

Experimental Methods Lecture 9

October 8th, 2020



Invertible operator, the role of input and output, and free evolution 1/3

- Some linear systems are described by operators that have an inverse:
- That is, the equation has just one solution
- For these systems the role of input and output can be interchanged
 - Example 1: multiplication by a constant
 - Example 2: Fourier transform

$$o(t) = \Im[i(t)] i(t) = \Im^{-1}[o(t)]$$
$$o(t) = \Im[i(t)]$$

$$o(t) = ci(t) \quad i(t) = \frac{1}{c}o(t)$$

$$o(\omega) = \int_{-\infty}^{\infty} i(t)e^{-i\omega t} dt \qquad i(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} o(t)e^{i\omega t} dt$$



Invertible operator, the role of input and output, and free evolution 2/3

• Some linear systems (e.g. those described by differential equations) are better described by

D[o(t)] = i(t)

• For these system there may be n solutions:

$$D[o_j(t)] = 0$$

• Because the operator is linear

$$D\left[o(t) + \sum_{j=1}^{n} c_{j} o_{j}(t)\right] = D\left[o(t)\right] + \sum_{j=1}^{n} c_{j} D\left[o_{j}(t)\right] = i(t)$$

• (c_i arbitrary constants)



Invertible operator, the role of input and output, and free evolution 3/3

$$D\left[o(t) + \sum_{j=1}^{n} c_{j} o_{j}(t)\right] = D\left[o(t)\right] + \sum_{j=1}^{n} c_{j} D\left[o_{j}(t)\right] = i(t)$$

For all functions such that

$$\tilde{o}(t) \neq \sum_{j=1}^{n} c_{j} o_{j}(t)$$

 $D[\tilde{o}(t)]=i(t)$ has an inverse

$$\tilde{o}(t) = D^{-1} [i(t)] = \int_{0}^{\infty} h(t,t')i(t')dt'$$

Finally

$$o(t) = \sum_{j=1}^{n} c_{j} o_{j}(t) + \int_{-\infty}^{\infty} h(t,t') i(t') dt'$$

Free evolution: output without an input



An example: the pendulum

- Equation of motion for the x coordinate
- $m\ddot{x} = -mgSin(\theta)Cos(\theta) + F_{ex}$

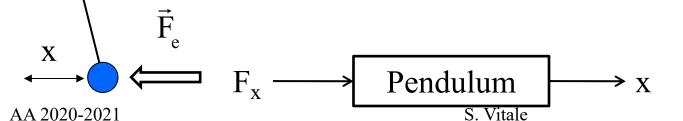
Converting angles

 $m\ddot{x} = -mg\frac{x}{L}\sqrt{1 - \left(\frac{x}{L}\right)^2 + F_{ex}}$

• Linear expansion to first order in x

 $m\ddot{x} = -mg\frac{x}{L} + F_{ex}$

$$\ddot{x} + \frac{g}{I}x \equiv \ddot{x} + \omega_o^2 x = F_{ex}/m$$





A basic example: the pendulum

- Linearized equation for the x coordinate $\ddot{x} + \omega_0^2 x = F_{ex}/m$
- Special solution $\tilde{x}(t) = \frac{1}{m \omega_0} \int_0^{\infty} \sin(\omega_0 t') F_{ex}(t t') dt'$
- Indeed $\dot{\tilde{x}}(t) = -\frac{1}{m \omega_o} \int_0^\infty \sin(\omega_o t') \frac{dF_{ex}(t-t')}{dt'} dt' =$ $= \frac{1}{m} \int_0^\infty \cos(\omega_o t') F_{ex}(t-t') dt'$
- and $\ddot{\ddot{x}}(t) = -\frac{1}{m} \int_0^\infty Cos(\omega_o t') \frac{dF_{ex}(t-t')}{dt'} dt' =$ $= -\frac{1}{m} Cos(\omega_o t') F_{ex}(t-t')]_0^\infty \frac{\omega_o}{m} \int_0^\infty Sin(\omega_o t') F_{ex}(t-t') dt' =$

$$= \frac{F_{ex}(t)]}{m} - \omega_0^2 \tilde{x}(t)$$

• then:

$$\ddot{\tilde{x}}(t) + \omega_o^2 \tilde{x}(t) = \frac{F_{ex}(t)}{m} - \omega_o^2 \tilde{x}(t) + \omega_o^2 \tilde{x}(t) = \frac{F_{ex}(t)}{m}$$

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A basic example: the pendulum

- Response to input: $\tilde{x}(t) = \frac{1}{m \omega_0} \int_0^{\infty} \sin(\omega_0 t') F_{ex}(t t') dt'$
- In addition, for arbitrary values of x_p and x_q :

$$x(t) = x_p Sin(\omega_o t) + x_q Cos(\omega_o t) \rightarrow \ddot{x}(t) + \omega_o^2 x(t) = 0$$

The most general solution is then:

$$x(t) = x_p Sin(\omega_o t) + x_q Cos(\omega_o t) + \frac{1}{m \omega_o} \int_0^\infty Sin(\omega_o t') F_{ex}(t - t') dt'$$
Free evolution Response

- Note: for an undamped pendulum, the free evolution never decays.
- Passive undamped pendulums do not exist in nature.

Inverting the relation to obtain the input

- Notice that the equation of motion D[o(t)]=i(t) allows for calculating the value of i(t) from o(t) even if this one includes some free evolution
- For the pendulum for instance by calculating $m\ddot{x}(t)$ at time t and adding up the value of mgx(t)/L at the same time, one obtains $F_{ex}(t)=m\ddot{x}(t)+mgx(t)/L$, no matter what's the value of the free evolution.
- A practical example with a torsion pendulum

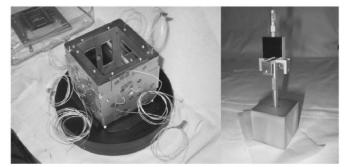
B. EVALUATION OF TORQUE AND BACKGROUND SUBTRACTION

The angular motion of the pendulum $\phi(t)$ is converted into an instantaneous applied torque N(t) as

$$N(t) = I_o\{\ddot{\phi}(t) + (2\pi/T_o Q)\dot{\phi}(t) + (2\pi/T_o)^2\phi(t)\}. \quad (1)$$

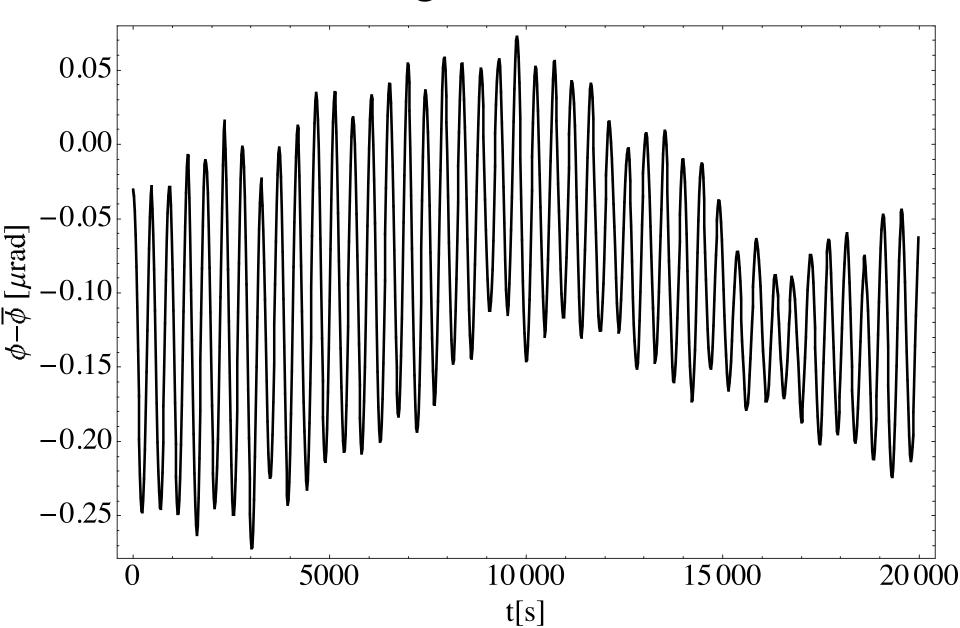
The derivatives are estimated from a sliding second order fit to 5 adjoining data.

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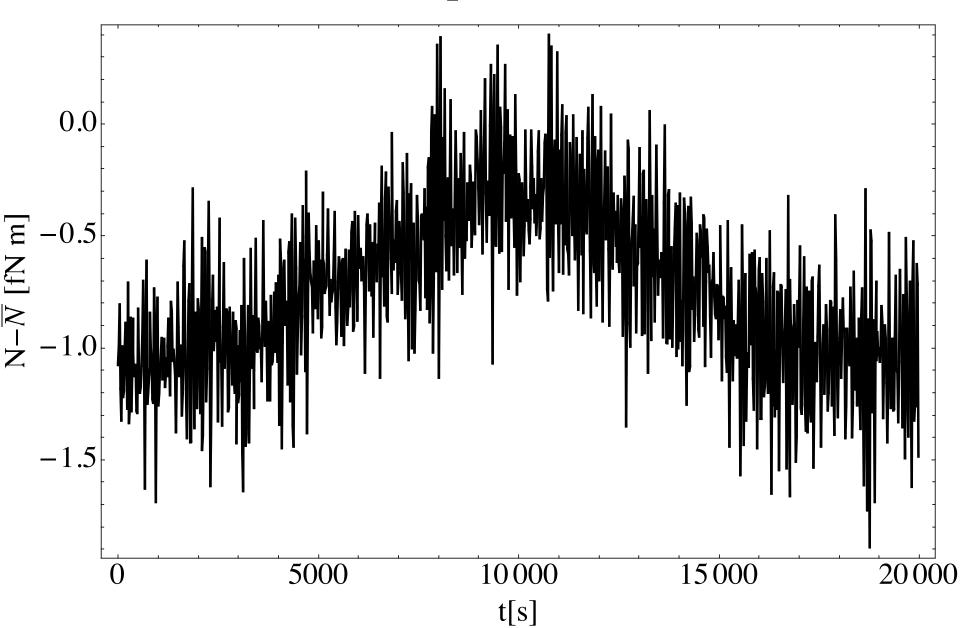


Angular data





Torque data





Step response

From

$$o(t) = \int_{-\infty}^{\infty} h(t')i(t-t')dt'$$

• We derived that h(t) is the impulse response

$$o(t) = \int_{0}^{\infty} h(t')\delta(t-t')dt' = h(t)$$

• Consider now the *step response* defined as

$$o_{-1}(t) = \int_{-1}^{\infty} h(t')\Theta(t-t')dt' = \int_{-1}^{t} h(t')dt'$$

• We can derive o₋₁

$$do_{-1}(t)/dt = h(t)$$

• Thus h(t) is both the impulse response and the derivative of the step response



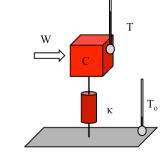
The importance of the step response

- As delta impulse cannot be obtained in reality, h(t) cannot be measured as the response of the system to an impulse.
- High but finite amplitude pulses, easily drive the system out of linearity
- On the contrary steps can be made very small and fed to the system under study.
- The derivative of the system response is proportional to h
- Example: the calorimeter. Response to a step at t=0

$$\Delta T(t) = (W_o/\kappa) \left(1 - e^{-\frac{t}{\tau}}\right) \Theta(t)$$

Derivative

$$d\Delta T(t)/dt = (W_o/\tau\kappa)e^{-\frac{t}{\tau}}\Theta(t) = (W_o/C)e^{-\frac{t}{\tau}}\Theta(t) = W_oh(t)$$

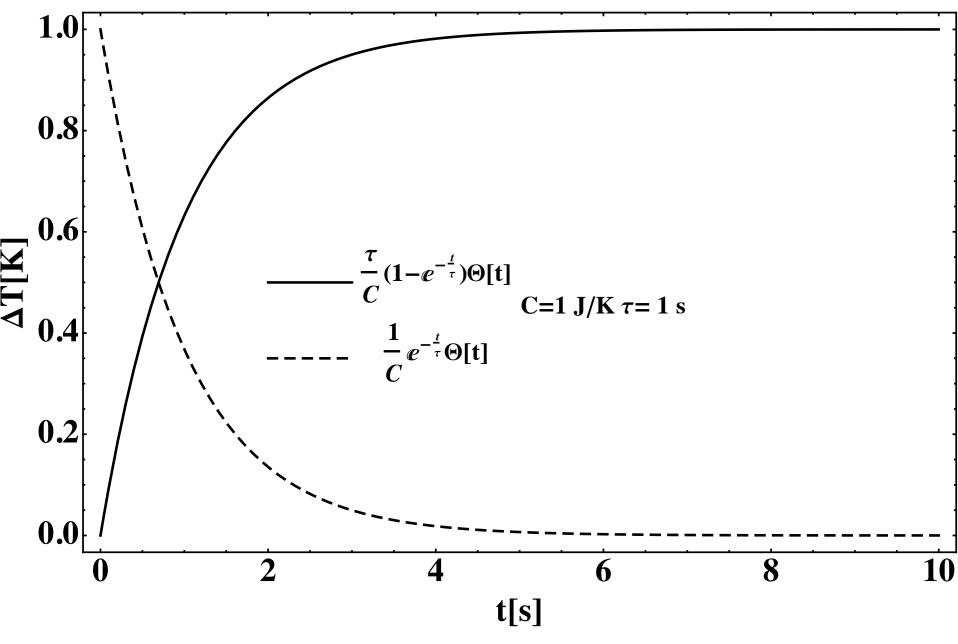


• Thus h(t) can be measured with W_o as small as the measurement noise allows for.

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Summary: linear stationary systems, continuous

A linear stationary system $o(t) = \int_{-\infty}^{\infty} i(t')h(t-t')dt' = \int_{-\infty}^{\infty} h(t')i(t-t')dt'$

• A linear, stationary, and causal system

$$o(t) = \int_{0}^{\infty} h(t')i(t-t')dt'$$

• A linear, stationary system with free evolution (not all systems have free evolution)

$$o(t) = \sum_{j=1}^{n} c_{j} o_{j}(t) + \int_{-\infty}^{\infty} h(t') i(t-t') dt'$$

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Linear response and Fourier Transforms

- Fourier Transforms convert input-output relations into algebraic equations
- Within linear response, frequencies don't mix!



Linear system in the frequency domain

 Output is the convolution between input and impulse response

$$o(t) = \int_{-\infty}^{\infty} h(t')i(t-t')dt'$$

Using convolution theorem

$$o(\omega) = h(\omega)i(\omega)$$

- h(t): impulse response
- h(ω): *frequency response*

Linear systems do not mix frequencies

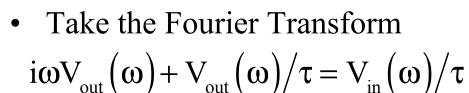


A remarkable example: differential equations

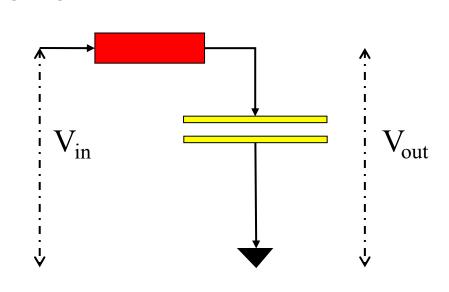
- Consider a low pass electrical circuit
- The circuit equation

$$C dV_{out}(t)/dt = \left[V_{in}(t) - V_{out}(t)\right]/R$$

• That is (define $\tau = RC$) $dV_{out}(t)/dt + V_{out}(t)/\tau = V_{in}(t)/\tau$



- That is $V_{out}(\omega) = V_{in}(\omega)/(1+i\omega\tau)$
- Or $h(\omega) = 1/(1 + i\omega\tau)$



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A remarkable example: differential equations

Input output relation in the frequency domain

relation in the frequency domain
$$V_{\text{out}}(\omega) = V_{\text{in}}(\omega)/(1+i\omega\tau) = h(\omega)V_{\text{in}}(\omega)$$

From convolution theorem (\mathcal{F}^{-1} = inverse Fourier transform)

$$V_{out}(t) = \int_{0}^{\infty} \mathcal{F}^{-1} \{h(\omega)\}(t')V_{in}(t-t')dt'$$

Let MathematicaTM calculate the inverse Fourier transform Simplify InverseFourierTransform $\left[\frac{1}{1+\frac{1}{2}\omega \tau}, \omega, t\right], \tau > 0$

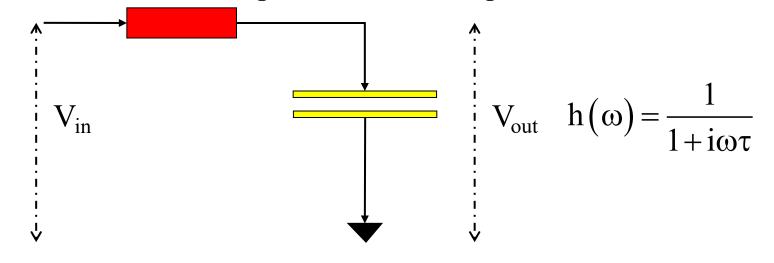
Then finally

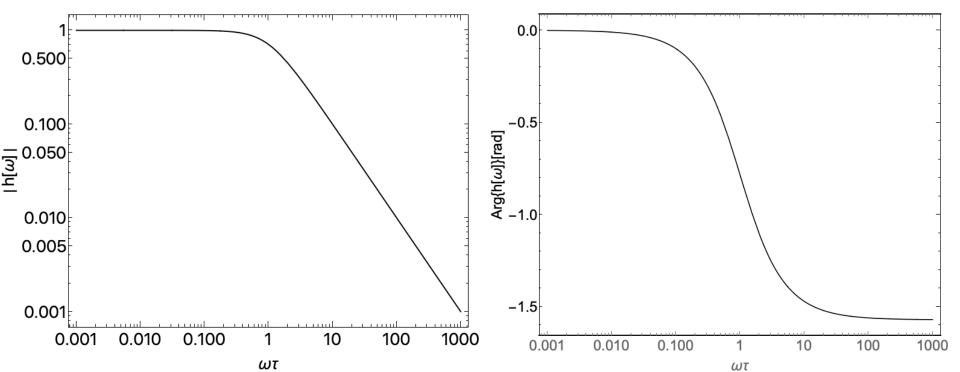
$$V_{out}(t) = \int_{0}^{\infty} \frac{1}{\tau} e^{-\frac{t'}{\tau}} \theta(t') V_{in}(t-t') dt'$$

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A remarkable example: differential equations









Frequency response and sinusoidal signals

• Take an (ever lasting) sinusoid

 $i(t) = Sin(\omega_o t)$

• Its Fourier Transform is

$$i(\omega) = \frac{\pi}{i} \left[\delta(\omega - \omega_o) - \delta(\omega + \omega_o) \right]$$

• Let's feed it to a system

$$i(\omega) \rightarrow h(\omega) \rightarrow o(\omega)$$

• The output is

$$o(\omega) = \frac{\pi}{i} \left[h(\omega_o) \delta(\omega - \omega_o) - h(-\omega_o) \delta(\omega + \omega_o) \right]$$

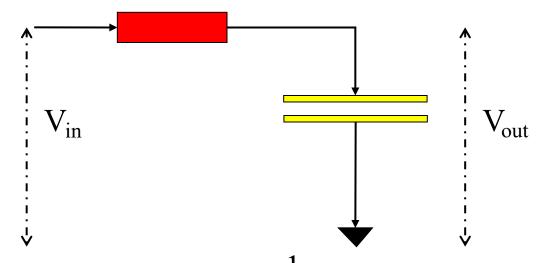
Using symmetry of h

$$= \frac{\pi}{i} h'(\omega_o) \left[\delta(\omega - \omega_o) - \delta(\omega + \omega_o) \right] + \pi h''(\omega_o) \left[\delta(\omega - \omega_o) + \delta(\omega + \omega_o) \right]$$

• In the time domain $o(t) = h'(\omega_o) Sin(\omega_o t) + h''(\omega_o) Cos(\omega_o t)$ = $|h(\omega_o)| Sin(\omega_o t + Arg\{h(\omega_o)\})$



The low pass



- The frequency response function
- $Sin(\omega_0 t)$ at input
- In the time domain

$$h(\omega) = \frac{1}{1 + i\omega\tau}$$

$$o(\omega) = \frac{\pi}{i} \left[\frac{\delta(\omega - \omega_o)}{1 + i\omega_o\tau} - \frac{\delta(\omega + \omega_o)}{1 - i\omega_o\tau} \right]$$

$$o(t) = \frac{\sin(\omega_o t - ArcTan[\omega_o\tau])}{\sqrt{1 + \omega_o^2\tau^2}}$$

Measuring the transfer function of a system

• Feed a system with an input i(t) which is wideband enough for your purposes. Measure the response o(t). The transfer function is

$$h(\omega) = o(\omega)/i(\omega) = |o(\omega)|/|i(\omega)|e^{i\left[Arg\left[o(\omega)-Arg\left[i(\omega)\right]\right]\right]}$$

Notice

$$h(\omega) = o(\omega)/i(\omega)$$

- Holds if $i(\omega)$ and $o(\omega)$ are the true continuous Fourier transform of the continuous signal
- Use of DFT is allowed if:
 - Sampling of o(t) and i(t) is fast enough to produce negligible aliasing
 - Both i(t) and o(t) die out at t→0 and t→ Δ T to make circular convolution equivalent to standard convolution

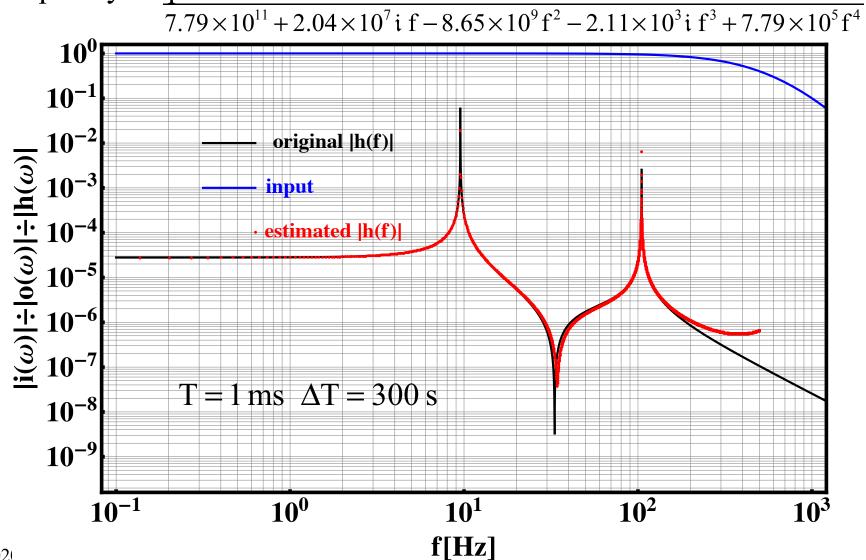


Numerical example

• Input
$$i(\omega) = \left[1 + (\omega/2\pi 1 \text{ kHz})^2\right]^{-1} \left[1 + (\omega/2\pi 500 \text{ Hz})^2\right]^{-1}$$

Frequency response

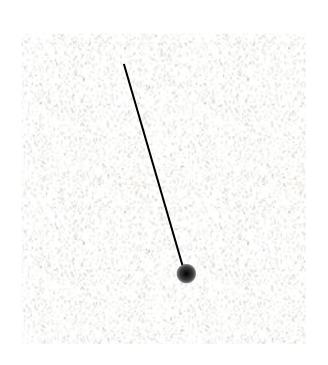
 $2.17 \times 10^{7} + 62.8i \text{ f} - 1.97 \times 10^{4} \text{ f}^{2}$





Exercise: the pendulum

- Take the standard, *viscously* damped pendulum
- Consider torque as input and angle as output
- Write the input-output relation
- Linearize for small angles
- Find the frequency response
- Find the impulse response
- Find the free evolution
- Calculate the response to a Gaussian pulse





Linear systems in series

• Two systems in series: the output of the first system is the input to the second one

$$i_1(\omega) \longrightarrow h_1(\omega) \xrightarrow{o_1(\omega)=i_2(\omega)} h_2(\omega) \longrightarrow o_2(\omega)$$

It follows that

$$o_2(\omega) = h_2(\omega)i_2(\omega) = h_2(\omega)o_1(\omega) = h_2(\omega)h_1(\omega)i_1(\omega)$$

• Thus the system series is equivalent to

$$i(\omega) \longrightarrow h(\omega) \longrightarrow o(\omega)$$

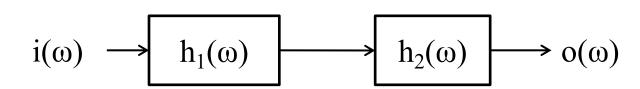
with

$$h(\omega) = h_1(\omega)h_2(\omega)$$

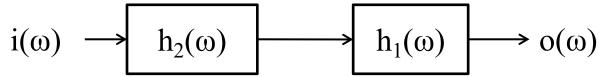


Linear systems in series

Notice



• Is equivalent to



As product is commutative

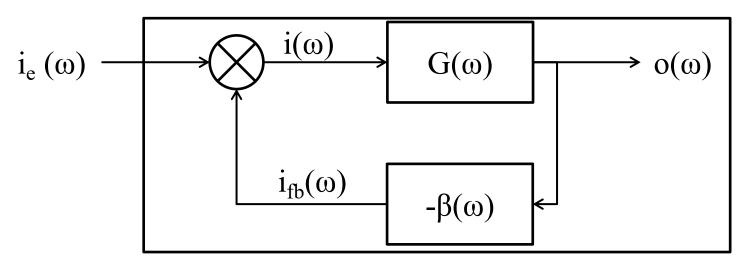
$$h_2(\omega)h_1(\omega) = h_2(\omega)h_1(\omega)$$

- Thus the order of the systems within the series is irrelevant
- Warning: physical interchanging two systems may alter their respective frequency response



A remarkable example: the feedback loop

• The output of a system is fed back and added to external input via another linear system:



• Deriving the input output relations of the full system $i_e \rightarrow o$

$$o(\omega) = G(\omega)i(\omega) = G(\omega)[i_e(\omega) + i_{fb}(\omega)]$$

• But:

$$i_{fb}(\omega) = -\beta(\omega)o(\omega)$$

Thus

$$o(\omega) = G(\omega) [i_e(\omega) - \beta(\omega)o(\omega)]$$