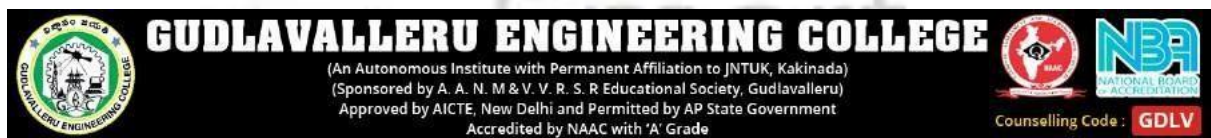


Internship Program Report

By

BANAVATHU SYAM NAYAK-19485A0259



In association with



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Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil& Gas, Power and Utility industrial sectors.

Program organiser

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical



sessions and Industrial Automation projects.

Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Mr. G. Srinivasa Rao – Internship coordinator

Mr. Ramesh V - Mentor

Mr. Vinay Kumar - System Support

Mr. Harikanth – Software/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May 2021

Daily schedule time shall be 4PM to 6.30PM

Mode of Classes: On line through ZOOM

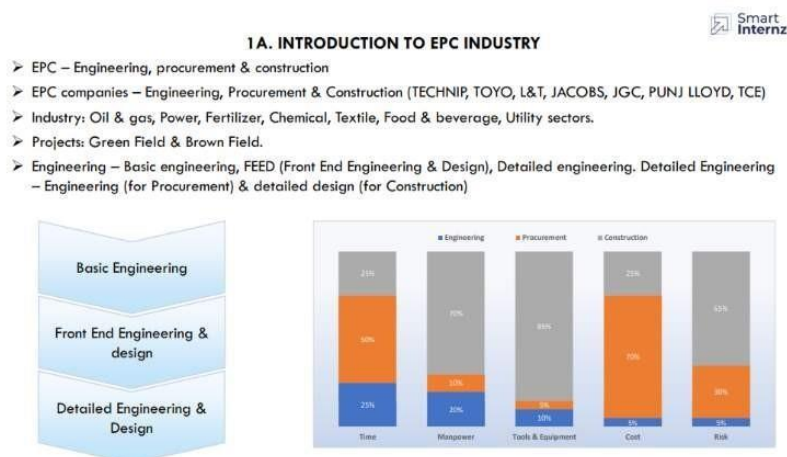
Presenter: Mr Ramesh V

Internship program

We have been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

3rd May2021: Introduction to EPC Industry

1	EPC Industry & Electrical Detailed Engineering	EPC Industry	Introduction
		Engineering	Types of Engineering
		Procurement	Engineering role in procurement
		Construction	Engineering role during construction



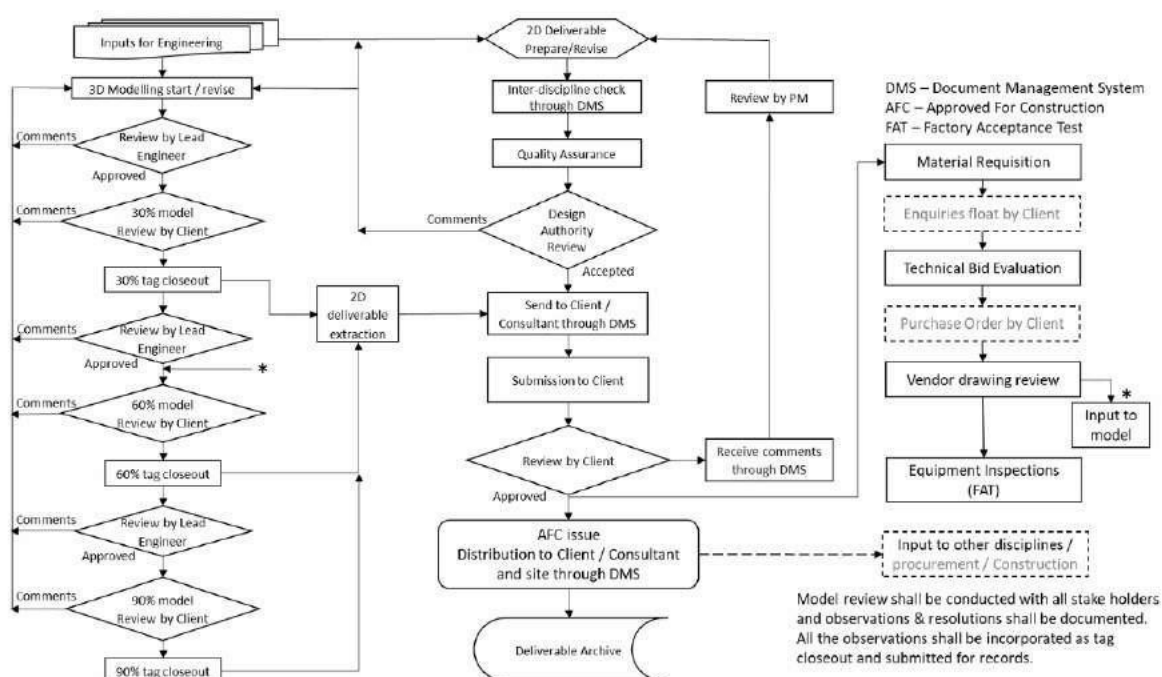
Topic details:

Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineer role at various phases of project.

4th May2021: Engineering documentation for EPC projects

2	Electrical Design Documentation	Engineering Deliverables list	Sequence of deliverables
		Detailed Engineering work flow	Detailed engineering process
		Document transmission	Document submission and info exchange
		Deliverables types	Different types of deliverables

3. ELECTRICAL DESIGN & DETAILED ENGINEERING - PROCESS



Topic details:

Engineering deliverables list, detailed engineering flow, engineering support flow, engineering support to procurements.

5 th May2021: Engineering documentation for commands and formulae

3	Document & Drawing tools	MS Word	Report / Calculations formats
		MS Excel	Basic excel commands
		Autocad	Basic line diagrams and layout commends

3C. AUTOCAD BASIC COMMANDS



A AUTOCAD BASIC KEYS							
STANDARD		DRAW		MODIFY		FORMAT	
NEW	Ctrl+N	LINE	L	ERASE	E	PROPERTIES	MO
OPEN	Ctrl+O	RAY	RAY	COPY	CO	SELECT COLOR	COL
SAVE	Ctrl+S	PLINE	PL	MIRROR	MI	LAYER	LA
PLOT	Ctrl+P	3DPOLY	3P	OFFSET	O	LINETYPE	LT
PLOT PREVIEW	PRE	POLIGONE	POL	ARRAY	AR	LINEWEIGHTS	LW
CUT	Ctrl+X	RECTANGLE	REC	MOVE	M	LT SCALE	LTS
COPY	Ctrl+C	ARC	A	ROTATE	RO	LIST	LI
PASTE	Ctrl+V	CIRCLE	C	SCALE	SC	DIMEN. STYLE	D
MATCH PROPE.	MA	SPLINE	SPL	STRECH	S	RENAME	REN
CLOSE	Ctrl+F4	ELLIPSE	EL	TRIM	TR	OPTION	OP
EXIT	Ctrl+Q	BLOCK	B	EXTENED	EX		
		POINT	PO	BRAKE	BR		
		HATCH	H	CHAMFER	CHA		
		GRADIENT	GD	FILLET	F		
		REGION	REG	EXPLODE	X		
		BOUNDARY	BO				
		DONUT	DO				

EXTRA				DRAFTING		PAPER SIZE
UNIT	UN	UCS	UCS	ORTHO	F8, Ctrl+L	A4=210*297
LIMITS	LIMITS	SINGLE TEXT	DT	OSNAP	F3, Ctrl+F	A3=297*420
(0,0;1000,1000)		MULTILINE TEXT	MT	POLAR	F10, Ctrl+U	A2=420*594
ZOOM	Z	EDIT TEXT	ED	GRID	F7, Ctrl+G	A1=594*841
ALL	A	OBJECT SNAP	OB	OTRACK	F11	A0=841*1189
PAN	P	DIMENTION	DIM	SNAP	F9	
CLEAN SCREEN	Ctrl+D	HORIZONTAL	HOR			
COMMAND WIN	Ctrl+9	VERTICAL	VER			



Topic details:

Here we need to learn the basis of the autocadbasic keys like standard, modify, draw, format, papersize etc..

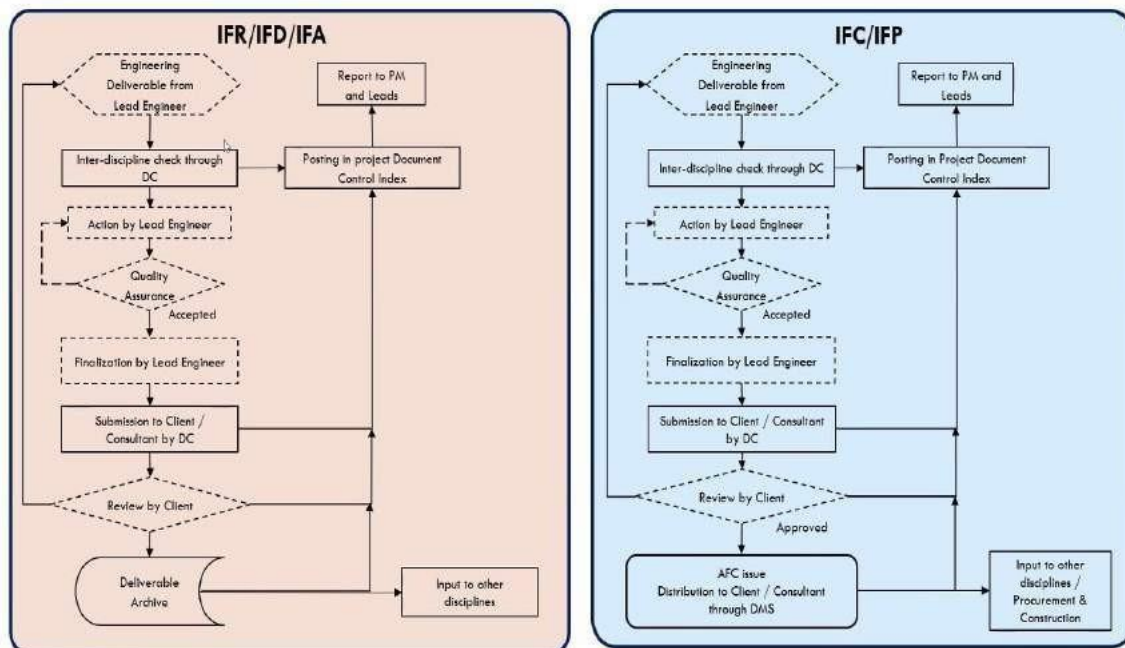
7 th May2021: Engineering documentation for Electrical system design

4	Electrical system design for a small small project	Overall plant description
		Sequence of approach
		Approach to detailed design

Topic details:



1C. DETAILED ENGINEERING



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

11th May2021: Classification of Transformers and Generators

6	Classification of Transformers and Generators	Different types of Transformers	Different types of Generators
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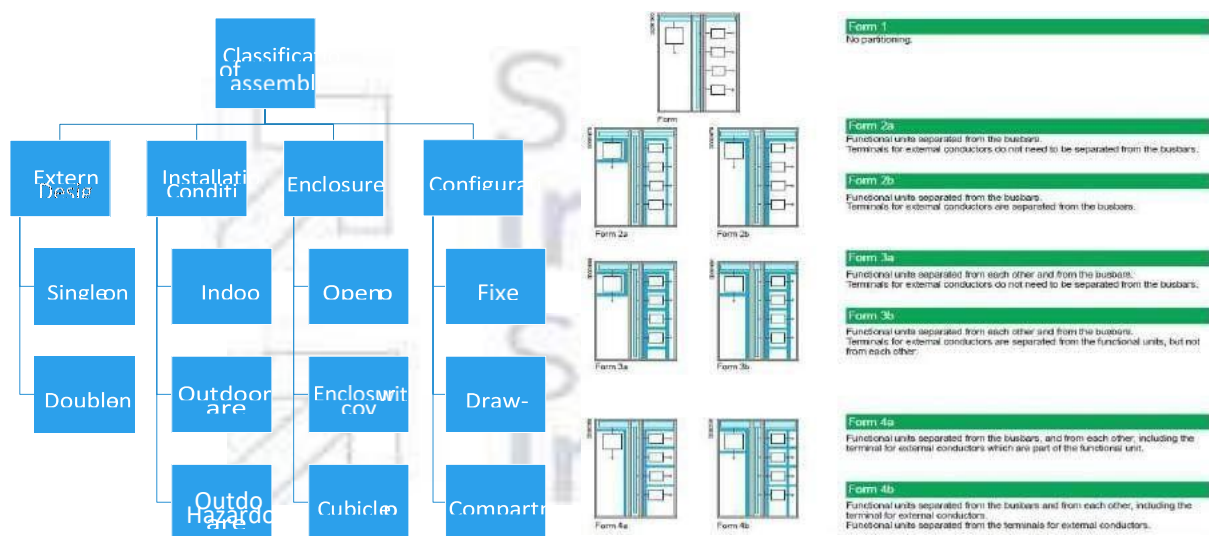


Topic details:

Classification of Transformers and Generators

12th May2021: Classification of Switchgear construction and power factor improvement

7	Classification of Switchgear construction and power factor improvement	Different types of Switchgear assemblies	Power factor improvement
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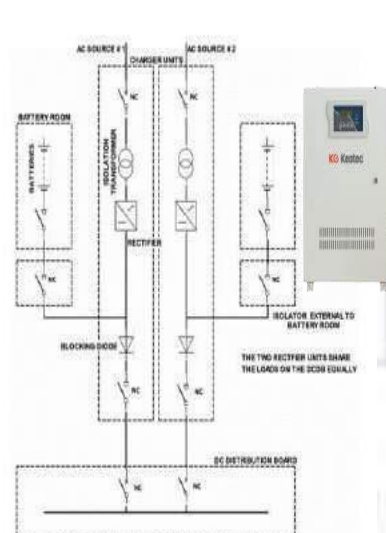


Topic details:

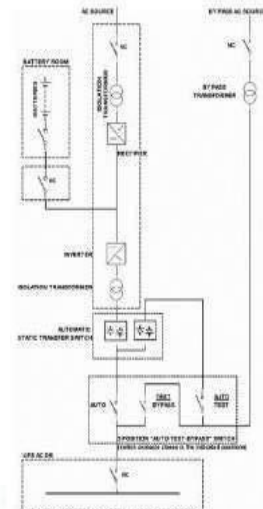
Classification of Switchgear construction and Power Factor Improvement

17th May2021: Detailing about UPS system and Busducts.

8	Detailing about UPS system and Busducts	Uninterruptible power supply system	Busducts of the system
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110V or 220V DC
UPS System



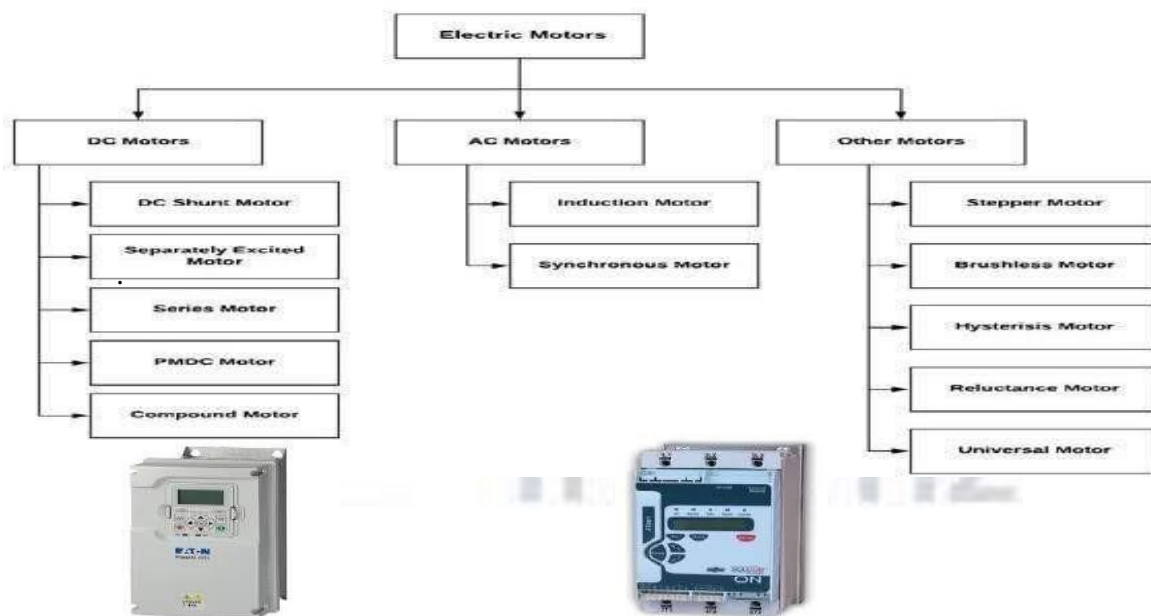
110V or 230V
AC UPS System

Topic details: Power distribution of UPS system and Busducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost Vs need.

18th May2021: Detailing about Motor Starters and Sizing of motors.

9	Detailing about Motor Starters and Sizing of motors	Motor starters and drives	Sizing and selection of motors
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Topic details: Detailing about Motor Starter and Sizing of motors and their selection.

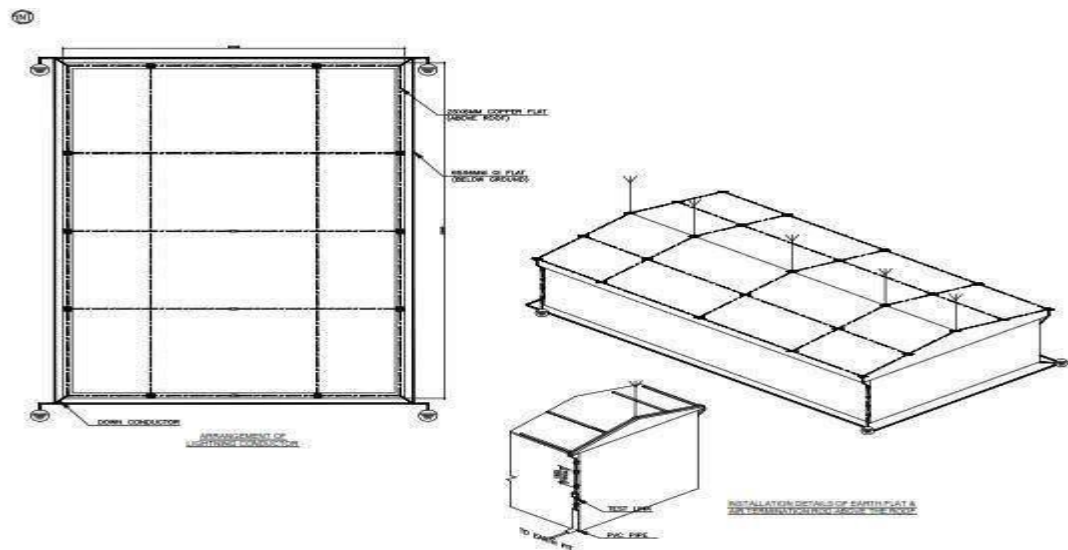
The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter

19th May2021: Discribing about Earthing system and Lighting Protection.

10	Discribing about Earthing system and Lighting Protection.	Plant Earthing system	Lighting Protection materials
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Topic details: Discribing about Earthing system and Lighting Protection.

Lightning protection required for high rise structures and important buildings against lightning currents during thunder storms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not.

20th May2021: Lighting or illumination systems and calculations.

11	Lighting or Illumination systems and Calculations	Lighting or illumination systems	Lighting calculations
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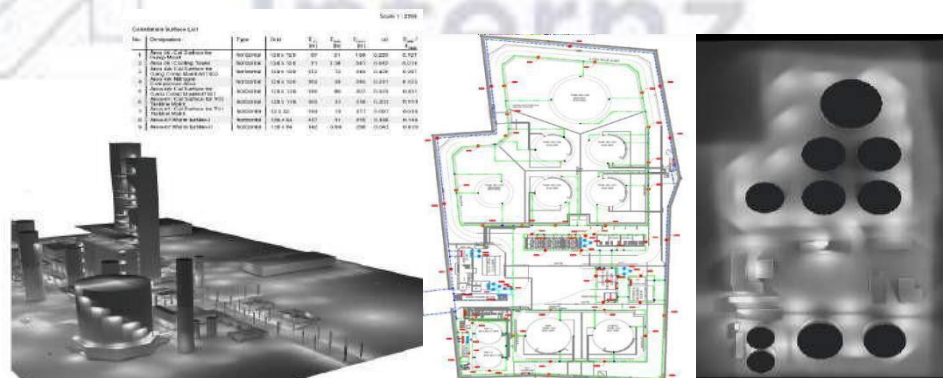
Topic details: Lighting or Illumination systems and Calculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLS PVC wires laid in cable trunks or conduits.

Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fittings to be used, required lux levels

Lighting calculations software: Dialux, Chalmite, Calculux, Relux, Luxicon,

CG Lux Applicable Standards: IS 6665: Code of practice for industrial



lighting, IS 3646: Code

of practice for interior illumination, IEC 60598: Luminaires, IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and area lighting layouts. BOQ.

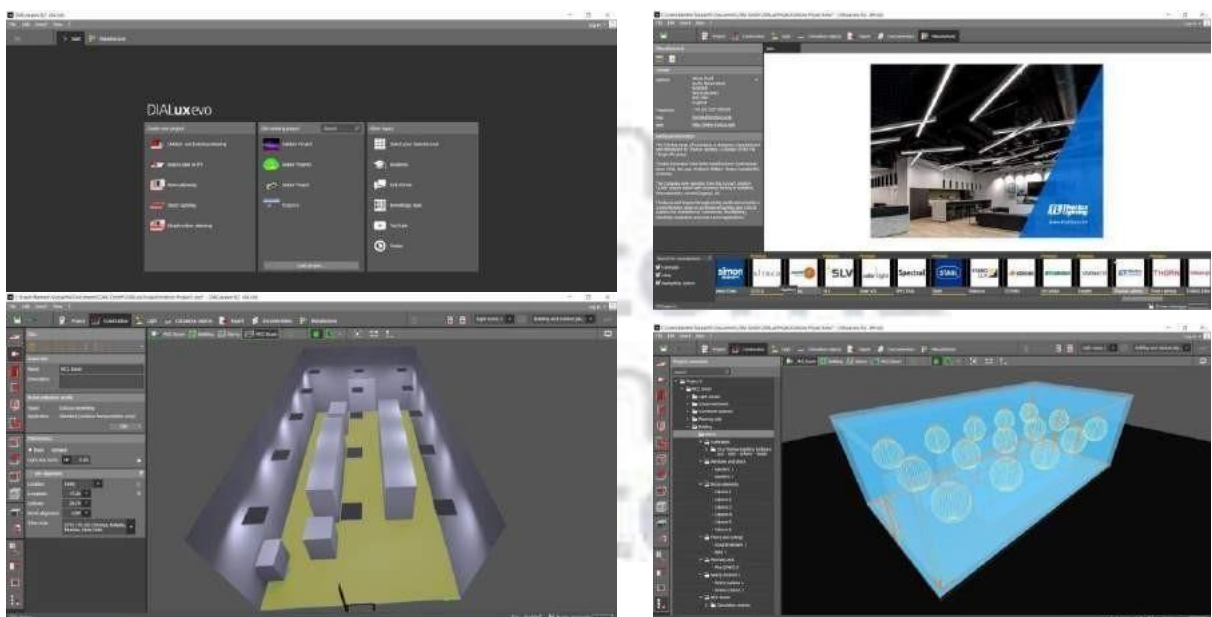
Types of light fittings: Industrial, flame proof type (EX d), increased safety type (Ex e).

21th May2021: Lighting or illumination systems using DIALUX software.

12	Lighting or Illumination using DIALUX software	Lighting or illumination systems	Operation of dialux software
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Topic details: Lighting or Illumination Calculations using DIALUX software.

Here we are using this Dialux evo 5.9.2 software windows to construct the power plant and we can perform the operation from this software.



24th May2021: Cabling and their calculations and types.

13	Cabling and their types and claculations	Cabling calculations	Types of cabling materials
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Topic details: Cabling and their types and claculations .

Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

25th May2021: Cabling calculations and Cable gland selection.

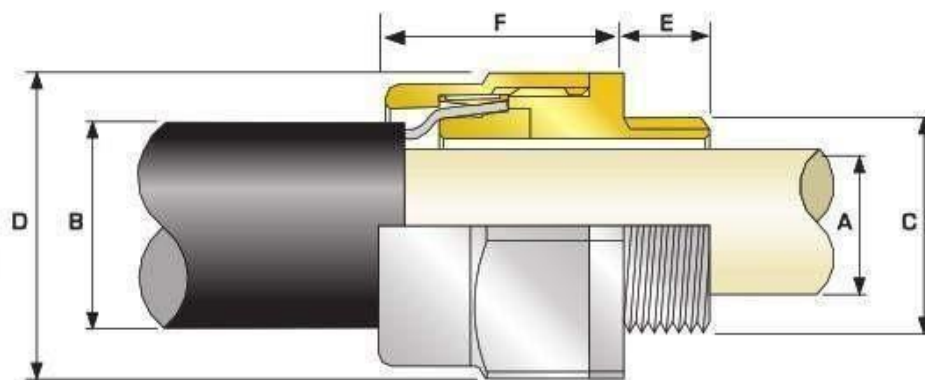
14	Cabling calculations and cable gland selection	Cabling calculations	Cable gland selection
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Topic details: Cable sizing calculation and cable gland selection.

Inputs required: Load List, Design basis, Electrical equipment layout, cable schedule, vendor catalogues for cable tray.

Cable tray sizing shall be performed for each branch of cable tray routing up to the load point. Results shall be checked with specified limits mentioned in design basis.

Cable gland:



Cable Gland Selection Table

Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

28 th May2021: Load calculations and Transformer sizing calculations

15	Load calculations and TR calculations	Load calculations	TR calculations
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Topic details:

List of electrical load calculations.

Sl. No.	Equipment No.	Equipment Description	Breaker Rating	Breaker Type	Breaker No. of Poles	ELCB Rating	Absorbed Load	Motor / Load Rating	Load Factor [A] / [B]	Efficiency at Load Factor [C]	Power Factor at Load Factor [C]	KW = [A] / [D]		Consumed Load		KVAR = KW x tan φ		R
												Continuous	Intermittent	Stand-by				
			A			mA	[A] kW	[B] kW	[C] decimal	[D] decimal	cos φ	KW	KVAR	KW	KVAR	KW	KVAR	
1	PU2315	Silica filter feed pump					116.62	132.00	0.88	0.93	0.82	125.40	87.53					
2	PU 2314-A	Absorbent/Neutral oil pump (W)					33.88	37.00	0.92	0.91	0.78	37.2	29.9					
3	PU 2314-B	Absorbent/Neutral oil pump (S)					29.13	37.00	0.79	0.91	0.78					32.0	25.7	
4	PU2305	Feed Pump (Separator)					117.78	132.00	0.89	0.93	0.82	126.6	88.4					
5	MX2305	MIXER (W)					118.69	132.00	0.90	0.93	0.82	127.6	89.1					
6	MX 2308	MIXER (S)					118.69	132.00	0.90	0.93	0.82					127.6	89.1	
7	BW2313	Blower					50.96	55.00	0.93	0.91	0.78	56.0	44.9					
8	Rotary valve	TK 2313B (I)					4.85	5.50	0.90	0.85	0.73			5.8	5.5			
9	SC2314	Screw conveyor (I)					11.44	15.00	0.76	0.85	0.73			13.46	12.60			
10	AG 2324A	Citric acid tank agitator (W)					8.60	9.20	0.93	0.85	0.73	10.12	9.47					
11	AG 2324B	Citric acid tank agitator (S)					8.60	9.20	0.93	0.85	0.73					10.1	9.5	
12	AG 2305	Citric oil reaction vessel agitator					31.25	37.00	0.84	0.91	0.78	34.34	27.55					
13	AG 2309	Lye oil reaction vessel agitator					11.37	15.00	0.76	0.85	0.73	13.38	12.52					
14	AG 2310	Lye oil reaction vessel agitator					11.37	15.00	0.76	0.85	0.73	13.38	12.52					
15	AG 2314	Soap Adsorbant Tank Agitator					19.90	22.00	0.90	0.91	0.78	21.87	17.54					
Maximum of normal running plant load : (Est. x%E + y%F)			571.8 KW			424.8 KVAR	sqrt (kW ² +KVAR ²) =			712.3 KVA	TOTAL	565.98	419.42	19.28	18.05	169.75	124.24	
Peak Load : (Est. x%E + y%F + z%G)			588.7 KW			437.3 KVAR	sqrt (kW ² +KVAR ²) =			733.4 KVA	KVA	704.45		26.41		210.36		

T/F calculation:

Calculation for Transformer Capacity

Example of calculation for Transformer Capacity

Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
Continuous load	565.98	419.4	704.45	--- (i)
Intermittent load / Diversity Factor	19.28	18.1	26.41	--- (ii)
Stand-by load required as consumed load	169.75	124.2	210.36	--- (iii)

Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =

588.7

437.3

733.35

Future expansion load (20% capacity)

117.7

87.5

146.67

Total Load =

706.5

524.7

880.03

Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load = 733.4 kVA

Spare capacity = 146.7 kVA

Required capacity = 880.0 kVA

Transformer rated capacity = 750 kVA

Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follows :

$P_1 = 750$ KVA (%Z) = 5.19 & Ratio %R = 5.4

Hence , %R = 0.941 %

%X = 5.10 %

$P_H = 132$ KW having (K = 6 & C = 1 & Cos θ = 0.93 & Eff.η = 0.83 & Cos θs = 0.21

$P_s = 1026.04$ KVA

29th May2021: DG set calculations

16	DG set calculations
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Topic details:

Transformer and DG set calculations,types ,sizing or selections

ASSIGNMENT-3		
DG SIZING CALCULATIONS		
Design Data		
Rated Voltage	415	KV
Power factor ($\cos\phi$)	0.77	Avg
Efficiency	0.89	Avg
Total operating load on DG set in KVA at 0.77 power factor	712.3	
Largest motor to start in the sequence - load in KW	132	KW
Running KVA of last motor ($\cos\phi = 0.91$)	193	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running KVA of last motor X Starting current ratio of motor)	1156	KVA
Base load of DG set in KVA (Total operating load in KVA + Running KVA of last motor)	520	KVA
A Continuous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	520	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor + Base load of DG set in KVA)	1675	KVA
Subtransient Reactance of Generator (X_d'')	7.91%	(Assumed)
Transient Reactance of Generator (X_d')	10.055%	(Assumed)
$X_d'' = (X_d' + X_d) / 2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d'' \times (1 - \text{Transient Voltage Dip})$ (Transient Voltage Dip)	853	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	1675	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	1117	KVA

5 th june 2021: Cable sizing and cable tray sizing calculations.

18	Cable sizing and cable tray sizing calculations	Cable sizing calculations	Cable tray calculation
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Topic details:

Cable sizing and cable tray sizing calculations for LV cables and MV/HV cables.

Assignment - 7
Cable tray sizing

LT CABLES									
CABLE TRAY: FROM									
		LT-4		TO	LT-5				
Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm ²)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	PU2315	4	50	1	46	29	3.25	3.25	
2	PU 2314A	4	25	1	14	22	1.4	1.4	
3	PU2324	4	6	1	46	18	0.9	0.9	
4	PU2305	4	70	1	14	29	3.25	3.25	
5	MX2305	4	70	1	46	29	3.25	3.25	
6	MX2308	4	70	1	14	29	3.25	3.25	
7	BW2313	4	35	1	22	24	1.8	1.8	
8	SC2314	4	10	1	22	18	0.9	0.9	
9	AG2324A	4	6	1	40	18	0.9	0.9	
10	AG2305	4	25	1	26	22	1.4	1.4	
11	AG2309	4	10	1	26	18	0.9	0.9	
12	AG2310	4	10	1	26	18	0.9	0.9	
13	AG2314	4	16	1	28	21	1	1	

Assignment - 8
Cable sizing

Sr.	Description	Equipment No.	Description	Conductor Size (mm ²)	Load Rating (kW)	Voltage (V)	No. of Phases	Full Load Current (A)	Motor Starting Current (A)	Load P.F. Rating	SSR 0 Rating	Motor P.F. Rating	SSR 0 Rating	Type	No. of Cables	No. of Cables	Size (mm ²)	Current Rating (A)	Starting Factor (K)	Starting Factor (K)	Starting Factor (K)	Starting Factor (K)	Overall Starting Factor (K)	Starting Current (A)	Cable Length (m)	Cable Cross-section (mm ²)	Cable Cross-section (mm ²)	Cable Cross-section (mm ²)	Voltage Drop (V/m)	Voltage Drop (V/m)	Voltage Drop (V/m)	Voltage Drop (V/m)	Cable Size (mm ²)	OS of Cable (mm ²)	Stand No.
1	LT MCC	PU2315	Slip Ring Motor	85.54	15	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
2	LT MCC	PU2314A	Slip Ring Motor	16.17	25	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
3	LT MCC	PU2324	Slip Ring Motor	4.07	11.5	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
4	LT MCC	PU2305	Slip Ring Motor	87.14	15	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
5	LT MCC	MX2305	Slip Ring Motor	87.08	15	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
6	LT MCC	MX2308	Slip Ring Motor	87.08	15	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
7	LT MCC	SC2314	Slip Ring Motor	16.17	25	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
8	LT MCC	AG2324A	Slip Ring Motor	4.07	11.5	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
9	LT MCC	AG2305	Slip Ring Motor	4.07	11.5	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
10	LT MCC	AG2309	Slip Ring Motor	4.07	11.5	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
11	LT MCC	AG2310	Slip Ring Motor	4.07	11.5	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42
12	LT MCC	AG2314	Slip Ring Motor	4.07	11.5	415	3	1100	224.71	0.8	0.8	0.8	2	1	42	42	42	42	0.8	0.8	0.8	0.8	0.8	42	42	42	42	42	42	42	42	42	42	42	42

Notes:

- Overall starting factor $K = 1.1 \times 1.2 \times 1.3 \times 1.4$
 - K_1 - Starting factor for variation in ambient temperature
 - K_2 - Starting factor for depth of bury
 - K_3 - Starting factor for spacing between two cables
 - K_4 - Starting factor for variation in internal quality of the soil
- 1/2 Motor - Starting Voltage Drop = 3%, Starting Voltage Drop = 15%
- Cable type:
 - TYPE 1 - A Conductor, XLPE Insulated, Armoured, PVC outer sheathed
 - TYPE 2 - Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed
- Effect of frequency variation ± 5%
- Combined Effect of Voltage & frequency variation ± 2%

Conclusion

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback

Smart Bridge

They conduct summer internships, work shops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good .

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

ELECTRICAL LOAD CALCULATIONS LV MCC

[illegible]

ASSIGNMENT-2

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	565.98	419.4		--- (i)
b. Intermittent load / Diversity Factor	19.28	18.1		--- (ii)
c. Stand-by load required as consumed load	169.75	124.2		--- (iii)

Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	588.7	437.3	733.35
Future expansion load (20% capacity)	117.7	87.5	146.67
Total Load =	706.5	524.7	880.03

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	733.4 kVA
Spare capacity	=	146.7 kVA
Required capacity	=	880.0 kVA
Transformer rated capacity	=	750 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follows :

$P_T =$	750 KVA	(%Z)=	5.19	& Ratio X/R =	5.4						
Hence , %R =		=	0.941	%							
%X		=	5.10	%							
$P_M =$	132 KW having (K =	6	& C =	1	& Cos $\theta =$	0.93	& Eff. $\eta =$	0.83	& Cos $\theta_s =$	0.21	
P_s		=	1026.04	KVA							
Cos $\theta_s = 0.25$,Corresponding to Angle $\theta_s =$			77.8776	Degrees for which Sin $\theta_s =$		0.98					
P_B		=	475.134	KVA	& PB in KW is =	403.863	&	P_B in Kvar =	237.567	\therefore Cos $\theta_B =$	0.850
Cos $\theta_B = 0.85$,Corresponding to Angle $\theta_s =$			31.7883	Degrees, for which Sin $\theta_s =$		0.53					
P_{CP}		=	619.332	KW							
P_{CQ}		=	1240.73	KVAR							
P_C		=	1386.71	KVA							
Cos $\theta_c =$			0.44662	, where as Sin $\theta_c =$		0.895					
Voltage Regulation ϵ		=	9.2	%							

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx. 6.5% , which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

750 kVA transformer selected.

ASSIGNMENT-3

DG SIZING CALCULATIONS		
Design Data		
Rated Voltage	415	KV
Power factor (CosØ)	0.77	Avg
Efficiency	0.89	Avg
Total operating load on DG set in kVA at 0.77 power factor	712.3	
Largest motor to start in the sequence - load in KW	132	KW
Running kVA of last motor (CosØ= 0.91)	193	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	1156	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	520	KVA
A Continuous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	520	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	1675	KVA
Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
Transient Reactance of Generator (Xd')	10.065%	(Assumed)
$X_d''' = (X_d'' + X_d')/2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d''' \times \frac{(1 - \text{Transient Voltage Dip})}{(\text{Transient Voltage Dip})}$	853	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	1675	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	1117	KVA
Considering the last value amongst P1, P2 and P3		
Continuous operation under load -P1	520	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	853	KVA
Overload capacity P3	1117	KVA
Considering the last value amongst P1, P2 and P3	1117	KVA
Hence, Existing Generator 1117 KVA is adequate to cater the loads as per re-scheduled loads		
NOTE:VOLTAGE DIP CONSIDERED - 15%		

Assignment 4 Earthing

2

Maximum line-to-ground fault in kA for 1 sec	17	
Earthing material (Earth rod & earth strip)	GI	
Depth of earth flat burial in meter	0.5	
Average depth / length of Earth rod in meters	4.5	
Soil resistivity Ω -meter	7.5	
Ambient temperature in deg C	55	
Plot dimensions (earth grid) L x B in meters	80	140
Number of earth rods in nos.	6	

Earth electrode sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

α_r - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρ_r - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
I _{lg} - RMS fault current in kA = 50 KA	14
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm ³ .oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293

The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:

14 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	114
Earth rod dia in mm	12
Earth rod dia (including 25% corrosion allowance) in mm	15

Earth flat sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

α_r - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρ_r - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
I _{lg} - RMS fault current in kA = 50 KA	14
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm ³ .oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293

The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:

$$14 = A_c * \quad 0.123$$

Ac - Required conductor cross section in sq.mm	114
Earth flat area in mm	12
Earth flat area (including 25% corrosion allowance) in mm	15
Selected flat size W * Thk in sq mm	20

R_g - Grid resistance

Grid resistance can be calculated using Eq. 52 of IEEE 80

ρ - Soil resistivity in Ω -meter=	7.5
L - Total buried length of ground conductor in meter	440
h - Depth of burial in meter	0.5
A - Grid area in sq. meter	11200

R_g - Grid resistance 0.048

R_r - Earth Electrode resistance

Grid resistance can be calculated using Eq. 55 of IEEE

$$R_r = \frac{\rho}{2 \times \pi \times n_r \times L_r} \left(1 + \frac{4 \times L_r}{n \times b} \right) - 1 + \frac{2 \times k_1 \times L_r}{\sqrt{A}} \left(\sqrt{n} - 1 \right)^2$$

ρ - Soil resistivity in Ω -meter, 16.96	7.5
n - No of earth electrodes	6
L_r - Length of earth electrode in meter	4.5
b - Diameter of earth electrode in meter	0.020
kl - co-efficient	1
A - Area of grid in square metre	11200

R_r - Earth Electrode resistance 2.75561

Grounding system resistance

Grounding system resistance can be calculated using equation 53 of IEEE 80 as follows:

$$R_s = R_g + \frac{R_g^2}{2R_m}$$

R_m - Mutual ground resistance between the group of ground conductors, R_g and group of electrodes, R_r in Ω . Neglected R_m , since this is for homogenous soil

R_s - Total earthing system resistance 0.048 Ohms

The calculated resistance grounding system is less than the allowable 1 Ω value.

ASSIGNMENT-5

	1
Location	Mangalore
Building	Concrete, Industrial
Type of Building	Flat Roofs (a)
Building Length (L)	14
Building breadth (W)	4
Building Height (H)	5

Risk Factor Calculation

1 Collection Area (A_c)

$$A_c = \frac{(L*W) + (2*L*H) + (2*W*H) + (3.14*H*H)}{314.5}$$

2 Probability of Being Struck (P)

$$P = \frac{A_c * N_g * 10^{-b}}{0.00059755}$$

3 Overall weighing factor

a) Use of structure (A)	=	1.2
b) Type of construction (B)	=	0.4
c) Contents or consequential effects (C)	=	0.8
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	$A * B * C * D * E$
	=	0.115

4 Overall Risk Factor

Po	=	$P * Wo$
Po	=	6.88378E-05
Pa	=	10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
 Since Po > Pa lightning protection required.

5 Air Terminations

Perimeter of the building	=	$2(L+W)$
	=	36 Mts.

6 Down Conductors

Perimeter of building	=	36 Mts.
No. of down conductors based on perimeter	=	2 Nos.

Hence 2 nos. of Down conductors have been selected.

Size of Down conductor = 20 X 2.5 mm Galvanized Steel Strip
 (As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)

ASSIGNMENT-6

S.NO.		Equipment No.	Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current (A)	Motor Starting Current (A)	Load P.F. Running	SIN Φ Running	Motor P.F Staring	SIN Φ Staring	Type	No. of Runs	No. of Cores	Size (mm2)	Current Rating (A)	Derating factor k1	Derating factor k2	Derating factor k3	Derating factor k4	Overall Derating factor k	Derated Current (A)	Cable Length (M)	Cable Resistance (Ohms/kM)	Cable Reactance (Ohms/kM)	Voltage drop (Running) (V)	Voltage drop (Running) (%)	Voltage drop (Starting) (V)	Voltage drop (starting) (%)	Cable size result	OD of Cable (mm)	Gland size	
		PU2315	Silica filter feed pump	116.62	132.00	415	3	202.8	1216.85	0.8	0.6	0.8	0.5	2	1	4.0	95	#REF!	0.98	0.9	1	1	0.882	#REF!	95	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
		PU 2314-A	Absorbent/Neutral oil pump (W)	33.95	37.00	415	3	58.9	353.52	0.8	0.6	0.8	0.5	2	1	4.0	25	#REF!	0.98	0.9	1	1	0.882	#REF!	95	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		PU 2314 -B	Absorbent/Neutral oil pump (S)	29.13	37.00	415	3	50.7	303.95	0.8	0.6	0.8	0.5	2	1	4.0	10	#REF!	0.98	0.9	1	1	0.882	#REF!	60	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		PU2305	Feed Pump (Separator)	117.76	132.00	415	3	204.8	1228.96	0.8	0.6	0.8	0.5	2	1	4.0	70	#REF!	0.98	0.9	1	1	0.882	#REF!	85	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		MX2305	MXER (W)	118.68	132.00	415	3	206.4	1238.45	0.8	0.6	0.8	0.5	2	1	4.0	70	#REF!	0.98	0.9	1	1	0.882	#REF!	75	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		MX 2308	MXER (S)	118.68	132.00	415	3	206.4	1238.45	0.8	0.6	0.8	0.5	2	1	4.0	120	#REF!	0.98	0.9	1	1	0.882	#REF!	105	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		BW 2313	Blower	50.99	55.00	415	3	88.6	531.73	0.8	0.6	0.8	0.5	2	1	4.0	35	#REF!	0.98	0.9	1	1	0.882	#REF!	100	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		Rotary valve	TK 2313B (I)	4.95	5.50	415	3	8.6	51.65	0.8	0.6	0.8	0.5	2	1	4.0	4	#REF!	0.98	0.9	1	1	0.882	#REF!	100	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		SC2314	Screw conveyor (I)	11.44	15.00	415	3	19.9	119.37	0.8	0.6	0.8	0.5	2	1	4.0	6	#REF!	0.98	0.9	1	1	0.882	#REF!	75	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
		AG 2324A	Citric acid tank agitator (W)	8.63	9.20	415	3	15.0	89.74	0.8	0.6	0.8	0.5	2	1	4.0	6	#REF!	0.98	0.9	1	1	0.882	#REF!	110	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		AG 2324B	Citric acid tank agitator (S)	8.63	9.20	415	3	15.0	89.74	0.8	0.6	0.8	0.5	2	1	4.0	4	#REF!	0.98	0.9	1	1	0.882	#REF!	75	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
		AG 2305	Citric oil reaction vessel agitator	31.25	37.00	415	3	54.3	326.07	0.8	0.6	0.8	0.5	2	1	4.0	25	#REF!	0.98	0.9	1	1	0.882	#REF!	105	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
		AG 2309	Lyse oil reaction vessel agitator	11.37	15.00	415	3	19.8	118.64	0.8	0.6	0.8	0.5	2	1	4.0	25	#REF!	0.98	0.9	1	1	0.882	#REF!	85	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	32
		AG 2310	Lyse oil reaction vessel agitator	11.37	15.00	415	3	19.8	118.64	0.8	0.6	0.8	0.5	2	1	4.0	10	#REF!	0.98	0.9	1	1	0.882	#REF!	95	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
		AG 2314	Soap Adsorbent Tank Agitator	19.98	22.00	415	3	34.6	207.64	0.8	0.6	0.8	0.5	2	1	4.0	10	#REF!	0.98	0.9	1	1	0.882	#REF!	65	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s

Basis:

1. Overall derating factor $k = k_1 \times k_2 \times k_3 \times k_4$
 - K1=Rating factor for variation in air/ground temperature
 - K2=Rating factor for depth of laying
 - K3=Rating factor for spacing between two circuits
 - K4=Rating factor for variation in thermal resistivity of the soil
2. LT Motors : Running Voltage Drop = 3%, Starting Voltage Drop = 15%
3. Cable type:
 - TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed
 - TYPE 2: Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed
4. Effect of Frequency Variation $\pm 5\%$
5. Combined Effect of Voltage & Frequency Variation $\pm 10\%$

ASSIGNMENT-7

LT CABLES									
CABLE TRAY: FROM									
		LT-4		TO	LT-5				
Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm2)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	PU2315	4.0	95	1	33	33	4	4	
2	PU 2314-A	4.0	25	1	22	22	1.4	1.4	
3	PU 2314 -B	4.0	10	1	18	18	0.9	0.9	
4	PU2305	4.0	70	1	29	29	3.25	3.25	
5	MX2305	4.0	70	1	29	29	3.25	3.25	
6	MX 2308	4.0	120	1	37	37	5	5	
7	BW2313	4.0	35	1	24	24	1.8	1.8	
8	Rotary valve	4.0	4	1	17	17	0.6	0.6	
9	SC2314	4.0	6	1	18	18	0.7	0.7	
10	AG 2324A	4.0	6	1	18	18	0.7	0.7	
11	AG 2324B	4.0	4	1	17	17	0.6	0.6	
12	AG 2305	4.0	25	1	22	22	1.4	1.4	
13	AG 2309	4.0	25	1	22	22	1.4	1.4	
14	AG 2310	4.0	10	1	18	18	0.9	0.9	
15	AG 2314	4.0	10	1	18	18	0.9	0.9	
16									
17									
18									
19									
20									
21									
Total									
Calculation					Result				
Maximum Cable Diameter:			37	mm	Selected Cable Tray width:			O.K	
Consider Spare Capacity of Cable Tray:			30%		Selected Cable Tray Depth:			O.K	
Distance between each Cable:			0	mm	Selectrd Cable Tray Weight:			O.K	Including Spare Capacity
Calculated Width of Cable Tray:			0	mm	Selected Cable Tray Size:			O.K	Including Spare Capacity
Calculated Area of Cable Tray:			0	Sq.mm					
No of Layer of Cables in Cable Tray:			1		Required Cable Tray Size:			600 x 100	mm
Selected No of Cable Tray:			1	Nos.	Required Nos of Cable Tray:			1	No
Selected Cable Tray Width:			600	mm	Required Cable Tray Weight:			90.00	Kg/Meter/Tray
Selected Cable Tray Depth:			100	mm	Type of Cable Tray:			Ladder	
Selected Cable Tray Weight Capacity:			90	Kg/Meter					
Type of Cable Tray:			Ladder		Cable Tray Width Area Remaning			100%	
Total Area of Cable Tray:			60000	Sq.mm	Cable Tray Area Remaning:			100%	