

## MODELO MATEMÁTICO:

$$\rho(T)c_p(T)\frac{\partial T(x,y,t)}{\partial t} = \nabla \cdot (k(T)\nabla T(x,y,t)) + g(T) \quad (1)$$

$$\frac{\partial T(0,y,t)}{\partial x} = \frac{\partial T(x,0,t)}{\partial y} = 0 \quad (2)$$

$$T(L_x, y, t) = T(x, L_y, t) = T_a \quad (3)$$

$$T(x, y, 0) = T_0 \quad (4)$$

$$-k\frac{\partial T(x,y,t)}{\partial x} = h(T_\infty - T(x,y,t)) \quad [a, b] \times [c, d] \quad (5)$$

Fazendo  $k$ ,  $\rho c_p$  e  $g$  constantes:

$$\rho c_p \frac{\partial T}{\partial t} = k \nabla^2 T + g \quad (6)$$

$$\frac{\rho c_p}{k} \frac{\partial T}{\partial t} = \nabla^2 T + \frac{g}{k} \quad (7)$$

Fazendo  $\alpha = \frac{k}{\rho c_p}$ :

$$\frac{1}{\alpha} \frac{\partial T}{\partial t} = \nabla^2 T + \frac{g}{k} \quad (8)$$

$$\frac{\partial T}{\partial t} = \alpha \nabla^2 T + \frac{g\alpha}{k} \quad (9)$$

$$\frac{\partial T}{\partial t} = \alpha \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) + \frac{g\alpha}{k} \quad (10)$$

Usamos uma aproximação de primeira ordem para a derivada temporal:

$$\left. \frac{\partial T}{\partial t} \right|_{i,j}^{n+1} = \frac{T_{i,j}^{n+1} - T_{i,j}^n}{\Delta t} \quad (11)$$

E uma aproximação de segunda ordem para a derivada espacial:

$$\left. \frac{\partial T}{\partial x} \right|_{i,j}^{n+1} = \frac{T_{i-1,j}^{n+1} - 2T_{i,j}^{n+1} + T_{i+1,j}^{n+1}}{\Delta x^2} \quad (12)$$

$$\left. \frac{\partial T}{\partial y} \right|_{i,j}^{n+1} = \frac{T_{i,j-1}^{n+1} - 2T_{i,j}^{n+1} + T_{i,j+1}^{n+1}}{\Delta y^2} \quad (13)$$

Assim, a equação 10 se torna:

$$\frac{T_{i,j}^{n+1} - T_{i,j}^n}{\Delta t} = \alpha \left( \frac{T_{i-1,j}^{n+1} - 2T_{i,j}^{n+1} + T_{i+1,j}^{n+1}}{\Delta x^2} + \frac{T_{i,j-1}^{n+1} - 2T_{i,j}^{n+1} + T_{i,j+1}^{n+1}}{\Delta y^2} \right) + \frac{g\alpha}{k} \quad (14)$$

Considerando uma malha uniforme constante ( $\Delta x = \Delta y$ ) :

$$\frac{T_{i,j}^{n+1} - T_{i,j}^n}{\Delta t} = \alpha \left( \frac{T_{i-1,j}^{n+1} - 2T_{i,j}^{n+1} + T_{i+1,j}^{n+1} + T_{i,j-1}^{n+1} - 2T_{i,j}^{n+1} + T_{i,j+1}^{n+1}}{\Delta x^2} \right) + \frac{g\alpha}{k} \quad (15)$$

$$T_{i,j}^{n+1} - T_{i,j}^n = \frac{\alpha \Delta t}{\Delta x^2} (T_{i-1,j}^{n+1} + T_{i+1,j}^{n+1} + T_{i,j-1}^{n+1} + T_{i,j+1}^{n+1} - 4T_{i,j}^{n+1}) + \frac{g\alpha}{k} \quad (16)$$

Fazendo  $r = \frac{\alpha \Delta t}{\Delta x^2}$  e  $\lambda = \frac{g\alpha}{k}$  :

$$T_{i,j}^{n+1} - T_{i,j}^n = r (T_{i-1,j}^{n+1} + T_{i+1,j}^{n+1} + T_{i,j-1}^{n+1} + T_{i,j+1}^{n+1} - 4T_{i,j}^{n+1}) + \lambda \quad (17)$$

Isolando no lado esquerdo os termos em  $n + 1$  :

$$-r (T_{i-1,j}^{n+1} + T_{i+1,j}^{n+1} + T_{i,j-1}^{n+1} + T_{i,j+1}^{n+1}) + (1 + 4r)T_{i,j}^{n+1} = T_{i,j}^n + \lambda \quad (18)$$

## 2. DISCRETIZAÇÃO EM NÓS ESPECIAIS:

### 2.1 Contorno externo superior e externo direito

Em  $x = L_x$  e em  $y = L_y$ , a temperatura é prescrita.

$$T_{0,j} = T_a \quad j = 0, 1, \dots, M \quad (19)$$

$$T_{i,M} = T_a \quad i = 0, 1, \dots, N \quad (20)$$

### 2.2 Contorno externo inferior e externo esquerdo

Em  $x = 0$  ( $j = 0$ ), o fluxo é nulo.

$$\left. \frac{\partial T}{\partial x} \right|_{j=0} = 0 \quad (21)$$

Utilizaremos uma aproximação avançada de segunda ordem, em três pontos:

$$\left. \frac{\partial T}{\partial x} \right|_{j=0}^{n+1} = \frac{-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1}}{2\Delta x} \quad (22)$$

$$\frac{-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1}}{2\Delta x} = 0 \quad (23)$$

$$-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1} = 0 \quad j = 0 \quad i = 1, 2, \dots, N \quad (24)$$

De maneira similar, para  $y = 0$  ( $i = N$ ), também não há troca de calor.

$$\left. \frac{\partial T}{\partial y} \right|_{i=N} = 0 \quad (25)$$

Utilizaremos derivada recuada (pois temos apenas as informações dos nós anteriores):

$$\left. \frac{\partial T}{\partial y} \right|_{i=N}^{n+1} = \frac{T_{N,j-2}^{n+1} - 4T_{N,j-1}^{n+1} + 3T_{N,j}^{n+1}}{2\Delta y} \quad (26)$$

$$\frac{T_{N,j-2}^{n+1} - 4T_{N,j-1}^{n+1} + 3T_{N,j}^{n+1}}{2\Delta y} = 0 \quad (27)$$

$$T_{N,j-2}^{n+1} - 4T_{N,j-1}^{n+1} + 3T_{N,j}^{n+1} = 0 \quad i = N \quad j = 1, 2, \dots, M - 1 \quad (28)$$

### 2.3 Contorno interno superior e interno inferior

Consideremos que  $T_{p,q}$  é o vértice superior esquerdo da região interna  $\Omega$  em contato com o meio sujeito à temperatura  $T_f$  e  $w$  é o número de nós necessários para preencher as arestas de comprimento  $d$ , tal que:

$$w = \frac{d}{\Delta x} + 1 \quad (29)$$

Para troca térmica por convecção, temos:

$$k \frac{\partial T}{\partial x|_y} = h(T_\infty - T(x, y, t)) \quad (30)$$

Na aresta superior ( $i = p$ ) ocorre a troca térmica por convecção no sentido do eixo  $y$ . Utilizaremos a derivada recuada:

$$k \left( \frac{T_{i-2,j}^{n+1} - 4T_{i-1,j}^{n+1} + 3T_{i,j}^{n+1}}{2\Delta y} \right) = h(T_f - T_{i,j}^{n+1}) \quad (31)$$

$$k (T_{i-2,j}^{n+1} - 4T_{i-1,j}^{n+1} + 3T_{i,j}^{n+1}) = 2h\Delta y T_f - 2h\Delta y T_{i,j}^{n+1} \quad (32)$$

$$T_{i-2,j}^{n+1} - 4T_{i-1,j}^{n+1} + 3T_{i,j}^{n+1} = \frac{2h\Delta y}{k} T_f - \frac{2h\Delta y}{k} T_{i,j}^{n+1} \quad (33)$$

Fazendo  $\gamma = \frac{2h\Delta y}{k}$ :

$$T_{i-2,j}^{n+1} - 4T_{i-1,j}^{n+1} + 3T_{i,j}^{n+1} = \gamma T_f - \gamma T_{i,j}^{n+1} \quad (34)$$

$$T_{i-2,j}^{n+1} - 4T_{i-1,j}^{n+1} + (3 + \gamma)T_{i,j}^{n+1} = \gamma T_f \quad i = p \quad q \leq j \leq q + w \quad (35)$$

De maneira similar, podemos expressar a discretização na aresta inferior ( $i = p + w$ ) onde também ocorre troca térmica por convecção no sentido do eixo  $y$ . Utilizaremos, desta vez, diferenças avançadas:

$$k \left( \frac{-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1}}{2\Delta y} \right) = h(T_f - T_{i,j}^{n+1}) \quad (36)$$

$$k (-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1}) = 2h\Delta y T_f - 2h\Delta y T_{i,j}^{n+1} \quad (37)$$

$$-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1} = \frac{2h\Delta y}{k} T_f - \frac{2h\Delta y}{k} T_{i,j}^{n+1} \quad (38)$$

$$-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1} = \gamma T_f - \gamma T_{i,j}^{n+1} \quad (39)$$

$$(\gamma - 3)T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1} = \gamma T_f \quad i = p + w \quad q \leq j \leq q + w \quad (40)$$

### 2.4 Contorno interno esquerdo e direito

Na aresta esquerda ( $j = q$ ) ocorre a troca térmica por convecção no sentido do eixo x. Utilizaremos uma aproximação recuada de segunda ordem, com pontos no interior do domínio, para representar a derivada primeira presente condição de contorno de terceiro tipo:

$$k \left( \frac{T_{i,j-2}^{n+1} - 4T_{i,j-1}^{n+1} + 3T_{i,j}^{n+1}}{2\Delta x} \right) = h(T_f - T_{i,j}^{n+1}) \quad (41)$$

$$k (T_{i,j-2}^{n+1} - 4T_{i,j-1}^{n+1} + 3T_{i,j}^{n+1}) = 2h\Delta x T_f - 2h\Delta x T_{i,j}^{n+1} \quad (42)$$

$$T_{i,j-2}^{n+1} - 4T_{i,j-1}^{n+1} + 3T_{i,j}^{n+1} = \frac{2h\Delta x}{k} T_f - \frac{2h\Delta x}{k} T_{i,j}^{n+1} \quad (43)$$

Fazendo  $\gamma = \frac{2h\Delta x}{k}$ :

$$T_{i,j-2}^{n+1} - 4T_{i,j-1}^{n+1} + 3T_{i,j}^{n+1} = \gamma T_f - \gamma T_{i,j}^{n+1} \quad (44)$$

$$T_{i,j-2}^{n+1} - 4T_{i,j-1}^{n+1} + (3 + \gamma)T_{i,j}^{n+1} = \gamma T_f \quad j = q \quad p \leq i \leq p + w \quad (45)$$

De maneira similar, podemos expressar a discretização na aresta direita ( $j = q + w$ ) onde também ocorre troca térmica por convecção no sentido do eixo x. Aqui utilizamos diferenças finitas avançadas:

$$k \left( \frac{-3T_{i,j}^{n+1} + 4T_{i,j+1}^{n+1} - T_{i,j+2}^{n+1}}{2\Delta y} \right) = h(T_f - T_{i,j}^{n+1}) \quad (46)$$

$$k (-3T_{i,j}^{n+1} + 4T_{i,j+1}^{n+1} - T_{i,j+2}^{n+1}) = 2h\Delta y T_f - 2h\Delta y T_{i,j}^{n+1} \quad (47)$$

$$-3T_{i,j}^{n+1} + 4T_{i,j+1}^{n+1} - T_{i,j+2}^{n+1} = \frac{2h\Delta y}{k} T_f - \frac{2h\Delta y}{k} T_{i,j}^{n+1} \quad (48)$$

$$-3T_{i,j}^{n+1} + 4T_{i,j+1}^{n+1} - T_{i,j+2}^{n+1} = \gamma T_f - \gamma T_{i,j}^{n+1} \quad (49)$$

$$(\gamma - 3)T_{i,j}^{n+1} + 4T_{i,j+1}^{n+1} - T_{i,j+2}^{n+1} = \gamma T_f \quad j = q + w \quad p \leq i \leq p + w \quad (50)$$

## RESUMO:

$T_{0,j}$	=	$T_a$	$i = 0$	$j = 0, 1, \dots, M$
$T_{i,M}$	=	$T_a$	$j = M$	$i = 0, 1, \dots, N$
$-3T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1}$	=	0	$j = 0$	$i = 1, 2, \dots, N$
$T_{N,j-2}^{n+1} - 4T_{N,j-1}^{n+1} + 3T_{N,j}^{n+1}$	=	0	$i = N$	$j = 1, 2, \dots, M - 1$
$T_{i-2,j}^{n+1} - 4T_{i-1,j}^{n+1} + (3 + \gamma)T_{i,j}^{n+1}$	=	$\gamma T_f$	$i = p$	$q \leq j \leq q + w$
$(\gamma - 3)T_{i,j}^{n+1} + 4T_{i+1,j}^{n+1} - T_{i+2,j}^{n+1}$	=	$\gamma T_f$	$i = p + w$	$q \leq j \leq q + w$
$T_{i,j-2}^{n+1} - 4T_{i,j-1}^{n+1} + (3 + \gamma)T_{i,j}^{n+1}$	=	$\gamma T_f$	$j = q$	$p \leq i \leq p + w$
$(\gamma - 3)T_{i,j}^{n+1} + 4T_{i,j+1}^{n+1} - T_{i,j+2}^{n+1}$	=	$\gamma T_f$	$j = q + w$	$p \leq i \leq p + w$
$-r(T_{i-1,j}^{n+1} + T_{i+1,j}^{n+1} + T_{i,j-1}^{n+1} + T_{i,j+1}^{n+1}) + (1 + 4r)T_{i,j}^{n+1}$	=	$T_{i,j}^n + \lambda$	caso contrário	