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# ME469: Common Discretization Approaches

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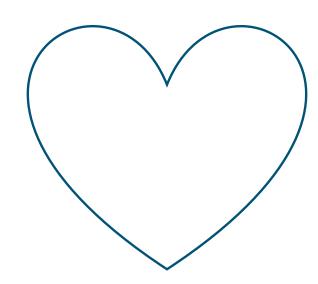
#### **Lecture Objectives**

- The Concept of Meshing
- Why Unstructured?
- Unstructured Element Types
- Cell-centered Finite Volume (FV)
- Edge-based Vertex-Centered (EBVC)
- Control-Volume Finite Element Method (CVFEM)
- Finite Element Method (FEM)
- Staggered arrangement



## Introducing a Mesh over Heart Domain, $\Omega$

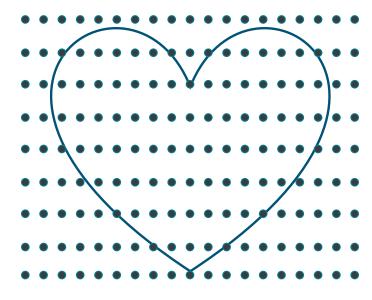
- Complex
- Curved
- Sharp





## Re-introducing a [Finite Difference] Mesh over Heart Domain, $\Omega$

- Complex
- Curved
- Sharp

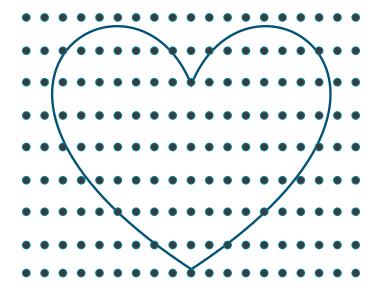




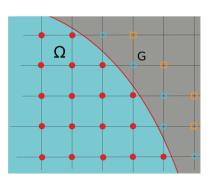
## Re-introducing a [Finite Difference] Mesh over Heart Domain, $\Omega$

#### Geometry is:

- Complex
- Curved
- Sharp



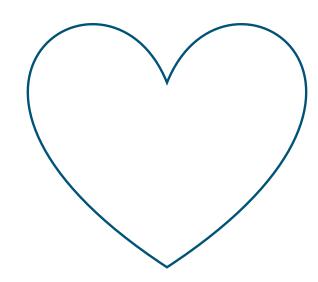
Not impossible: Chertock, et al., "A Second-Order Finite-Difference Method for Compressible Fluids in Domains with Moving Boundaries", Commun. Comput. Phys., 2018





## Introducing a [Structured Mesh] over Heart Domain, $\Omega$ ;

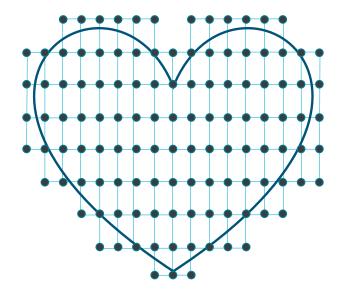
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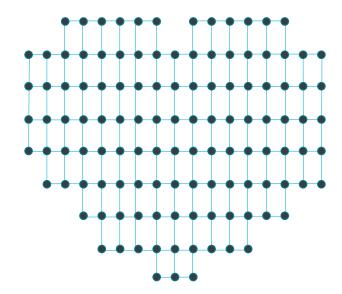
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## Introducing a [Structured Mesh] over Heart Domain, $\Omega$ ;

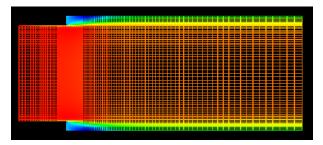
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- Curved
- Sharp



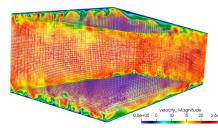


#### Structured vs Unstructured

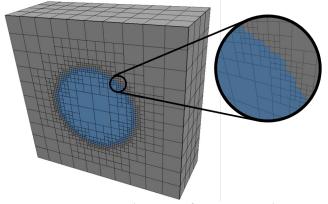
Many times, canonical flows of interest are represented by simplified geometries that allow for cartesian meshes – with "stair-stepping"



RANS-based backward facing step (Domino, 2012)



Re<sup>T</sup> 395 plane-channel (Jofre, Domino, laccarino, 2018)

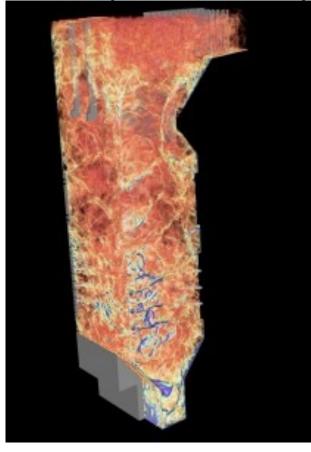


Often times, not!

https://www.itascainternational.com/software/introduction-to-meshing



## Example: The Carbon-Capture Multidisciplinary Simulation Center



http://ccmsc.utah.edu/about.html

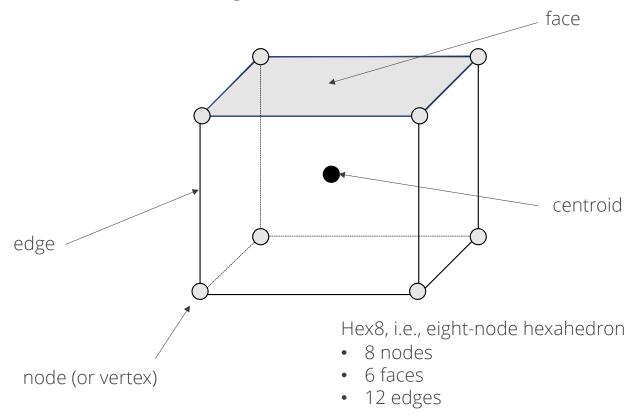
15MW coal-fired boiler volume rendered image of large (90  $\mu$ m) particles

Staggered schemes have been demonstrated to support complex applications

Cut-cells and embedded approaches help

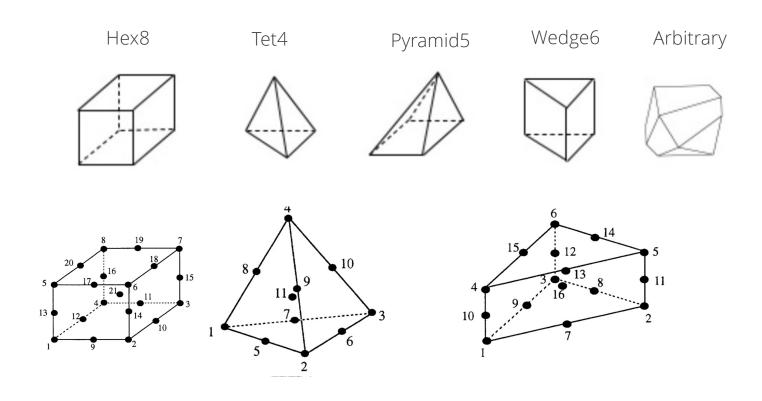
#### **Attributes of an Element**

An element consists of nodes, edges, and faces





## **Examples of Various Topologies**

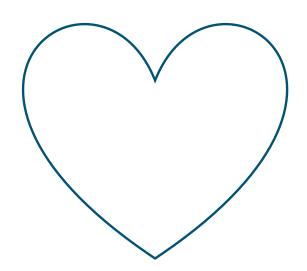


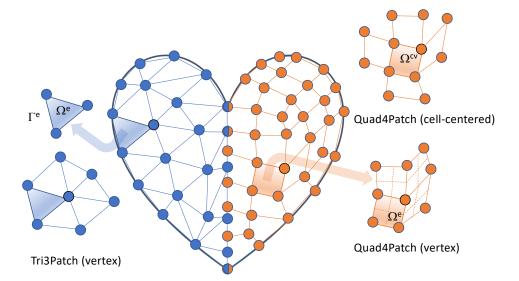
Higher-order promoted elements (Hex27, Tet10, Wedge16, Hex64, etc.)



#### Introducing a Mesh over Heart Domain, $\Omega$

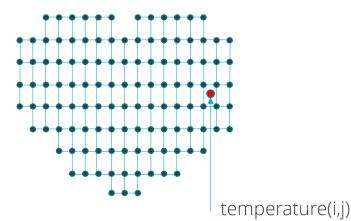
- Elements of size 4 (Quad4) or 3 (Tri3) have been introduced
- Exterior domain is faceted
- Non-conformal interface between the Tri3 and Quad4 block
- Two types of connectivity have been presented: node:element and element:face:element
- Two types of integration:  $\Omega^e$  vs  $\Omega^{cv}$



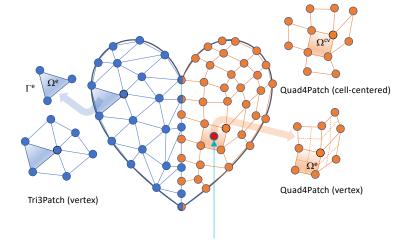




#### Data Structure Ramifications: A bit more complex...



- Element and associated data structures are indexed directly via **i**<sup>th</sup> and **j**<sup>th</sup>
  - location, e.g., **temperature** (i,j), over the range: **temperature**(0:nX-1,0:nY-1)
- Neighbors are directly indexed, e.g., "north" neighbor of (i,j) is (i,j+1)



- Element and associated data structures are indexed indirectly via a data structure, e.g., temperature(k), over the range: temperature(0:nElem-1)
- Nodes of element(k) are obtained via connectivity relationship mappings
  - std::vector<mesh\_type> nodes = elem\_nodes (k)
- Nodal fields, for element k via:
  - pressure = field\_data(nodes[0,..,numElem)

#### Integration Over the Domain: The "Finite" in Finite-Volume and Finite Element

Consider a simple model equation with the heart domain in mind:

$$\frac{\partial F_j}{\partial x_j} = S$$

Where  $F_i$  is a flux and S is a source term

Integrating over the entire domain,  $\Omega$ :  $\int_{\Omega} \frac{\partial F_j}{\partial x_j} dV = \int_{\Omega} S dV$ 

$$\int_{\Omega} \frac{\partial Y_j}{\partial x_j} dV = \int_{\Omega}$$

Without loss of generality, let us define a set of subdomains,  $\Omega_k$ :

$$\sum_{k} \int_{\Omega_k} \frac{\partial F_j}{\partial x_j} dV = \sum_{k} \int_{\Omega_k} S dV$$

As present, only volumetric integrals appear

Note: The formality of  $\Sigma_k$  and  $\Omega_k$ is implied to exist over the full domain and is often times dropped – integral type implied by dV and dS

Tri3Patch (vertex)

## Fundamentals of Discretization: Surface vs Volume Integrations

• Given a partial differential equation (PDE) and associated volumetric form:

$$\int \frac{\partial F_j}{\partial x_j} dV = \int SdV$$

 Applying Gauss Divergence provides the standard finite volume form for fluxes in surface integral form:

$$\int \frac{\partial F_j}{\partial x_j} dV = \int F_j n_j dS \quad \longrightarrow \quad \int F_j n_j dS = \int S dV$$

• We can also multiple PDE by an arbitrary test function, w, and integrate over a volume,

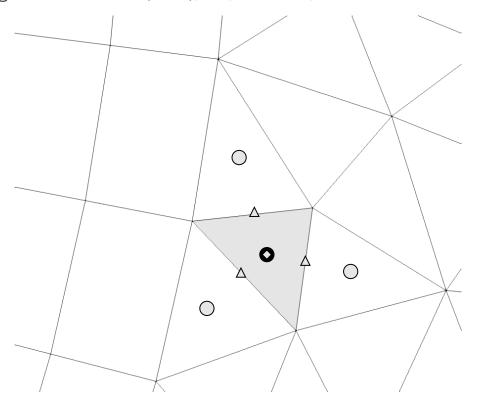
$$\int w \frac{\partial F_j}{\partial x_j} dV = \int w S dV$$
$$\int \frac{\partial w}{\partial x_j} F_j dV - \int w F_j dS = \int w S dV$$

Next, integrate by parts and apply Gauss-Divergence. Note, that test function must be differentiable – shown here, at least once..

$$\frac{\partial w F_j}{\partial x_j} = w \frac{\partial F_j}{\partial x_j} + \frac{\partial w}{\partial x_j} F_j$$

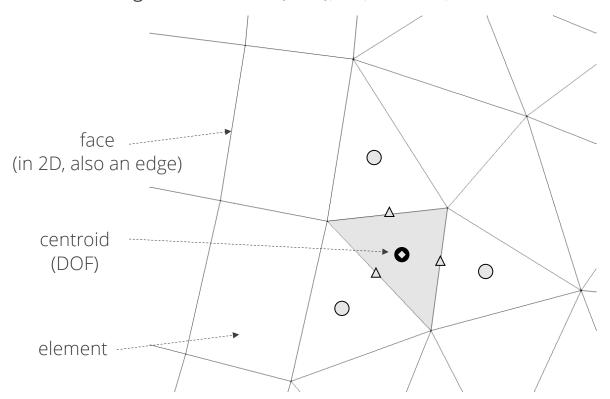


- Cell-centered, finite volume (shaded region)
  - Degree of freedom (DOF), i.e., solution, resides at the centroid of the element



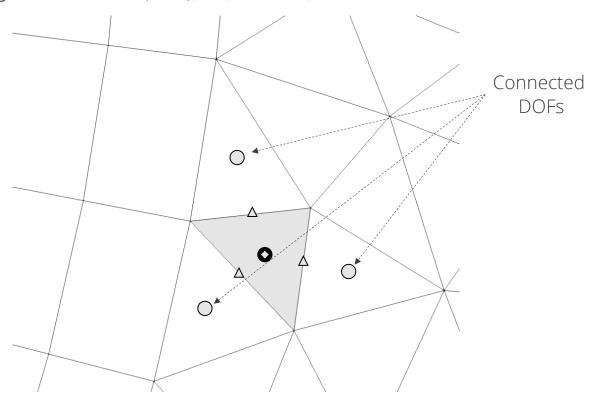


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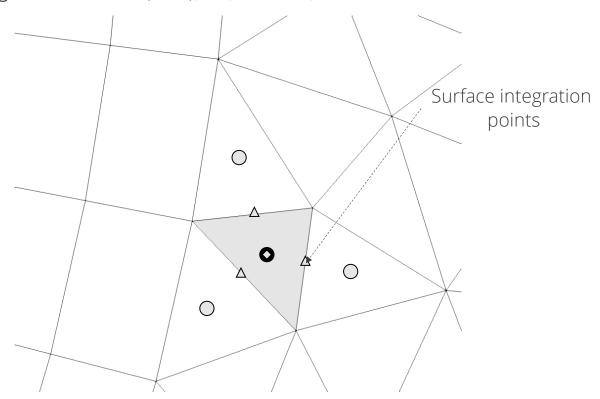


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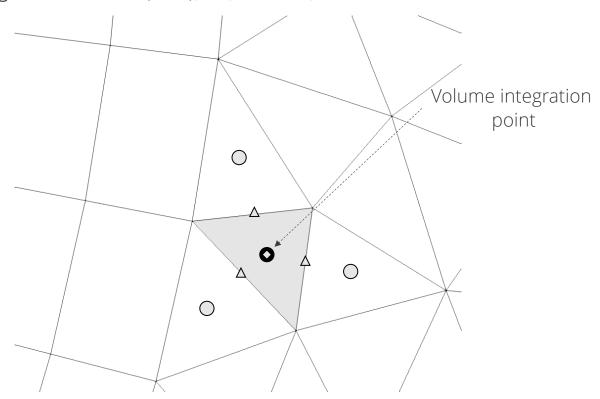


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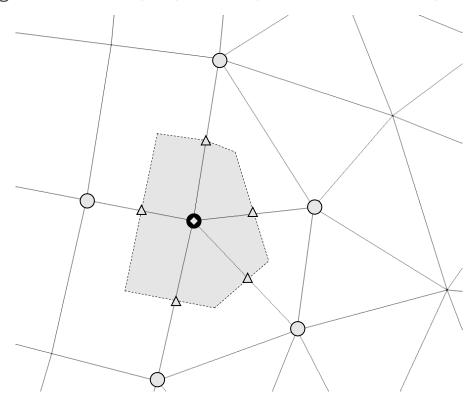


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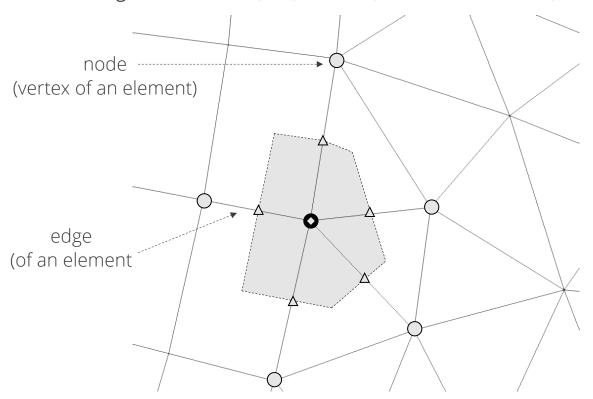


- Edge-based, vertex (or node)-centered finite volume (shaded region)
  - Degree of freedom, i.e., solution, resides at the node, or vertex



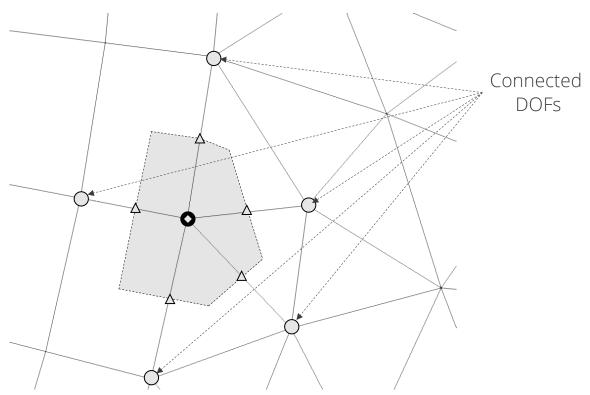


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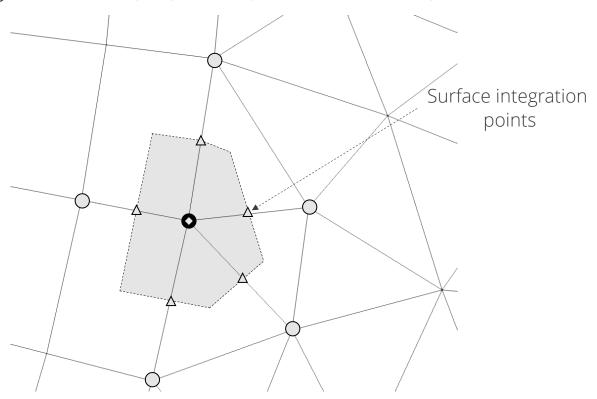


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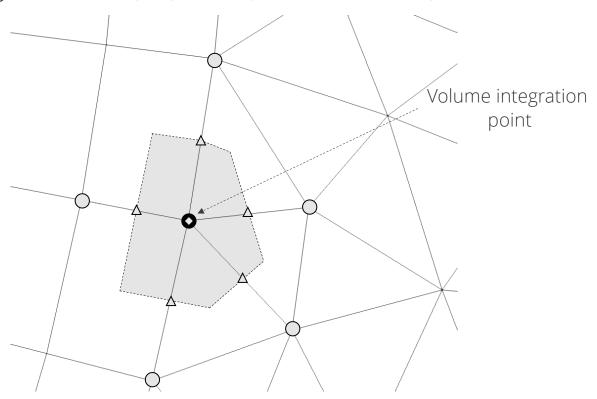


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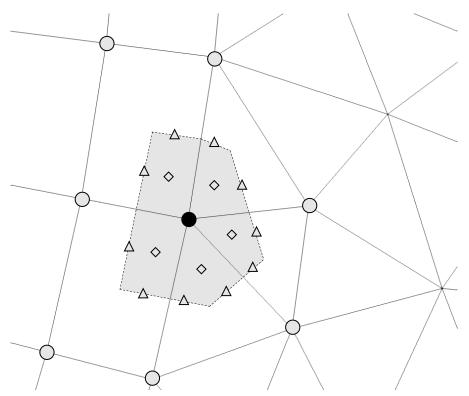


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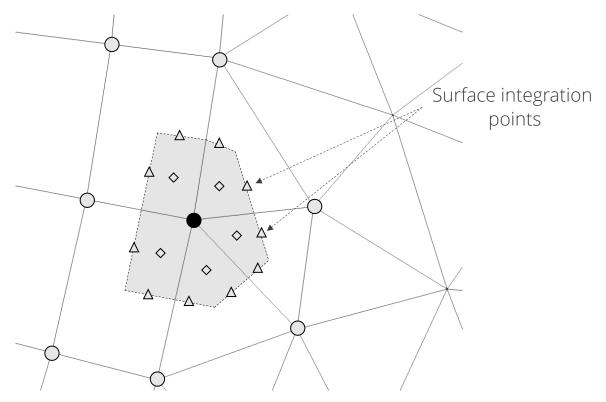


- Choice #1, Element-based, vertex (or node)-centered finite volume (shaded region)
  - Degree of freedom, i.e., solution, resides at the node, or vertex



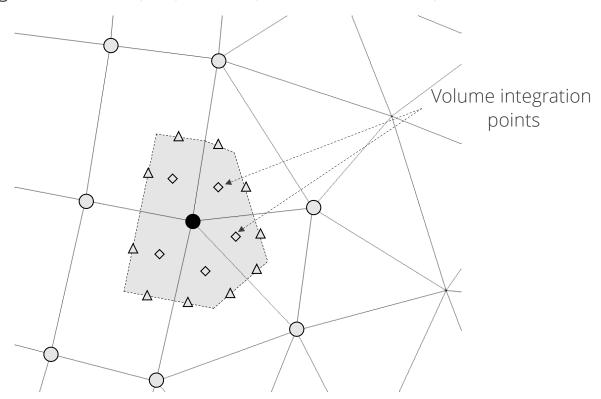


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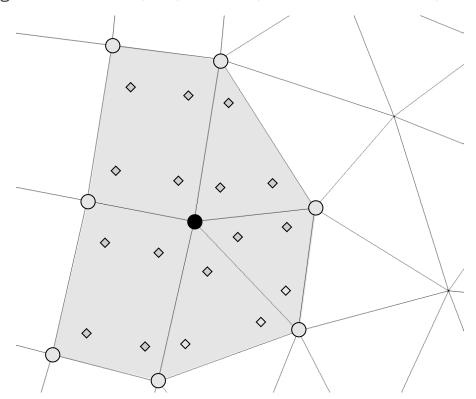


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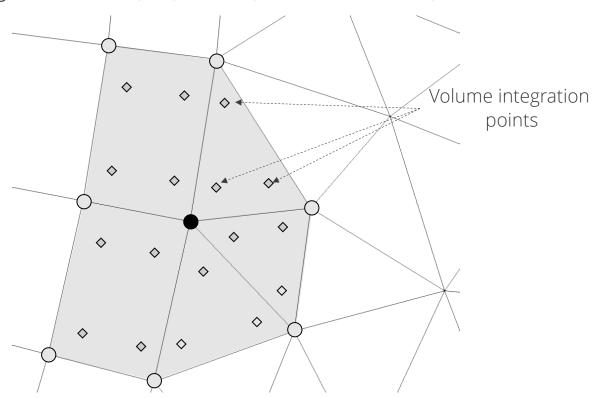


- Choice #2, Element-based, finite element
  - Degree of freedom, i.e., solution, resides at the node, or vertex





- Choice #2, Element-based, finite element
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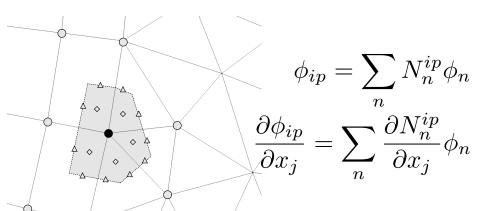


#### **VOF Transport Discretization Nuance: Volume- or Surface-based?**

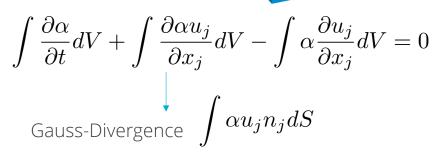
• Simple enough, define the volume (fraction) of fluid (absent evaporation):  $\frac{\partial \alpha}{\partial t} + u_j \frac{\partial \alpha}{\partial x_j} = 0$ 

Option 1: volumetric-form: 
$$\int \frac{\partial \alpha}{\partial t} dV + \int u_j \frac{\partial \alpha}{\partial x_j} dV = 0$$

CVFEM/FEM (really, any element-based approach) Evaluated as a volumetric-contribution (diamonds)



Option 2: divergence-form:



Traditional finite volume (element, edge, cell-centered) Evaluated as a surface integral (triangle)

Allows for a consistent advecting velocity (mass conserving) that is obtained from the continuity equation

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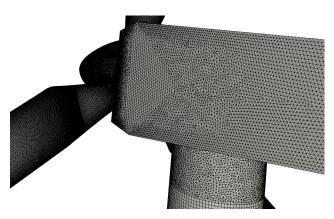


## Reality: Meshing time for complex applications remains a significant bottleneck!

- Many applications of interest contain complex geometries low-Mach fluids users interested in highquality simulation results tend towards hexahedralbased topologies (if possible)
- However, if a scheme is "design-order" accurate, any topology may suffice as it is simply a matter of mesh size and efficiency – not unlike the active discussion on low- vs higher-order
- Sometimes, the penetration of a low-Mach fluids physics addition in common analysis is high as the meshing can be prohibitively complex



Very complex world – stair-stepped!





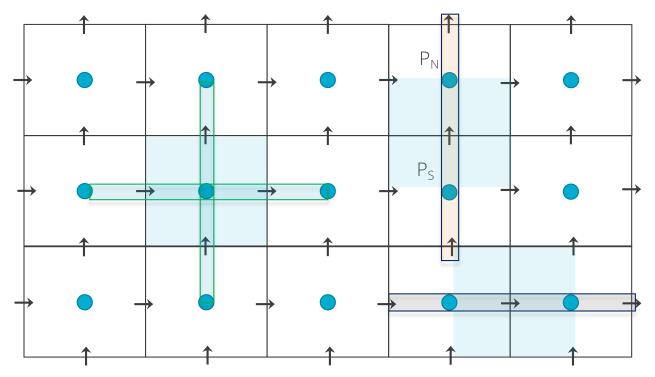


## **Classic Staggered Finite Volume**

 Velocity degree-of-freedom is staggered relative to pressure and other primitives, e.g., enthalpy, mixture fraction, etc. Stencil for CC-quantities 

Stencil for x-velocity →

Stencil for y-velocity ↑





#### Attributes of a Staggered Scheme

- By design, non-orthogonality is absent, however, complex geometry will be stair-stepped
- From a fluids perspective, the operators are ideal, i.e., pressure gradient for momentum is compact, e.g.,  $(P_E P_W)\Delta x^{-1}$
- As will be seen in future lecture topics, the skew-adjoint nature of the Divergence operator,
   D, and Gradient operator,
   G, allows for a Laplace operator,
   E = DG
- Can be extended to higher-order
- Frequently, meshing complex geometries can be extremely difficult (consider our V27 example)



### An Informal Survey....

- Cell-Centered: (Sometimes generalized Polyhedra)
  - Ansys Fluent, OpenFOAM (FireFOAM, NavyFOAM), CD-Adapco (Star-CCM), Soleil-X (Stanford)
- EBVC: (Most typical in the acoustically compressible space)
  - SU2, FUN3D, CHAD, Nalu-Wind (production), Nalu (option to explore discretizations)
- CVFEM
  - Fluent (originally!), CFX-TASC-FLOW, Sierra Fuego (SNL), Nalu
- FEM
  - FIDAP, COMSOL, EDDY (NASA), AcuSim, PHASTA
- Staggered
  - Arches (Utah)

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Common Water-Cooler CFD Arguments:

- Structured vs. Un-structured
- FEM vs. Finite Volume
- Node-centered vs. Cell-centered
- Monolithic vs. Operator Split
- Compressible vs. (acoustically) Incompressible
- Explicit vs. Implicit



#### An Informal Survey....

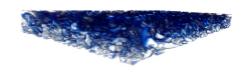
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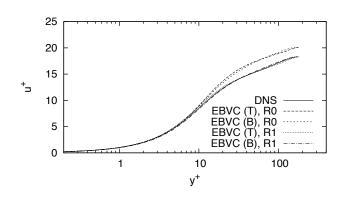
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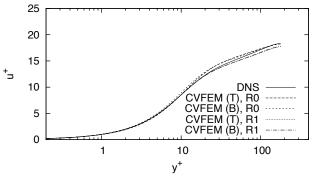
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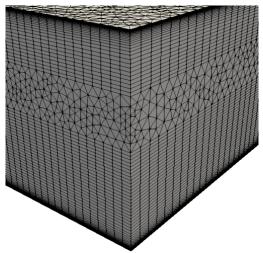
## **Hybrid Meshes, Even for LES!**



- Hybrid mesh study based on Ham and Iaccarino, CTR Annual Brief, 2006, found that simulations were extremely sensitive to mesh topology
- Non-symmetric time mean flow found for cell-centered; better for the CTR node-centered formulation
- Native CVFEM and EBVC are both symmetric in mean quantities







Domino, et. al, "The suitability of hybrid meshes for low-Mach large-eddy simulation" Stanford CTR Summer Program, 2018

## **Recent Generalized Unstructured Findings**

• Domino, et. al, "An assessment of atypical mesh topologies for low-Mach large-eddy simulation", Comput. Fluids (2019)

