

SATELLITE LINK DESIGN

The satellite communication system design is a complex process, involved compromises between many factors, in order to obtain maximum performance. The factors are:

1. The weight of the satellite.
2. The dc power that can be generated onboard.
3. The maximum dimensions of satellite and ground station antennas.
4. The multiple access technique used to share communication capacity between many earth stations.
5. The frequency band of a satellite.

The weight of the satellite is limited by highest of launching a spacecraft into geostationary orbit. The weight of the satellite is driven by two factors.

- a) The number and output power of transponders on satellites.
- b) Weight of station, keeping fuel.

High power transponders require lots of electrical power, which can only be generated by solar cells. If increasing the total output power of transponders raises the demand for electrical power and also dimensions of solar cells.

A communication system must be designed to meet certain minimum performance standard like minimum tx/rx power and RF bandwidth. SNR is an important parameter.

While designing a satellite system, we must try to guarantee a minimum SNR in the receiver's baseband channel.

Increasing total op power of transponders raises the demand for

"SNR is a channel depends on

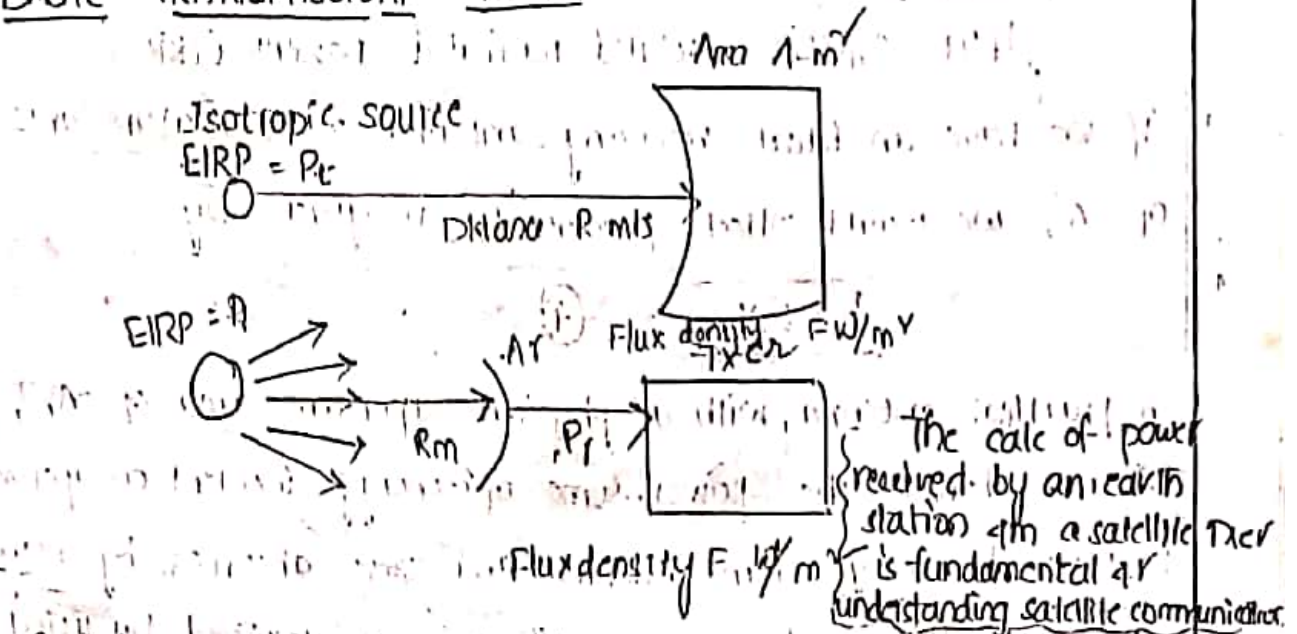
a) g_M of RF signal in receiver.

b) type of modulation used.

c) The RF and channel bandwidth in receiver.

The g/M is calculated at input of receiver and at output terminals of receiving antenna. Designing a satellite system therefore requires knowledge of required performance of uplink & downlink.

BASIC TRANSMISSION THEORY :-



Consider a transmitting source in a free space radiating in all directions (uniformly) with total power P_t . Such a source is called isotropic source. At a distance R mts from hypothetical isotropic source transmitting RF power P_t watts, the flux density crossing the surface of sphere with a radius R is given

by

$$F = \frac{P_t}{4\pi R^2} \quad \text{--- (1)}$$

All real antennas are directional. Any real antenna has a gain $g(\theta)$ is defined as the ratio of power per unit solid angle radiated in a direction θ to average power radiated per unit solid angle.

$$G(\theta) = \frac{P(\theta)}{(P_0/4\pi)} \quad \text{--- (2)}$$

For a transmitter P_t for a driving lossless antenna, with a gain G_t , the flux density in a direction of antenna at a distance R is

$$F = \frac{P_t G_t}{4\pi R^2} \quad \text{--- (3)}$$

$P_t G_t$: effective isolated radiated power = EIRP

If we have an ideal receiving antenna with aperture area of A , we would collect power P_r is given by

$$P_r = F \times A \quad \text{--- (4)}$$

A practical antenna, with a physical aperture area of A_r , will not deliver the power. Some of the energy incident on aperture is reflected away from antenna and some absorbed by lossy components. This reduction in efficiency is described by using an effective aperture A_e .

$$A_e = \eta_A \times A_r \quad \text{--- (5)}$$

η_A : efficiency : $\begin{cases} 50 \text{ to } 75\% \text{ for paraboloid} \\ 90\% \text{ for horn} \end{cases}$

The power received by a real antenna with physical receiving area A_r and effective aperture A_e is given as

$$P_r = \frac{P_t G_t A_e}{4\pi R^2} \quad \text{--- (6)}$$

The fundamental of an antenna theory is gain and

area of antenna is related by

$$G_v = \left(\frac{4\pi}{\lambda^2} \right) A_e \quad \text{--- (7)}$$

$$G_v = \left(\frac{4\pi}{\lambda^2} \right) \left(\frac{P_r}{P_t G_t} \right)$$

$$P_r = \left(\frac{\lambda^2}{4\pi} \right)^2 \frac{P_t G_t G_r}{R^2} = \left(\frac{\lambda}{4\pi R} \right)^2 (P_t G_t G_r)$$

$$P_r = \underbrace{\left(\frac{\lambda}{4\pi R} \right)^2}_{\text{Path loss}} P_t G_t G_r$$

Collecting various factors, we can write

$$P_r = \frac{(EIRP) \times \text{Received antenna gain}}{\text{Path loss } (L_p)}$$

$$P_r \text{ db} = [EIRP + G_r - L_p] \text{ db} \quad \text{--- (8)}$$

The equation 8 represents in ideal condition. But in practice we need to consider

- 1) Atmospheric loss due to signal attenuation by rain, water, water.
- 2) Losses due to antenna at the each end of the link.
- 3) Possible loss of gain due to antenna mispointing.

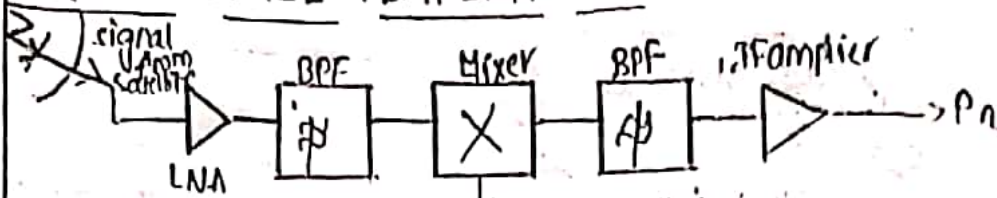
$$P_r = EIRP + G_r - L_p - L_a - L_{ta} - L_{ra}$$

L_a : atmospheric loss

L_{ta} : loss associated with txing antenna.

L_{ra} : loss associated with Rxing antenna.

SYSTEM SIGNAL NOISE TEMPERATURE



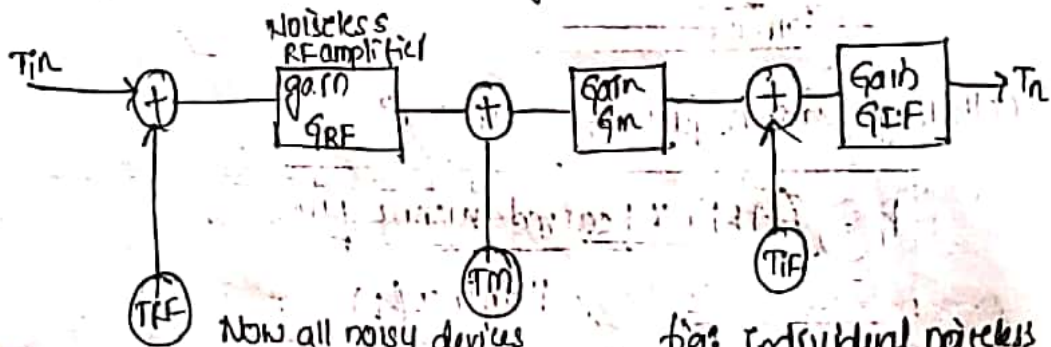
As FET
temp \rightarrow 30K - 200K
30 Kelvin for 4GHz
100 Kelvin for 11GHz

Local oscillator

\rightarrow consider a general translation radi with antenna, RF or freq converter, 10% IF amplifier

\rightarrow Now above ckt can be represented by an equl noise generators.

Equivalent ckt for above design



Now all noisy devices are replaced by a simple noise source

fig: Individual noiseless devices with fig + noiseless amp & freq converter.

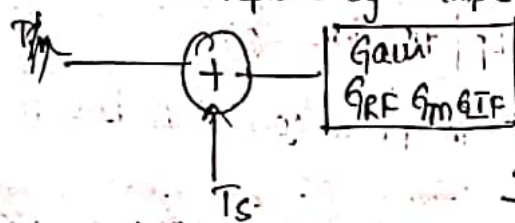


fig: single noise source

from fig 1 $P_n = K T_{IF} G_{IF} B + K T_m G_{IF} G_m B + K T_{RF} G_{IF} G_m G_{RF} B$ (1)

from fig 2 $P_n = K G_{RF} G_m G_{IF} T_s B$ (2)

From equation (1)

$$P_n = K G_{RF} G_m G_{IF} B \left[\frac{T_{IF}}{G_{RF}} + \frac{T_m}{G_{RF}} + T_{RF} + T_{in} \right]$$

from eq's (2) & (3)

$$T_s = \frac{T_{IF}}{G_m G_{RF}} + \frac{T_m}{G_{RF}} + T_{RF} + T_{in}$$
(4)

Noise figure is used frequently used to specify the noise generated within a device.

$$\text{Noise figure} = \frac{(S/N)_{\text{in}}}{(S/N)_{\text{out}}}$$

Because noise temperature is more useful in satellite communication systems. It is best to convert noise figure to noise temperature.

$$T_d = T_0 [NF - 1]$$

T_0 : reference temp = 290K

T_d : noise temp

NF: Noise figure.

G/T ratio for earth station:

The link equation can be rewritten in terms of C/N is

$$C/N = \frac{P_t G_t G_r}{K T_s B} \left[\frac{\lambda}{4\pi R} \right]^2$$

$$C/N = \left[\frac{P_t G_t}{K B} \right] \left[\frac{\lambda}{4\pi R} \right]^2 \left[\frac{G_r}{T_s} \right]$$

$(C/N) \propto \left(\frac{G_r}{T_s} \right) \rightarrow$ for determining quality in system.

$\frac{G_r}{T_s}$ also called as figure of merit.

If you want to calculate carrier to noise ratio, (downlink)

$$C/N = \frac{\text{Power input}}{\text{Noise power}}$$

$C/N = \frac{P_r G_r}{K T_s B G_x}$ \rightarrow A standard A authorization used in initial n/w is required to have a G/T ratio of 40.7 dB/K at 49h3 & 5° elevation angle.

$$\frac{C}{N} = \frac{P_r}{K T_s B}$$

Satellite systems using small earth stations:-

Direct Broadcast TV (DBS-TV or DTH)

Europe - Analog - FM tx'n

USA - digital tx'n

Hughes Company } - 200 television and audio channels.

Typical mass of domestic satellite - 6800 kg

4.2 GHz \rightarrow 4 spotbeam \rightarrow 1.4 m

diameter of satellite antenna.

DIRECT BROADCAST SERVICE:-

C/N calculation is simplified by use of "LINK BUDGET". A

link budget is a tabular form method for evaluating received power and noise power in a radio link.

LINK BUDGET FOR KU BAND DBS-TV RX'er:-

DBS-TV terminal rx'd signal power:-

Transponder o/p power 160W	22.0 dBW
Antenna beam on axis	34.3 dB
RX'ing antenna gain on axis	33.5 dB
Path loss at 12.2 GHz, 38,000 km	-205.7 dB

Above values belongs to united states DBS TV

Edge of beam loss	-3.0 dB
Clearsky atmosphere	-0.4 dB
Rx'd power C/N	-119.7 dBW

DBS-TV terminal Rx'd noise power

Boltzmann's constant : -228.6 dBW/K/Hz

clearsky noise temperature : 21.6 dBK

Rxer noise bandwidth : 73.0 dBHz

noise power : -134.0 dBW

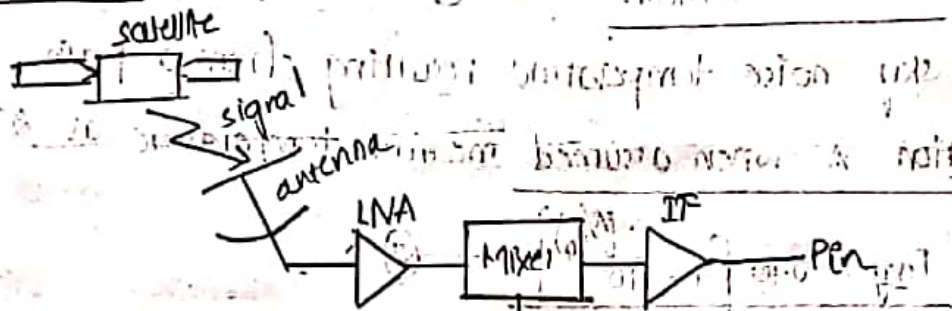
DBS-TV terminal c/N in clearsky

clearsky overall c/N : 14.3 dB

link margin over 8.6 dB threshold is 5.7 dB

link availability throughout is better than 99.7%

Calculations:-



$$A = (A_{at} + A_{rain}) \text{ dB} \quad \text{--- (1)}$$

$$T_{sky} = \text{sky noise temperature} \approx 270 \text{ K} \quad \text{--- (2)}$$

$$T_S = T_{LNA} + T_A \quad \text{--- (3)}$$

T_A : Antenna noise temperature

T_{LNA} : low noise amplifier

$$T_A = T_{sky} \times \eta_c \quad \text{--- (4)}$$

η_c : coupling coefficient

$$\Delta N_{rain} = \left[\frac{k T_{rain} B_n}{k T_{sca} B_n} \right]$$

(C/N) dn rain ↓

downlink when
rain attenuation is present.

Theory:-

The C/N ratio in home receiver will fall when rain is present in a path between satellite & receiver antenna. Much of reduction in C/N ratio is caused by sky noise temperature. The total attenuation is given as

N.B. A_0 = attenuation due to clear sky atmospheric gases +
attenuation due to rain

$$A_0 = A_{atm} + A_{rain} \quad \text{--- (1)}$$

The sky noise temperature resulting from a path attenuation A when assumed medium temperature as 270K, then

$$T_{sky} = 270 \left[1 - 10^{-\frac{A}{10}} \right] \quad \text{--- (2)}$$

The antenna noise temperature may be assumed to be equal to sky noise temperature. The coupling coefficient η_c of 90-95% is often used when calculating antenna noise temperature.

$$T_A = \eta_c \times T_{sky} \quad \text{--- (3)}$$

The system noise temperature when a satellite receiver using high gain low noise amplifier is given as

$$T_S = T_{LNA} + T_A \quad \text{--- (4)}$$

T_A : Antenna's noise temperature.

We will assume there are no feed losses. The increase in noise power ΔN_{rain} caused by increase in sky noise temperature

$$\Delta N_{rain} = 10 \log_{10} \left[\frac{K T_{s,rain} B_n}{K T_{sca} B_n} \right] \text{ dB} \quad \text{--- (5)}$$

The total received power is reduced by attenuation caused by rain, so in rain the carrier power value is

$$C_{rain} = [C_{ca} - A_{rain}] \text{ dB} \quad \text{--- (6)}$$

The resulting C/N downlink rain gives

$$(C/N)_{dn,rain} = (C/N)_{dn,ca} - A_{rain} - \Delta N_{rain} \quad \text{--- (7)}$$

Design for uplink and downlink:

① The primary objective is to guarantee continuity of link.

② To provide many channels in a minimum capital cost.

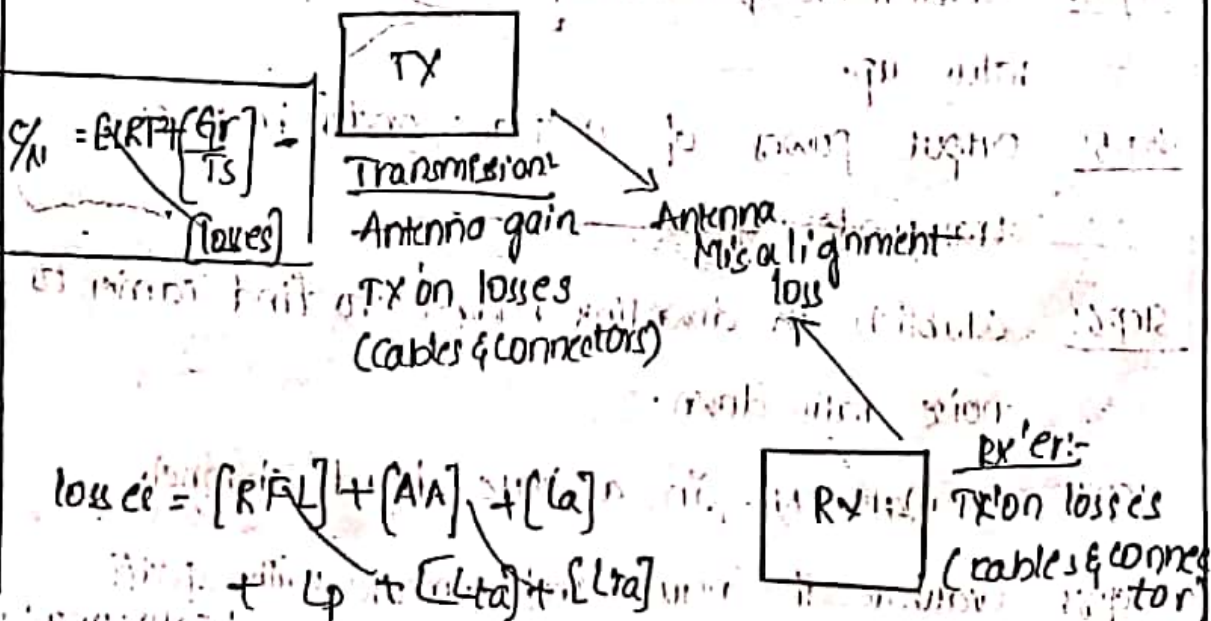
LINK BUDGET:-

$$(C/N)_{uplink} = [EIRP] + [G_r] + [L_A] - [losses] - (C/N)_0 = (C/N)_0 \text{ up} + (C/N)_0 \text{ down} \rightarrow \text{bent pipe}$$

$$(C/N)_0 \text{ downlink} = [EIRP]_{dn} + [G_t]_{dn} - [L_A] - [K] - [B_0]_{\text{dB}}$$

BoI: Input back of

LINK POWER BUDGET:-



$$P_r = [EIRP] + [G_r] - [\text{losses}]$$

$$\text{losses} = [FSL] + [RFL] + [AML] + [AA] + [PL]$$

FSL : free space loss in db

RFL : Receiver feeder loss in db

AA : Atmospheric absorption loss in db

AML : antenna misalignment loss

PL : Depolarisation loss

System Noise temp : Thermal noise due to active & passive components.

Noise temp of Rxcr : Thermal noise due to RF amplifier, mixer and IF amplifier.

20-9-13

* Satellite communication link design procedure

Step 1: choose the frequency band for your system.

Step 2: Determining the parameters of communication.

Step 3: Determine the parameters of rxing & txing earth stations (antenna gain, temperature, efficiency etc).

Step 4: Establish an uplink budget to find carrier to noise ratio up.

Step 5: output power of a transponder based on transponder gains.

Step 6: Establish an downlink budget to find carrier to noise ratio down.

Step 7: calculate SNR in a base band channel.

Step 8: Evaluate the result and compare with specific requirements.

Step 9: Choose the propagation method.

Step 10: Re-design the system with modified parameters.

Design of specified C/N:

- 1) Hypothetical reference circuit.
- 2) C/N & C/I addition.
- 3) Reciprocal method.

Reciprocal method:-

$$(C/N)_0 = \frac{1}{\left[\frac{1}{(C/N)_1} + \frac{1}{(C/N)_2} + \frac{1}{(C/N)_3} + \dots \right]} \quad \text{--- ①}$$

$$(C/N)_0 = \frac{C}{[N_1 + N_2 + N_3 + \dots]}$$

In decibels

$$(C/N)_0 = C \text{ dBW} - 10 \log (N_1 + N_2 + N_3 + \dots) \text{ dB.}$$

C: single carrier power C.

Specific thumbrules:-

1) If both (C/N) values are equal, (C/N)₀ is 3dB of either value.

$$2) \quad (C/N)_{up} = 20 \text{ dB}$$

$$(C/N)_{down} = 20 \text{ dB}$$

$$(C/N)_{out} = ?$$

$$(C/N)_0 = \frac{1}{\frac{1}{(C/N)_{up}} + \frac{1}{(C/N)_{down}}} = \frac{1}{\frac{1}{100} + \frac{1}{100}} = 50$$

$$(C/N)_{out} \text{ dB} = 10 \log (50) = 16.98 \text{ dB}$$

$$(C/N)_{out} = 17 \text{ dB}$$

2) If one C/N value is 10db smaller than other (C/N) value, $(C/N)_0$ is 0.4db smaller than smaller of C/N value.

3) If one C/N value is 20db (or more) greater than other (C/N) value, the overall (C/N) is equal to smaller of 2 (C/N) values within accuracy of decibel calculations.

Eq- $(C/N)_{up} = 20db = 10^4$ $10 \log x = 20$
 $x = 10^4$
 $(C/N)_{dn} = 20db = 10^2$ $10 \log x = 20$
 $x = 10^2$

① $(C/N)_0 = \frac{1}{\frac{1}{10^4} + \frac{1}{10^2}} = 99,0099$
 $(C/N)_0 \text{ db} = 10 \log(99,0099)$
 $= 19,95678$
 $\approx 20db$

* Rain attenuation in uplink and downlink:

$$(C/N)_{0, \text{rain}} = \frac{1}{\left[\frac{1}{(C/N)_{\text{uplink}}} + \frac{1}{(C/N)_{\text{downlink}}} \right]}$$

$$(C/N)_{0, \text{uplink}} = [(C/N)_{\text{clear air}} - A_{\text{rain}}] \text{ db}$$

$$(C/N)_{0, \text{downlink}} = [(C/N)_{\text{clear air}} - A_{\text{rain}}] \text{ db}$$

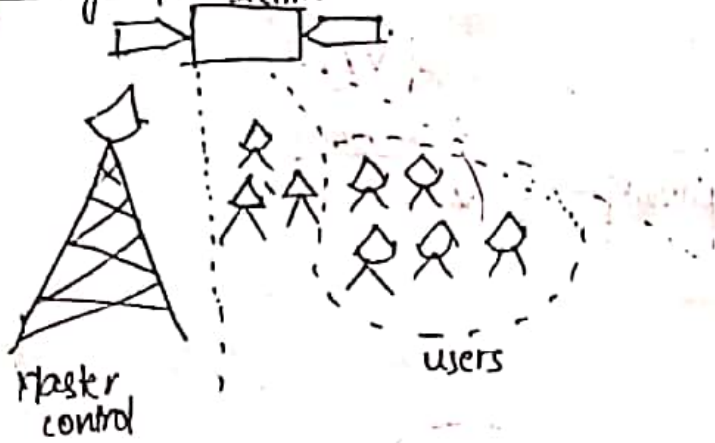
22-9-13

* VSAT: [Very Small Aperture terminal]

architecture of VSAT network:-

- 1) One way implementation
- 2) Split two way implementation (split IP)
- 3) Two way implementation
 - Star
 - Mesh

One-way Imp. no. in line

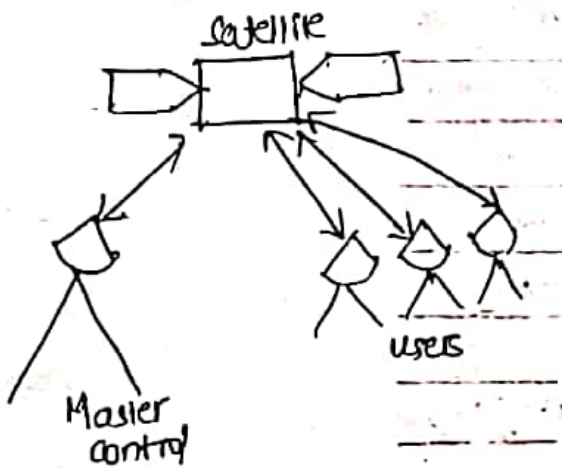


TERIP \rightarrow n/w layer

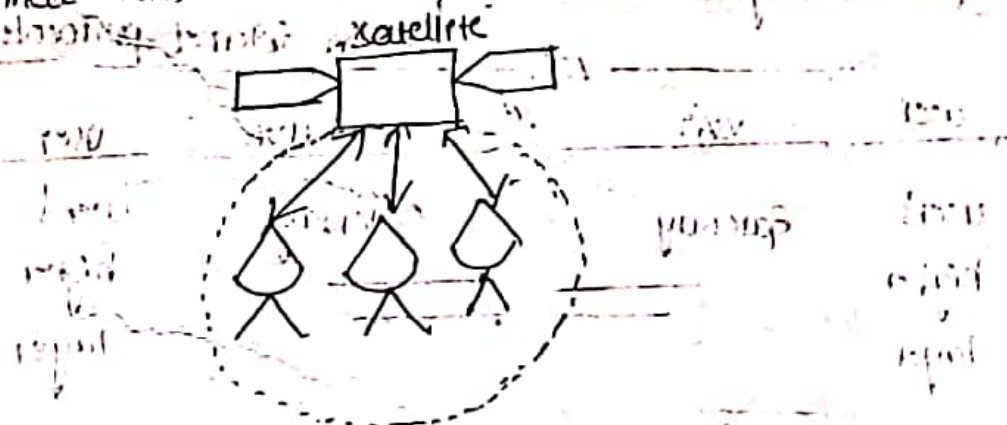
layers

1. Physical layer
2. Datalink layer
3. n/wing layer
4. Transport layer
5. Presentation layer
6. Session layer
7. Application layer

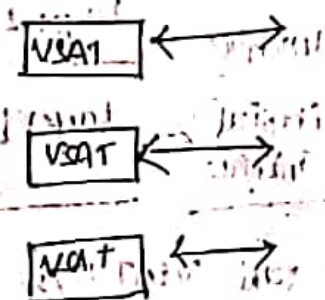
Star architecture



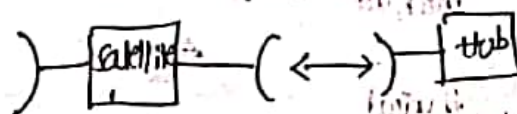
In Mesh, without design of hub station, any user can connect with another user.



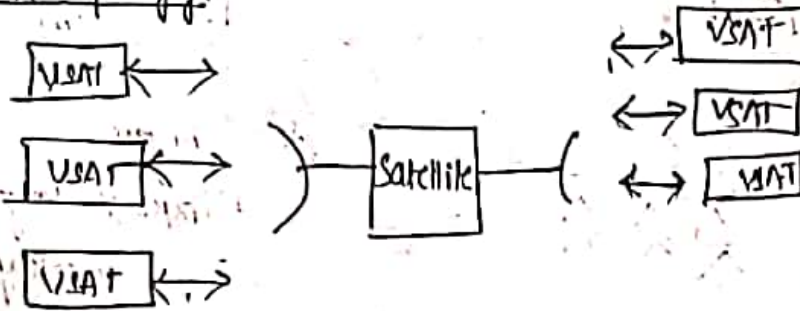
Satellite topology view:



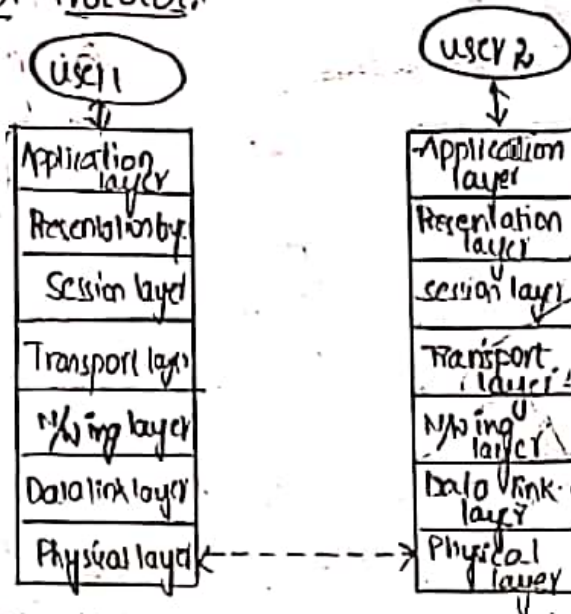
Star topology



Mesh topology:



Access Control Protocol:-

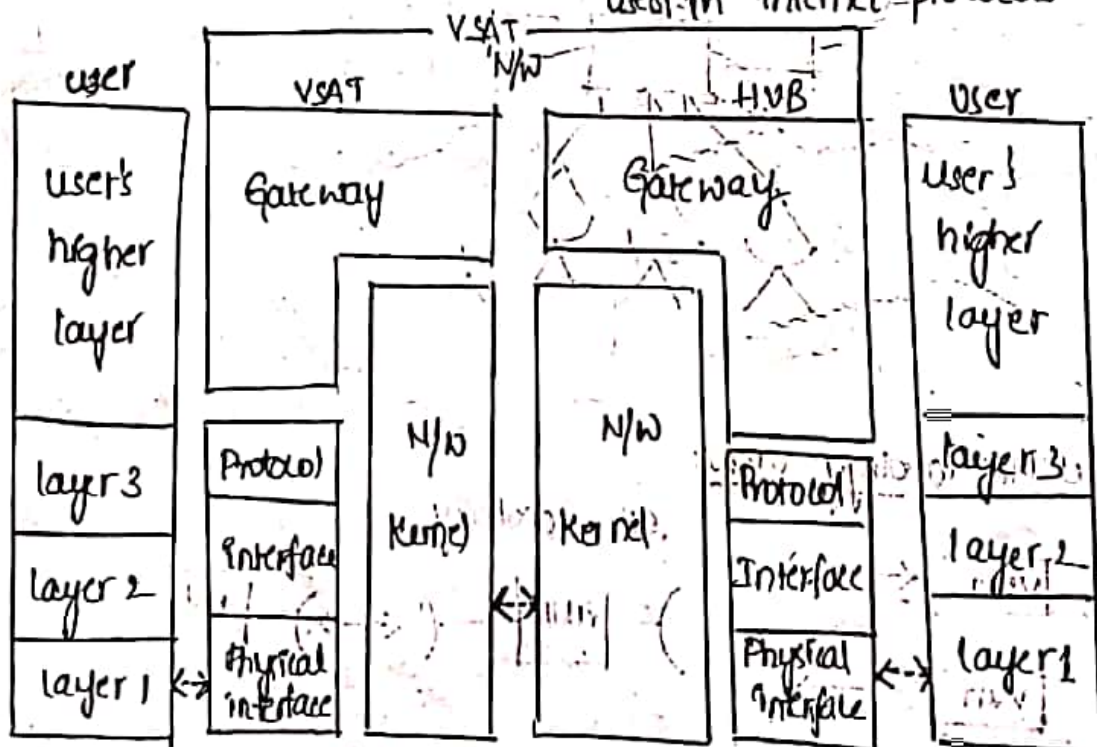


① Acknowledgement (ACK)

② Non-Acknowledgement (NAK)

→ Automatic Repeat request (ARQ)

used in internet protocols.



figs Protocol architecture of sat VSAT N/w

"Spoofing" - separating the satellite link and terrestrial link.

- 1. modulo-8 } operations made by users while forming a link.
- 2. modulo-128

modulo-8 : user can transmit 7 packets at a time.

modulo-128 : user can transmit 127 packets at a time. Most VSATs uses this modulo-128 operation.

VSAT EARTH STATION ENGINEERING:

- 1. outdoor unit (ODU) :-
- 2. Inter-facility link (IFL) :-
- 3. Indoor Unit (IDU) :-

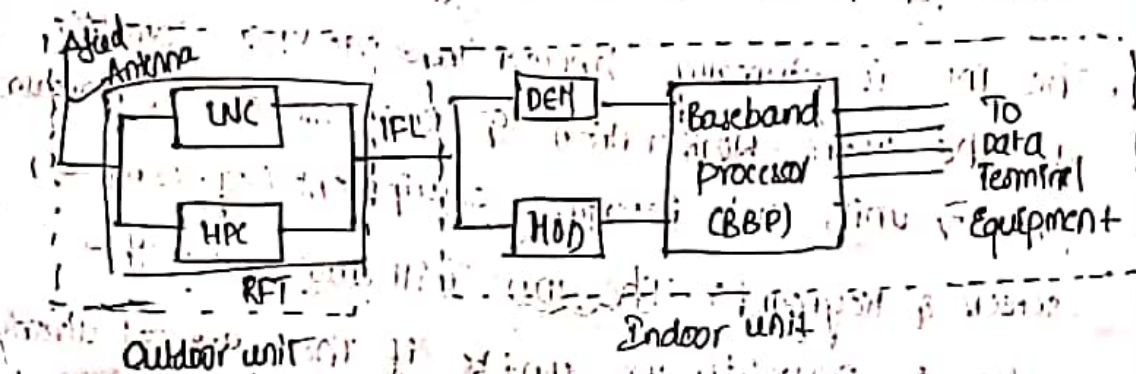
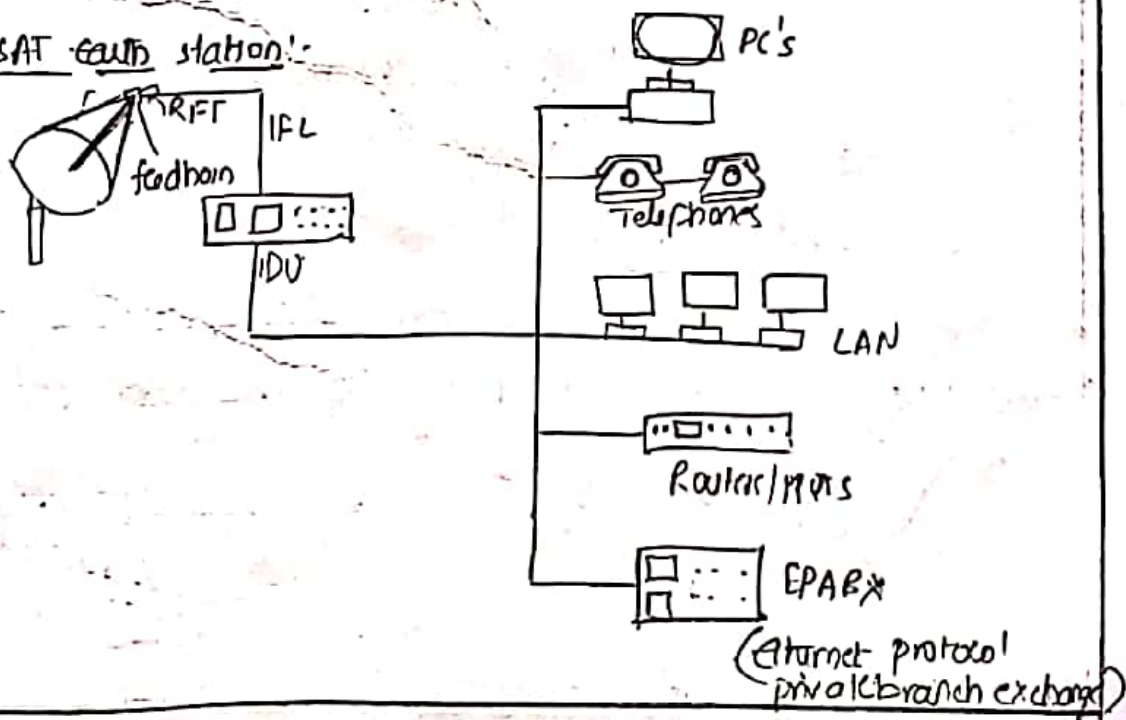


fig: VSAT earth station block dgm.

VSAT earth station:-



Horn \rightarrow more coverage antenna

DTH \rightarrow antenna \rightarrow cable gain-fed system

priced away
antenna \rightarrow Telephone conversation

* VSAT Earth Station:-

The VSAT outdoor unit is located where it will have a clear line of sight to the satellite & is free from casual blockage by people and/or equipment moving in front of it. It includes the Radio freq. transceiver (RFT).

The Interfacility link (IFL) carries the electronic signal b/w the ODU and the indoor unit as well as power cables for the ODU & control signals from the IDU.

The IDU is normally housed in a desktop computer at the user's workstation & consists of the baseband processor units and interface equipment (eg. computer screen & keyboard). The IDU will also house the modem & mux/demux units if these are not already housed in the ODU.

UNIT-III : GLOBAL POSITIONING SYSTEM

Navigation satellite Timing & Ranging.

NAVSTAR \rightarrow first GPS satellite - 1978 - U.S.

later it is converted into GPS satellite.

24 GPS satellites are launched by us.

4 satellite \rightarrow constellation
together

Placed at 12,000 kms away - from the surface of earth.

12 : ^{public use} precise code \rightarrow L band
11 : military code

GPS is a space-based satellite navigation system.

Galileo - European

Glonass - Russia

Navstar - USA

GPS satellite Vehicle

• 4 atomic clocks

• 3 Ni-cd battery

• Two solar panels

\rightarrow battery charging

200W \rightarrow 1136W

\rightarrow power generation

S band \rightarrow satellite control

GPS signals:

• signals driven by an atomic clock.

\rightarrow fundamental freq at 10.23 MHz

• 2 carrier signals (sine waves)

\rightarrow L1 : $f = 1575.43 \text{ MHz}$ ($\lambda = 19 \text{ cm}$)

\rightarrow L2 : $f = 1227.6 \text{ MHz}$ ($\lambda = 24 \text{ cm}$)

→ephemeris → stores information in a tabular form.

→almanacs → status of satellite orbit

* GPS are made up of 3 segment

1. space segment: 6 orbital planes are placed with an inclination of 55° .

2. user segment.

3. control segment.

* 1 sidereal period = 2 [time of GPS to rotate].

* CS consists of 3 entities

1. Master control system.

2. Monitor station.

3. Ground antennas.

• Receiver performs following tasks:

1. selecting one or more satellites.

2. Acquiring GPS signals.

3. Measuring & tracking.

4. Recovering navigation data.

GPS provides

• SPS → standard positioning service → C/A code → used for general purpose. → Civilian purpose

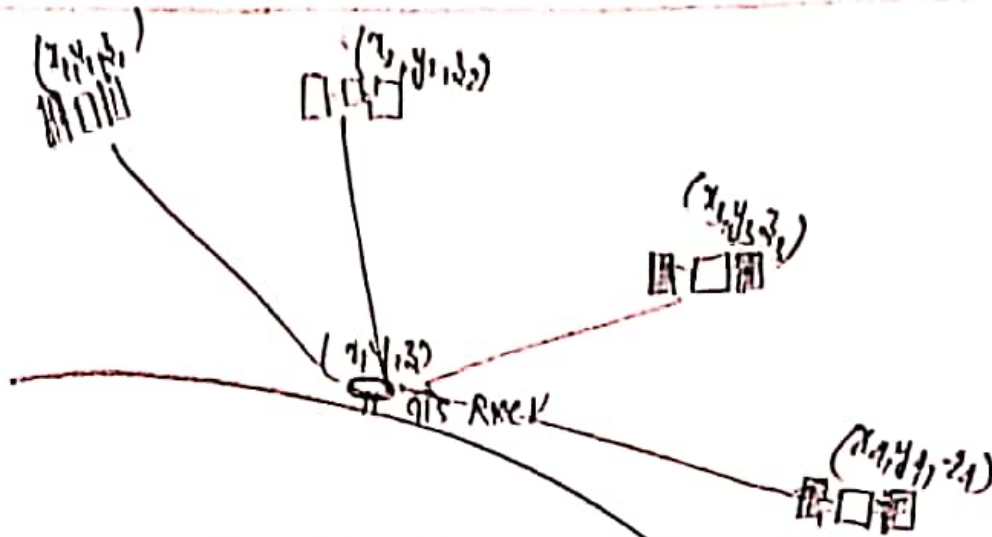
• PPS → precise positioning service.

• C/A → coarse/acquisition or clear/access. ← SPS

• PPS → both P code and C/A code.

• Trilateration method → method used to locate the user on the surface of the earth.





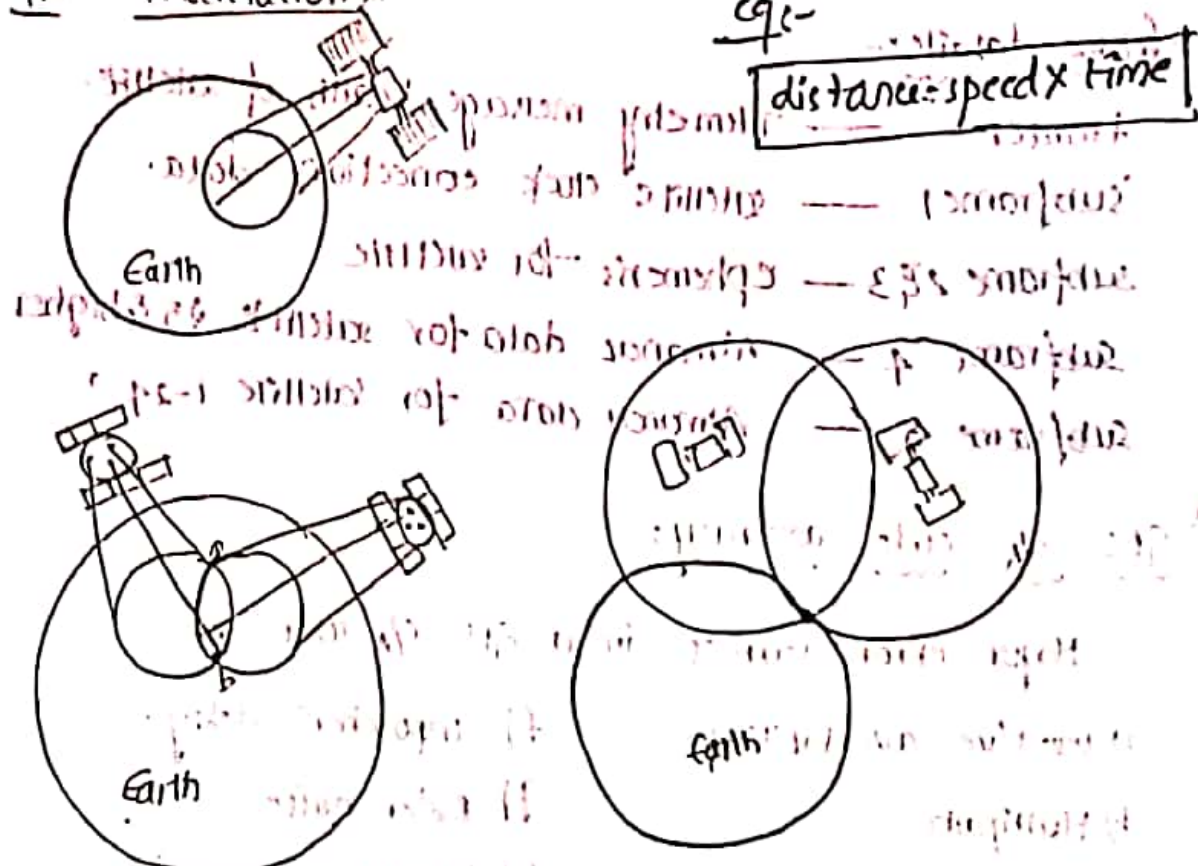
$$S_1 = \sqrt{(x_1 - x)^2 + (y_1 - y)^2 + (z_1 - z)^2} + c \cdot \Delta t$$

$$S_2 = \sqrt{(x_2 - x)^2 + (y_2 - y)^2 + (z_2 - z)^2} + c \cdot \Delta t$$

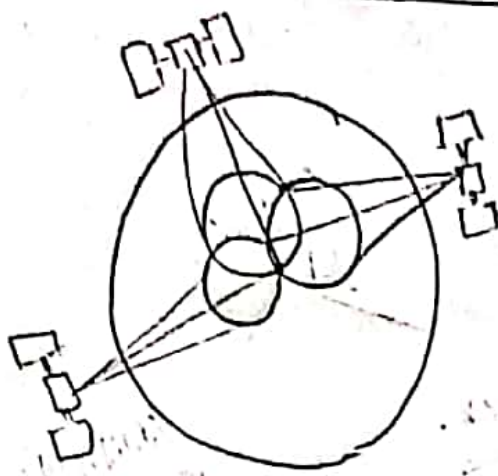
$$S_3 = \sqrt{(x_3 - x)^2 + (y_3 - y)^2 + (z_3 - z)^2} + c \cdot \Delta t$$

$$S_4 = \sqrt{(x_4 - x)^2 + (y_4 - y)^2 + (z_4 - z)^2} + c \cdot \Delta t$$

GPS Trilateration



Distance of GPS satellites from surface of earth is 20,200 km
Placed in MEO orbit.



Milestones of satellite systems:-

Introduction:-

From invention to upto now.

1st unit \rightarrow history of satellite.

GPS navigation message:-

1500 bits \rightarrow 12.5 minutes.

frame details:-

Header

Telemetry message health of satellite.

Subframe 1 — satellite clock correction data.

Subframe 2 & 3 — ephemeris for satellite

Subframe 4 — Almanac data for satellite 25 & higher

Subframe 5 — Almanac data for satellite 1-24

GPS C/A code accuracy:-

Major error sources in a GPS C/A code are:

a) selective availability.

f) Tropospheric delay.

b) Multipaths.

g) Receiver noise.

c) satellite clock.

h) Satellite geometry.

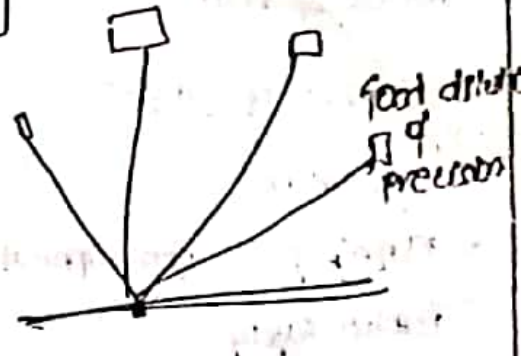
d) Ephemeris error.

e) Ionospheric delay.

The selective availability was designed by the Department of Defense which deliberately degrades the signal and provides less accuracy in determining the position of a user on earth. It is switched off on May 1, 2000.

Ionosphere - X-rays & UV rays present in ionosphere.

Dilution of precision:- [Satellite Geometry]



Four dilution of precision:-

GDOP :- A combination of navigational position & time geometric error.

PDOP :- The spatial geometrical quality of the positional solution.

HDOP :- Horizontal :- Measure of the quality of the horizontal position.

VDOP :- Vertical :- Measure of the quality of the vertical position.

TDOP :- Time :- Mean error of the time estimation.

As DOP \uparrow , accuracy \downarrow

DOP —

ROP Rating

1 Ideal

2-3 Excellent

4-6 Good

7-8 Moderate

9-20 Fair

20-50 Poor

Applications of GPS

Industry

- 1) Agriculture.
- 2) Mapping & Geographical Information system (GIS) data collection
- 3) Public safety.
- 4) Surveying.
- 5) Telecommunications.

Military

- Intelligence & Target location.
- Navigation.
- Weapon aiming & Guidance.

Transportation

- Aviation.
- Fleet tracking.
- Marine.

Science

- Archeology.
- Atmospheric science.
- Environmental.
- Geology & Geophysics.
- Oceanography.
- Wildlife.

SPADE:-

single channel ^{carrier} per carrier ^{PCM} multiple access demand alignment technique. It is an example of CDMA.

→ With SPADE, 800 PCM encoded voice band channels separately QPSK modulate on IF carrier signal [Hence named as single channel per carrier].

→ Each 4 kHz voice band channel is sampled at 8 kHz rate and are converted into 8 bit PCM code.

⇒ 30 4 kbps PCM code for each voice band channel.

→ For QPSK, min req b-w = $\frac{1}{2}$ bitrate = 30 kHz.

→ Each channel is allocated 45 kHz with 13 kHz as GP.

→ 36 MHz is divided producing 2 400 channel bands (each 45 kHz)

⇒ 600 channels for TX and 400 for RX.

→ Channels 1, 2 & 400 are left unused. So used band channels are 397.

→ Centre of transponder band is marked by pilot freq. (7.04 MHz)

→ Each RF channel capacity is 397.

→ Each RF channel has CSC

CSC code is used to establish or disconnect voice band link when 2 earth stations. When demand alignment channel allocation is used.