Homework 2

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- Reasoning and work must be shown to gain partial/full credit
- Please include the cover-page on your homework PDF with your name and student ID. Failure of doing so is considered bad citizenship.

In this homework, you are going to run a power flow simulation and estimate the state of a synthetic power test case, the IEEE-118 system. The IEEE 118-bus test case represents a simple approximation of the American Electric Power transmission system (in the U.S. Midwest). This test case is widely used for research purposes and you may find plenty of information online¹. All the data you need to run these studies is provided to you in the datasets folder that contains the following

- 1. branches_ieee118_subset.csv. This file contains information about the edges of the IEEE-118 network. The file contains the following features.
 - fbus: The "from" bus ID
 - tbus" The "to" bus ID
 - r: The resistance in p.u.
 - x: The reactance in p.u.
 - ratio: transformer off nominal turns ratio
- 2. buses_ieee118_subset.csv. This file contains information about the nodes of the IEEE-118 network. The file contains the following features.
 - bus_i: ID of the bus
 - Pd: Real power demand in MW
 - Vm: Voltage magnitude in p.u.
 - Va: Voltage angle in degrees
 - baseKV: base voltage in kV
- 3. generators_ieee118_subset.csv. This file contains information about the nodes of the IEEE-118 network. The file contains the following features.
 - bus: ID of the bus that the generator is connected to
 - Pg: Real power output in MW
 - mBase: Total MVA base of machine

¹https://icseg.iti.illinois.edu/ieee-118-bus-system/

- 1. (1–4 points) **DC Power Flow**: In this problem, we are going to use the DC approximation to model the flow of electricity through transmission lines. Power networks can be denoted as a graph $\mathcal{G} := \{\mathcal{V}, \mathcal{E}\}$ where \mathcal{V} is the set of nodes and \mathcal{E} is the set of edges. Each edge $e := \{i, j\} \in \mathcal{E}$ connects two buses $i, j \in \mathcal{V}$. Also, $N := |\mathcal{V}|$ denotes the number of buses and $E := |\mathcal{E}|$ is the number of deges (the operator |.| denotes the cardinality of a set). The DC model works under the following assumptions
 - Voltage magnitudes are 1 p.u., $\forall i \in \mathcal{V}$
 - Voltage angle differences between two buses $i, j \in \mathcal{V}$ are small, thus $\sin(\theta_i \theta_j) \approx \theta_i \theta_j$
 - The resistance of the line is neglected, i.e. $r_e \ll x_e, \forall e \in \mathcal{E}$

The DC power flow can be expressed by the following equation

$$\mathbf{p} = \mathbf{B}\boldsymbol{\theta},\tag{1}$$

where $\mathbf{p} \in \mathbb{R}^N$ is the vector of net power injections, i.e. $\mathbf{p} := \mathbf{p}_{\text{inj}} - \mathbf{p}_{\text{d}}$ where \mathbf{p}_{inj} is the power injected by the generators and \mathbf{p}_{d} is the power demand (from the loads). Also, $\mathbf{B} \in \mathbb{R}^{N \times N}$ is the susceptance matrix and $\boldsymbol{\theta} \in \mathbb{R}^N$ is the vector of bus angles. In the DC power flow problem, all the decisions regarding the setpoints of the generators or the loads that will be served have been made, i.e. \mathbf{p} is given. In addition, voltage magnitudes are 1 p.u. by definition. Thus, the state of your system and your variable of interest is $\boldsymbol{\theta}$.

(a) (0.25 pts) What are you trying to calculate when solving a DC power flow problem?

Solution: We are trying to calculate the vector of voltage angles θ when solving a DC power flow problem which is our variable of interest. Calculating the voltage angles across all buses we can accurately calculate the power flow and losses across transmission lines.

(b) (0.5 pts) Calculate the directed incidence matrix $\mathbf{M} \in \{-1,0,1\}^{E \times N}$ of the graph \mathcal{G} defined by the edges provided in $branches_ieee118_subset.csv$ (Note: Even though power can flow on either direction of an edge, \mathbf{M} is the incidence matrix of a directed graph.)

```
In [1]:
       2 # Incidence Matrix Calculation
       3 import numpy as np
       4 import pandas as pd
       5 branches = pd.read_csv('/kaggle/input/energy-systems-hw2/
             datasets/branches_ieee118_subset.csv')
       6 buses = pd.read_csv('/kaggle/input/energy-systems-hw2/datasets/
             buses_ieee118_subset.csv')
       7 generators = pd.read_csv('/kaggle/input/energy-systems-hw2/
             datasets/generators_ieee118_subset.csv')
       9 E = len(branches['fbus'])
       10 N = max(branches['tbus'])
       11 M = [[O for _ in range(N)] for _ in range(E)]
       12 fbus = list(branches['fbus'])
      tbus = list(branches['tbus'])
      15 for edge_num in range(E):
            node1 = fbus[edge_num]
             node2 = tbus[edge_num]
             M[edge_num][node1-1] = -1
             M[edge_num][node2-1] = 1
      20 M = np.array(M)
      21 print(M)
```

(c) (0.25 pts) Calculate the vector of susceptances $\mathbf{b} \in \mathbb{R}^E$. Each entry $b_e, \forall e \in \mathcal{E}$ in \mathbf{b} can be obtained as follows

$$b_e := \frac{1}{\tau_e x_e} \tag{2}$$

where τ_e are the transformer turn ratios, and x_e is the reactance of the line in p.u.

```
In [2]:
    # b_e calculation
    stransformer_turn_ratios = list(branches['ratio'])
    reactance = list(branches['x'])
    susceptances = [0 for _ in range(E)]

for edge_num in range(E):
    susceptances[edge_num] = 1/(transformer_turn_ratios[
        edge_num]*reactance[edge_num])
    b = np.array(susceptances)

print(b)
```

```
Out[2]:
            10.01001001
                          23.58490566 125.31328321
                                                        9.25925926
                                                                     18.51851852
            48.07692308
                          32.78688525
                                        38.02353657
                                                       31.05590062
                                                                     14.53488372
        4
                                                                     29.41176471
            14.6627566
                           51.02040816
                                         16.23376623
                                                        6.25
            13.67989056
                           14.14427157
                                         4.09165303
                                                        5.12820513
                                                                     11.99040767
            22.88329519
                           5.55247085
                                         19.8019802
                                                       20.28397566
                                                                      8.54700855
            25.38071066
                          11.77856302
                                         10.30927835
                                                        6.28930818
                                                                     20.32520325
        8
            12.5
                           27.26876091
                                         6.13496933
                                                       11.69590643
                                                                     10.60445387
                                                                     30.21148036
            26.84707904
                          19.84126984
                                         11.62790698
                                                        6.39795266
             8.67302689
                           10.15228426
                                         13.24503311
                                                        8.03858521
                                                                      4.048583
        12
            98.03921569
                           20.12072435
                                         7.04225352
                                                       37.31343284 106.38297872
        13
            28.52049911
                           9.43396226
                                         5.95238095
                                                       18.51851852
                                                                     16.52892562
            20.5338809
                           5.46448087
                                         7.40740741
                                                        4.07497963
                                                                      5.94883998
        14
            11.09877913
                           7.37463127
                                         7.87401575
                                                        5.29100529
                                                                     16.
             3.09597523
                           3.09597523
                                         5.37634409
                                                       19.8019802
                                                                     13.29787234
             7.29927007
                           17.00680272
                                         6.11620795
                                                        8.19672131
                                                                      3.46020761
        17
             3.43642612
                           14.14427157 104.71204188
                                                       66.22516556
                                                                     10.35196687
        18
             7.46268657
                           10.35196687
                                         13.90820584
                                                        4.361099
                                                                      3.98406375
        19
                                                        6.6666667
             4.18410042
                           4.6339203
                                         6.89655172
                                                                     74.07407407
        20
                          26.59574468
                                         26.98618307
                                                                     37.8816577
            17.82531194
                                                       50.
        21
                                                       10.88139282
            10.14198783
                          33.11258278
                                         10.88139282
                                                                      4.58715596
        23
             8.54700855
                          28.90591126
                                         9.85221675
                                                       62.5
                                                                      3.59971202
             3.08641975
                          28.90591126
                                         7.87401575
                                                        2.43013366
                                                                     28.16901408
        24
             5.10204082
                           5.5555556
                                         22.02643172
                                                        7.55857899
                                                                      7.09219858
             8.19672131
                          24.63054187
                                         6.75675676
                                                        9.9009901
                                                                      5.00250125
        26
                                                                     14.20454545
            80.64516129
                          40.98360656
                                         20.6185567
                                                        9.52380952
        28
            49.5049505
                           28.90591126
                                         11.72332943
                                                       27.2851296
                                                                      7.57575758
             6.75675676
                          15.60062402
                                         8.1300813
                                                        4.82160077
                                                                      9.80392157
        29
             5.78034682
                          14.04494382
                                         5.31914894
                                                       10.03009027
                                                                     11.96172249
        30
            19.8019802
                           6.32511069
                                         7.86163522
                                                       11.79245283
                                                                      6.32911392
        31
            13.66120219
                          23.04147465
                                         5.49450549
                                                       18.86792453
                                                                     11.50747986
            10.70663812
                           9.25925926
                                         4.85436893
                                                        3.38983051
                                                                     17.24137931
        33
            18.28153565
                           11.29943503
                                         5.58659218
                                                       12.300123
                                                                      7.92393027
        34
        35
            17.88908766
                           8.92857143
                                        19.04761905
                                                        4.90196078
                                                                      6.31313131
             6.15384615
                           4.36681223
                                        26.45502646
                                                       18.28153565
                                                                      5.46448087
        36
            14.22475107
                           5.46448087
                                        34.7222222
                                                        5.5157198
                                                                     13.12335958
        37
            13.24503311
                          15.625
                                         33.22259136
                                                        4.92610837
                                                                     16.33986928
        38
        39
            13.49527665
                          96.15384615 246.91358025
                                                        7.14285714
                                                                     20.79002079
            18.38235294]
        40
```

(d) (0.5 pts) Calculate the susceptance matrix $\mathbf{B} := \mathbf{M}^{\mathsf{T}} \operatorname{diag}(\mathbf{b}) \mathbf{M}$. (Note: \mathbf{B} is a weighted laplacian matrix where the weights are the susceptances of the lines)

```
Out[3]: 1
        3 [[ 33.59491567 -10.01001001 -23.58490566 ...
                                                                            0.
                                                             0.
              0.
            [-10.01001001 26.24377624
                                                                            0.
                                           0.
                                                             0.
            [-23.58490566
                                          39.09416492 ...
                                                             0.
                                                                            0.
                            0.
              0.
           [ 0.
                             0.
                                           0.
                                                       ... 246.91358025
                                                                            0.
        10
                         ]
              0.
        11
           [ 0.
                             0.
                                           0.
                                                             0.
        12
              7.14285714
              0.
        13
            [ 0.
                                                                            0.
                                           0.
                                                             0.
             39.17237373]]
```

(e) (0.25 pts) Now, change the direction of the edge you assumed in part (b). Do the results change? Comment your results.

Out[4]: 1 True

(f) (0.25 pts) Calculate the condition number of the matrix **B**. What do you observe? Does this have any implications when solving Eq. (1)? Comment your results.

```
In [5]:
    #Calculating the condition number of B
    #The condition number seems to be approaching infinity which
        indicates to us that the matrix B is non-invertible since
        cond(B) = norm(B)*norm(inv(B))

#What this means is that solving equation (1) would not be
        possible since B is non-invertible and we would not be able
        to calculate inv(B)*p

5 condition_number = np.linalg.cond(B)
6 condition_number
```

Out[5]: 1 8.251707700206938e+17

(g) (**0.5 pts**) Calculate the vector of net power injections **p**. (**Note**: To match the per unit system used for the reactance and the voltage, you must divide the quantities in MWs by 100. See below²)

²https://en.wikipedia.org/wiki/Per-unit_system

```
Out[6]: 1
        2 array([-5.1000e-01, -2.0000e-01, -3.9000e-01, -3.9000e-01,
              0.0000e+00,
                 -5.2000e-01, -1.9000e-01, -2.8000e-01, 0.0000e+00,
        3
             4.5000e+02,
                 -7.0000e-01, 8.4530e+01, -3.4000e-01, -1.4000e-01,
              -9.0000e-01,
                 -2.5000e-01, -1.1000e-01, -6.0000e-01, -4.5000e-01,
             -1.8000e-01,
                 -1.4000e-01, -1.0000e-01, -7.0000e-02, -1.3000e-01,
             2.2000e+02,
                  3.1400e+02, -7.1000e-01, -1.7000e-01, -2.4000e-01,
             0.0000e+00,
                  6.5700e+00, -5.9000e-01, -2.3000e-01, -5.9000e-01,
              -3.3000e-01,
                 -3.1000e-01, 0.0000e+00, 0.0000e+00, -2.7000e-01,
        9
              -6.6000e-01,
                 -3.7000e-01, -9.6000e-01, -1.8000e-01, -1.6000e-01,
       10
              -5.3000e-01,
                  1.8720e+01, -3.4000e-01, -2.0000e-01, 2.0313e+02,
       11
              -1.7000e-01,
                 -1.7000e-01, -1.8000e-01, -2.3000e-01, 4.6870e+01,
              -6.3000e-01,
                 -8.4000e-01, -1.2000e-01, -1.2000e-01, 1.5223e+02,
       13
              -7.8000e-01,
                  1.6000e+02, -7.7000e-01, 0.0000e+00, 0.0000e+00,
       14
             3.9100e+02,
                  3.9161e+02, -2.8000e-01, 0.0000e+00, 5.1640e+02,
              -6.6000e-01,
                  0.0000e+00, -1.2000e-01, -6.0000e-02, -6.8000e-01,
              -4.7000e-01,
                 -6.8000e-01, -6.1000e-01, -7.1000e-01, -3.9000e-01,
       17
             4.7570e+02,
                  0.0000e+00, -5.4000e-01, -2.0000e-01, -1.1000e-01,
       18
              -2.4000e-01,
                 -2.1000e-01, 4.0000e+00, -4.8000e-01, 6.0700e+02,
       19
              -1.6300e+00,
                 -1.0000e-01, -6.5000e-01, -1.2000e-01, -3.0000e-01,
       20
              -4.2000e-01,
                 -3.8000e-01, -1.5000e-01, -3.4000e-01, -4.2000e-01,
       21
             2.5163e+02,
                 -2.2000e-01, -5.0000e-02, 3.9770e+01, -3.8000e-01,
              -3.1000e-01,
                 -4.3000e-01, -5.0000e-01, -2.0000e-02, -8.0000e-02,
       23
              -3.9000e-01,
                  3.6000e+01, -6.8000e-01, -6.0000e-02, -8.0000e-02,
       24
              -2.2000e-01,
                 -1.8400e+00, -2.0000e-01, -3.3000e-01])
```

(h) (1 pts) Finally, solve Eq. (1). Since B is non-invertible, you must fix the voltage angle of one of the buses, and use that information to compute your inverse. You should solve

$$\boldsymbol{\theta}' = (\mathbf{B}')^{-1} (\mathbf{p}' - \mathbf{b}_0 \theta_0) \tag{3}$$

where θ' , \mathbf{p}' are the corresponding vectors without the i-th entry, \mathbf{B}' is the susceptance matrix without the i-th row and j-th column, \mathbf{b}_0 is the j-th column of \mathbf{B} without the i-th entry, and θ_0 is the voltage angle at the reference bus. For this problem, we set i = j := 69 (that is, we use Bus ID 69 as the reference bus). The voltage angle at that bus θ_0 can be obtained from the Va column in buses ieee118 subset.csv (**Hint**: $\theta_0 := 30$ degrees but you must use radians. Also, please be careful with 0-indexed lists in Python)

Solution:

```
In [7]:
       2 #Fixing the voltage angle
       3 i = 68
       5 angle_buses = np.array([np.radians(deg) for deg in list(buses['
             Va'])])
       6 theta_0 = angle_buses[i]
       7 p_new = np.concatenate((p[0:i],p[i+1:]), axis=0)
       8 b_0 = np.concatenate((B[:,j][:i], B[:,j][i+1:]), axis=0)
       9 temp = np.concatenate((B[:i], B[i+1:]), axis=0)
       10 B_new = np.concatenate((temp[:,:j], temp[:,j+1:]), axis=1)
       11 theta_prime = np.linalg.inv(B_new) @ (p_new - b_0*theta_0)
       12 print (theta_prime)
Out[7]: 1
         [0.2566869 0.26844121 0.27332208 0.33961817 0.34790097 0.30082574
          0.29350907 0.43667087 0.57392087 0.71882087 0.29503963 0.28800911
          0.26840658 0.27394613 0.26245856 0.28032816 0.30876636 0.26773569
          0.25726001 0.2698412 0.29425262 0.33572317 0.41960067 0.40919044
          0.55518049 0.58775332 0.32804443 0.29987361 0.28483434 0.39410028
          0.28749945 0.31748798 0.24865268 0.25677521 0.24875968 0.24867906
          0.26555355 0.35060505 0.20528037 0.18721417 0.17803056 0.20252293
          0.24942367 0.28286356 0.30955721 0.35539118 0.39125132 0.38291815
                               0.31407454 0.29759914 0.28121742 0.29705376
          0.40037323 0.362064
          0.29222229 0.29538314 0.3165802 0.30115243 0.36825617 0.43146208
          0.44664503 0.43658062 0.42456645 0.45495844 0.51036111 0.51554751
```

0.46364692 0.50067874 0.40639826 0.40266383 0.39452869 0.39993983 0.38499066 0.40602914 0.38687334 0.4827733 0.47751049 0.48447862

0.56663942 0.57493542 0.64356992 0.71685042 0.60890113 0.606649 0.6159423 0.56396844 0.52788821 0.50774216 0.50532471 0.51150593 0.50699993 0.50348329 0.52635933 0.54775024 0.59137425 0.46659136 0.41610579 0.39799277 0.39328652 0.34988965 0.38094997 0.37454399 0.36369085 0.39087085 0.32017085 0.30831978 0.31223513 0.31217449

0.56040044 0.58754942

(i) (0.5 pts) Install the python package pandapower and run a DC and AC power flow. Run the code below and compare your results. You should make a scatter plot where you compare the solution you obtained for θ to the DC and AC results you obtained from pandapower. Do they match? You should provide the Mean Absolute Percent Error of the voltage angle and voltage magnitude (Note: The DC solutions should match. Hint: The voltage magnitude of the DC solution is 1 p.u. by definition)

0.5320394 0.51223974 0.49787969 0.519013

0.49322674 0.26000911 0.38861562]

```
In [9]:
       1 !pip install pandapower
       2 import pandapower
       3 import pandapower.networks
       4 theta_powerflow = np.insert(theta_prime,68,theta_0)
       5 net_dc = pandapower.networks.case118()
       pandapower.rundcpp(net_dc)
       7 net_ac = pandapower.networks.case118()
       8 pandapower.runpp(net_ac)
       9 df = net_dc.res_bus # DC results
      10 df2 = net_ac.res_bus # AC results
      dc_theta = np.array([np.radians(deg) for deg in df['va_degree'
            11)
       ac_theta = np.array([np.radians(deg) for deg in df2['va_degree'
            ]])
      14
      15 import matplotlib.pyplot as plt
      fig = plt.figure(figsize=(10,10))
      plt.scatter(theta_powerflow, dc_theta)
      18 plt.title('Comparison of Voltage Angles Power Flow vs DC')
      19 plt.xlabel('Voltage Angle Power Flow (Radians)')
      20 plt.ylabel('Voltage Angle DC (Radians)')
      21 fig.savefig('scatter_plot_voltage_angle_powerflow_vs_dc.png')
      22 plt.show()
```

```
In [10]:
    fig = plt.figure(figsize=(10,10))
    plt.scatter(theta_powerflow, ac_theta, color='r')
    plt.title('Comparison of Voltage Angles for Power Flow vs AC')
    plt.xlabel('Voltage Angle Power Flow (Radians)')
    plt.ylabel('Voltage Angle AC (Radians)')
    fig.savefig('scatter_plot_voltage_angle_powerflow_vs_ac.png')
    plt.show()
```

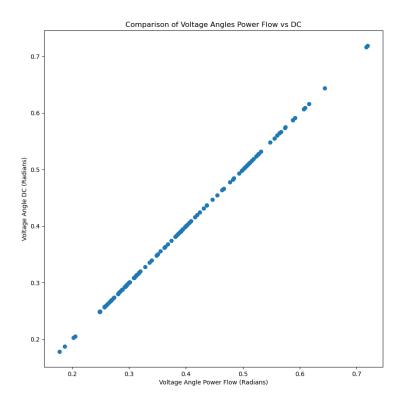


Figure 1: Comparison of Voltage Angles DC vs Power Flow

```
Out[11]: 1
2 Mean Absolute Percentage Error for Voltage Magnitudes for DC vs
Power Flow is 2.277118644067797%
3 Mean Absolute Percentage Error for Voltage Magnitudes for AC vs
Power Flow is 0.05366115320849697%
```

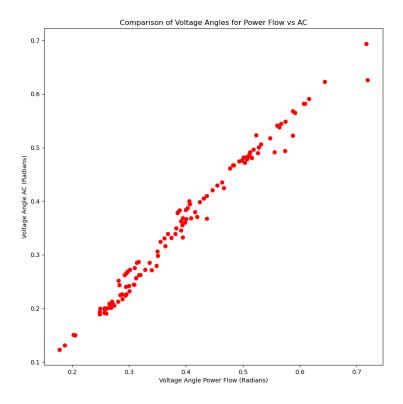


Figure 2: Comparison of Voltage Angles AC vs Power Flow

```
In [12]:
    #Mean Absolute Percentage Error for Voltage Angles
    mape_va_dc = np.mean(np.abs(dc_theta-theta_powerflow)/dc_theta)
        *100

4 print(f'Mean Absolute Percentage Error for Voltage Angles for
        DC vs Power Flow is {mape_va_dc}%')

5
6 mape_va_ac = np.mean(np.abs(ac_theta-theta_powerflow)/ac_theta)
        *100
7 print(f'Mean Absolute Percentage Error for Voltage Angles for
        AC vs Power Flow is {mape_va_ac}%')
```

```
Out[12]: 1

2 Mean Absolute Percentage Error for Voltage Angles for DC vs Power
Flow is 0.0033763106551810453%

3 Mean Absolute Percentage Error for Voltage Angles for AC vs Power
Flow is 14.777733670273927%
```

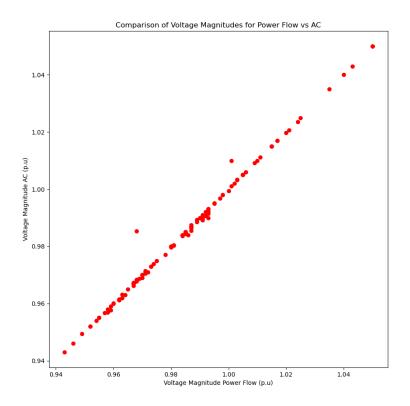


Figure 3: Comparison of Voltage Magnitudes AC vs Power Flow

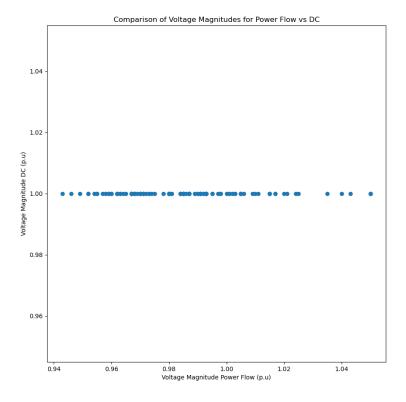


Figure 4: Comparison of Voltage Magnitudes DC vs Power Flow

- 2. (1–4 points) **DC** state estimation: The power flow problem that you solved in Problem 1 is an integral part of any power market mechanism in North America. It is used to understand how the flows of electricity will be distributed throughout the network. The power flow problem (and in the particular the DC power flow model) is used by market operators for multiple applications, e.g. to dispatch generation (a.k.a. economic dispatch), to run contingency analysis (to ensure that the system can sail through any unplanned event), or for long-term planning (to understand how congestion in the lines may impact future flows in a specific area). In real-time operations, running a power flow is not possible. Instead, the market operator monitors the conditions of the system (in a subset of nodes) and estimates the state of the system (i.e., the voltages), which is the goal of this problem. DC state estimation is similar to other estimation problems you may have seen in your detection and estimation theory course (e.g. Maximum Likelihood Estimation). Usually, in DC state estimation, the quantities that are measured are the following
 - 1. Voltage magnitude and angle
 - 2. Active and reactive power flows at the "from" and "to" bus, i.e. on both sides of the line.
 - 3. Currents at the "from" and "to" bus
 - 4. Power injections at the generator buses

In this problem, we will only use active power flows at the "from" and "to" bus (See Fig. 5 for reference). Thus, we should have models of the form.

$$\mathbf{w}_{m} = \mathbf{p}_{ij} + \boldsymbol{\epsilon}_{w}, \quad \boldsymbol{\epsilon}_{w} \sim \mathcal{N}\left(0, \boldsymbol{\Sigma}_{w}\right) \tag{4}$$

$$\mathbf{w}_{m}' = \mathbf{p}_{ji} + \boldsymbol{\epsilon}_{w'}, \quad \boldsymbol{\epsilon}_{w'} \sim \mathcal{N}\left(0, \boldsymbol{\Sigma}_{w'}\right)$$
 (5)

where \mathbf{w}_m , \mathbf{w}'_m are the measurements of the power flow at the "from" and "to" nodes, respectively, \mathbf{p}_{ij} and \mathbf{p}_{ji} are the power flows at the "from" and "to" node, and ϵ_w , $\epsilon_{w'}$ are the vectors of noise. Noise is assumed to be Gaussian i.i.d. (i.e. independent and identically distributed)

(a) (0.25 pts) What are you trying to estimate when solving a DC state estimation?

Solution: The DC state estimation allows us to come up with an estimate for our variables of interest θ with the help of certain measurements of power flow at the "from" and "to" node. DC state estimation is important due to the inability to solve the DC Power Flow equations in the time required to respond to the demands of the market.

(b) (0.5 pts) Using Eq. (1), derive a linear expression for \mathbf{p}_{ij} and \mathbf{p}_{ji} as a function of $\boldsymbol{\theta}$ and calculate the numerical values using the $\boldsymbol{\theta}$ from Problem 1. (**Hint**: $[\mathbf{p}_{ij}]_e = b_e (\theta_i - \theta_j)$ and $[\mathbf{p}_{ji}]_e = b_e (\theta_j - \theta_i)$. $[\mathbf{p}_{ij}]_e$ denotes the *e*-th entry of vector \mathbf{p}_{ij} . You need to use \mathbf{M} to express the equations in matrix-vector form.)

$$\stackrel{i \xrightarrow{p_{ij}}}{\longrightarrow} \stackrel{p_{ji} \ j}{\longleftarrow}$$

Figure 5: Edge variables. The scalar p_{ij} denotes the power flow going from bus i to bus j. Similarly, p_{ji} denotes the power flow going from bus j to bus i

$$\mathbf{p_{ij}} = \mathbf{diag}(\mathbf{b})\mathbf{M}\boldsymbol{\theta}$$

$$p_{ii} = -diag(b)M\theta$$

```
In [15]:
1  p_ij = np.diag(b) @ M @ theta_powerflow
2  p_ij
```

```
Out[15]: 1 array([-1.17660783e-01, -3.92339217e-01, -1.03794398e+00,
             -6.90545256e-01,
                 8.71763363e-01, 3.51763363e-01, -4.50000000e+00,
             3.37534555e+00,-4.50000000e+00, 6.47943985e-01,
             7.75092949e-01, 3.58699730e-01, -3.17660783e-01,
             -9.17939609e-02, 1.61763363e-01, 3.64337204e-01,
             1.98910605e-01, 2.43372042e-02, 5.89106046e-02,
             9.20977434e-02, -1.05967488e+00, -1.57902257e-01,
             8.12488401e-01, 2.12488401e-01, -1.07531467e-01,
             1.31942898e-01, -2.87531467e-01, -4.27531467e-01,
             -5.27531467e-01, 2.11590174e-01, -1.69474774e+00,
             8.88220538e-01, 1.39347280e+00, 3.29483217e-01,
             1.59483217e-01, 2.29096664e+00, 8.44654448e-01,
             2.25177946e+00, 1.36064665e-01, -8.05167828e-02,
             8.85626102e-01, -3.04452118e-01, 1.39820441e-01,
             1.10979791e-01, 1.96276648e-03, 7.90469756e-03,
             -3.37904698e-01, -1.19020209e-01, 3.02095302e-01,
             -9.33865668e-01, 2.42571127e+00, 5.68614878e-01,
                 4.66305817e-01, 8.05467269e-01, 2.98614878e-01,
        3
             1.88575094e-01, -8.36543998e-02, -1.81424906e-01,
             -1.36266868e-01, 4.37331319e-02, -2.96266868e-01,
             -3.38008651e-01, -2.82363327e-01, -1.45645325e-01,
                -1.45950604e-01, -6.12539653e-01, -6.12539653e-01,
             -4.88258217e-01, -3.45645325e-01, 5.09431313e-01,
             6.29917449e-01, 2.80193979e-01, 1.00193979e-01,
             -1.29806021e-01, 3.57506842e-01, 3.55049750e-01
                  6.83375339e-02, 1.74933827e-01, -2.09327523e-01,
        5
             -2.19431313e-01, 3.39431313e-01, -5.97234709e-02,
             1.79723471e-01, -3.10520789e-01, -2.90330817e-01,
             -3.04908096e-01, -3.52334943e-01, -4.35902783e-01,
             -5.22592371e-01, -1.12466311e+00, -9.12396717e-02,
             2.67670384e-01, 1.51959949e+00, -1.51959949e+00,
             3.14925866e-01, -1.62024400e+00,
                -1.83452536e+00, -1.25325653e+00, -1.25325653e+00,
        6
             -3.62233424e-01,
                 8.60374373e-02, 2.62858601e-01, 2.42429643e-01,
             2.37141399e-01,
                 2.22429643e-01, 5.67570357e-01, 1.42429643e-01,
        9
             -3.6000000e-01,
                 6.80000000e-01, 1.48364371e-02, 4.51635629e-02,
             8.58308627e-02,
                 2.14169137e-01, 5.83086265e-03, 1.84000000e+00,
             2.00000000e-01,
                 3.62027270e-01, -3.20272698e-02])
```

```
In [16]:
    p_ij = - np.diag(b) @ M @ theta_powerflow
    p_ij
```

```
Out[16]: 1 array([ 1.17660783e-01,  3.92339217e-01,  1.03794398e+00,
             6.90545256e-01,
                 -8.71763363e-01, -3.51763363e-01, 4.50000000e+00,
        2
             -3.37534555e+00,
                 4.50000000e+00, -6.47943985e-01, -7.75092949e-01,
        3
             -3.58699730e-01,
                 3.17660783e-01, 9.17939609e-02, -1.61763363e-01,
             -3.64337204e-01,
                -1.98910605e-01, -2.43372042e-02, -5.89106046e-02,
        5
             -9.20977434e-02,
                  1.05967488e+00, 1.57902257e-01, -8.12488401e-01,
        6
             -2.12488401e-01,
                 1.07531467e-01, -1.31942898e-01, 2.87531467e-01,
             4.27531467e-01.
                 5.27531467e-01, -2.11590174e-01, 1.69474774e+00,
             -8.88220538e-01,
                -1.39347280e+00, -3.29483217e-01, -1.59483217e-01,
        9
             -2.29096664e+00,
                 -8.44654448e-01, -2.25177946e+00, -1.36064665e-01,
       10
             8.05167828e-02,
                -8.85626102e-01, 3.04452118e-01, -1.39820441e-01,
             -1.10979791e-01,
                -1.96276648e-03, -7.90469756e-03, 3.37904698e-01,
       12
             1.19020209e-01,
                -3.02095302e-01, 9.33865668e-01, -2.42571127e+00,
             -5.68614878e-01,
                -4.66305817e-01, -8.05467269e-01, -2.98614878e-01,
       14
             -1.88575094e-01,
                 8.36543998e-02, 1.81424906e-01, 1.36266868e-01,
             -4.37331319e-02,
                  2.96266868e-01, 3.38008651e-01, 2.82363327e-01,
       16
             1.45645325e-01,
                 1.45950604e-01, 6.12539653e-01, 6.12539653e-01,
       17
             4.88258217e-01,
                 3.45645325e-01, -5.09431313e-01, -6.29917449e-01,
       18
             -2.80193979e-01,
                 -1.00193979e-01, 1.29806021e-01, -3.57506842e-01,
             -3.55049750e-01,
                -6.83375339e-02, -1.74933827e-01, 2.09327523e-01,
       20
             2.19431313e-01,
                 -3.39431313e-01, 5.97234709e-02, -1.79723471e-01,
       21
             3.10520789e-01,
                 2.90330817e-01, 3.04908096e-01, 3.52334943e-01,
             4.35902783e-01,
                  5.22592371e-01, 1.12466311e+00, 9.12396717e-02,
             -2.67670384e-01,
                -1.51959949e+00, 1.51959949e+00, -3.14925866e-01,
             1.62024400e+00,
                 1.83452536e+00, 1.25325653e+00, 1.25325653e+00,
       25
             3.62233424e-01,
       26 . . .
                 -8.60374373e-02, -2.62858601e-01, -2.42429643e-01,
             -2.37141399e-01,
                  -2.22429643e-01, -5.67570357e-01, -1.42429643e-01,
             3.6000000e-01,
                  -6.80000000e-01, -1.48364371e-02, -4.51635629e-02,
       29
             -8.58308627e-02,
                 -2.14169137e-01, -5.83086265e-03, -1.84000000e+00,
             -2.00000000e-01,
```

-3.62027270e-01, 3.20272698e-02])

(c) (0.5 pts) Using the expression you obtained in part (b), and stacking Eqs. (4),(5), you may arrive at an expression like the following

$$\mathbf{w} = \mathbf{H}\boldsymbol{\theta} + \boldsymbol{\epsilon} \tag{6}$$

where $\mathbf{w} := [\mathbf{w}_m^\intercal, (\mathbf{w}_m')^\intercal]^\intercal$ and $\boldsymbol{\epsilon} := [\boldsymbol{\epsilon}_w^\intercal, \boldsymbol{\epsilon}_{w'}^\intercal]^\intercal$. Provide an expression for \mathbf{H}

Solution:

$$\mathbf{w} = \begin{pmatrix} \mathbf{w}_m \\ \mathbf{w}_m' \end{pmatrix} = \begin{pmatrix} \mathbf{p}_{ij} \\ \mathbf{p}_{ji} \end{pmatrix} \theta + \epsilon = \begin{pmatrix} diag(b) \times \mathbf{M} \\ -diag(b) \times \mathbf{M} \end{pmatrix} \boldsymbol{\theta} + \epsilon$$
 (7)

Therefore, we can conclude that

$$\mathbf{H} = \begin{pmatrix} diag(b) \times \mathbf{M} \\ -diag(b) \times \mathbf{M} \end{pmatrix}$$
 (8)

Thus we obtain H which is a (372,118) matrix

```
Out[17]: 1
        2 array([[-10.01001001, 10.01001001,
                                                                      0.
                    0. ,
                 [-23.58490566,
                                                 23.58490566, ...,
                                             ],
                                                  0.
                                             ],
        9
                   -7.14285714,
       11
                                 -20.79002079],
       12
       13
                                 -18.38235294]])
```

(d) (1 pts) Using Eq. (6), formulate a weighted least squares and provide a closed-form solution in matrix-vector form to calculate $\hat{\boldsymbol{\theta}}$. (Hint: Use the Maximum Likelihood Estimate.)

We are provided with the measurement -

$$\mathbf{w} = \mathbf{H}\boldsymbol{\theta} + \boldsymbol{\epsilon}, \quad \boldsymbol{\epsilon} \sim \mathbf{N}(\mathbf{0}, \mathbf{I}\boldsymbol{\sigma^2})$$

We make use of MLE to minimize the Gaussian noise. Maximum Likelihood estimation on PMU measurements yields an unconstrained convex quadratic Weighted Least Squares fit:

$$\hat{\boldsymbol{\theta}} = \arg\min_{\boldsymbol{\theta}} ||\mathbf{w} - \mathbf{H}\boldsymbol{\theta}||_2^2 \tag{9}$$

Which provides us with the following closed form solution in matrix-vector form:

$$\hat{\boldsymbol{\theta}} = (\mathbf{H}^{\mathbf{T}}\mathbf{H})^{-1}\mathbf{H}^{\mathbf{T}}\mathbf{w} \tag{10}$$

(e) (0.5 pts) Generate synthetic measurements by adding Gaussian noise ($\sigma^2 := 0.01$) to the power flow values you calculated in part(b). We will use these values as a proxy to model $\mathbf{w}_m, \mathbf{w}'_m$. However, in the real-world, these measurements would come from sensors.

```
In [18]:
        np.random.seed(42)
        2 epsilon_w = np.random.normal(0,0.1,186)
        g epsilon_w_prime = np.random.normal(0,0.1,186)
        4 \text{ w_m} = \text{p_ij} + \text{epsilon_w}
        5 w_m_prime = p_ji + epsilon_w_prime
        6 w = np.concatenate((w_m.T,w_m_prime.T), axis=0).T
        7 \text{ np.round}(w,3)
Out[18]: 1
         array([-6.800e-02, -4.060e-01, -9.730e-01, -5.380e-01,
        2
                  3.280e-01, -4.342e+00, 3.452e+00, -4.547e+00, 7.020e-01,
                  7.290e-01, 3.120e-01, -2.930e-01, -2.830e-01, -1.100e-02,
                  3.080e-01,
                             9.800e-02, 5.600e-02, -3.200e-02, -4.900e-02,
                 -9.130e-01, -1.800e-01, 8.190e-01, 7.000e-02, -1.620e-01,
                  1.430e-01, -4.030e-01, -3.900e-01, -5.880e-01, 1.820e-01,
                 -1.755e+00, 1.073e+00, 1.392e+00,
                                                      2.240e-01, 2.420e-01,
                                                      3.000e-03, -6.100e-02,
                  2.169e+00, 8.660e-01, 2.056e+00,
        9
                  9.590e-01, -2.870e-01, 1.280e-01, 8.100e-02, -1.460e-01,
                 -6.400e-02, -3.840e-01, -1.300e-02,
                                                      3.360e-01, -1.110e+00,
       11
                  2.458e+00, 5.300e-01, 3.990e-01, 8.670e-01, 4.020e-01,
       12
                  2.820e-01, -1.680e-01, -2.120e-01, -1.030e-01, 1.410e-01,
       13
                 -3.440e-01, -3.570e-01, -3.930e-01, -2.650e-01, -6.500e-02,
       14
                 -4.770e-01, -6.200e-01, -3.880e-01, -3.090e-01, 4.450e-01,
                                                      2.700e-02, 9.600e-02,
                  6.660e-01, 4.340e-01, 9.700e-02,
                  4.370e-01, 7.700e-02, 1.450e-01, -2.000e-01, -4.180e-01,
       17
                  3.170e-01, -2.400e-02, 3.280e-01, -3.620e-01, -3.710e-01,
       18
                 -3.550e-01, -2.610e-01, -4.030e-01, -5.760e-01, -1.073e+00,
       19
                 -8.200e-02, 3.650e-01, 1.449e+00, -1.552e+00, 2.760e-01,
       20
                 -1.767e+00, -1.805e+00, -1.227e+00, -1.253e+00, -3.860e-01,
       21
                 -3.730e-01, -1.920e-01, 4.770e-01, 5.250e-01, -4.930e-01,
       22
                 -3.400e-01, -4.740e-01, 9.400e-01,
                                                      3.300e-02, 9.800e-02,
                 -1.170e-01, 4.300e-02, 6.600e-02,
                                                     4.080e-01, -1.700e-02,
       24
                  9.940e-01, -5.220e-01, -7.650e-01, 5.180e-01, -3.090e-01,
                  5.040e-01, -3.770e-01, -8.760e-01, -6.090e-01, -6.170e-01,
       26
       27
                 -2.880e-01, -2.750e-01, -4.950e-01, -4.950e-01, -8.800e-02,
       28
                 -3.630e-01, -2.440e-01, -2.660e-01, -1.900e-01, -6.500e-01,
                 -9.000e-02, 5.130e-01, -6.910e-01, 2.500e-02, 2.400e-02,
       30
                 -1.260e-01, -1.920e-01, -5.000e-03, -1.830e+00, -2.770e-01,
       31
                 -3.600e-01, 8.200e-02])
```

(f) (0.75 pts) Using w from part (e), the H you obtained from (c) and the expression you derived in (d), provide the estimate for $\hat{\theta}$. Plot your results, and compare them to the

real values you previously calculated (before adding noise). How good is your estimate?

6 fig.savefig('voltage_angle_comparison_powerflow_vs_estimate.png

4 plt.ylabel('Voltage Angles DC')
5 plt.title('Voltage Angle Comparison')

')
7 plt.show()

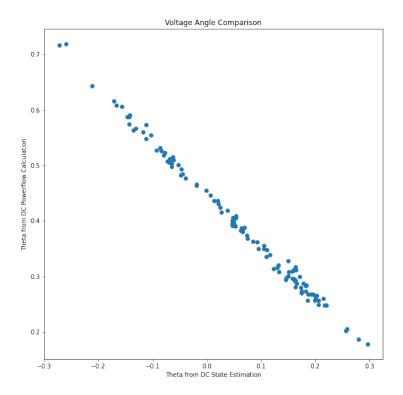


Figure 6: Comparison of Voltage Angles from DC State Estimation vs Power Flow

```
In [21]:
    fig = plt.figure(figsize=(10,10))
    plt.scatter(theta_cap, dc_theta, color='r')
    plt.xlabel('Theta from DC State Estimation')
    plt.ylabel('Voltage Angles DC (Radians)')
    plt.title('Voltage Angle Comparison')
    fig.savefig('theta_estimate_vs_dc_voltage_angles.png')
    plt.show()
```

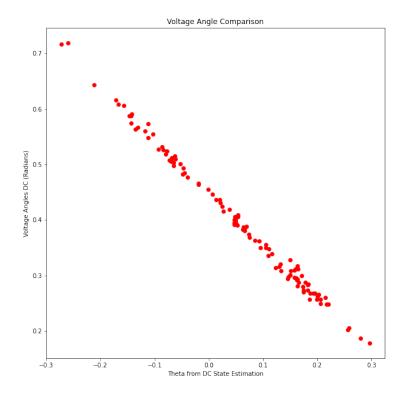


Figure 7: Comparison of Voltage Angles from State Estimation vs DC

```
In [22]:
1  fig = plt.figure(figsize=(10,10))
2  plt.scatter(theta_cap, ac_theta, color='g')
3  plt.xlabel('Theta from DC State Estimation')
4  plt.ylabel('Voltage Angles AC (Radians)')
5  plt.title('Voltage Angle Comparison')
6  fig.savefig('theta_estimate_vs_ac_voltage_angles.png')
7  plt.show()
```

(g) (0.5 pts) In part (f) you used a model with complete information about the system (you had measurements for every single line in the system). Now, select a subset of measurements (any subset) containing 70% of the measurements and repeat part (f). Plot your results and compare them to the results from part (f). Why did your results change? Are they better or worse? Comment your results.

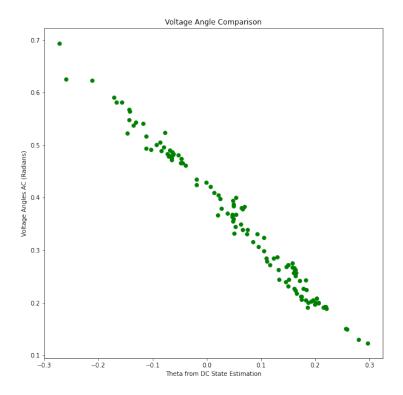


Figure 8: Comparison of Voltage Angles from State Estimation vs AC

Solution:

Out[23]: 1 Mean Absolute Percentage Error between real valued theta vs estimate theta_prime after dropping 30 percent of estimates for powerflow is: 97.65899652776238%

It can be observed that the Mean Absolute Percentage Error between $\boldsymbol{\theta}$ and $\boldsymbol{\dot{\theta}}$ increased from 77.2% to 97.65% after dropping 30% of the measurements. This was to be expected since dropping measurements from \mathbf{H} results in a larger residual value $\mathbf{w} - \mathbf{H}\boldsymbol{\theta}$ due to

which the final estimate for $\hat{\boldsymbol{\theta}}$ is more noisy than the one calculated before resulting in a greater Mean Absolute Percent Error. It can be observed that dropping measurements from \mathbf{H} results in a more noisy \mathbf{w} due to the greater contribution of $\boldsymbol{\epsilon}$ than before, leading to a more noisy estimate of $\hat{\boldsymbol{\theta}}$. Since $\hat{\boldsymbol{\theta}} = (\mathbf{H}^T\mathbf{H})^{-1}\mathbf{H}^T\mathbf{w}$

On calculating the mean absolute residual before and after removing 30% of the measurements we can also observe that the residual $\mathbf{r} = \mathbf{w} - \mathbf{H}\hat{\boldsymbol{\theta}}$ has increased.