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# **Engineering Electromagnetics**

Electric Flux Density, Gauss's Law & Divergence







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# Electric Flux Density, Gauss's Law & Divergence

- 1. Electric Flux Density
- 2. Gauss's Law
- 3. Divergence
- 4. Maxwell's First Equation
- 5. The Vector Operator  $\nabla$
- 6. The Divergence Theorem

# Electric Flux Density (1)

- M. Faraday (1837)
- *Phenomenon*: the total charge on the outer sphere was equal in *magnitude* to the original charge placed on the inner sphere, regardless of the dielectric material between the 2 spheres
- *Conclusion*: there was a "displacement" from the inner sphere to the outer, independent of the medium:

$$\Psi = Q$$

• Ψ: electric flux







# Electric Flux Density (2)

$$S_a = 4\pi a^2 \text{ (m}^2\text{)}$$

Density of the flux at the inner sphere:

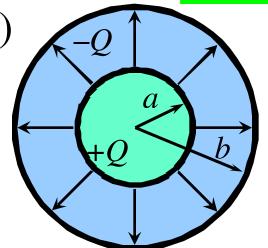
$$\frac{\Psi}{4\pi a^2} = \frac{Q}{4\pi a^2}$$



$$\mathbf{D}\big|_{r=a} = \frac{Q}{4\pi a^2} \mathbf{a}_r$$

$$\mathbf{D}\big|_{r=b} = \frac{Q}{4\pi b^2} \mathbf{a}_r$$

$$\mathbf{D}\big|_{a \le r \le b} = \frac{Q}{4\pi r^2} \mathbf{a}_r$$









Electric Flux Density (3)

$$\mathbf{D} = \frac{Q}{4\pi r^2} \mathbf{a}_r \quad (a \le r \le b)$$

$$\mathbf{D} = \frac{Q}{4\pi r^2} \mathbf{a}_r$$

$$\mathbf{E} = \frac{Q}{4\pi\varepsilon_0 r^2} \mathbf{a}_r$$

$$\rightarrow \mathbf{D} = \boldsymbol{\varepsilon}_0 \mathbf{E}$$

$$\begin{bmatrix}
\mathbf{D} = \frac{Q}{4\pi r^2} \mathbf{a}_r \\
\mathbf{E} = \frac{Q}{4\pi \varepsilon_0 r^2} \mathbf{a}_r
\end{bmatrix} \rightarrow \begin{bmatrix}
\mathbf{D} = \varepsilon_0 \mathbf{E} \\
\text{(in free space)}
\end{bmatrix}$$
(in free space)
$$\mathbf{E} = \int_V \frac{\rho_v dv}{4\pi \varepsilon_0 R^2} \mathbf{a}_r$$

$$\mathbf{E} = \int_V \frac{\rho_v dv}{4\pi \varepsilon_0 R^2} \mathbf{a}_r$$

$$\mathbf{D} = \int_{V} \frac{\rho_{v} dv}{4\pi R^{2}} \mathbf{a}_{r}$$



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#### Ex. 1

# Electric Flux Density (4)

Infinite uniform line charge of 10 nC/m lie along the x & y axes in free space. Find **D** at (0, 0, 3).





#### **Ex. 2**

# Electric Flux Density (5)

The x & y axes are charged with uniform line charge of 10 nC/m. A point charge of 20nC is located at (3, 3, 0). The whole system is in free space. Find **D** at (0, 0, 3).





#### **Ex. 3**

# Electric Flux Density (6)

Given 3 infinite uniform sheets (all parallel to x0y) at z = -3, z = 2 & z = 3. Their surface charge density are 4 nC/m<sup>2</sup>, 6 nC/m<sup>2</sup> & -9 nC/m<sup>2</sup> respectively. Find **D** at P(5, 5, 5).







# Electric Flux Density, Gauss's Law & Divergence

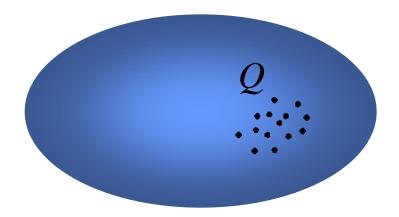
- 1. Electric Flux Density
- 2. Gauss's Law
- 3. Divergence
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# Gauss's Law (1)

- Generalization of Faraday's experiment
- Gauss's Law: the electric flux passing through any closed surface is equal to the total charge enclosed by that surface









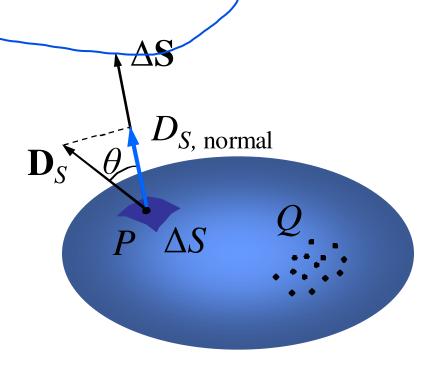
# Gauss's Law (2)

$$\Delta \Psi = \text{flux crossing } \Delta S$$

$$= D_S \cos\theta \Delta S$$

$$= \mathbf{D}_S . \Delta \mathbf{S}$$

$$\rightarrow \Psi = \int d\psi = \oint_{\text{closed surface}} \mathbf{D}_S . d\mathbf{S}$$



$$\Psi = \oint_{S} \mathbf{D}_{S}.d\mathbf{S} = \text{charge enclosed} = Q$$







# Gauss's Law (3)

$$\Psi = \oint_{S} \mathbf{D}_{S} . d\mathbf{S} = \text{charge enclosed} = Q$$

$$Q = \sum Q_n$$

$$Q = \int \rho_L dL$$

$$Q = \int_S \rho_S dS$$

$$Q = \int_V \rho_V dV$$

$$\oint_{S} \mathbf{D}_{S} . d\mathbf{S} = \int_{V} \rho_{v} dv$$

Electric Flux Density, Gauss's Law & Divergence





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## Gauss's Law (4)

$$\mathbf{E} = \frac{Q}{4\pi\varepsilon_0 r^2} \mathbf{a}_r$$

$$\mathbf{D} = \varepsilon_0 \mathbf{E}$$

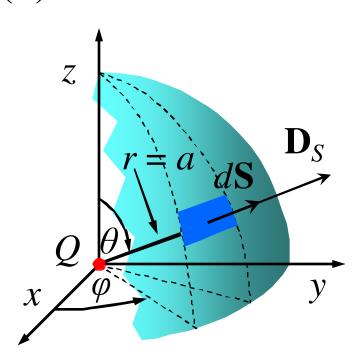
$$\rightarrow \mathbf{D} = \frac{Q}{4\pi r^2} \mathbf{a}_r$$

$$\rightarrow \mathbf{D}_S = \frac{Q}{4\pi a^2} \mathbf{a}_r \text{ (at the surface)}$$

$$\rightarrow \oint_{S} \mathbf{D}_{S}.d\mathbf{S} = \oint_{S} \frac{Q}{4\pi a^{2}} \mathbf{a}_{r} d\mathbf{S}$$

$$dS = r^2 \sin\theta d\theta d\phi = a^2 \sin\theta d\theta d\phi$$
  $\Rightarrow \oint_S \mathbf{D}_S . d\mathbf{S} = \oint_S \frac{Q}{4\pi} \sin\theta d\theta d\phi$ 

$$\to d\mathbf{S} = a^2 \sin\theta d\theta d\varphi \mathbf{a}_r$$



$$\oint_{S} \mathbf{D}_{S} . d\mathbf{S} = \oint_{S} \frac{Q}{4\pi} \sin \theta d\theta d\varphi$$







## Gauss's Law (5)

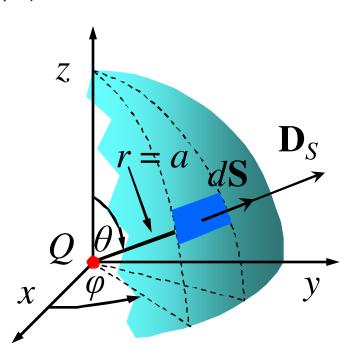
$$\oint_{S} \mathbf{D}_{S} . d\mathbf{S} = \oint_{S} \frac{Q}{4\pi} \sin \theta d\theta d\varphi$$

$$= \int_{\varphi=0}^{\varphi=2\pi} \int_{\theta=0}^{\theta=\pi} \frac{Q}{4\pi} \sin \theta d\theta d\varphi$$

$$= \int_{0}^{2\pi} \frac{Q}{4\pi} (-\cos \theta) \Big|_{0}^{\pi} d\varphi$$

$$= \int_{0}^{2\pi} \frac{Q}{2\pi} d\varphi$$

$$= Q$$







#### Ex. 1

# Gauss's Law (6)

Given a point charge 1 nC at (2, 0, 3) & another point charge 2 nC at (4, -5, 6). Find the total electric flux leaving the enclosed surface formed by the six planes  $x, y, z = \pm 8$ .





# Gauss's Law (7)

- Coulomb's law is to find  $\mathbf{E} = f(Q)$
- Sometimes it is difficult to find E using Coulomb's law
- Gauss may find  $\mathbf{D} (\to \mathbf{E})$  for a given Q

$$Q = \oint_{S} \mathbf{D}_{S} . d\mathbf{S}$$

- The solution is easy if we are able to find a closed surface satisfying 2 conditions:
  - $\mathbf{D}_S$  is everywhere either normal or tangential to the closed surface, so that  $\mathbf{D}_S.d\mathbf{S}$  becomes  $D_SdS$  or zero, respectively
  - On that portion of that surface for which  $\mathbf{D}_S.d\mathbf{S} \neq 0$ ,  $D_S = \text{const}$
- (Gaussian surface)







# Gauss's Law (8)

$$E = ?$$

$$\mathbf{D} = D_{\rho} \mathbf{a}_{\rho}; D_{\rho} = f(\rho)$$

$$Q = \oint_{\text{cylinder}} \mathbf{D}_S.d\mathbf{S}$$

$$= D_S \int_{\text{sides}} dS + 0 \int_{\text{top}} dS + 0 \int_{\text{bottom}} dS$$

$$=D_{S}\int_{z=0}^{z=L}\int_{\varphi=0}^{\varphi=2\pi}\rho d\varphi dz = D_{S}2\pi\rho L \rightarrow D_{S} = D_{\rho} = \frac{Q}{2\pi\rho L}$$

$$Q = \rho_{L}L$$

$$\to D_{\rho} = \frac{\rho_L}{2\pi\rho} \quad \to E_{\rho} = \frac{\rho_L}{2\pi\varepsilon_0\rho}$$









# Gauss's Law (9)

2 coaxial cylindrical conductors. The outer surface of the inner cylinder has a  $\rho_S$ .

$$Q = D_S 2\pi \rho L$$

(total charge of a right circular cylinder of  $L \& \rho \ (a < \rho < b)$ )

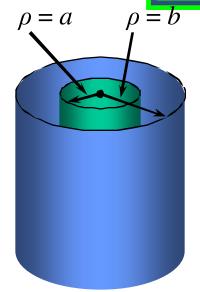
$$Q = \int_{z=0}^{z=L} \int_{\varphi=0}^{\varphi=2\pi} \rho_S ad\varphi dz = 2\pi aL\rho_S$$

(total charge of the inner cylinder of length L)

$$\rightarrow D_{S} = \frac{a\rho_{S}}{\rho} \qquad \mathbf{D} = \frac{a\rho_{S}}{\rho} \mathbf{a}_{\rho} (a < \rho < b)$$

$$\rho_{L} = Q|_{l=1} = \rho_{S} S|_{l=1} = \rho_{S}.2\pi a.1 = 2\pi a\rho_{s}$$

$$\rightarrow \left[ \mathbf{D} = \frac{\rho_L}{2\pi\rho} \mathbf{a}_{\rho} \right]$$









# Gauss's Law (10)

$$Q_{\rm outer\,cylinder} = -Q_{\rm inner\,cylinder}$$

$$Q_{\text{outer cylinder}} = 2\pi b L \rho_{S, \text{outer cylinder}}$$

$$Q_{\text{inner cylinder}} = 2\pi a L \rho_{S, \text{inner cylinder}}$$

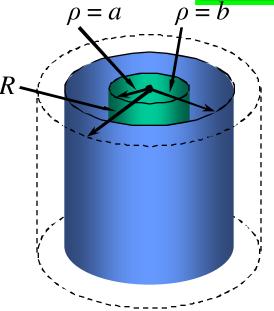
$$\rho = a$$
 $\rho = b$ 

$$\rightarrow \rho_{S,\text{outer cylinder}} = -\frac{a}{b} \rho_{S,\text{inner cylinder}}$$





# Gauss's Law (11)



$$\Psi_{R,R>b} = Q_{\text{outer cylinder}} + Q_{\text{inner cylinder}} = 0 = D_{S,R} 2\pi RL$$

$$\rightarrow D_{S,R} = 0$$

The coaxial cable/capacitor has no external field & there is no field within the inner cylinder



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#### **Ex. 2**

# Gauss's Law (12)

Consider a coaxial cable of 1-m length, its inner radius is 1mm, the outer one is 4mm. Conductors are separated by air. The total charge on the inner cylinder is 40nC. Find charge density on each conductor, **E** & **D**.

$$\rho_{S,\text{inner cylinder}} = \frac{Q_{\text{inner cylinder}}}{2\pi aL} = \frac{40 \times 10^{-9}}{2\pi \times 10^{-3} \times 1} = 6.37 \ \mu\text{C/m}^2$$

$$\rho_{S,\text{outer cylinder}} = \frac{Q_{\text{outer cylinder}}}{2\pi bL} = \frac{-40 \times 10^{-9}}{2\pi \times 4 \times 10^{-3} \times 1} = -1.59 \ \mu\text{C/m}^2$$

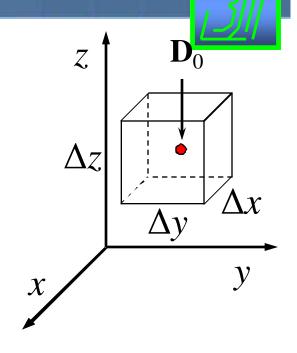
$$D_{\rho}\Big|_{10^{-3} < \rho < 4.10^{-3}} = \frac{a\rho_{S,inner cylinder}}{\rho} = \frac{1 \times 10^{-3} \times 6.37 \times 10^{-6}}{\rho} = \frac{6.37}{\rho} \text{ nC/m}^{2}$$

$$E_{\rho}\Big|_{10^{-3} < \rho < 4.10^{-3}} = \frac{D_{\rho}}{\varepsilon_{0}} = \frac{6.37 \times 10^{-9}}{8.854 \times 10^{-12} \rho} = \frac{719}{\rho} \text{ V/m}^{2}$$



# Gauss's Law (13)

- The application of Gauss's law (to find **D**) needs a gaussian surface
- *Problem*: hard to find such surface
- *Solution*: choose a very small closed surface (approaching zero)

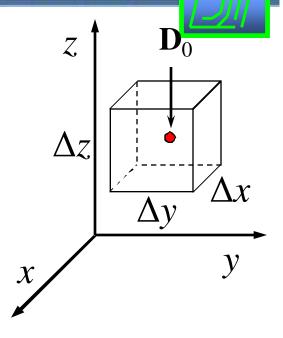


$$\mathbf{D} = \mathbf{D}_0 = D_{x0}\mathbf{a}_x + D_{y0}\mathbf{a}_y + D_{z0}\mathbf{a}_z$$





$$Q = \oint_{S} \mathbf{D}_{S}.d\mathbf{S}$$



$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}}$$

Because the closed surface is very small, **D** is almost constant over the surface

$$\int_{\text{front}} \dot{=} \mathbf{D}_{\text{front}} . \Delta \mathbf{S}_{\text{front}} \dot{=} \mathbf{D}_{\text{front}} . \Delta y \Delta z \mathbf{a}_{x} \dot{=} D_{x, \text{ front}} \Delta y \Delta z$$





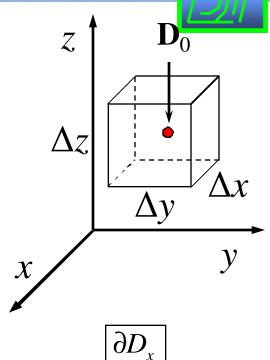
# Gauss's Law (15)

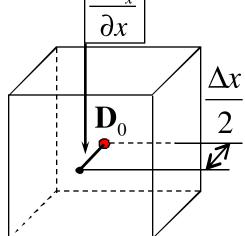
$$\int_{\text{front}} \dot{=} D_{x, \text{front}} \Delta y \Delta z$$

$$D_{x,\text{front}} \doteq D_{x0} + \frac{\Delta x}{2} \times (\text{rate of change of } D_x \text{ with } x)$$

$$\doteq D_{x0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x}$$

$$\rightarrow \int_{\text{front}} \dot{=} \left( D_{x0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \Delta z$$









# Gauss's Law (16)

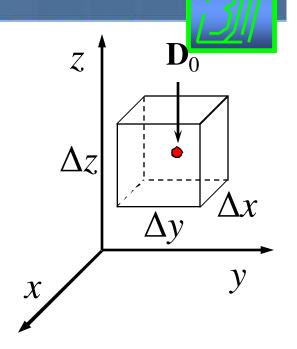
$$\int_{\text{front}} \dot{=} \left( D_{x0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \Delta z$$

$$\int_{\text{back}} \doteq \mathbf{D}_{\text{back}} \cdot \Delta \mathbf{S}_{\text{back}} \doteq \mathbf{D}_{\text{back}} \cdot (-\Delta y \Delta z \mathbf{a}_{x})$$

$$\doteq -D_{x, \text{back}} \Delta y \Delta z$$

$$D_{x, \text{back}} \doteq D_{x0} - \frac{\Delta x}{2} \frac{\partial D_{x}}{\partial x}$$

$$\rightarrow \int_{\text{back}} \dot{=} \left( -D_{x0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \Delta z$$







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# Gauss's Law (17)

$$\int_{\text{front}} \doteq \left( D_{x0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \Delta z$$

$$\int_{\text{back}} \doteq \left( -D_{x0} + \frac{\Delta x}{2} \frac{\partial D_x}{\partial x} \right) \Delta y \Delta z$$

$$\rightarrow \int_{\text{front}} + \int_{\text{back}} \doteq \frac{\partial D_x}{\partial x} \Delta x \Delta y \Delta z$$







### Gauss's Law (18)

$$\int_{\text{front}} + \int_{\text{back}} \dot{=} \frac{\partial D_x}{\partial x} \Delta x \Delta y \Delta z$$

$$\int_{\text{right}} + \int_{\text{left}} \dot{=} \frac{\partial D_y}{\partial y} \Delta x \Delta y \Delta z$$

$$\int_{\text{top}} + \int_{\text{bottom}} \dot{=} \frac{\partial D_z}{\partial z} \Delta x \Delta y \Delta z$$

$$\oint_{S} \mathbf{D} \cdot d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}} \int_{\text{bottom}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{bottom}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{bottom}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{bottom}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{\text{bottom}} d\mathbf{S} = \int_{\text{front}} d\mathbf{S} = \int_{$$

$$\rightarrow \oint_{S} \mathbf{D}.d\mathbf{S} \doteq \left( \frac{\partial D_{x}}{\partial x} + \frac{\partial D_{y}}{\partial y} + \frac{\partial D_{z}}{\partial z} \right) \Delta x \Delta y \Delta z$$



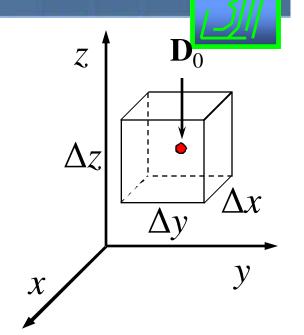
# Gauss's Law (19)

$$\oint_{S} \mathbf{D}.d\mathbf{S} \doteq \left( \frac{\partial D_{x}}{\partial x} + \frac{\partial D_{y}}{\partial y} + \frac{\partial D_{z}}{\partial z} \right) \Delta x \Delta y \Delta z$$

$$\Delta v = \Delta x \Delta y \Delta z$$

$$\rightarrow \oint_{S} \mathbf{D}.d\mathbf{S} \doteq \left( \frac{\partial D_{x}}{\partial x} + \frac{\partial D_{y}}{\partial y} + \frac{\partial D_{z}}{\partial z} \right) \Delta v$$

$$Q_{\text{enclosed in}\Delta v} \doteq \left(\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}\right) \times \Delta v$$







#### **Ex. 3**

# Gauss's Law (20)

Find the approximate value for the total charge inclosed in an incremental volume of  $10^{-10}$  m<sup>3</sup> located at the origin. Given  $\mathbf{D} = e^{-x} \sin y \mathbf{a}_x - e^{-x} \cos y \mathbf{a}_y + 2z \mathbf{a}_z$  C/m<sup>2</sup>.

$$Q_{\text{enclosed in }\Delta v} \doteq \left(\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}\right) \times \Delta v$$

$$\frac{\partial D_x}{\partial x} = -e^{-x} \sin y \quad \Rightarrow \frac{\partial D_x}{\partial x} \Big|_{x=0} = 0$$

$$\frac{\partial D_y}{\partial y} = e^{-x} \sin y \quad \Rightarrow \frac{\partial D_y}{\partial y} \Big|_{y=0} = 0$$

$$\frac{\partial D_z}{\partial z} = 2$$

$$\rightarrow Q_{\text{enclosed in }\Delta v} \doteq (0+0+2)10^{-10} = 0.2 \text{ nC}$$





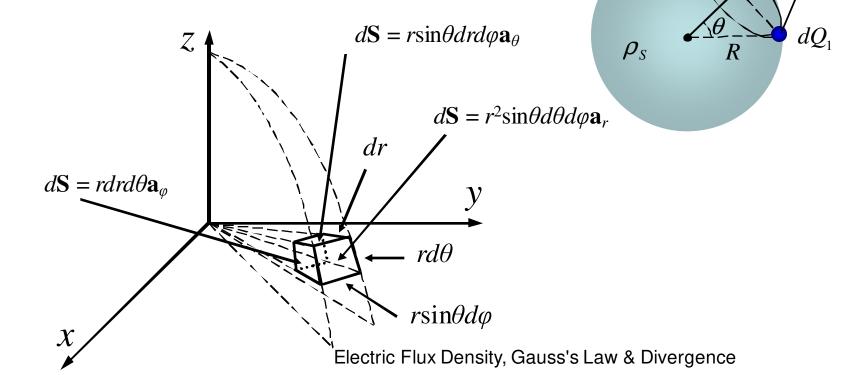
 $d\mathbf{E}_{1}$ 

#### Ex. 4

# Gauss's Law (21)

A sphere of radius R has a uniform surface charge density  $\rho_S$ . Find  $\mathbf{E}$  at P?

$$dQ_1 = \rho_S dS_1 = \rho_S R^2 \sin\theta d\theta d\varphi$$









#### Ex. 4

# Gauss's Law (21)

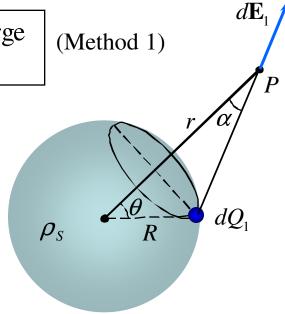
A sphere of radius R has a uniform surface charge density  $\rho_S$ . Find  $\mathbf{E}$  at P?

$$dQ_1 = \rho_S dS_1 = \rho_S R^2 \sin\theta d\theta d\varphi$$

$$dE_1 = \frac{dQ_1}{4\pi\varepsilon_0 R_{Q_1P}^2} \cos \alpha$$
$$= \frac{\rho_S R^2 \sin \theta d \theta d \varphi}{4\pi\varepsilon_0 R_{Q_1P}^2} \cos \alpha$$

$$= \frac{\rho_S R^2 \sin \theta d\theta d\phi}{4\pi \varepsilon_0 R_{Q_1 P}^2} \times \frac{r - R \cos \theta}{\sqrt{r^2 + R^2 - 2rR \cos \theta}}$$

$$\rightarrow E_P = \int_{\varphi=0}^{2\pi} \int_{\theta=0}^{\pi} \frac{\rho_S R^2 \sin \theta (r - R \cos \theta) d\theta d\varphi}{4\pi \varepsilon_0 (r^2 + R^2 - 2rR \cos \theta)^{3/2}} = ???$$







#### Ex. 4

Gauss's Law (22)

A sphere of radius R has a uniform surface charge density  $\rho_S$ . Find  $\mathbf{E}$  at P?

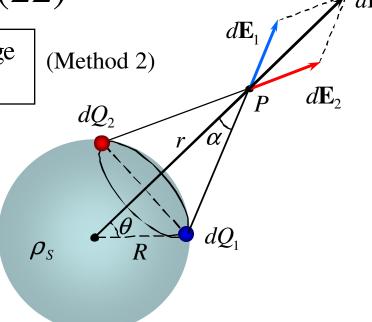
$$\oint_{S} \varepsilon_{0} \mathbf{E}.d\mathbf{S} = Q$$

$$\oint_{S} \varepsilon_{0} \mathbf{E}.d\mathbf{S} = \varepsilon_{0} E_{Pr} (4\pi r^{2})$$

$$Q = \rho_{S} (4\pi R^{2})$$

$$\rightarrow \varepsilon_0 E_{Pr}(4\pi r^2) = \rho_S(4\pi R^2)$$

$$\rightarrow E_{Pr} = \frac{\rho_S R^2}{\varepsilon_0 r^2}, \quad r > R$$









#### **Ex. 5**

# Gauss's Law (23)

An infinitely long cylinder of radius a has a uniform surface charge density  $\rho_S$ . Find **E**?

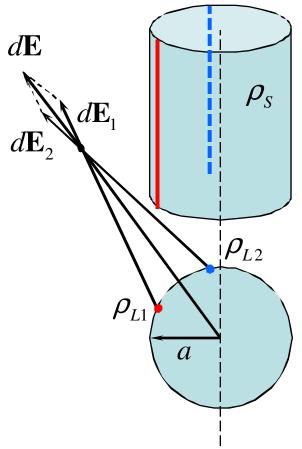
$$\oint_{S} \varepsilon_{0} \mathbf{E}.d\mathbf{S} = Q$$

$$\oint_{S} \varepsilon_{0} \mathbf{E}.d\mathbf{S} = \varepsilon_{0} E_{r}(2\pi rL)$$

$$Q = \rho_{S}(2\pi aL)$$

$$\to \varepsilon_0 E_r(2\pi r L) = \rho_s(2\pi a L)$$

$$\rightarrow \boxed{E_r = \frac{\rho_S a}{\varepsilon_0 r}}, \quad r > a$$









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# Divergence (1)

$$\oint_{S} \mathbf{D}.d\mathbf{S} = Q \doteq \left( \frac{\partial D_{x}}{\partial x} + \frac{\partial D_{y}}{\partial y} + \frac{\partial D_{z}}{\partial z} \right) \Delta v$$

$$\rightarrow \left(\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}\right) \doteq \frac{\oint_S \mathbf{D}.d\mathbf{S}}{\Delta v} = \frac{Q}{\Delta v}$$

$$\rightarrow \left(\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}\right) = \lim_{\Delta v \to 0} \frac{\oint_S \mathbf{D}.d\mathbf{S}}{\Delta v} = \lim_{\Delta v \to 0} \frac{Q}{\Delta v}$$

$$\rightarrow \left(\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}\right) = \lim_{\Delta v \to 0} \frac{\oint_S \mathbf{A}.d\mathbf{S}}{\Delta v}$$

Divergence of 
$$\mathbf{A} = \operatorname{div} \mathbf{A} = \lim_{\Delta v \to 0} \frac{\oint_{S} \mathbf{A} \cdot d\mathbf{S}}{\Delta v}$$





# Divergence (2)

Divergence of 
$$\mathbf{A} = \operatorname{div} \mathbf{A} = \lim_{\Delta v \to 0} \frac{\oint_{S} \mathbf{A} . d\mathbf{S}}{\Delta v}$$

- *Definition*: the divergence of the vector flux density **A** is the outflow of flux from a small closed surface per unit volume as the volume shrinks to zero
- Divergence is an operation which is performed on a vector, but the result is a scalar
- Divergence only tells us *how much* flux is leaving a small volume (on a per-unit-volume basis), not *direction*



https://www.khanacademy.org/math/multivariable-calculus/multivariable-derivatives/divergence-and-curl-articles/a/divergence





# Divergence (3)

Divergence of 
$$\mathbf{A} = \operatorname{div} \mathbf{A} = \lim_{\Delta v \to 0} \frac{\oint_{S} \mathbf{A} . d\mathbf{S}}{\Delta v}$$

$$\operatorname{div} \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \quad \text{(Descartes)}$$

$$\operatorname{div} \mathbf{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_{\rho}) + \frac{1}{\rho} \frac{\partial D_{\varphi}}{\partial \varphi} + \frac{\partial D_{z}}{\partial z} \quad \text{(Cylindrical)}$$

$$\operatorname{div} \mathbf{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta D_{\theta}) + \frac{1}{r \sin \theta} \frac{\partial D_{\phi}}{\partial \phi} \quad \text{(Spherical)}$$





#### **Ex.** 1

# Divergence (4)

Find divergence at the origin, given  $\mathbf{D} = e^{-x} \sin y \mathbf{a}_x - e^{-x} \cos y \mathbf{a}_y + 2z \mathbf{a}_z$  C/m<sup>2</sup>.





#### Ex. 2

## Divergence (5)

Find the divergence of the following vectors:

$$\mathbf{a})\mathbf{A} = xy^2 z^3 (\mathbf{a}_x + \mathbf{a}_y + \mathbf{a}_z)$$

b) 
$$\mathbf{A} = \rho \cos \varphi \mathbf{a}_{\rho} + \frac{z}{\rho} \sin \varphi \mathbf{a}_{z}$$

$$c)\mathbf{A} = r^2 \sin \theta \cos \varphi (\mathbf{a}_r + \mathbf{a}_\theta + \mathbf{a}_\varphi)$$







# Electric Flux Density, Gauss's Law & Divergence

- 1. Electric Flux Density
- 2. Gauss's Law
- 3. Divergence
- 4. Maxwell's First Equation
- 5. The Vector Operator  $\nabla$
- 6. The Divergence Theorem





### Maxwell's First Equation (1)

$$\oint_{S} \mathbf{D}.d\mathbf{S} = Q \rightarrow \frac{\oint_{S} \mathbf{D}.d\mathbf{S}}{\Delta v} = \frac{Q}{\Delta v}$$

$$\rightarrow \lim_{\Delta v \to 0} \frac{\oint_{S} \mathbf{D}.d\mathbf{S}}{\Delta v} = \lim_{\Delta v \to 0} \frac{Q}{\Delta v}$$

$$\operatorname{div} \mathbf{D} = \lim_{\Delta v \to 0} \frac{\oint_{S} \mathbf{D}.d\mathbf{S}}{\Delta v} \qquad \lim_{\Delta v \to 0} \frac{Q}{\Delta v} = \rho_{v}$$

$$\rightarrow |\operatorname{div} \mathbf{D} = \rho_{v}|$$
 Maxwell's first equation





## Maxwell's First Equation (2)

$$\operatorname{div} \mathbf{D} = \boldsymbol{\rho}_{v}$$

- Apply to electrostatic & steady magnetic fields
- The electric flux per unit volume leaving a vanishingly small volume unit is exactly equal to the volume charge density there





#### Ex.

### Maxwell's First Equation (3)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup>, find  $\rho_v$  of the region about P(1,1,1).

$$\rho_{v} = \operatorname{div} \mathbf{D}$$

$$\operatorname{div} \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} = \frac{\partial}{\partial x} 4xy + \frac{\partial}{\partial y} z^2 + \frac{\partial}{\partial z} 0 = 4y$$

$$\rightarrow \rho_{v} = 4y$$

$$\rightarrow \rho_{v,P} = \rho_v \big|_{x=y=z=1} = 4 \times 1 = \boxed{4 \text{ C/m}^3}$$







# Electric Flux Density, Gauss's Law & Divergence

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# $\nabla(1)$

$$\left| \nabla = \frac{\partial}{\partial x} \mathbf{a}_x + \frac{\partial}{\partial y} \mathbf{a}_y + \frac{\partial}{\partial z} \mathbf{a}_z \right|$$

$$\nabla .\mathbf{D} = \left(\frac{\partial}{\partial x}\mathbf{a}_{x} + \frac{\partial}{\partial y}\mathbf{a}_{y} + \frac{\partial}{\partial z}\mathbf{a}_{z}\right).\left(D_{x}\mathbf{a}_{x} + D_{y}\mathbf{a}_{y} + D_{z}\mathbf{a}_{z}\right)$$

$$= \frac{\partial}{\partial x}(D_{x}) + \frac{\partial}{\partial y}(D_{y}) + \frac{\partial}{\partial z}(D_{z})$$

$$= \frac{\partial D_{x}}{\partial x} + \frac{\partial D_{y}}{\partial y} + \frac{\partial D_{z}}{\partial z} = \operatorname{div}\mathbf{D}$$





 $\nabla(2)$ 

#### Ex.

Given  $\mathbf{D} = e^{-x} \sin y \mathbf{a}_x - e^{-x} \cos y \mathbf{a}_y + 2z \mathbf{a}_z$  C/m<sup>2</sup>, find  $\nabla \cdot \mathbf{D}$ ?







# Electric Flux Density, Gauss's Law & Divergence

- 1. Electric Flux Density
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## The Divergence Theorem (1)

 Applies to any vector field for which the appropriate partial derivatives exist

$$\oint_{S} \mathbf{D}.d\mathbf{S} = Q$$

$$Q = \int_{V} \rho_{v} dv$$

$$\nabla .\mathbf{D} = \rho_{v}$$

$$\Rightarrow \oint_{S} \mathbf{D}.d\mathbf{S} = Q = \int_{V} \rho_{v} dv = \int_{V} \nabla .\mathbf{D} dv$$

$$\Rightarrow \oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D} dv$$

• *Theorem*: the integral of the normal component of any vector field over a closed surface is equal to the integral of the divergence of this vector field throughout the volume enclosed by the closed surface





Z

#### Ex.

# The Divergence Theorem (2)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}} \\
\int_{\text{front}} = \int_{z=0}^{z=3} \int_{y=0}^{y=2} \mathbf{D}_{\text{front}}.d\mathbf{S}_{\text{front}} \\
\mathbf{D}_{\text{front}} = (4xy\mathbf{a}_{x} + z^{2}\mathbf{a}_{y})\Big|_{x=1} = 4y\mathbf{a}_{x} + z^{2}\mathbf{a}_{y} \\
d\mathbf{S}_{\text{front}} = dydz\mathbf{a}_{x}$$

$$\rightarrow \int_{\text{front}} = \int_{z=0}^{z=3} \int_{y=0}^{y=2} (4y\mathbf{a}_{x} + z^{2}\mathbf{a}_{y}).(dydz\mathbf{a}_{x}) = \int_{z=0}^{z=3} \int_{y=0}^{y=2} 4ydydz$$





Z

#### Ex.

The Divergence Theorem (3)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}}$$

$$\int_{\text{front}} = \int_{z=0}^{z=3} \int_{y=0}^{y=2} (4y\mathbf{a}_x + z^2\mathbf{a}_y) \cdot (dydz\mathbf{a}_x) = \int_{z=0}^{z=3} \int_{y=0}^{y=2} 4ydydz$$

$$=12 C$$





Z

#### Ex.

The Divergence Theorem (4)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

$$\oint_{S} \mathbf{D} \cdot d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}}$$

$$\int_{\text{back}} = \int_{z=0}^{z=3} \int_{y=0}^{y=2} \mathbf{D} \Big|_{x=0} . (-dy dz \mathbf{a}_x) = -\int_{z=0}^{z=3} \int_{y=0}^{y=2} D_x \Big|_{x=0} dy dz$$

$$D_x \Big|_{x=0} = (4xy) \Big|_{x=0} = 0$$

$$\rightarrow \int_{\text{back}} = 0$$





Z

#### Ex.

# The Divergence Theorem (5)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}}$$

$$\int_{\text{right}} = \int_{z=0}^{z=3} \int_{x=0}^{x=1} \mathbf{D} \Big|_{y=2} . (dx dz \mathbf{a}_y) = \int_{z=0}^{z=3} \int_{x=0}^{x=1} D_y \Big|_{y=2} dx dz$$

$$D_y \Big|_{y=2} = (z^2) \Big|_{y=2} = z^2$$

$$\rightarrow \int_{\text{right}} = \int_{z=0}^{z=3} \int_{x=0}^{x=1} z^2 dx dz$$





Z

#### Ex.

The Divergence Theorem (6)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

#### Left side:

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}}$$

$$\int_{\text{left}} = \int_{z=0}^{z=3} \int_{x=0}^{x=1} \mathbf{D} \Big|_{y=0} . (-dxdz\mathbf{a}_y) = -\int_{z=0}^{z=3} \int_{x=0}^{x=1} D_y \Big|_{y=0} dxdz$$

$$D_y \Big|_{y=0} = (z^2) \Big|_{y=0} = z^2$$

$$\rightarrow \int_{\text{left}} = -\int_{z=0}^{z=3} \int_{x=0}^{x=1} z^2 dx dz$$

Electric Flux Density, Gauss's Law & Divergence



#### NG BẠI HỌC BÁCH KHOA HÀ NỘI



Z

#### Ex.

# The Divergence Theorem (7)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}}$$

$$\int_{\text{top}} = \int_{x=0}^{x=1} \int_{y=0}^{y=2} (4xy\mathbf{a}_x + z^2\mathbf{a}_y) \cdot (dxdy\mathbf{a}_z) = \int_{x=0}^{x=1} \int_{y=0}^{y=2} 0 = 0$$

$$\int_{\text{bottom}} = \int_{x=0}^{x=1} \int_{y=0}^{y=2} (4xy\mathbf{a}_x + z^2\mathbf{a}_y) \cdot (dxdy\mathbf{a}_z) = \int_{x=0}^{x=1} \int_{y=0}^{y=2} 0 = 0$$





Z

#### Ex.

The Divergence Theorem (8)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

$$\oint_{S} \mathbf{D} \cdot d\mathbf{S} = \int_{\text{front}} + \int_{\text{back}} + \int_{\text{left}} + \int_{\text{right}} + \int_{\text{top}} + \int_{\text{bottom}} + \int_{\text{bottom}} + \int_{\text{sol}} \int_{\text{reft}} + \int_{\text{sol}} \int_{\text{reft}} + \int_{\text{bottom}} + \int_{\text{bottom}} + \int_{\text{bottom}} + \int_{\text{sol}} \int_{\text{reft}} + \int_{\text{bottom}} + \int_{\text{bottom}} + \int_{\text{bottom}} + \int_{\text{sol}} \int_{\text{reft}} + \int_{\text{bottom}} + \int_{\text{bottom$$

$$= 24C$$





#### Ex.

# The Divergence Theorem (9)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla.\mathbf{D}dV \ (=Q)$$

#### Right side:

$$\int_{V} \nabla .\mathbf{D} dV$$

$$\nabla .\mathbf{D} = \frac{\partial}{\partial x} 4xy + \frac{\partial}{\partial y} z^{2} + \frac{\partial}{\partial z} 0 = 4y$$

$$dV = dxdydz$$





#### Ex.

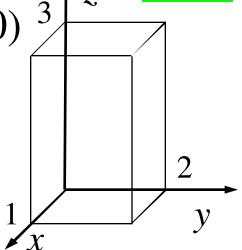
The Divergence Theorem (10)

Given  $\mathbf{D} = 4xy\mathbf{a}_x + z^2\mathbf{a}_y$  C/m<sup>2</sup> & a rectangular parallelepiped. Verify the divergence theorem.

$$\oint_{S} \mathbf{D}.d\mathbf{S} = \int_{V} \nabla .\mathbf{D}dV \ (=Q)$$

Left side: 
$$\oint_{S} \mathbf{D} . d\mathbf{S} = 24 \text{ C}$$

Left side: 
$$\oint_{S} \mathbf{D}.d\mathbf{S} = 24 \text{ C}$$
Right side:  $\int_{V} \nabla.\mathbf{D}dV = 24 \text{ C}$ 

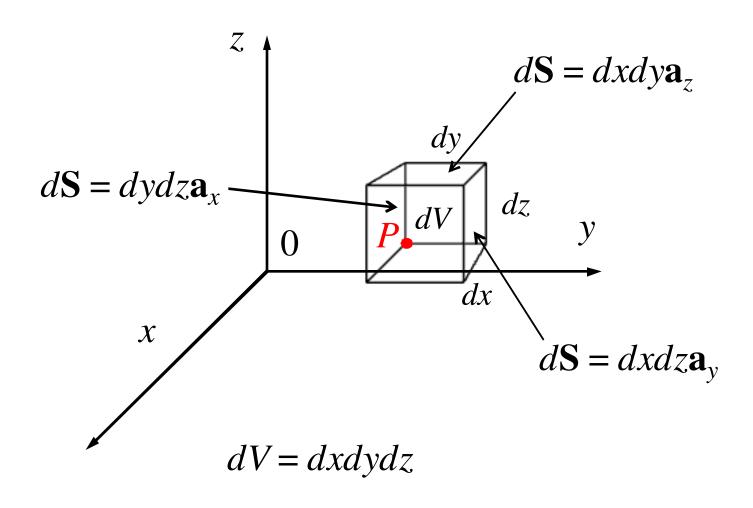




#### TRƯ**ờng Bại Học** BÁCH KHOA HÀ NỘI



## The Rectangular Coordinate System

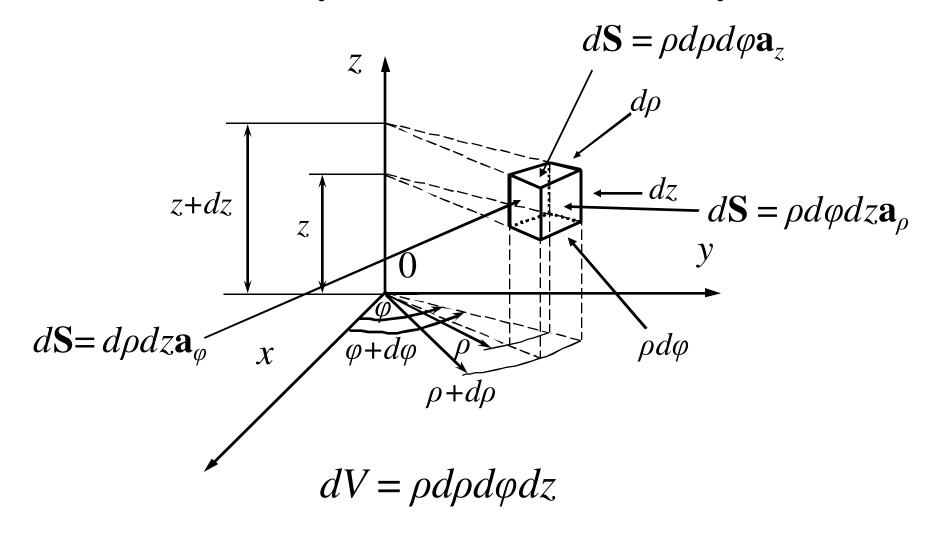




#### TRƯ**ờng Bại Học** BÁCH KHOA HÀ NỘI



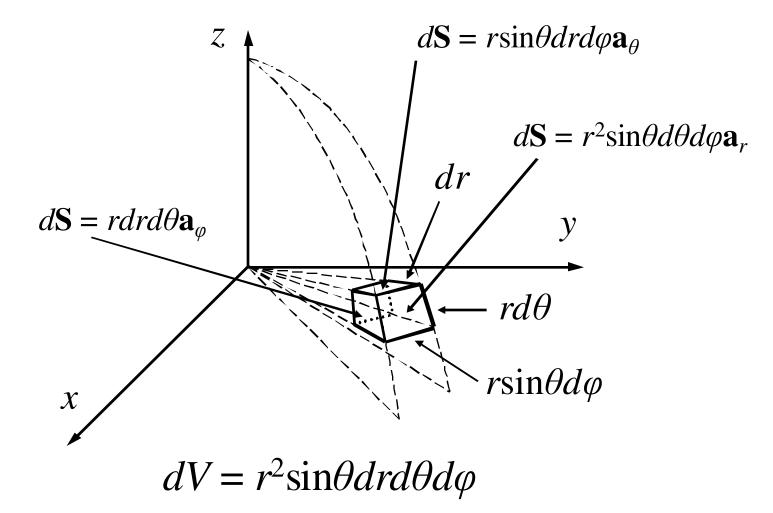
# The Circular Cylindrical Coordinate System







## The Spherical Coordinate System









$$Q \longrightarrow \mathbf{F} = \frac{Q_1 Q_2}{4\pi \varepsilon R^2} \mathbf{a}_R \longrightarrow \mathbf{E} = \frac{Q}{4\pi \varepsilon R^2} \mathbf{a}_R \longrightarrow \mathbf{D} = \varepsilon \mathbf{E}$$