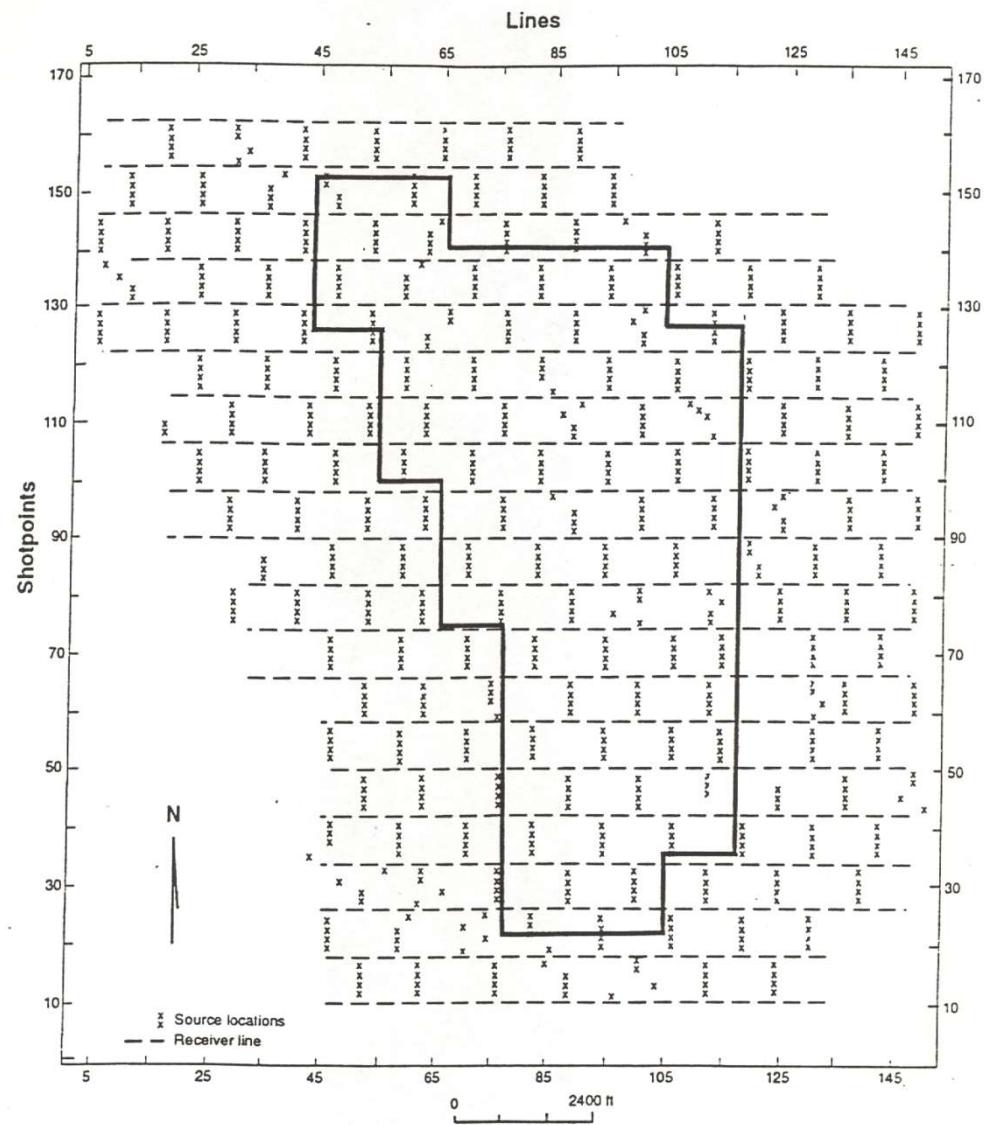
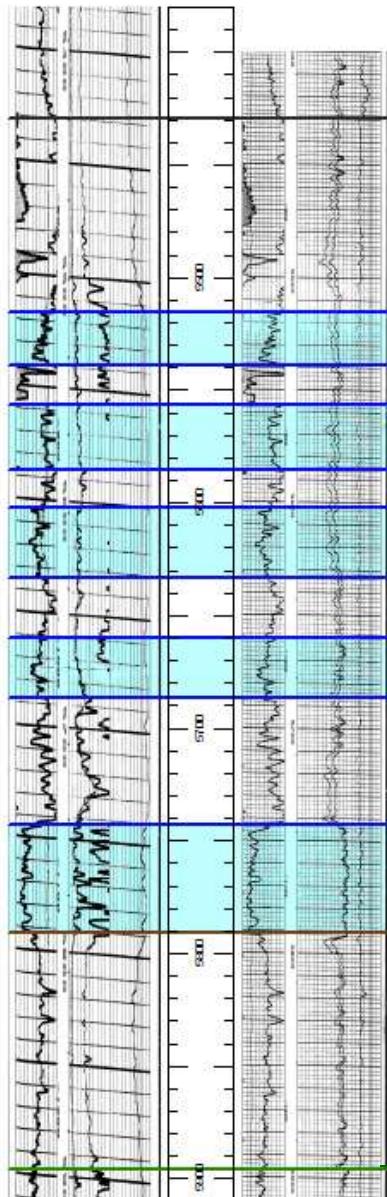


Figure 9 - The source-receiver geometry used to produce a 3-D image of the D reservoirs within the Sooner Unit. The heavy line defines the boundary of the Sooner Unit property.

DIVERSIFIED OPERATING CORPORATION
DOO SOONER
1021A
TBN RSSW 528
1940 FSL 2010 FEL



PIERRE

Sharon Springs

A

B1

B2

C

Fort Hays

Codell SS mbr.

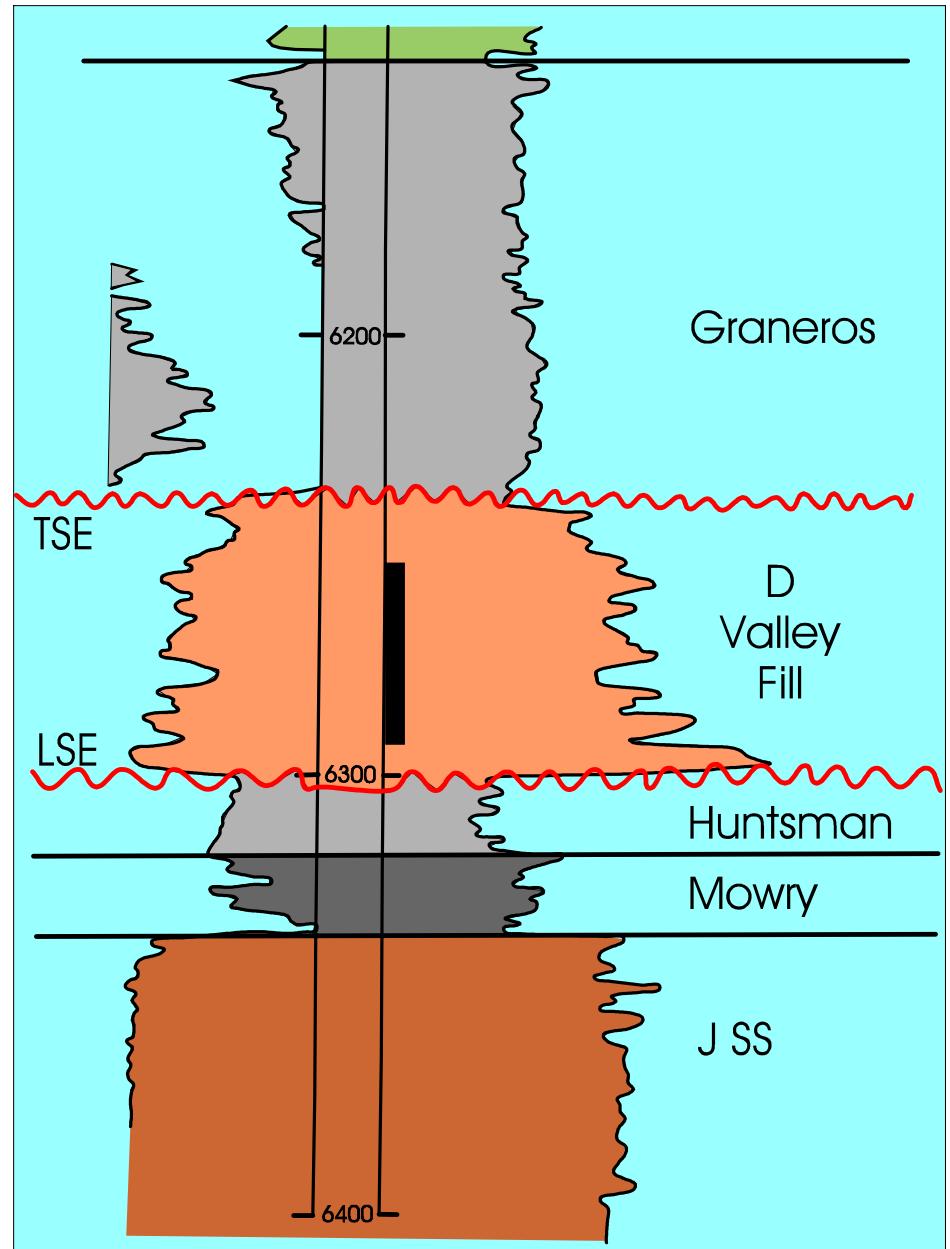
Carlile

Greenhorn

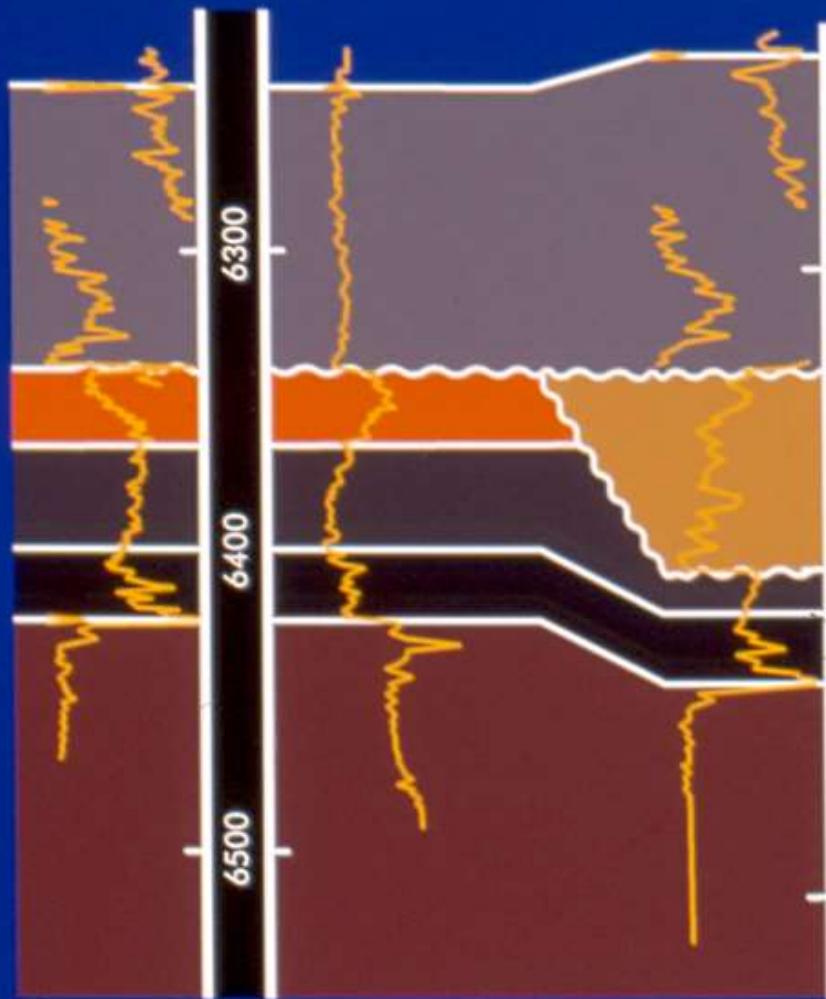
Type Log Sooner Field Area Denver Basin

Type Log Sooner Field

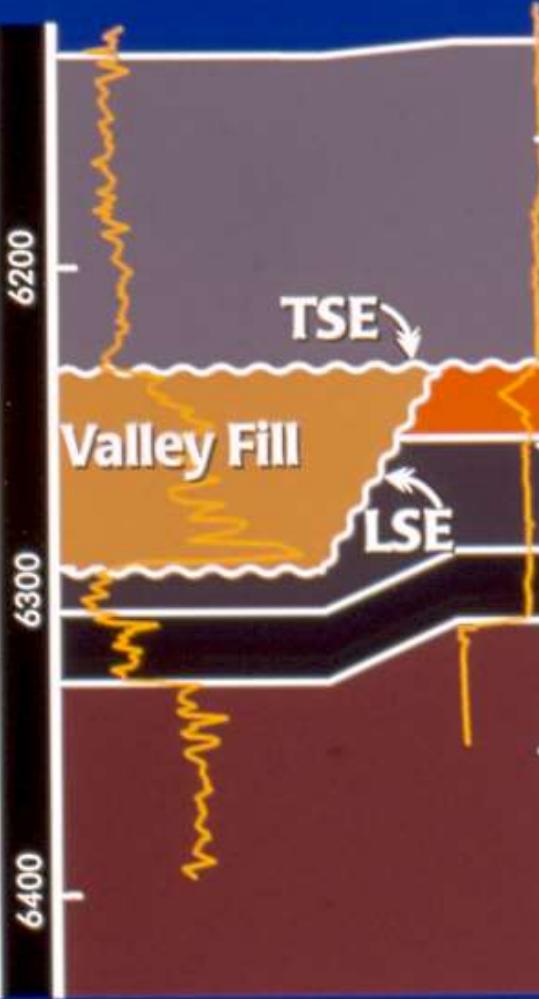
- Diversified
Sooner 14-21
- Pfs: 6253-6290
- IPF: 511 BOPD,
400 MCFD



DIVERSIFIED
Gallop #16-20



DIVERSIFIED
Sooner #14-21



DAVIDOR & DAVIDOR
Gov't #1-22



Well No. Fed. Sooner #7-21
 Location Sec 21, T8N, R58W
Weld County, CO

Date Dec. 31, 1992
 Strat. Unit "D" Sandstone
 Measured by F. G. Ethridge

