

UNIT 2

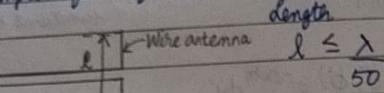
HERZIAN DIPOLE ANTENNA & RADIATION CHARACTERISTICS

30/1/24

Hertzian dipole antenna

• Simplest form of antenna

length.



Area of plot = Idl

The wire antenna is called Hertzian dipole antenna

$$\bar{H} = \frac{1}{\mu} \nabla \times \bar{A}$$

$$dl$$

$$I = I$$

$$\nabla \times \bar{H} = j\omega \epsilon \bar{E} + \bar{J}$$

$$\frac{1}{\mu} \nabla \times \nabla \times \bar{A} = j\omega \epsilon \bar{E} + \bar{J}$$

$$\nabla(\nabla \cdot \bar{A}) - \nabla^2 \bar{A} = \mu(j\omega \epsilon \bar{E} + \bar{J})$$

$$\bar{E} = \frac{1}{j\omega \epsilon \mu} [\nabla(\nabla \cdot \bar{A}) - \nabla^2 \bar{A} - \mu \bar{J}]$$

For an operating frequency of $f = 1 \text{ GHz}$,

$$c = \lambda f \Rightarrow \lambda = \frac{c}{f} = \frac{3 \times 10^8}{1 \times 10^9} = 0.3 \text{ m}$$

$$\lambda = \frac{0.3}{50} = 6 \text{ mm}$$

Length of antenna had to be $\leq 6 \text{ mm}$ to be called a HERTZIAN DIPOLE

$$\int dV' = \int dx' dy' dz'$$

current density

$$= I dz'$$

$$I = I \cos(\omega t)$$

constant phase throughout the

length of the antenna

Replacing $\int dV'$ in \bar{A} expression

$$\bar{A} = \int_{-dl/2}^{dl/2} \mu e^{-jkz} I dz'$$

$$\text{Scalar form } A_z = \int_{-dl/2}^{dl/2} \frac{\mu I}{4\pi r} e^{-jkz} dz'$$

\bar{A} is a vector $\therefore I$ is a scalar

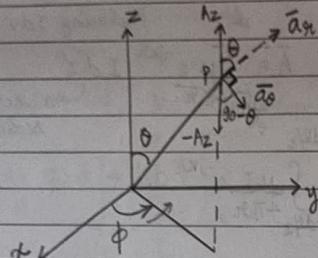
Assume I is constant throughout the length of the antenna
This approximation does not hold good for long antennas (Not constant with time)

$$A_z = \frac{\mu I e^{-jkz}}{4\pi r} \int_{-dl/2}^{dl/2} dz' = \frac{\mu I e^{-jkz}}{4\pi r} \left[\frac{dl}{2} - \left(-\frac{dl}{2} \right) \right]$$

$$= \frac{\mu(I dl)}{4\pi r} e^{-jkz}$$

$$A_z = \frac{\mu(I dl)}{4\pi r} e^{-jkz}$$

$$\bar{H} = \frac{1}{\mu} \nabla \times \bar{A} = \frac{1}{\mu} \times \frac{1}{r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & r\bar{a}\theta & r\sin\theta \bar{a}\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & rA_\theta & r\sin\theta A_\phi \end{vmatrix}$$



$$\begin{aligned} A_r &= A_z \cos\theta \\ A_\theta &= -A_z \cos(\theta - \phi) \\ &= -A_z \sin\phi \\ A_\phi &= A_z \cos 90^\circ = 0 \end{aligned}$$

$$\bar{H} = \frac{1}{\mu} \times \frac{1}{r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & r\bar{a}\theta & r\sin\theta \bar{a}\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_z \cos\theta & (-A_z \sin\theta)r & 0 \end{vmatrix}$$

Dipole is placed
Symmetrical to
z-axis

$$= \frac{1}{\mu r^2 \sin\theta} \times \left[\frac{\partial(-A_z \sin\theta)}{\partial r} - \frac{\partial(A_z \cos\theta)}{\partial \theta} \right] \bar{a}_r \Rightarrow \text{No } \phi \text{ variation}$$

$$\therefore \frac{\partial}{\partial \phi} = 0$$

$$= \frac{1}{\mu} \times \frac{1}{r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & r\bar{a}\theta & r\sin\theta \bar{a}\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & 0 \\ A_z \cos\theta & -rA_z \sin\theta & 0 \end{vmatrix}$$

$$= \frac{1}{\mu r^2 \sin\theta} \times \left\{ \left[\frac{\partial(-rA_z \sin\theta)}{\partial r} - \frac{\partial(rA_z \cos\theta)}{\partial \theta} \right] \bar{a}_r - r\bar{a}\theta \left[\frac{\partial(-A_z \sin\theta)}{\partial r} - 0 \right] \right\} + r\sin\theta \bar{a}\phi \left[\frac{\partial(-rA_z \sin\theta)}{\partial \theta} \right]$$

$$= \frac{1}{\mu r^2 \sin\theta} \left\{ (A_z \sin\theta + A_z \sin\theta) \bar{a}_r + 0 + r\sin\theta (-A_z \sin\theta + A_z \sin\theta) \bar{a}\phi \right\}$$

$$\boxed{H = 0}$$

Dipole is placed symmetrical to z-axis
⇒ No ϕ -variation $\therefore \frac{\partial}{\partial \phi} = 0$

$$\bar{H} = \frac{1}{\mu} \times \frac{1}{r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & r\bar{a}\theta & r\sin\theta \bar{a}\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & 0 \\ A_z \cos\theta & -rA_z \sin\theta & 0 \end{vmatrix}$$

$$= \frac{1}{\mu r^2 \sin\theta} \left\{ \bar{a}_r \left[\frac{\partial(0)}{\partial \theta} + 0 \right] - r\bar{a}\theta \left[\frac{\partial(0)}{\partial r} - 0 \right] \right. \\ \left. + r\sin\theta \bar{a}\phi \left[\frac{\partial(-rA_z \sin\theta)}{\partial r} - \frac{\partial(A_z \cos\theta)}{\partial \theta} \right] \right\}$$

$$= \frac{1}{\mu r^2 \sin\theta} r\sin\theta (-A_z \sin\theta) +$$

$$\bar{H} = -\bar{a}\phi \left[\frac{\partial(rA_z \sin\theta)}{\partial r} - A_z \sin\theta \right]$$

$$= -\bar{a}\phi \sin\theta \left[\frac{\partial(rA_z)}{\partial r} - A_z \right]$$

$$\frac{\partial(rA_z)}{\partial r} = r \frac{\partial A_z}{\partial r} + A_z$$

$$= -\bar{a}\phi \sin\theta \left[r \frac{\partial A_z}{\partial r} + A_z - A_z \right]$$

$$\bar{H} = -\bar{a}\phi \sin\theta \left(r \frac{\partial A_z}{\partial r} \right)$$

$$\frac{\partial A_z}{\partial r} = \frac{1}{2\pi r} \left\{ \frac{\mu I d \ell}{4\pi r} e^{-jk\frac{r}{\lambda}} \right\} = \frac{\mu I d \ell}{4\pi} \left[\frac{\partial}{\partial r} \left(\frac{e^{-jk\frac{r}{\lambda}}}{r} \right) \right]$$

$$\frac{\partial A_z}{\partial r} = \frac{\mu_{\text{Idl}}}{4\pi} \left[\frac{jk(-jk)e^{-jkr}}{r^2} - e^{-jkr} \right]$$

$$\frac{\partial \theta}{\partial r} A_z = -\frac{\mu_{\text{Idl}}}{4\pi} \left[jk + \frac{1}{r^2} \right] e^{-jkr}$$

$$\bar{H} = -\bar{a}\phi \sin\theta \left[-\frac{\mu_{\text{Idl}}}{4\pi} \left(jk + \frac{1}{r^2} \right) e^{-jkr} \right]$$

$$\bar{H} = \bar{a}\phi \sin\theta \left(\frac{\text{Idl}}{4\pi} \right) \left(jk + \frac{1}{r^2} \right) e^{-jkr}$$

2/2/24

To determine electric field \bar{E}

$$\nabla \times \bar{H} = j\omega \epsilon \bar{E} + \bar{J}$$

In the field region $\bar{J} = 0$ 

$$\Rightarrow \nabla \times \bar{H} = j\omega \epsilon \bar{E} \Rightarrow \bar{E} = \frac{1}{j\omega \epsilon} (\nabla \times \bar{H})$$

$$\bar{E} = \frac{1}{j\omega \epsilon} \times \frac{1}{r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ H_r & r H_\theta & r \sin\theta H_\phi \end{vmatrix}$$

 \bar{H} has only \bar{a}_ϕ component $\Rightarrow H_\theta = 0$

$$\Rightarrow H_\theta = 0$$

Source placed symmetrical about z-axis \rightarrow No variation of $\frac{\partial}{\partial \phi} = 0$

$$\bar{E} = \bar{a}_r E_r + \bar{a}_\theta E_\theta$$

$$\bar{E} = \frac{1}{j\omega \epsilon} \times \frac{1}{r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & 0 \\ 0 & 0 & r \sin\theta H_\phi \end{vmatrix}$$

$$\bar{E} = \frac{1}{j\omega \epsilon} \times \frac{1}{r^2 \sin\theta} \left\{ \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} \\ \frac{\partial}{\partial \theta} & 0 \end{vmatrix} (r \sin\theta H_\phi) - \begin{vmatrix} \bar{a}_r & \bar{a}_{\phi} \\ 0 & \frac{\partial}{\partial r} \end{vmatrix} (r \sin\theta H_\phi) \right\}$$

$$E_r = \frac{1}{j\omega \epsilon} \times \frac{1}{r^2 \sin\theta} \frac{\partial}{\partial \theta} (r \sin\theta H_\phi) = \frac{1}{j\omega \epsilon r \sin\theta} \frac{\partial}{\partial \theta} (\sin\theta H_\phi)$$

$$= \frac{1}{j\omega \epsilon r \sin\theta} \left\{ \frac{\partial}{\partial \theta} \left[\frac{\text{Idl} \sin^2 \theta}{4\pi} \left(jk + \frac{1}{r^2} \right) e^{-jkr} \right] \right\}$$

$$= \frac{1}{j\omega \epsilon r \sin\theta} \times \frac{2 \sin\theta \cos\theta}{4\pi} \left(\frac{\text{Idl}}{4\pi} \right) \left(jk + \frac{1}{r^2} \right) e^{-jkr}$$

$$E_r = \frac{\text{Idl} \cos\theta}{j\omega \epsilon 2\pi} \left(jk + \frac{1}{r^2} \right) e^{-jkr}$$

$$E_\theta = \frac{-r}{j\omega \epsilon r^2 \sin\theta} \frac{\partial}{\partial r} (\sin\theta H_\phi)$$

~~$$E_\theta = j\frac{\partial}{\partial r} \frac{1}{r^2 \sin\theta} \left[\frac{\partial}{\partial r} (\sin\theta H_\phi) + \sin\theta H_\phi \right]$$~~

~~$$E_\theta = j\frac{\partial}{\partial r} \left[\frac{1}{r^2 \sin\theta} \left(\frac{\partial}{\partial r} (\sin\theta H_\phi) + \sin\theta H_\phi \right) \right]$$~~

~~$$= j \frac{\partial}{\partial r} \left[\left(\frac{\text{Idl} \sin\theta}{4\pi} \right) \left(jk + \frac{1}{r^2} \right) e^{-jkr} + \frac{r}{4\pi} \text{Idl} \sin\theta \right]$$~~

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Page 58

$$\begin{aligned}
 E_\theta &= \frac{j}{\omega \epsilon r} \sin \theta \left(jk H_\phi \right) \\
 &= \frac{j}{\omega \epsilon r} \frac{\partial}{\partial r} \left(jk H_\phi \right) \\
 &= \frac{j}{\omega \epsilon r} \frac{\partial}{\partial r} \left[I_d l \sin \theta \left(jk + \frac{1}{r} \right) e^{-jkr} \right] \\
 &= \frac{j}{4\pi \omega \epsilon r} \left[jk \frac{\partial}{\partial r} \left(jk + \frac{1}{r} \right) e^{-jkr} + \left(jk + \frac{1}{r} \right) \frac{\partial}{\partial r} e^{-jkr} \right] \\
 &= \frac{j}{4\pi \omega \epsilon r} \left[-\frac{1}{r^2} e^{-jkr} + \left(jk + \frac{1}{r} \right) (-jk) e^{-jkr} \right] \\
 &= \frac{j}{4\pi \omega \epsilon r} \left[\frac{k^2 - jk - 1}{r^2} \right] e^{-jkr} \\
 &= \frac{I_d l \sin \theta}{4\pi \omega \epsilon} \left[\frac{jk^2 - j(jk+1)}{r^2} \right] e^{-jkr} \\
 &= \frac{I_d l \sin \theta}{4\pi \omega \epsilon} \left[\frac{jk^2}{r^2} + \frac{jk - j}{r^2} \right] e^{-jkr}
 \end{aligned}$$

$$E_\theta = \frac{I_d l \sin \theta}{4\pi \omega \epsilon} \left[\frac{jk^2}{r^2} + \frac{k}{r^2} - \frac{j}{r^3} \right] e^{-jkr}$$

* Fields which vary as $\frac{1}{r}$ are known as distant fields
for fields radiation fields

* Fields which vary as $\frac{1}{r^2}$ are known as inductive fields

* Fields which vary as $\frac{1}{r^3}$ are known as capacitive fields electrostatic fields

DISTANT FIELDS (FAR FIELDS) OR RADIATION FIELDS

$$H_{\phi \text{ rad}} = \frac{jk I_d l \sin \theta}{4\pi r} e^{-jkr}$$

$$E_{\theta \text{ rad}} = \frac{jk^2 I_d l \sin \theta}{4\pi \epsilon \omega r} e^{-jkr}$$

$$\text{Ratio } \frac{E_{\theta \text{ rad}}}{H_{\phi \text{ rad}}} = \frac{jk^2 I_d l \sin \theta}{4\pi \epsilon \omega r} e^{-jkr}$$

$$= \frac{jk I_d l \sin \theta}{4\pi r} e^{-jkr}$$

$$= \frac{k}{\omega \epsilon} = \frac{\omega \sqrt{\mu \epsilon}}{\omega \epsilon} = \frac{\sqrt{\mu \epsilon}}{\epsilon}$$

$$\frac{E_{\theta \text{ rad}}}{H_{\phi \text{ rad}}} = \sqrt{\frac{\mu}{\epsilon}} = \eta$$

η is the intrinsic impedance of the medium into which the antenna is radiating

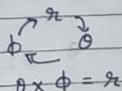
* If medium is free space $\eta = \eta_0 = 120\pi$

POWER DENSITY $\bar{S} = \frac{1}{2} \operatorname{Re} \{ \bar{E} \times \bar{H}^* \}$ $\bar{E} \rightarrow \text{V/m}$ $\bar{H} \rightarrow \text{A/m}$
 $\Rightarrow \bar{S} \rightarrow \text{W/m}^2$

$$\bar{E} = \bar{A}_\theta E_{\theta \text{ rad}}$$

$$\bar{H} = \bar{A}_\phi H_{\phi \text{ rad}}$$

$$\bar{H}^* = \bar{A}_\phi H_{\phi \text{ rad}}^*$$



$$\bar{S} = \frac{1}{2} \operatorname{Re} \{ (\bar{A}_\theta E_{\theta \text{ rad}}) \times (\bar{A}_\phi H_{\phi \text{ rad}}^*) \}$$

$$= \frac{1}{2} \operatorname{Re} \{ E_{\theta \text{ rad}} H_{\phi \text{ rad}}^* \bar{A}_\theta \}$$

$$= \bar{A}_\theta \frac{1}{2} \operatorname{Re} \{ \eta H_{\phi \text{ rad}} H_{\phi \text{ rad}}^* \}$$

$$\bar{S} = \bar{a}_r \frac{\eta}{2} \operatorname{Re} \left\{ H_{\phi, \text{rad}}^* H_{\phi, \text{rad}} \right\}$$

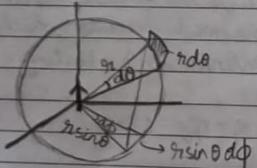
$$\boxed{\bar{S} = \bar{a}_r \frac{\eta}{2} |H_{\phi, \text{rad}}|^2}$$

$$\bar{S} = \bar{a}_r \frac{\eta}{2} \left(\frac{K I d \sin \theta}{4\pi r_2} \right)^2$$

$$\bar{S} = \bar{a}_r \frac{\eta}{2} \left(\frac{k^2 I^2 d l^2 \sin^2 \theta}{16\pi^2 r_2^2} \right)$$

$$\boxed{\bar{S} = \bar{a}_r \frac{\eta k^2 I^2 d l^2 \sin^2 \theta}{32\pi^2 r_2^2}}$$

TOTAL POWER RADIATED BY HERTZIAN DIPOLE



$$da = r^2 \sin \theta d\theta d\phi$$

$$\bar{da} = \bar{a}_r r^2 \sin \theta d\theta d\phi$$

$$P = \int \bar{S} \cdot \bar{da} = \int_{\theta=0}^{\pi} \int_{\phi=0}^{2\pi} \int r^2 \sin^2 \theta d\theta d\phi$$

$$\text{Area} = \int_{\theta=0}^{\pi} \int_{\phi=0}^{2\pi} \left(\frac{\eta k^2 I^2 d l^2 \sin^2 \theta}{32\pi^2 r_2^2} \right) d\theta d\phi$$

$$P = \frac{\eta k^2 I^2 d l^2}{32\pi^2} \times 2\pi \int_{\theta=0}^{\pi} \int_{\phi=0}^{2\pi} \sin^2 \theta d\theta d\phi$$

$$\sin 3\theta = 3\sin \theta - 4\sin^3 \theta$$

$$\sin^3 \theta = \frac{3\sin \theta - \sin 3\theta}{4}$$

$$P = \frac{\eta k^2 I^2 d l^2}{16\pi} \int_{\theta=0}^{\pi} \sin^3 \theta d\theta$$

$$= \frac{\eta k^2 I^2 d l^2}{16\pi} \int_{\theta=0}^{\pi} \left(\frac{3\sin \theta - \sin 3\theta}{4} \right) d\theta$$

$$= \frac{\eta k^2 I^2 d l^2}{64\pi} \left[3 \int_{\theta=0}^{\pi} \sin \theta d\theta - \int_{\theta=0}^{\pi} \sin 3\theta d\theta \right]$$

$$= \frac{\eta k^2 I^2 d l^2}{64\pi} \left[-3(\cos \pi - \cos 0) + \frac{1}{3} (\cos 3\pi - \cos 0) \right]$$

$$= \frac{\eta k^2 I^2 d l^2}{64\pi} \left[-3(-1 - 1) + \frac{1}{3} (-1 - 1) \right]$$

$$= \frac{\eta k^2 I^2 d l^2}{64\pi} \left[\frac{6 - 2}{3} \right] = \frac{\eta k^2 I^2 d l^2}{64\pi} \times \frac{16}{3}$$

$$\boxed{P = \frac{\eta k^2 I^2 d l^2}{12\pi}}$$

Q. Determine the power radiated by a dipole length $\frac{1}{50}$ which carries a current of 5 A.

$$c = \lambda f$$

$$\frac{f}{\lambda} = \frac{c}{\lambda}$$

$$\omega = 2\pi f = \frac{2\pi c}{\lambda}$$

$$\eta = 120\pi$$

$$k = \omega \sqrt{\mu \epsilon} = \frac{\omega}{c} = \frac{2\pi c}{\lambda c} = \frac{2\pi}{\lambda}$$

$$P = \frac{\eta k^2 I^2 dl^2}{12\pi} = \frac{120\pi}{\lambda} \left(\frac{2\pi}{\lambda}\right)^2 \left(5\right)^2 \left(\frac{1}{50}\right)^2$$

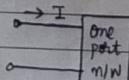
$$= \frac{4\pi^2}{\lambda^2} \times \frac{25}{3500} \times \frac{\lambda^2}{10^8} \times 10$$

$$= 0.4\pi^2$$

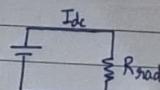
$$P = 3.95 \text{ W}$$

5/2/24

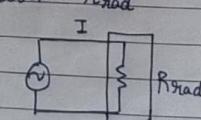
Consider the dipole to be a one-port network



Equivalent resistance of the network: R_{rad}



$$DC \Rightarrow P = I_{dc}^2 R_{\text{rad}}$$



$$AC \quad P = \frac{(I)}{\sqrt{2}}^2 R_{\text{rad}}$$

$$i(t) = Re\{Ie^{j\omega t}\} = I \cos \omega t$$

$$I_{\text{rms}} = I_{\text{eff}} = \frac{I_{dc}}{\sqrt{2}}$$

$$P = \frac{I^2 R_{\text{rad}}}{2} = \frac{\eta k^2 I^2 dl^2}{12\pi}$$

$$R_{\text{rad}} = \frac{\eta k^2 \Xi^2 dl^2}{6\pi}$$

If the dipole is radiated into free space, obtain R_{rad} in terms of $(\frac{dl}{\lambda})$

$$\eta = \eta_0 = 120\pi$$

$$k = \omega \sqrt{\mu \epsilon} = \omega \sqrt{\mu_0 \epsilon_0} = \frac{\omega}{c} = \frac{2\pi f}{c} = \frac{2\pi}{\lambda}$$

$$R_{\text{rad}} = \frac{120\pi}{\lambda} \left(\frac{2\pi}{\lambda}\right)^2 dl^2 \times \frac{1}{6\pi} = \frac{480\pi^3}{6\pi} \left(\frac{dl}{\lambda}\right)^2$$

$$R_{\text{rad}} = \frac{80\pi^2 (dl)^2}{\lambda}$$

example: A Hertzian dipole of length 5 cm is radiating into free space at 100 MHz. Determine the power radiated and the radiation resistance of the dipole if the instantaneous current flowing into the dipole is $i(t) = 10 \cos(2\pi \times 10^8 t)$

$$\omega = 2\pi \times 10^8 \text{ rad/s} \quad dl = 5 \text{ cm} \quad \eta = \eta_0 = 120\pi \\ f = 10^8 \text{ Hz} = 100 \text{ MHz} \quad \lambda = \frac{c}{f} = \frac{3 \times 10^8}{10^8} = 3 \text{ m}$$

$$R_{\text{rad}} = 80\pi^2 \left(\frac{dl}{\lambda}\right)^2 = 80\pi^2 \left(\frac{0.05}{3}\right)^2$$

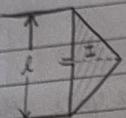
$$R_{\text{rad}} = 0.219 \Omega$$

$$P = \frac{I^2 R_{\text{rad}}}{2} = \frac{(10)^2}{2} \times 0.219 \Rightarrow P = 10.95 \text{ W}$$

SHORT / SMALL DIPOLE

$$l \sim \lambda$$

$$10$$



$$\text{Area of the plot} = \frac{1}{2} l I$$

$$H_{\text{rad}} = \frac{j k I l \sin \theta}{8\pi r^2} e^{-jkz}$$

$$E_{\text{rad}} = \eta H_{\text{rad}}$$

$$P_{\text{rad}} = \frac{\eta k^2 I^2 l^2}{48\pi}$$

$$R_{\text{rad}} = 20\pi^2 \left(\frac{l}{\lambda}\right)^2$$

6/2/24

Example 1 A short dipole of 15cm is operating at 200 MHz. Determine the power radiated and the radiation resistance of the dipole if the instantaneous current flowing in the dipole is $i(t) = 5 \cos(\omega t)$. Ref: $Ie^{j\omega t}$.

↳ phasor current $= I \cos \omega t$

$$R_{\text{rad}} = 20\pi^2 \left(\frac{l}{\lambda}\right)^2 = 20\pi^2 \left(\frac{15}{3 \times 10^8}\right)^2 = 200 \times 10^6$$

$$R_{\text{rad}} = 1.974 \Omega$$

$$P_{\text{rad}} = \frac{I^2 R_{\text{rad}}}{2} = \frac{5^2 \times 1.974}{2}$$

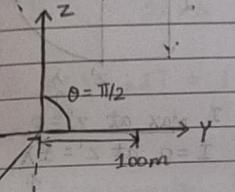
$$P_{\text{rad}} = 24.67 \text{ W}$$

$$W = 28.01 \times 8 \times 218.0 \times 0.01 = 16000 \text{ J}$$

distant

Example 2

The magnetic field at a distance of 100m, due to a z-directed short dipole at origin is $H_{\text{rad}} = 0.1 e^{-jkz}$. Determine the maximum power density at a distance 100m, power radiated and radiation resistance of the dipole.



on Y-axis

* Power density depends on distance ($\propto \frac{1}{r^2}$)

* Power radiated is independent of distance r

$$H_{\text{rad}} = \frac{j k I l \sin \theta}{8\pi r^2} e^{-jkz}$$

$$l \sim \lambda$$

$$j(0.1) e^{-j200\pi} = \frac{j k I l \sin \theta}{8\pi r^2} e^{-jkz}$$

$$r = 100 \text{ m} \Rightarrow k = 2\pi$$

$$\theta = 90^\circ$$

$$j 2\pi \times 100 \times 1 e^{-j200\pi} = j(0.1) e^{-j200\pi}$$

$$Il = 0.1$$

$$\bar{S} = \frac{\eta}{2} |H_{\text{rad}}|^2 \bar{a}_y = \frac{120\pi (0.1)^2}{2} \bar{a}_y$$

$$Il = 40 \text{ A}$$

$$\bar{S} = 1.885 \bar{a}_y \text{ W/m}^2$$

$$\bar{S} = \frac{\eta k^2 I^2 l^2 \sin^2 \theta}{128\pi^2 r^2} \bar{a}_y = \frac{(120\pi)(2\pi)^2 (40)^2 (1)^2}{128\pi^2 (100)^2} \bar{a}_y$$

$$\bar{S} = 1.885 \bar{a}_y \text{ W/m}^2$$

$\bar{a}_x = \bar{a}_y$ on Y-axis

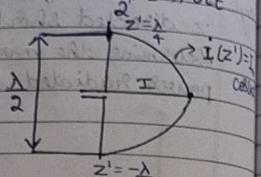
$$P = \frac{\eta k^2 I^2 l^2}{48\pi} = \frac{(120\pi)(2\pi)^2 (40)^2}{48\pi} \Rightarrow P = 157.914 \text{ kW}$$

$$R_{\text{rad}} = \frac{20\pi^2}{\lambda^2} \left(\frac{l}{\lambda}\right)^2 = \frac{20\pi^2}{\lambda^2} \left(\frac{100}{3 \times 10^8}\right)^2 = 20\pi^2 \frac{100^2}{100} \Rightarrow R_{\text{rad}} = 1.974 \Omega$$

HERTZIAN DIPOLE



SHORT DIPOLE

 $\lambda/2$ DIPOLE I max at $z' = 0$ $I = 0$ at $z' = \pm \frac{\lambda}{4}$

Sinusoidal distribution in between

 λ Dipole

mm

phase constant

$I(z) = I_0 \cos(kz')$

$I(z') = I_0$

$@ z' = 0$ $I(z') = I_0$
 $@ z' = \pm \frac{\lambda}{4}$ $k = 2\pi$

$kz' = \frac{2\pi}{\lambda} (\pm \frac{\lambda}{4}) = \pm \frac{\pi}{2}$

$\cos(\pi/2) = 0$

$I(z') = 0$

$A_z = \frac{\mu}{4\pi} \int_{-\infty}^{\infty} I(z') e^{-jkz'} dz'$

$= \frac{\mu}{4\pi k r} e^{-jkz} \int_{-\infty}^{\infty} I(z') dz'$

$= \frac{\mu}{4\pi k r} e^{-jkz} \int_{-\infty}^{\infty} I_0 \cos(kz') dz'$

$= \frac{\mu I_0}{4\pi k r} \int_{-\infty}^{\infty} \sin(kz') dz'$

$= \frac{\mu I_0}{4\pi k r} \left[-\frac{1}{k} \right] = -\frac{\mu I_0}{4\pi k r}$

$= -\frac{\mu I_0}{4\pi k r} \sin(kz)$

$= -\frac{\mu I_0}{4\pi k r} \sin(kr)$

$= -\frac{\mu I_0}{4\pi k r} \sin(kr)$

$A_z = \frac{\mu I_0}{4\pi k r} [1 - (-1)]$

$A_z = \frac{\mu I_0 e^{-jkz}}{2\pi k r}$

approximation

$$\bar{H} = \frac{1}{\mu} (\nabla \times \bar{A}) = \frac{1}{\mu} \times \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & A_\theta & A_\phi \end{vmatrix}$$

due to symmetry $\frac{\partial}{\partial \phi} = 0$ $A_\phi = 0$

$$\bar{H} = \frac{1}{\mu} \times \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & 0 \\ A_r & A_\theta & 0 \end{vmatrix}$$

$A_r = A_z \cos \theta$

$A_\theta = A_z \sin \theta$ $A_\phi = 0$

$$\bar{H} = \frac{1}{\mu} \times \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & 0 \\ A_z \cos \theta & -A_z \sin \theta & 0 \end{vmatrix}$$

$$= \frac{1}{\mu} \times \frac{1}{r} \times \frac{\partial}{\partial \theta} \left(A_z \cos \theta \right) - \frac{\partial}{\partial r} \left(A_z \cos \theta \right)$$

$$= \frac{1}{\mu} \times \frac{1}{r} \left\{ -\sin \theta \frac{\partial}{\partial r} (r A_z) + \sin \theta \frac{\partial}{\partial \theta} (A_z) \right\} \bar{a}_\phi$$

$$\bar{H} = \frac{\sin \theta}{\mu r} \left\{ A_z - \frac{\partial}{\partial r} (r A_z) \right\} \bar{a}_\phi = \frac{\sin \theta}{\mu r} \left\{ A_z - A_z - \frac{\partial}{\partial r} A_z \right\} \bar{a}_\phi$$

$$\bar{H} = -\frac{\partial}{\partial r} \sin \theta \frac{\partial}{\partial r} (r A_z)$$

$$\frac{\partial A_z}{\partial z} = \frac{\mu}{2\pi k} \left[\frac{\mu I_0 e^{-jkz}}{2\pi k z} + \frac{\partial}{\partial z} \left(\frac{e^{-jkz}}{z} \right) \right] = \frac{\mu I_0}{2\pi k} \frac{\partial}{\partial z} \left(\frac{e^{-jkz}}{z} \right)$$

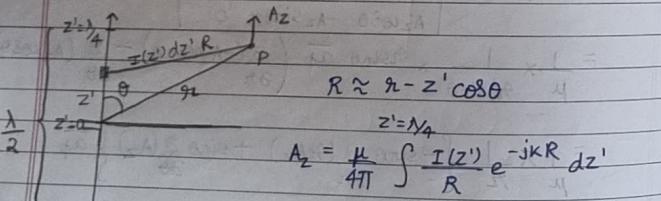
$$= \frac{\mu I_0}{2\pi k} \left[-\frac{e^{-jkz}}{z^2} + \frac{(-jk)z e^{-jkz}}{z^2} \right]$$

$$\frac{\partial A_z}{\partial z} = -\frac{\mu I_0}{2\pi k} \left[\frac{jk+1}{z^2} \right] e^{-jkz}$$

$$z \frac{\partial A_z}{\partial z} = -\frac{\mu I_0}{2\pi k} \left[jk+1 \right] e^{-jkz}$$

$$\bar{H} = -\frac{\bar{A}_0 \sin \theta}{\mu R} \left\{ -\frac{\mu I_0}{2\pi k} \left[\frac{jk+1}{z^2} \right] e^{-jkz} \right\}$$

$$\bar{H} = \frac{I_0 \sin \theta}{2\pi k} \left[\frac{jk+1}{z^2} \right] e^{-jkz}$$



$$A_z = \frac{\mu}{4\pi} \int \frac{I(z')}{R} e^{-jkR} dz'$$

$$A_z = \frac{\mu}{4\pi} \int_{-\lambda/4}^{\lambda/4} \frac{I_0 \cos(kz')}{R - z' \cos \theta} e^{-jk(z_r - z' \cos \theta)} dz'$$

In the amplitude term $R \approx z_r$

$$kz' \Big|_{\lambda/4} = \frac{2\pi}{\lambda} \times \frac{\lambda}{4} = \frac{\pi}{2}$$

$$A_z = \frac{\mu I_0}{4\pi} \int_{-\lambda/4}^{\lambda/4} \frac{\cos(kz')}{z_r} e^{-jk(z_r - z' \cos \theta)} dz'$$

$$A_z = \frac{\mu I_0}{4\pi z_r} e^{-jkz_r} \int_{-\lambda/4}^{\lambda/4} \cos(kz') \left\{ \cos(kz' \cos \theta) + j \sin(kz' \cos \theta) \right\} dz'$$

$$= \frac{\mu I_0}{4\pi z_r} e^{-jkz_r} \int_{-\lambda/4}^{\lambda/4} \cos(kz') \cos(kz' \cos \theta) dz'$$

$$+ j \int_{-\lambda/4}^{\lambda/4} \cos(kz') \sin(kz' \cos \theta) dz'$$

even function

odd function

\Rightarrow symmetric integration

$= 0$

$$= \frac{\mu I_0}{4\pi z_r} e^{-jkz_r} \int_{-\lambda/4}^{\lambda/4} 2 \cos(kz' \cos \theta) dz'$$

$$= \frac{\mu I_0}{2\pi z_r} e^{-jkz_r} \int_{-\lambda/4}^{\lambda/4} [\cos(kz' + kz' \cos \theta) + \cos(kz' - kz' \cos \theta)] dz'$$

$$= \frac{\mu I_0}{4\pi z_r} e^{-jkz_r} \int_0^{\lambda/4} [\cos(k(i + \cos \theta)z') + \cos(k(i - \cos \theta)z')] dz'$$

$$= \frac{\mu I_0}{4\pi z_r} e^{-jkz_r} \left[\frac{1}{k(i + \cos \theta)} \sin(k(i + \cos \theta)z') \right]_0^{\lambda/4} + \left[\frac{1}{k(i - \cos \theta)} \sin(k(i - \cos \theta)z') \right]_0^{\lambda/4}$$

$$= \frac{\mu I_0}{4\pi z_r} e^{-jkz_r} \left[\frac{\sin(\frac{\pi}{2}(i + \cos \theta))}{k(i + \cos \theta)} + \frac{\sin(\frac{\pi}{2}(i - \cos \theta))}{k(i - \cos \theta)} \right]$$

$$A_z = \frac{\mu I_0}{4\pi z_r k} e^{-jkz_r} \left[\frac{(1 - \cos \theta) \sin(\frac{\pi}{2} + \frac{\pi}{2} \cos \theta)}{\sin^2 \theta} + \frac{(1 + \cos \theta) \sin(\frac{\pi}{2} - \frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \right]$$

$$A_z = \frac{\mu I_0 e^{-jkz}}{4\pi k \sin^2 \theta} \left[(1 - \cos \theta) \cos \left(\frac{\pi}{2} \cos \theta \right) + (1 + \cos \theta) \cos \left(\frac{\pi}{2} \cos \theta \right) \right]$$

$$= \frac{\mu I_0 e^{-jkz}}{4\pi k \sin^2 \theta} \left\{ 2 \cos \theta \cos \left(\frac{\pi}{2} \cos \theta \right) \right\}$$

$$A_z = \left(\frac{\mu I_0}{2\pi k} \right) \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \right) e^{-jkz}$$

8/2/24

$$\bar{H} = \frac{1}{\mu} (\nabla \times \bar{A}) = \frac{1}{\mu} \times \frac{1}{r^2 \sin \theta} \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \partial/\partial r & \partial/\partial \theta & \partial/\partial \phi \\ A_r & A_{\theta} & A_{\phi} \end{vmatrix}$$

Symmetrically placed on z-axis $\frac{\partial}{\partial \phi} = 0$ $A_{\phi} = 0$

$$A_r = A_z \cos \theta \quad A_{\theta} = -A_z \sin \theta$$

$$\bar{H} = \frac{1}{\mu} \times \frac{1}{r^2 \sin \theta} \begin{vmatrix} \bar{a}_r & \bar{a}_{\theta} & \bar{a}_{\phi} \\ \partial/\partial r & \partial/\partial \theta & 0 \\ A_r & A_{\theta} & 0 \end{vmatrix}$$

$$\bar{H}_{\phi} = \frac{1}{\mu r^2 \sin \theta} \times r \sin \theta \left\{ \frac{\partial (r A_{\theta})}{\partial r} - \frac{\partial (A_r)}{\partial \theta} \right\} \hat{a}_{\phi}$$

$$= \frac{1}{\mu r} \left\{ (A_{\theta}) + r \frac{\partial (A_{\theta})}{\partial r} - \frac{\partial (A_r)}{\partial \theta} \right\}$$

$$\bar{H}_{\phi} = \frac{1}{\mu r} \left\{ -A_z \sin \theta + r \frac{\partial (-A_z \sin \theta)}{\partial r} - \frac{\partial (A_z \cos \theta)}{\partial \theta} \right\}$$

$$\cancel{\frac{\partial (-A_z \sin \theta)}{\partial r}} = r \frac{\partial}{\partial r} \left(\frac{-\mu I_0}{2\pi k} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \right) e^{-jkz} \times \sin \theta \right)$$

$$\bar{H}_{\phi} = \frac{1}{\mu r} \frac{\partial (r(-A_z \sin \theta))}{\partial r} = \frac{1}{\mu r} \frac{\partial}{\partial r} \left\{ r \left(\frac{-\mu I_0}{2\pi k} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \right) e^{-jkz} \times \sin \theta \right) \right\}$$

$$= \frac{1}{\mu r} \left\{ \frac{-\mu I_0}{2\pi k} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \right) \frac{\partial}{\partial r} (e^{-jkz}) \right\}$$

$$= \frac{-I_0}{2\pi k} \frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} (-jk) e^{-jkz}$$

$$\frac{1}{\mu r} \frac{\partial (r A_{\theta})}{\partial r} = \frac{j I_0}{2\pi k} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \right) e^{-jkz}$$

$$\frac{-1}{\mu r} \frac{\partial (A_z \cos \theta)}{\partial \theta} = \frac{-1}{\mu r} \times \frac{\mu I_0}{2\pi k} e^{-jkz} \frac{\partial}{\partial \theta} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \cos \theta \right)$$

$$= \frac{-I_0}{2\pi k} \frac{\partial}{\partial \theta} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \right) \cos \theta$$

* This term varies with $\frac{1}{r^2}$ and hence does not contribute to radiation/distant field. Therefore, this term can be ignored while computing the expression for \bar{H}_{rad} .

for 1 dipole, the expression for \bar{H}_{rad} is

$$\bar{H}_{\text{rad}} = \frac{j I_0}{2\pi k} \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \right) e^{-jkz}$$

$$E_{\text{rad}} = \eta \bar{H}_{\text{rad}}$$

$$E_{\text{rad}} = j \left(\frac{\mu I_0}{2\pi k} \right) \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \right) e^{-jkz}$$

* Power density for $\lambda/2$ dipole

$$\bar{S} = \frac{1}{2} R_E \left\{ \bar{E} \times \bar{H}^* \right\} = \frac{\bar{a}_0}{2} \operatorname{Re} \left\{ E_{\text{rad}} \cdot H_{\text{rad}} \right\}$$

$$E_{\text{rad}} = \eta H_{\text{rad}}$$

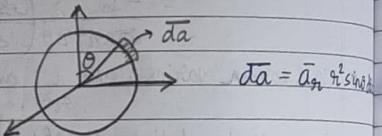
$$\bar{S} = \frac{\bar{a}_0}{2} \eta |H_{\text{rad}}|^2$$

$$g = \frac{\eta}{2} \left[\left(\frac{I_0}{2\pi r} \right) \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \right) \right]^2$$

NOTE: Sometimes I_0 can be a complex quantity as it is phasor current.

* Power radiated for λ dipole

$$P = \int \bar{S} \cdot d\bar{a}$$



$$P = \int_{\theta=0}^{\pi} \int_{\phi=0}^{2\pi} S r^2 \sin \theta d\phi d\theta$$

$$P = r^2 \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} \frac{\eta}{2} \left(\frac{I_0}{2\pi r} \right) \left(\frac{\cos(\frac{\pi}{2} \cos \theta)}{\sin \theta} \right)^2 \sin \theta d\theta d\phi$$

$$= \frac{\eta I_0^2}{8\pi^2} \times 2\pi \int_{\theta=0}^{\pi} \frac{\cos^2(\frac{\pi}{2} \cos \theta)}{\sin \theta} d\theta$$

$$P = \frac{\eta I_0^2}{4\pi} \times (1.218)$$

$$|I_0|^2 \Rightarrow I_{\text{eff}} = \frac{I_0}{\sqrt{2}} \Rightarrow I_0 = \sqrt{2} I_{\text{eff}}$$

$$I_0^2 = 2 I_{\text{eff}}^2$$

$$P = \frac{\eta I_{\text{eff}}^2}{4\pi} \times 2 \times 1.218$$

$$P = \frac{1.218\eta}{2\pi} I_{\text{eff}}^2$$

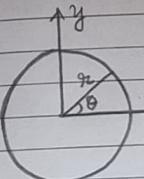
$$\text{In free space } \eta = \eta_0 = \frac{120\pi}{1.218 \times 120\pi \times I_{\text{eff}}^2} = \frac{73.08}{2\pi} I_{\text{eff}}^2$$

$$P_{\text{free space}} \approx 73 I_{\text{eff}}^2$$

* Radiation resistance

$$P_{\text{rad}} = R_{\text{rad}} I_{\text{eff}}^2 \Rightarrow R_{\text{rad}} = 73 \Omega$$

Some more antenna parameters:



$$\text{Circumference} = 2\pi r$$

A complete arc of a circle subtends an angle of 2π at the centre.
 $2\pi^c \rightarrow$ arc of $2\pi r$ length
 $1^c \rightarrow$ arc of r length

* In 3D, angle is measured in terms of STERADIAN
A spherical surface of $4\pi r^2$ subtends a solid angle of 4π steradian.

$4\pi r^2$ surface area \rightarrow covered by 4π steradian
 $\Rightarrow 1$ steradian covers a surface area of $\underline{r^2}$.

Power radiated in 1 steradian = Power radiated through surface area of r^2

$$= \text{Power density} \times r^2$$

$$\rightarrow \text{Radiation intensity } U = S r^2$$

$$U = S r^2$$

* Types of radiators (or antennas)

(1) ISOTROPIC RADIATOR radiates uniformly in all directions

(2) DIRECTIONAL RADIATOR → In certain directions, it has more (antenna) radiation compared to that in other directions

→ A sub-class of this radiator is the OMNI-DIRECTIONAL RADIATOR

→ Radiates uniformly in a particular plane.

→ While in plane orthogonal to this plane, the radiation is directional.

ISOTROPIC ANTENNA

P is power radiated

$$\text{Power density } S = \frac{P}{4\pi r^2}$$

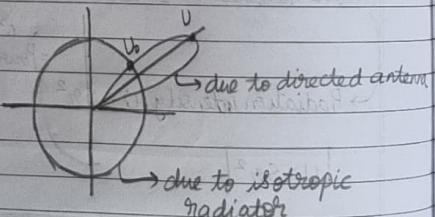
$$\text{Radiation intensity } U_0 = S r^2 = \frac{P}{4\pi}$$

(U₀ notation is used only for Isotropic antennas)

* DIRECTIVITY OF AN ANTENNA

The ratio of radiation intensity in a particular direction to the radiation intensity due to isotropic radiator's.

$$D = \frac{U}{U_0}$$



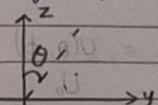
9/3/24

RADIATION PATTERN

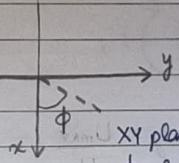
It is a graphical representation of some parameters of an antenna

- * E-field
- * H-field
- * U
- * P
- * Plane

Radiation pattern is plotted along 2 orthogonal planes

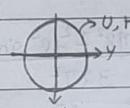
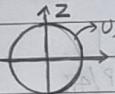


yz plane (E-plane or theta-plane) plot



xy plane (H-plane or phi-plane) plot

* Isotropic antenna



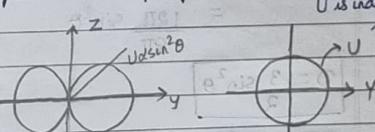
Example Determine the radiation intensity of a Hertzian dipole and plot it along theta-plane and phi-plane

$$U = S r^2$$

$$S = \frac{\eta k^2 I^2 dl^2 \sin^2 \theta}{32\pi^2 r^2}$$

$$U = \frac{\eta k^2 I^2 dl^2 \sin^2 \theta}{32\pi^2 r^2}$$

$$\Rightarrow U \propto \sin^2 \theta$$



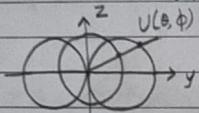
OMNIDIRECTIONAL ANTENNA

- * No antenna radiates uniformly
 Isotropic antenna is just used as a mathematical model
 to define Directivity
 It is fictitious.

DIRECTIVITY

$$\text{Directivity} = \frac{U(\theta, \phi)}{U_0}$$

$U_0 = U_{iso}$ Radiation intensity of an isotropic antenna which radiates the same power



$$\text{Max Directivity} = \frac{U_{max}}{U_0}$$

HERTZIAN DIPOLE

$$\begin{aligned}\text{Directivity} &= \frac{U}{U_0} = \frac{\eta k^2 I^2 d l^2 \sin^2 \theta}{32\pi^2 P / 4\pi} \\ &= \frac{\eta k^2 I^2 d l^2}{32\pi^2 8\pi} \times \frac{4\pi}{\eta k^2 I^2 d l^2} \sin^2 \theta \\ &= \frac{1.2\pi}{8\pi} \sin^2 \theta\end{aligned}$$

$$D = \frac{3}{2} \sin^2 \theta$$

$$D_{max} = \frac{3}{2}$$

$$D_{max} (\text{dB}) = 10 \log_{10} (D_{max})$$

$$D_{max} (\text{dB}) = 1.76 \text{ dB}$$

SHORT DIPOLE

$$\text{Directivity} = \frac{U}{U_0} = \frac{\eta k^2 I^2 d l^2 \sin^2 \theta}{128\pi^2} \times \frac{4\pi}{\eta k^2 I^2 d l^2} = \frac{4\pi}{48\pi}$$

$$D = \frac{3 \sin^2 \theta}{2}$$

$$D_{max} = \frac{3}{2}$$

1/2 DIPOLE

$$\begin{aligned}\text{Directivity} D &= \frac{4\pi U}{P} = \frac{4\pi S \pi r^2}{P} = 4\pi \times \frac{\eta}{2} \left(\frac{I_0}{2\pi r} \right)^2 \left(\frac{\cos^2(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta} \right) \\ &= \frac{\eta I_0^2}{2 \cdot 4\pi^2 r^2} \times \frac{(1.218)}{\sin^2 \theta} \\ &= \frac{1.218}{2 \cdot 4\pi^2 r^2} \times \frac{\eta I_0^2}{\sin^2 \theta} \\ &= \frac{2}{1.218} \frac{\cos^2(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta}\end{aligned}$$

$$D = 1.642 \frac{\cos^2(\frac{\pi}{2} \cos \theta)}{\sin^2 \theta}$$

$$\frac{\partial D}{\partial \theta} = \frac{\sin^2 \theta \{ 2 \cos(\frac{\pi}{2} \cos \theta) (-\sin(\frac{\pi}{2} \cos \theta)) \frac{\pi}{2} (-\sin \theta) \} - 2 \sin \theta \cos \theta \cos^2(\frac{\pi}{2} \cos \theta)}{\sin^4 \theta}$$

Longest path - innermost

$$\frac{\partial D}{\partial \theta} = 0 \Rightarrow \pi \cos\left(\frac{\pi}{2} \cos\theta\right) \sin\left(\frac{\pi}{2} \cos\theta\right) \sin^3\theta - 2\sin\theta \cos\theta \cos^2\left(\frac{\pi}{2} \cos\theta\right) = 0$$

D will be max at $\theta = 90^\circ$

$$D_{max} = 1.642$$

$$U \propto \frac{\cos^2\left(\frac{\pi}{2} \cos\theta\right)}{\sin^2\theta} \quad @ \theta = 0^\circ \quad 0 \text{ from obtained}$$

→ Apply L'Hospital's rule

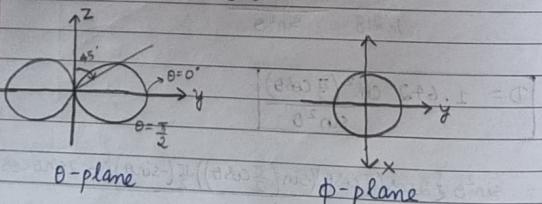
$$\lim_{\theta \rightarrow 0} \frac{\cos^2\left(\frac{\pi}{2} \cos\theta\right)}{\sin^2\theta} = \lim_{\theta \rightarrow 0} \frac{2' \cos\left(\frac{\pi}{2} \cos\theta\right) \sin\left(\frac{\pi}{2} \cos\theta\right) \sin\theta \frac{\pi}{2}}{2 \sin\theta \cos\theta}$$

$$\frac{\frac{\pi}{2} \cos\left(\frac{\pi}{2}\right) \sin\left(\frac{\pi}{2}\right)}{\cos\theta}$$

$$\therefore U = 0 \quad @ \theta = 0^\circ$$

$$U @ \theta = 45^\circ \Rightarrow \cos^2\left(\frac{\pi}{2} \times \frac{1}{\sqrt{2}}\right) = 0.3943$$

$$\left(\frac{1}{\sqrt{2}}\right)^2$$



Omni-directional

Example

$$\begin{aligned} \cos 2\theta &= 1 - 2\sin^2\theta \\ \sin^2\theta &= \frac{1 - \cos 2\theta}{2} \end{aligned}$$

The radiation intensity of an antenna is given by

$$U(\theta, \phi) = \sin\theta \sin\phi, \quad 0 \leq \theta \leq \pi$$

$$0 \leq \phi \leq \pi$$

$$= 0, \quad \text{elsewhere}$$

Determine the total power radiated and the directivity of the antenna.

$$U = S \Omega^2 \quad P = \int S \cdot dA$$

$$S = U = \frac{1}{4} \sin\theta \sin\phi$$

$$dA = \frac{\pi}{4} \sin\theta \sin\phi \cdot d\theta \cdot d\phi$$

$$\theta = 0, \phi = 0 \quad \frac{\pi}{4} \sin\theta \sin\phi \cdot d\theta \cdot d\phi$$

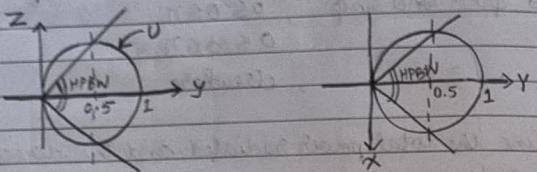
$$D = \frac{4\pi U}{P} = \frac{4\pi \cdot \frac{1}{4} \sin\theta \sin\phi}{\frac{\pi}{4} \sin\theta \sin\phi} = \frac{16\pi}{\pi} = 16$$

$$= 4\pi \times \sin\theta \sin\phi = -\cos\phi \int_0^\pi \int_0^\pi \int_0^{\pi/2} 1 - \cos 2\theta \, d\theta \, d\phi$$

$$P = (1 - (-1)) \frac{1}{2} \left[\phi - \frac{1}{2} \sin 2\theta \right]_0^\pi = 2 \times \frac{1}{2} [(\pi - 0) - 1 (\sin \pi - \sin 0)] = \pi \text{ Watts}$$

$$D_{max} = 4 \quad \text{at } \theta = \frac{\pi}{2}, \phi = \frac{\pi}{2}$$

$$da = \pi^2 \sin\theta d\phi d\theta$$

HALF-POWER BEAM WIDTH (HPBW)

Example determine HPBW in θ -plane and ϕ -plane of an antenna whose radiation intensity is

$$U(\theta, \phi) = \sin^2 \theta \sin \phi \quad 0 \leq \theta \leq \pi; \quad 0 \leq \phi \leq \pi \\ = 0 \quad \text{otherwise}$$

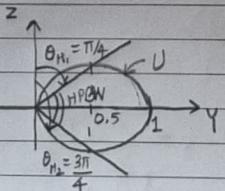
In θ -plane (YZ-plane or E-plane)

$$U\left(\theta, \frac{\pi}{2}\right) = \sin^2 \theta \quad 0 \leq \theta \leq \pi, \quad 0 \leq \phi \leq \pi$$

$$\frac{1}{2} = 0.5 = \sin^2(\theta_H)$$

$$\sin(\theta_H) = \frac{1}{\sqrt{2}} \Rightarrow \theta_H = \frac{\pi}{4}, \frac{3\pi}{4}$$

$$\text{HPBW}(\theta\text{-plane}) = \theta_{H_2} - \theta_{H_1} = \frac{3\pi}{4} - \frac{\pi}{4} = \frac{\pi}{2}$$

In ϕ -plane (XY-plane or H-plane)

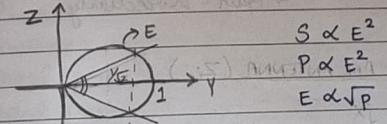
$$U\left(\frac{\pi}{2}, \phi\right) = \sin \phi \quad 0 \leq \theta \leq \pi, \quad 0 \leq \phi \leq \pi$$

$$0.5 = \sin(\phi_H)$$

$$\phi_H = \frac{\pi}{6}, \frac{5\pi}{6}$$

$$\text{HPBW}(\phi\text{-plane}) = \phi_{H_2} - \phi_{H_1} = \frac{5\pi}{6} - \frac{\pi}{6} = \frac{2\pi}{3}$$

Example determine HPBW in θ and ϕ plane if the radiation pattern of an antenna is $E(\theta, \phi) = \sin \theta \sin \phi \quad 0 \leq \theta \leq \pi, \quad 0 \leq \phi \leq \pi$



$$\text{In } \theta\text{-plane} \quad E\left(\theta, \frac{\pi}{2}\right) = \sin \theta$$

$$\frac{1}{2} = \sin \theta_H \Rightarrow \theta_H = \frac{\pi}{4}, \frac{3\pi}{4}$$

$$\text{HPBW}(\theta\text{-plane}) = \theta_{H_2} - \theta_{H_1} = \frac{\pi}{2}$$

$$\text{In } \phi\text{-plane} \quad E\left(\frac{\pi}{2}, \phi\right) = \sin \phi$$

$$\frac{1}{2} = \sin \phi_H \Rightarrow \phi_H = \frac{\pi}{4}, \frac{3\pi}{4}$$

$$\text{HPBW}(\phi\text{-plane}) = \phi_{H_2} - \phi_{H_1} = \frac{\pi}{2}$$

ANTENNA EFFICIENCY (e)

$$e = \frac{\text{Radiated power}}{\text{Input power}} = \frac{P}{P_{in}} = \frac{I_{eff}^2 R_{rad}}{I_{eff}^2 (R_{loss} + R_{rad})}$$

$$e = \frac{R_{rad}}{R_{loss} + R_{rad}}$$

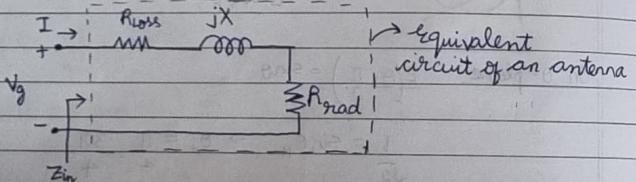
R_{loss} is the resistance of the antenna wire

ANTENNA GAIN (G)

$$G = e D$$

$$\text{if } R_{loss} \approx 0, e = 1, D = 100\% \\ \Rightarrow \text{Gain} = \text{directivity}$$

INPUT IMPEDANCE OF AN ANTENNA (Z_{in})



$$Z_{in} = R_{loss} + jX + R_{rad}$$

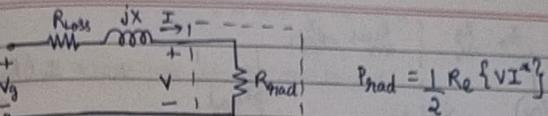
$$P_{in} = \frac{1}{2} \operatorname{Re} \{ V_g I^* \} \quad \text{where } V_g \text{ and } I \text{ are phasors}$$

$$P_{in} = \frac{1}{2} \operatorname{Re} \{ I_{in} I^{*in} \}$$

$$P_{in} = \frac{1}{2} |I|^2 \operatorname{Re} \{ Z_{in} \}$$

$$P_{in} = \frac{1}{2} |I|^2 (R_{loss} + R_{rad})$$

$$P_{in} = I_{eff}^2 (R_{loss} + R_{rad})$$



$$P_{rad} = \frac{1}{2} \operatorname{Re} \{ I R_{rad} I^* \}$$

$$= \frac{1}{2} |I|^2 R_{rad}$$

$$P_{rad} = I_{eff}^2 R_{rad}$$

Example A voltage source $V_g = (50 + j40) \text{ V}$ with source impedance of 50Ω is connected to an antenna with $R_{rad} = 70 \Omega$, $R_{loss} = 1 \Omega$ and reactance $jX = j25 \Omega$. Calculate

- i) antenna efficiency
- ii) real power delivered by the source
- iii) real power input to the antenna
- iv) power radiated by the antenna
- v) power loss in the antenna

$$\begin{aligned} I &\rightarrow \frac{50 \Omega}{\parallel} \frac{1 \Omega}{\parallel} \frac{j25 \Omega}{\parallel} \\ &= \frac{V_g}{R_g + R_{loss} + jX} = \frac{(50 + j40)}{70 + j40} \end{aligned}$$

i) antenna efficiency

$$e = \frac{R_{rad}}{R_{rad} + R_{loss}} = \frac{70}{70 + 1} = 0.98591$$

$$e = 98.6\%$$

- i) real (or average) power delivered by the source

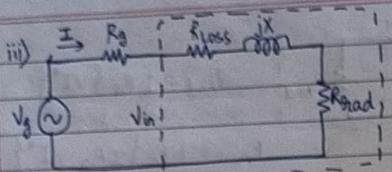
$$P_g = \frac{1}{2} \operatorname{Re} \{ V_g I^* \} \quad I = \frac{V_g}{R_g + R_{loss} + R_{rad} + jX}$$

$$= \frac{1}{2} \operatorname{Re} \{ (10\sqrt{1} \angle 38.659^\circ) (0.5182 \angle -26.98^\circ) \} = \frac{50 + j40}{121 + j25}$$

$$= \frac{1}{2} \operatorname{Re} \{ 32.494 + 6.7167 \} \quad I = 0.5182 \angle -26.98^\circ \text{ A} \\ I^* = 0.5182 \angle 26.98^\circ \text{ A}$$

$$= \frac{1}{2} [32.494]$$

$$P_g = 16.247 \text{ W}$$



$$V_{in} = I (R_{loss} + R_{grad} + jx)$$

Peak power (average power) input to the antenna

$$= \frac{1}{2} \operatorname{Re} \left\{ V_{in} I^* \right\} = \frac{1}{2} \operatorname{Re} \left\{ I (R_{load} + jX) I^* \right\}$$

$$= \frac{1}{2} |I|^2 (R_{\text{loss}} + R_{\text{rad}})$$

$$= \frac{1}{2} (0.5182)^2 (1+70)$$

$$P_{in} = 9.525 \text{ W}$$

iv) power radiated by antenna $P_{\text{rad}} = I_{\text{eff}}^2 R_{\text{rad}}$

$$= \left(\frac{0.518}{\sqrt{2}} \right)^2 \times$$

$$P_{\text{rad}} = 9.39 \text{ W}$$

$$\Rightarrow \text{power loss in antenna } I_{eff}^2 R_{Losc} = (0.518)^2 \times 1$$

$$= 0.134W$$

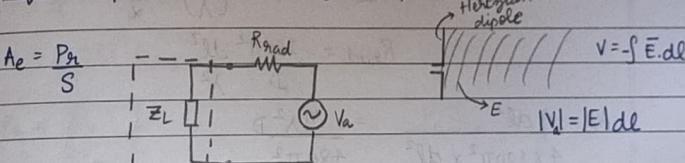
$$= 0.134W$$

Effective aperture of an antenna

(P_a) is the ratio of the power received by the antenna to the power density of the electromagnetic wave impinged on the antenna.

$$A_e = \frac{Pr}{s}$$

Effective aperture of a Hertzian dipole



When the antenna is matched $Z_L = R_{\text{rad}}$

$$P_{R_1} = \frac{1}{2} \operatorname{Re} \left\{ VI^* \right\} = \frac{1}{2} \operatorname{Re} \left\{ R_{\text{grad}} I I^* \right\}$$

$$= \frac{1}{2} |I|^2 R_{\text{rad}} = \frac{1}{2} \frac{V_0^2}{4R_{\text{rad}}^2} \times R_{\text{rad}}$$

$$P_g = \frac{V_a^2}{8 R_{gad}}$$

$$P_R = \frac{|E|^2 dl^2}{8 R_{\text{rad}}}$$

$$S = \frac{1}{2} \operatorname{Re} \left\{ \bar{E} \times \bar{H}^* \right\} = \frac{1}{2} E_0 H_0^* = \frac{1}{2} \eta |H_0|^2 = \frac{1}{2} \eta E_0 E_0^*$$

$$S = \frac{|E_0|^2}{2\eta}$$

$$S = \frac{|E|^2}{2\eta}$$

$$A_e = \frac{P_R}{S} = \frac{|E|^2 dl^2}{8 R_{rad}} \times \frac{|E|^2}{2\eta}$$

$$A_e = \frac{\eta dl^2}{4 R_{rad}}$$

$$R_{rad} = 80\pi^2 \left(\frac{dl}{\lambda}\right)^2$$

$$D = \frac{3}{2}$$

$$R_{rad} D = 80\pi^2 \left(\frac{dl}{\lambda}\right)^2 \times \frac{3}{2}$$

$$R_{rad} = \frac{120\pi^2}{D} \frac{dl^2}{\lambda^2}$$

$$A_e = \frac{\eta dl^2}{4 \times \frac{120\pi^2}{D} \frac{dl^2}{\lambda^2}} = \frac{\eta \lambda^2 D}{480\pi^2}$$

$$\text{In free space } A_e = \frac{120\pi \lambda^2 D}{480\pi^2} = \frac{(\lambda^2)}{(4\pi)} D$$

$$G = eD$$

$$R_{loss} = 0 \Rightarrow e = 1$$

$$G = D$$

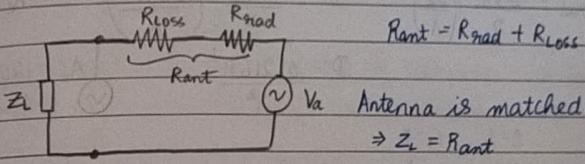
$$A_e = \left(\frac{\lambda^2}{4\pi}\right) G \text{ m}^2$$

Aperture is essentially the area

Larger aperture \Rightarrow antenna can receive more power

Consider lossy Hertzian dipole $R_{loss} \neq 0$

Equivalent circuit of receiver antenna



$$R_{ant} = R_{rad} + R_{loss}$$

$$\Rightarrow Z_L = R_{ant}$$

$$I = \frac{V_a}{R_{ant}}$$

$$P_R = \frac{1}{2} \operatorname{Re} \{ V_a I^* \} = \frac{1}{2} \operatorname{Re} \{ R_{ant} I I^* \} = \frac{|V_a|^2}{2 R_{ant}}$$

$$= \frac{1}{2} |I|^2 R_{ant} = \frac{1}{2} \frac{|V_a|^2}{4 R_{ant}} R_{ant}$$

$$P_R = \frac{|V_a|^2}{8 R_{ant}}$$

$$S = \frac{|E|^2}{2\eta}$$

$$A_e = P_R = \frac{|V_a|^2 2\eta}{8 R_{ant} |E|^2} = \frac{|V_a|^2}{4 R_{ant} |E|^2}$$

$$A_e = \frac{\eta dl^2}{4 R_{ant}}$$

$$R_{ant} = R_{loss} + R_{rad}$$

$$e = \frac{R_{rad} R_{loss}}{R_{loss} + R_{rad}} = \frac{R_{rad}}{R_{loss} + R_{rad}}$$

$$R_{ant} = \frac{R_{rad}}{e}$$

$$A_e = \frac{\eta dl^2}{4 R_{rad}} \times e = \frac{\eta dl^2 e}{4 \times 120\pi^2 \frac{dl^2}{D} \frac{dl^2}{\lambda^2}}$$

$$\text{In free space } \frac{120\pi e D \lambda^2}{4 \times 120\pi^2} = \left(\frac{\lambda^2}{4\pi}\right) e D \Rightarrow A_e = \left(\frac{\lambda^2}{4\pi}\right) G$$

Example Determine the effective aperture of a Hertian dipole of length 6 cm and radiation resistance of 2 Ω

$$R_{\text{rad}} = \frac{120\pi^2}{D} \left(\frac{dl}{\lambda}\right)^2 \Rightarrow D = \frac{120\pi^2}{2} \left(\frac{6 \times 10^{-2}}{\lambda}\right)^2$$

$$D = \frac{0.216\pi^2}{\lambda^2} \quad A_e = \frac{120\pi}{4R_{\text{rad}}} \left(\frac{6 \times 10^{-2}}{\lambda}\right)^2$$

$$\epsilon = 1 \quad G = D$$

$$A_e = \left(\frac{\lambda^2}{4\pi}\right)G = \frac{\lambda^2}{4\pi} \times \frac{0.216\pi^2}{\lambda^2} = 0.216\pi \quad [A_e = 0.1696 \text{ m}^2]$$

$$[A_e = 0.1696 \text{ m}^2]$$

$$R_{\text{rad}} = \frac{80\pi^2}{\lambda} (dl)^2$$

$$\lambda^2 = \frac{80\pi^2 dl^2}{R_{\text{rad}}} = \frac{80\pi^2 (6 \times 10^{-2})^2}{2} = 0.144\pi^2$$

$$G = D_{\max} = \frac{3}{2} \quad \text{with } \epsilon = 1$$

$$A_e = \left(\frac{\lambda^2}{4\pi}\right)G = \frac{0.144\pi^2}{4\pi} \times \frac{3}{2}$$

$$[A_e = 0.1696 \text{ m}^2]$$

Example 2 Determine the effective aperture of a Hertian dipole received a power of 1 mW when an electric field of 1 V/m is impinged on it.

$$S = \frac{|E|^2}{2\eta} = \frac{1^2}{2 \times 120\pi} = 1.3263 \times 10^{-3}$$

$$A_e = \frac{P_R}{S} = \frac{1 \times 10^{-3}}{1.3263 \times 10^{-3}} = 753.982 \times 10^{-3} \Rightarrow [A_e = 0.7539 \text{ m}^2]$$

POLARISATION

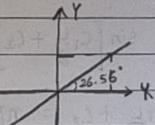
Polarization of an antenna is the polarization of electromagnetic wave it has radiated in the farfield.

Polarization is the locus of tip of instantaneous electric field on the plane perpendicular to the direction of wave propagation.

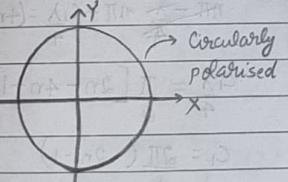
(1) when only E_x or E_y present \rightarrow Wave is said to be LINEARLY POLARISED

(2) when $E_x = E_y$ but with same phase \rightarrow Wave is LINEARLY POLARISED

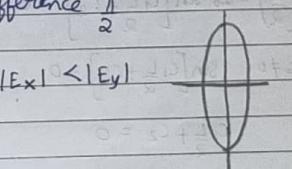
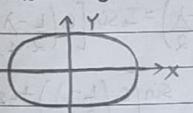
i) $|E_x| = 2|E_y|$ but with same phase



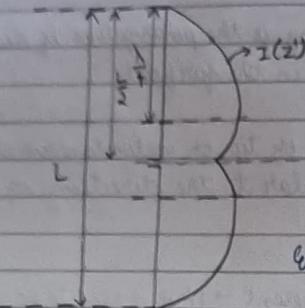
(3) $|E_x| = |E_y|$ but with phase difference of $\frac{\pi}{2}$



iii) $|E_x| > |E_y|$ with phase difference $\frac{\pi}{2}$



FINITE LENGTH DIPOLE



$$I(z') = I_0 \sin [C_1 z' + C_2]$$

$$I(z') \text{ at } z' = \frac{L}{2} \Rightarrow I(z') = 0$$

$I(z')$ at $z' = \frac{L-\lambda}{2}$ is I_0 (max value)
Even function $I(z') = I(-z')$

$$I\left(\frac{L}{2}\right) = I_0 \sin \left[C_1 \frac{L}{2} + C_2 \right] = 0$$

$$I_0 \neq 0 \quad \sin \left[C_1 \frac{L}{2} + C_2 \right] = 0$$

$$C_1 \frac{L}{2} + C_2 = n\pi$$

$$\frac{2\pi}{\lambda} \left(-\frac{3\lambda}{4} - \frac{\lambda}{2} \right) + C_2 = n\pi$$

$$C_2 = \frac{n\pi\lambda}{\lambda} + \frac{3\pi\lambda}{4}(2n+1)$$

$$\sin \left[C_1 \left(\frac{L-\lambda}{2} \right) + C_2 \right] = 1$$

$$C_1 \left(\frac{L-\lambda}{2} \right) + C_2 = \frac{(4n+1)\pi}{2}$$

~~$$\frac{n\pi}{4} - \frac{\lambda}{4} - C_1 \lambda = \frac{(4n+1)\pi}{2}$$~~

$$C_1 \frac{\lambda}{4} = \frac{\pi}{2} [2n - 4n - 1]$$

$$C_1 = \frac{2\pi}{\lambda} (-2n-1)$$

$$I\left(\frac{L}{2}\right) = I_0 \sin \left[C_1 \frac{L}{2} + C_2 \right] = 0$$

$$I_0 \neq 0 \quad \sin \left[C_1 \frac{L}{2} + C_2 \right] = 0$$

$$C_1 \frac{L}{2} + C_2 = 0$$

$$C_2 = -C_1 \frac{L}{2}$$

$$C_2 = \frac{\pi L}{\lambda}$$

$$C_1 = -\frac{2\pi}{\lambda}$$

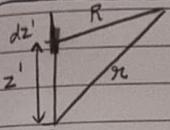
$$C_1 = -\frac{2\pi}{\lambda} = -K$$

$$C_2 = \frac{\pi L}{\lambda} = \frac{KL}{2}$$

$$I(z') = I_0 \sin \left[-Kz' + \frac{KL}{2} \right]$$

$$I(z') = I_0 \sin \left[K \left(\frac{L-z'}{2} \right) \right]$$

for top arm (positive z')



$$A_z = \frac{\mu}{4\pi} \int_{-L/2}^{L/2} \frac{I(z') dz'}{R} e^{-jKR}$$

In phase term $R \approx r - z' \cos \theta$

In amplitude term $R \approx r$

$$A_2 = \frac{\mu}{4\pi} \int_{-L/2}^{L/2} \frac{I(z') dz'}{r} e^{-jk(r-z' \cos \theta)}$$

$$= \frac{\mu e^{-jk\frac{L}{2}}}{4\pi r} \int_{-L/2}^{L/2} I(z') e^{jkz' \cos \theta} dz'$$

→ for whole arm

$$= \frac{\mu e^{-jk\frac{L}{2}}}{4\pi r} \int_{-L/2}^{L/2} I(z') [\cos(kz' \cos \theta) + j \sin(kz' \cos \theta)] dz'$$

$$= \frac{\mu e^{-jk\frac{L}{2}}}{4\pi r} \int_{-L/2}^{L/2} I(z') \cos(kz' \cos \theta) dz' + j \int_{-L/2}^{L/2} I(z') \sin(kz' \cos \theta) dz'$$

even × even → even
odd × odd → odd
even × odd = 0

$$= \frac{\mu e^{-jk\frac{L}{2}}}{4\pi r} \int_0^{L/2} I(z') \cos(kz' \cos \theta) dz'$$

→ for top arm

$$= \frac{\mu I_0 e^{-jk\frac{L}{2}}}{4\pi r} \int_0^{L/2} \sin \left[K \left(\frac{L-z'}{2} \right) \right] \cos(Kz' \cos \theta) dz'$$

$$= \frac{\mu I_0 e^{-jk\frac{L}{2}}}{4\pi r} \int_0^{L/2} \left[\sin \left(\frac{KL - Kz' + Kz' \cos \theta}{2} \right) + \sin \left(\frac{KL - Kz' - Kz' \cos \theta}{2} \right) \right] dz'$$

$$A_2 = \frac{\mu I_0}{4\pi R} e^{-jkR} \left[\underbrace{\int_{z'=0}^{z_2} \sin \left[\frac{KL - kz'}{2} (1 - \cos \theta) \right] dz'}_{I_2} + \underbrace{\int_{z'=0}^{z_2} \sin \left[\frac{KL - kz'}{2} (1 + \cos \theta) \right] dz'}_{I_1} \right]$$

$$I_1 = \int_{z'=0}^{z_2} \sin \left[\frac{KL - kz'}{2} (1 - \cos \theta) \right] dz' \quad \text{Let } \frac{KL - kz'}{2} (1 - \cos \theta) = u$$

$$-k(1 - \cos \theta) dz' = du \\ dz' = -du \\ \frac{dz'}{k(1 - \cos \theta)}$$

$$\begin{aligned} &= \frac{1}{k(1 - \cos \theta)} \cos u \Big|_{z'=0}^{z_2} \\ &= \frac{1}{k(1 - \cos \theta)} \cos \left(\frac{KL - kz'}{2} (1 - \cos \theta) \right) \Big|_0^{z_2} \\ &= \frac{1}{k(1 - \cos \theta)} \left\{ \cos \left[\frac{KL}{2} - \frac{kL}{2} + \frac{kL \cos \theta}{2} \right] - \cos \left[\frac{KL}{2} \right] \right\} \end{aligned}$$

$$I_1 = \frac{1}{k(1 - \cos \theta)} \left\{ \cos \left(\frac{KL \cos \theta}{2} \right) - \cos \left(\frac{KL}{2} \right) \right\}$$

$$I_2 = \int_{z'=0}^{z_2} \sin \left[\frac{KL - kz'}{2} (1 + \cos \theta) \right] dz' \quad \text{Let } \frac{KL - kz'}{2} (1 + \cos \theta) = v$$

$$\begin{aligned} &= \int_{z'=0}^{z_2} \sin v \left(-dv \right) \\ &\quad -k(1 + \cos \theta) dz' = dv \\ &\quad dz' = -dv \\ &\quad \frac{dz'}{k(1 + \cos \theta)} \end{aligned}$$

$$\begin{aligned} I_2 &= \frac{1}{k(1 + \cos \theta)} \cos v \Big|_{z'=0}^{z_2} = \frac{1}{k(1 + \cos \theta)} \cos \left[\frac{KL - kz'}{2} (1 + \cos \theta) \right] \Big|_0^{z_2} \\ &= \frac{1}{k(1 + \cos \theta)} \left\{ \cos \left[\frac{KL}{2} - \frac{kL}{2} - \frac{kL \cos \theta}{2} \right] - \cos \left[\frac{KL}{2} \right] \right\} \end{aligned}$$

$$I_2 = \frac{1}{k(1 + \cos \theta)} \left\{ \cos \left(\frac{KL \cos \theta}{2} \right) - \cos \left(\frac{KL}{2} \right) \right\}$$

$$\begin{aligned} A_2 &= \frac{\mu I_0}{4\pi R} e^{-jkR} \left\{ \frac{1}{k(1 - \cos \theta)} \left[\cos \left(\frac{KL \cos \theta}{2} \right) - \cos \frac{KL}{2} \right] \right. \\ &\quad \left. + \frac{1}{k(1 + \cos \theta)} \left[\cos \left(\frac{KL \cos \theta}{2} \right) - \cos \frac{KL}{2} \right] \right\} \\ &= \frac{\mu I_0}{4\pi R k} \left[\cos \left(\frac{KL \cos \theta}{2} \right) - \cos \frac{KL}{2} \right] \left\{ \frac{1}{1 - \cos \theta} + \frac{1}{1 + \cos \theta} \right\} e^{-jkR} \end{aligned}$$

$$= \frac{\mu I_0}{4\pi R k} \left(\frac{2 \cos \theta}{\sin^2 \theta} \right) \left[\cos \left(\frac{KL \cos \theta}{2} \right) - \cos \frac{KL}{2} \right] e^{-jkR}$$

$$A_2 = \frac{\mu I_0}{2\pi R k \sin^2 \theta} \left[\cos \left(\frac{KL \cos \theta}{2} \right) - \cos \frac{KL}{2} \right] e^{-jkR}$$

$$A_2 = \frac{\mu I_0}{2\pi R k} e^{-jkR} \left[\frac{\cos \left(\frac{KL \cos \theta}{2} \right) - \cos \left(\frac{KL}{2} \right)}{\sin^2 \theta} \right] \quad \text{general expression}$$

(can be used for
any length of dipole)

$$L = \frac{\lambda}{2} \quad K = \frac{2\pi}{\lambda} \quad \frac{KL}{2} = \frac{2\pi}{\lambda} \times \frac{\Delta}{2} \times \frac{1}{2} = \frac{\pi}{2}$$

$$A_2 = \frac{\mu I_0}{2\pi R k} e^{-jkR} \left[\frac{\cos \left(\frac{\pi}{2} \cos \theta \right) - \cos \left(\frac{\pi}{2} \right)}{\sin^2 \theta} \right]$$

$$A_2 = \frac{\mu I_0}{2\pi R k} e^{-jkR} \frac{\cos \left(\frac{\pi}{2} \cos \theta \right)}{\sin^2 \theta} \quad \text{for } \frac{\lambda}{2} \text{ dipole}$$

To find fields

$$\bar{H} = \frac{1}{\mu} \nabla \times \bar{A} = \frac{1}{\mu r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & \bar{a}_\theta & \bar{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & A_\theta & A_\phi \end{vmatrix}$$

Dipole is about z-axis; ϕ symmetry (no variation)

$$A_r = A_z \cos\theta \quad A_\phi = 0$$

$$A_\theta = -A_z \sin\theta$$

$$\bar{H} = \frac{1}{\mu r^2 \sin\theta} \begin{vmatrix} \bar{a}_r & \bar{a}_\theta & \bar{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & 0 \\ A_r & A_\theta & 0 \end{vmatrix}$$

$$= \frac{1}{\mu r^2 \sin\theta} \left\{ \left[\frac{\partial (r A_\phi)}{\partial r} - \frac{\partial A_r}{\partial \theta} \right] \sin\theta \bar{a}_\phi \right\}$$

$$\bar{H} = \frac{1}{\mu r} \left[\frac{\partial (r A_\phi)}{\partial r} - \frac{\partial A_r}{\partial \theta} \right] \bar{a}_\phi$$

$$H_\phi = \frac{1}{\mu r} \left[\frac{\partial}{\partial r} \left[r \cos\theta \frac{\mu I_0}{2\pi r k} e^{-jkR} \frac{\cos(\frac{\pi}{2} \cos\theta)}{\sin^2\theta} \right] \right]$$

$$H_\phi = \frac{1}{\mu r} \left[\frac{-\partial (r \sin\theta A_z)}{\partial r} - \frac{\partial (A_z \cos\theta)}{\partial \theta} \right]$$

$$= \frac{1}{\mu r} \left[-\sin\theta \left\{ A_z + r \frac{\partial A_z}{\partial r} \right\} + \sin\theta \frac{\partial A_z}{\partial \theta} \right]$$

$$H_\phi = \frac{\sin\theta}{\mu r} \left[\frac{\partial A_z}{\partial \theta} - A_z - r \frac{\partial A_z}{\partial r} \right]$$

$$H_\phi = \left\{ \frac{1}{\mu r} \frac{\partial (r A_\phi)}{\partial r} - \frac{1}{\mu r} \frac{\partial A_r}{\partial \theta} \right\}$$

$$\frac{1}{\mu r} \frac{\partial (r A_\phi)}{\partial r} = \frac{1}{\mu r} \frac{\partial}{\partial r} (-r \sin\theta A_z)$$

$$= \frac{1}{\mu r} \frac{\partial}{\partial r} \left\{ -r \sin\theta \times \frac{\mu I_0}{2\pi r k} \frac{e^{-jkR}}{\sin^2\theta} \frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{\sin^2\theta} \right\}$$

$$= \frac{1}{\mu r} \times \frac{-\mu I_0}{2\pi r k \sin\theta} \left\{ \frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{2} \right\} \frac{\partial}{\partial r} (e^{-jkR})$$

$$= -\frac{I_0}{2\pi k r \sin\theta} \left(\frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{2} \right) (-jk) e^{-jkR}$$

$$\frac{1}{\mu r} \frac{\partial (r A_\phi)}{\partial r} = \frac{j I_0}{2\pi r} \left(\frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{\sin\theta} \right) e^{-jkR}$$

$$\frac{-1}{\mu r} \frac{\partial (A_z)}{\partial \theta} = \frac{-1}{\mu r} \frac{\partial (A_z \cos\theta)}{\partial \theta}$$

$$= -\frac{1}{\mu r} \frac{\partial}{\partial \theta} \left\{ \frac{\mu I_0}{2\pi r k} e^{-jkR} \frac{(\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})) \cos\theta}{\sin^2\theta} \right\}$$

$$= -\frac{I_0}{2\pi r^2 k} \frac{\partial}{\partial \theta} \left\{ \left(\frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{2} \right) \left(\frac{\cos\theta}{\sin^2\theta} \right) \right\}$$

This term varies with $\frac{1}{r^2}$ and hence does not contribute to radiation/distant field and can be ignored while computing the expression for H_{rad}

for finite length dipole

$$H_{\phi \text{ rad}} = \frac{j I_0}{2\pi r} e^{-jkR} \left\{ \frac{\cos(\frac{\pi}{2} \cos\theta) - \cos(\frac{\pi}{2})}{\sin\theta} \right\}$$

$$E_{\text{rad}} = \eta H_{\text{rad}}$$

$$S = \frac{1}{2} \operatorname{Re} \left\{ E_{\text{rad}} H_{\phi, \text{rad}}^* \right\} = \frac{1}{2} \operatorname{Re} \left\{ \eta H_{\phi, \text{rad}} H_{\phi, \text{rad}}^* \right\}$$

$$S = \frac{\eta}{2} |H_{\phi, \text{rad}}|^2$$

Power density in W/m^2

$$P = \int S \cdot da = \int \int S r^2 \sin \theta d\theta d\phi$$

Area

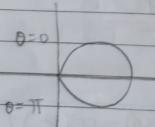
$$= \int_0^{\pi} \int_0^{2\pi} \frac{\eta}{2} \left\{ \left[\left(\frac{I_0}{2\pi R} \right) \left(\frac{\cos(kL \cos \theta) - \cos(kL)}{2} \right) \right]^2 \right\} r^2 \sin \theta d\theta d\phi$$

$$= \frac{\eta}{2} \int_0^{2\pi} d\phi \int_0^{\pi} \frac{I_0^2}{4\pi^2 R^2} \left[\frac{\cos(kL \cos \theta) - \cos(kL)}{2} \right]^2 \frac{r^2 \sin \theta}{\sin^2 \theta} d\theta$$

$$= \frac{\eta}{2} \times \frac{I_0^2}{4\pi^2} \times 2\pi \int_0^{\pi} \frac{\left[\cos(kL \cos \theta) - \cos(kL) \right]^2}{\sin \theta} d\theta$$

$$P = \frac{\eta I_0^2}{4\pi} \int_0^{\pi} \frac{1}{\sin \theta} \left[\cos\left(\frac{kL \cos \theta}{2}\right) - \cos\left(\frac{kL}{2}\right) \right]^2 d\theta$$

Power in watts (can be found for a specific L)



$$U \propto \sin^2 \theta$$

$$U = 0 \quad \theta = 0, \pi$$

$$\text{Null to Null Beam Width} = \pi - 0 = \pi$$

$$= 180^\circ$$

22/2/24

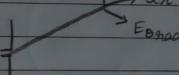
POYNING VECTOR

The instantaneous Poynting vector is the cross-product of instantaneous electric field vector and instantaneous magnetic field vector

$$\tilde{S} = \tilde{E} \times \tilde{H}$$

Direction of $\tilde{E} \times \tilde{H}$ indicates the direction of wave propagation (or the direction of power flow)

$$\bar{S} = \frac{1}{T} \int_0^T \tilde{S} dt$$



For the Hertzian dipole

$$H_{\phi, \text{rad}} = \frac{jK I d \sin \theta}{4\pi R} e^{-jkR}$$

$$e^{j\pi/2} = \cos \frac{\pi}{2} + j \sin \frac{\pi}{2} = j$$

$$= \frac{K I d \sin \theta}{4\pi R} e^{-jkR} e^{j\pi/2}$$

$$H_{\phi, \text{rad}} = H_{\phi_0} e^{-j(kR - \pi/2)}$$

$$E_{\phi, \text{rad}} = \eta H_{\phi, \text{rad}} = \eta H_{\phi_0} e^{-j(kR - \pi/2)}$$

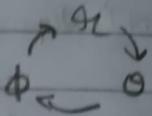
$$\tilde{H}_{\phi, \text{rad}} = \operatorname{Re} \left\{ H_{\phi_0} e^{-j(kR - \pi/2)} e^{j\omega t} \right\}$$

$$= H_{\phi_0} \cos(\omega t - kR + \pi/2)$$

$$\tilde{H}_{\phi, \text{rad}} = -H_{\phi_0} \sin(\omega t - kR)$$

$$\tilde{H}_{\phi, \text{rad}} = -H_{\phi_0} \sin(\omega t - kR) \bar{a}_\phi$$

$$\tilde{E}_{\theta \text{ grad}} = -\eta H_{\phi_0} \sin(\omega t - kr)$$



$$\tilde{E}_{\theta \text{ grad}} = -\eta H_{\phi_0} \sin(\omega t - kr) \bar{a}_y$$

Instantaneous Poynting vector

$$\tilde{\vec{S}} = \tilde{\vec{E}} \times \tilde{\vec{H}} = \eta H_{\phi_0}^2 \sin^2(\omega t - kr) \bar{a}_z$$

Time average of $\tilde{\vec{S}}$ is $\bar{S} = \frac{1}{T} \int_0^T \tilde{\vec{S}} dt$

$$= \frac{\bar{a}_z}{T} \int_0^T \eta H_{\phi_0}^2 \sin^2(\omega t - kr) dt$$

$$= \frac{\eta H_{\phi_0}^2}{2T} \bar{a}_z \int_0^T (1 - \cos[2(\omega t - kr)]) dt$$

$$\bar{S} = \frac{\eta H_{\phi_0}^2}{2T} \bar{a}_z \left\{ t - \frac{1}{2\omega} \sin(2\omega t - 2kr) \right\} \Big|_0^T$$

$$= \frac{\eta H_{\phi_0}^2}{2T} \bar{a}_z \left[(T - 0) - \frac{1}{2\omega} (\sin(2 \times \frac{2\pi}{T} \times T - 2kr) - \sin(-2kr)) \right]$$

$$= \frac{\eta H_{\phi_0}^2}{2T} \left[T - \frac{1}{2\omega} (-\sin(2kr) + \sin(2kr)) \right] \bar{a}_z$$

$$= \frac{\eta H_{\phi_0}^2}{2T} \times T \bar{a}_z$$

$$\bar{S} = \frac{\eta H_{\phi_0}^2}{2} \bar{a}_z$$

$S = \frac{\eta H_{\phi_0}^2}{2}$

Power density. The ~~insta~~ time average of instantaneous poynting vector gives power density