



TRƯỜNG ĐẠI HỌC  
BÁCH KHOA HÀ NỘI



Nguyễn Công Phương

# Engineering Electromagnetics

## The Steady Magnetic Field

# Contents

- I. Introduction
- II. Vector Analysis
- III. Coulomb's Law & Electric Field Intensity
- IV. Electric Flux Density, Gauss' Law & Divergence
- V. Energy & Potential
- VI. Current & Conductors
- VII. Dielectrics & Capacitance
- VIII. Poisson's & Laplace's Equations
- IX. The Steady Magnetic Field**
- X. Magnetic Forces & Inductance
- XI. Time – Varying Fields & Maxwell's Equations
- XII. The Uniform Plane Wave
- XIII. Plane Wave Reflection & Dispersion
- XIV. Guided Waves & Radiation

## The Steady Magnetic Field (1)

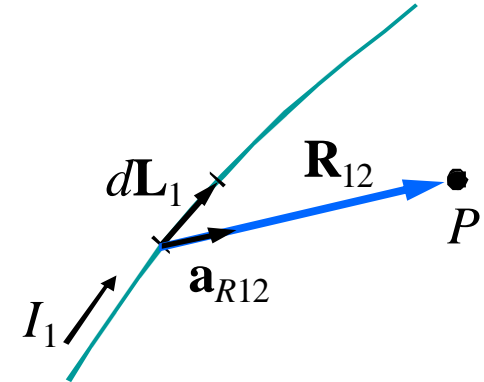
1. Biot – Savart Law
2. Ampere's Circuital Law
3. Curl
4. Stokes' Theorem
5. Magnetic Flux & Magnetic Flux Density
6. Magnetic Potential
7. Derivation of the Steady – Magnetic – Field Law

## The Steady Magnetic Field (2)

- The source of the steady magnetic field may be:
  - Permanent magnet
  - Electric field changing linearly with time
  - Direct current
- Consider the field produced by a differential dc element in free space only

## Biot – Savart Law (1)

$$d\mathbf{H} = \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2} = \frac{Id\mathbf{L} \times \mathbf{R}}{4\pi R^3}$$



**H**: magnetic field intensity (A/m)

The direction of **H** is determined by the right-hand rule

$$d\mathbf{H}_2 = \frac{I_1 d\mathbf{L}_1 \times \mathbf{a}_{R12}}{4\pi R_{12}^2}$$

$$d\mathbf{H} = \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2} \rightarrow \mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2}$$

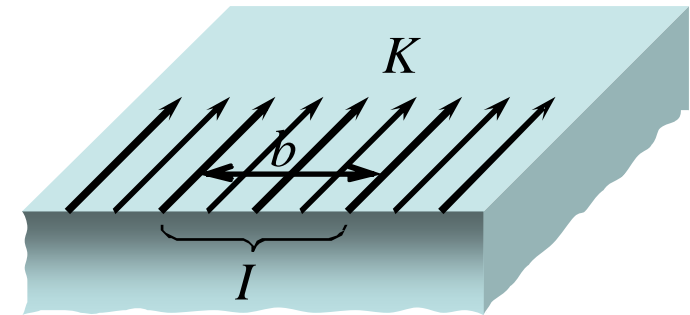
## Biot – Savart Law (2)

$$I = Kb$$

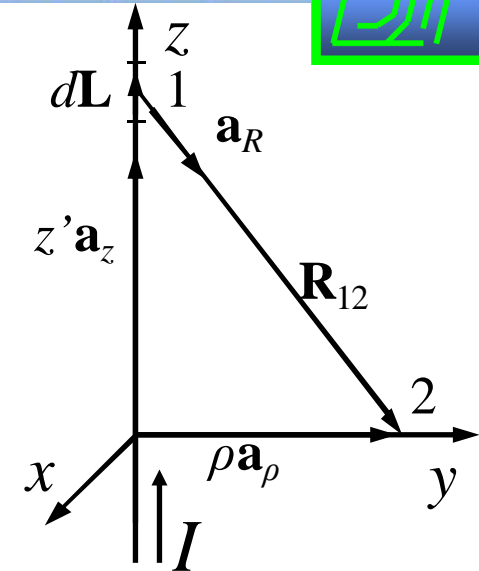
$$I = \int K dN$$

$$Id\mathbf{L} = \mathbf{K}dS$$

$$\mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2} = \int_S \frac{\mathbf{K} \times \mathbf{a}_R dS}{4\pi R^2}$$



## Biot – Savart Law (3)

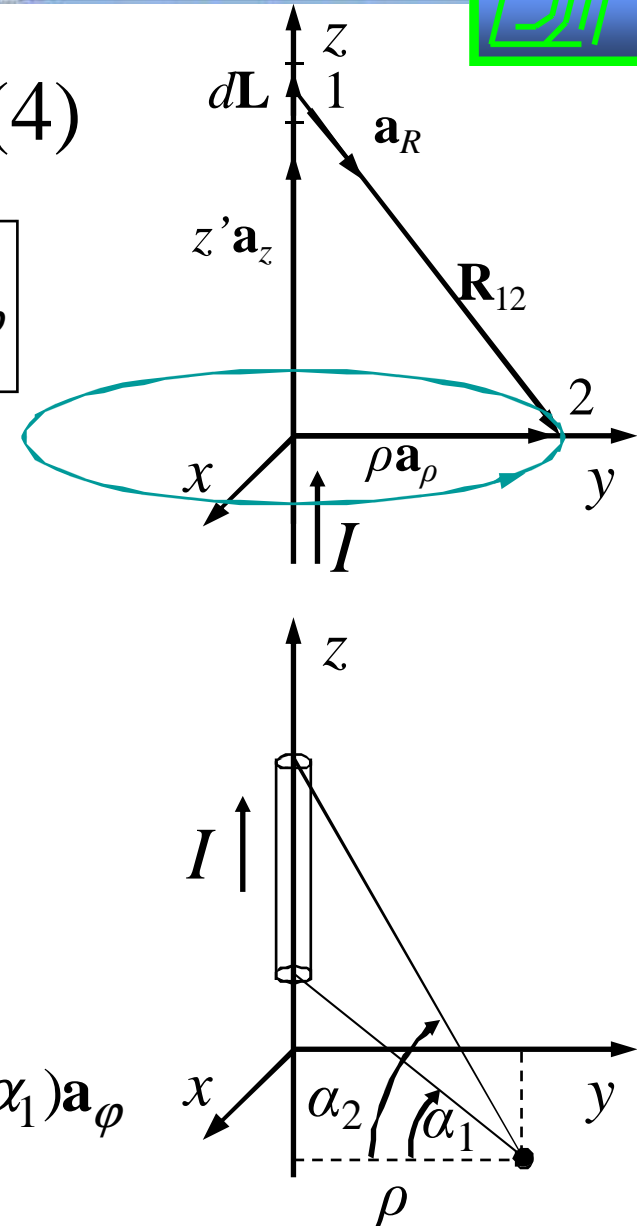
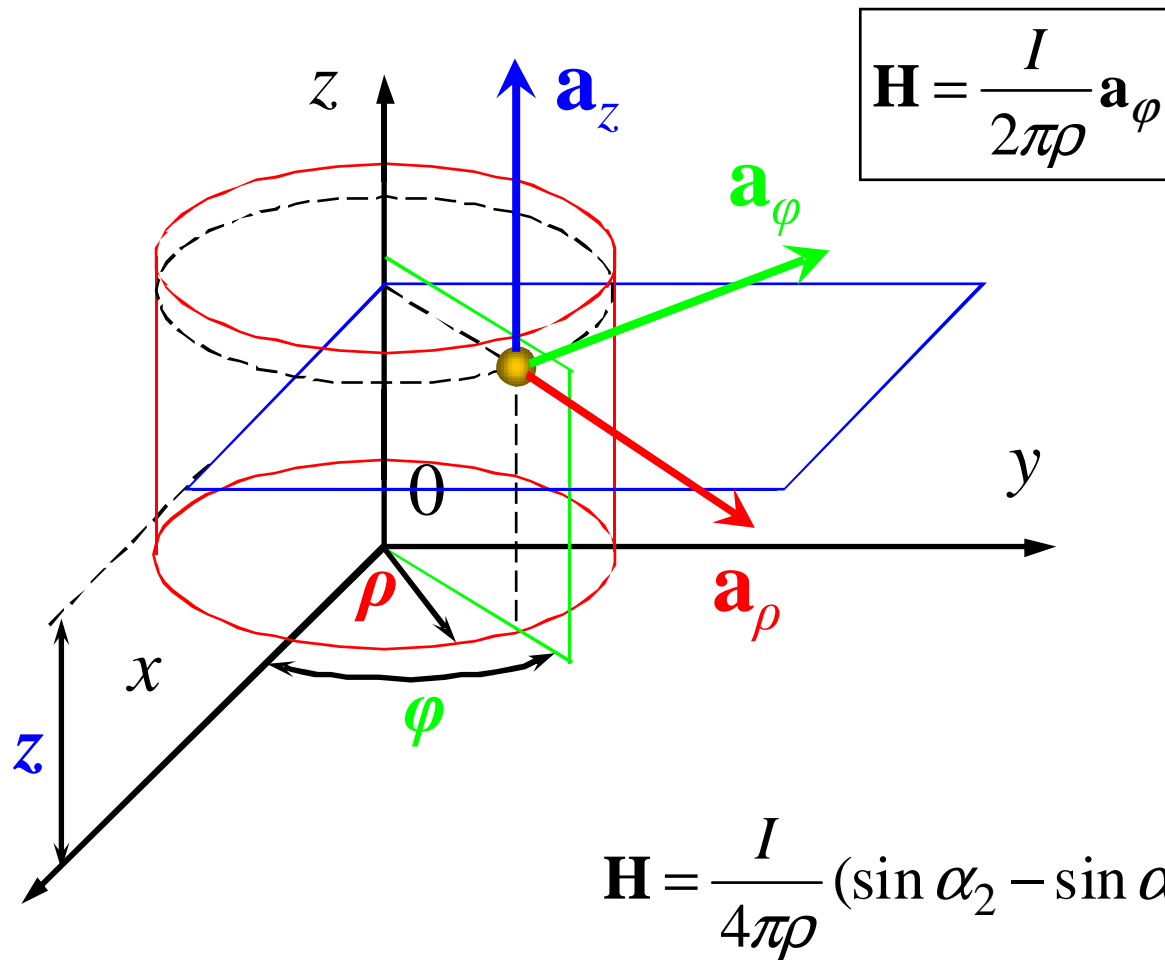


$$\left. \begin{aligned} d\mathbf{H}_2 &= \frac{Id\mathbf{L}_1 \times \mathbf{a}_{R12}}{4\pi R_{12}^2} \\ d\mathbf{L}_1 &= dz' \mathbf{a}_z \\ \mathbf{R}_{12} &= \rho \mathbf{a}_\rho - z' \mathbf{a}_z \rightarrow \mathbf{a}_{R12} = \frac{\rho \mathbf{a}_\rho - z' \mathbf{a}_z}{\sqrt{\rho^2 + z'^2}} \end{aligned} \right\}$$

$$\rightarrow d\mathbf{H}_2 = \frac{Idz' \mathbf{a}_z \times (\rho \mathbf{a}_\rho - z' \mathbf{a}_z)}{4\pi(\rho^2 + z'^2)^{3/2}} \rightarrow \mathbf{H}_2 = \int_{-\infty}^{\infty} \frac{Idz' \mathbf{a}_z \times (\rho \mathbf{a}_\rho - z' \mathbf{a}_z)}{4\pi(\rho^2 + z'^2)^{3/2}} \left. \begin{aligned} &\mathbf{a}_z \times \mathbf{a}_\rho = \mathbf{a}_\phi; \mathbf{a}_z \times \mathbf{a}_z = 0 \end{aligned} \right\}$$

$$\begin{aligned} \rightarrow \mathbf{H}_2 &= \frac{I}{4\pi} \int_{-\infty}^{\infty} \frac{\rho dz' \mathbf{a}_\phi}{(\rho^2 + z'^2)^{3/2}} = \frac{I \rho \mathbf{a}_\phi}{4\pi} \int_{-\infty}^{\infty} \frac{dz'}{(\rho^2 + z'^2)^{3/2}} \\ &= \frac{I \rho \mathbf{a}_\phi}{4\pi} \left. \frac{z'}{\rho^2 \sqrt{\rho^2 + z'^2}} \right|_{z'=-\infty}^{z'=\infty} = \boxed{\frac{I}{2\pi\rho} \mathbf{a}_\phi} \end{aligned}$$

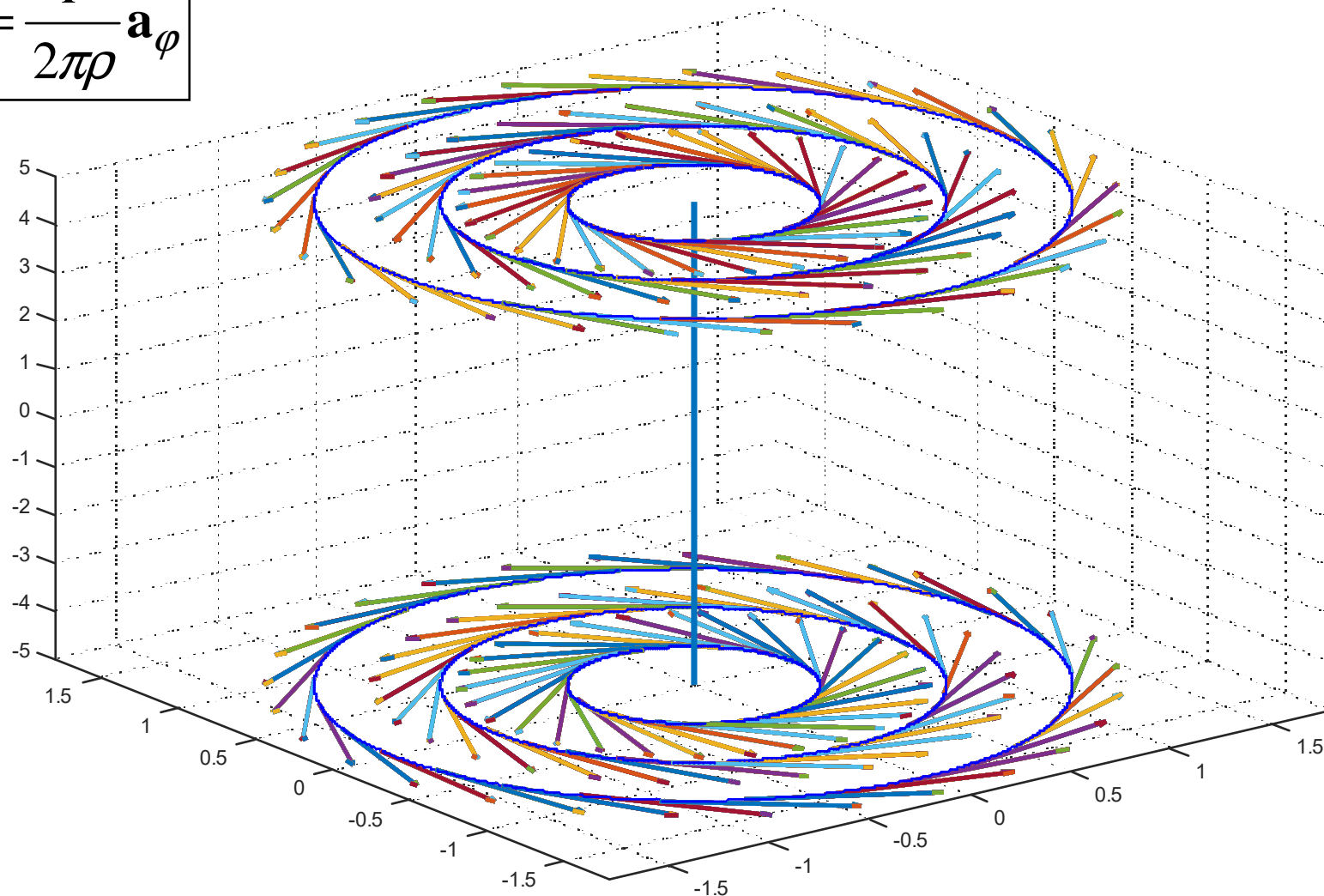
## Biot – Savart Law (4)





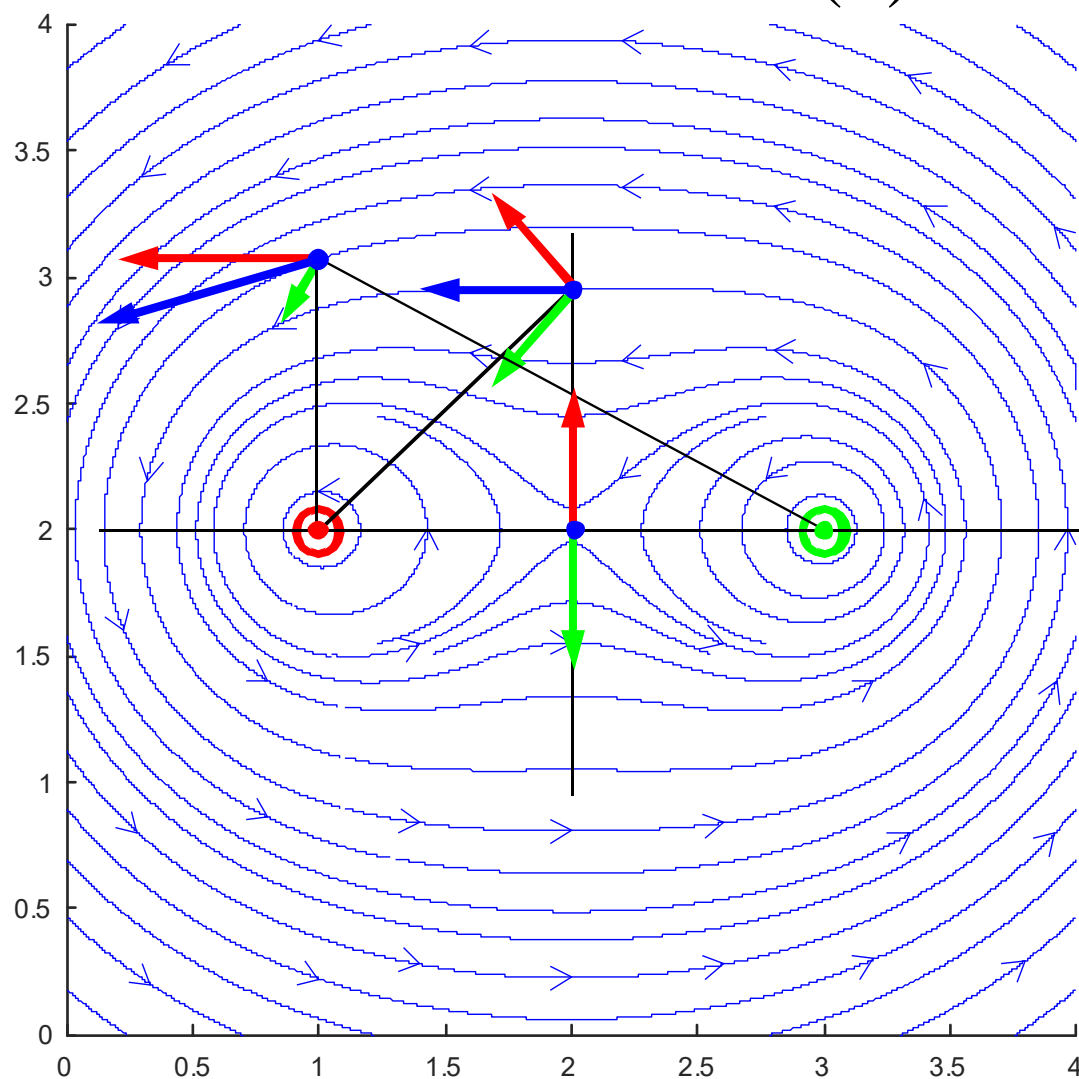
## Biot – Savart Law (5)

$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\varphi$$



## Biot – Savart Law (6)

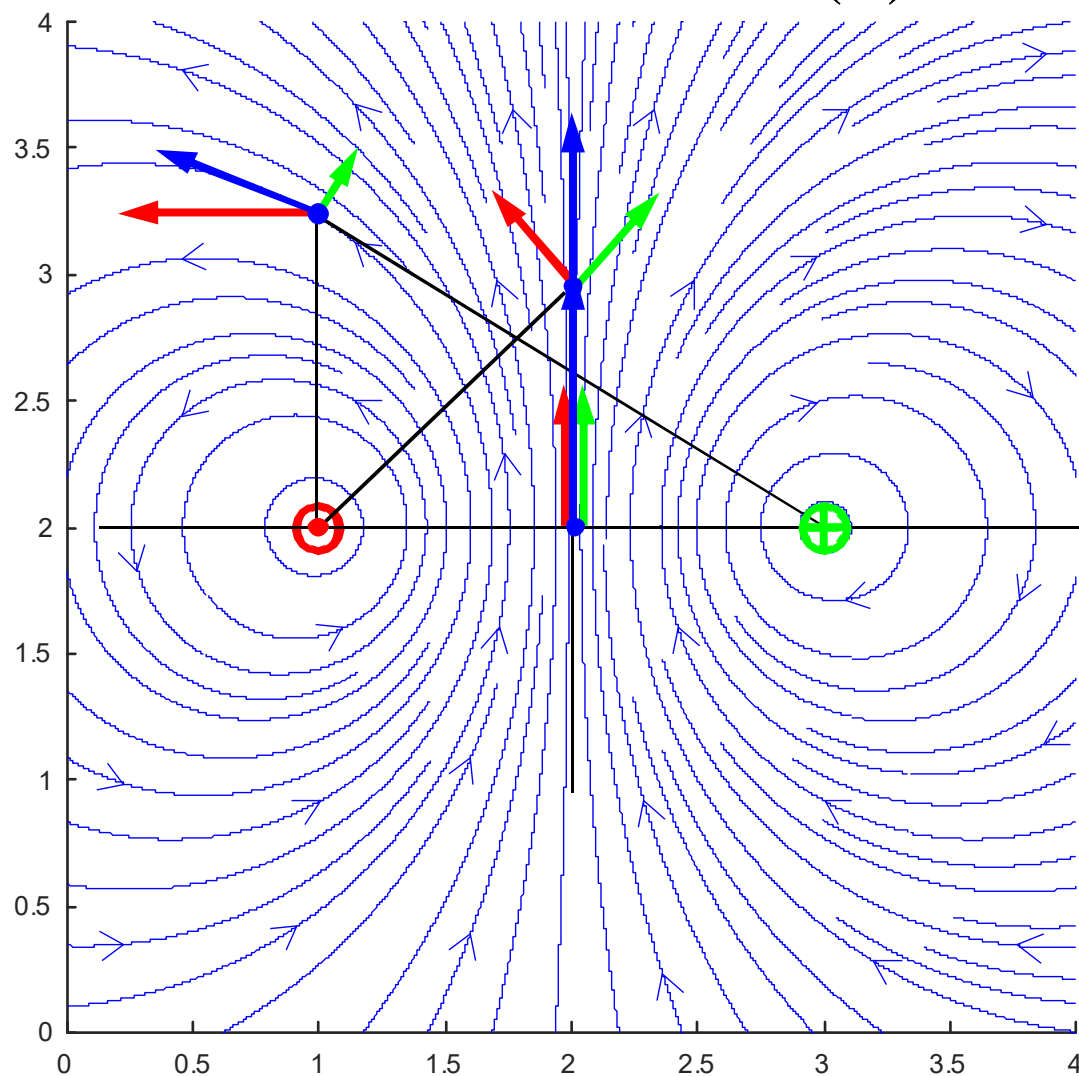
$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi$$



The Steady Magnetic Field - [sites.google.com/site/ncpdhbkhn](https://sites.google.com/site/ncpdhbkhn)

## Biot – Savart Law (7)

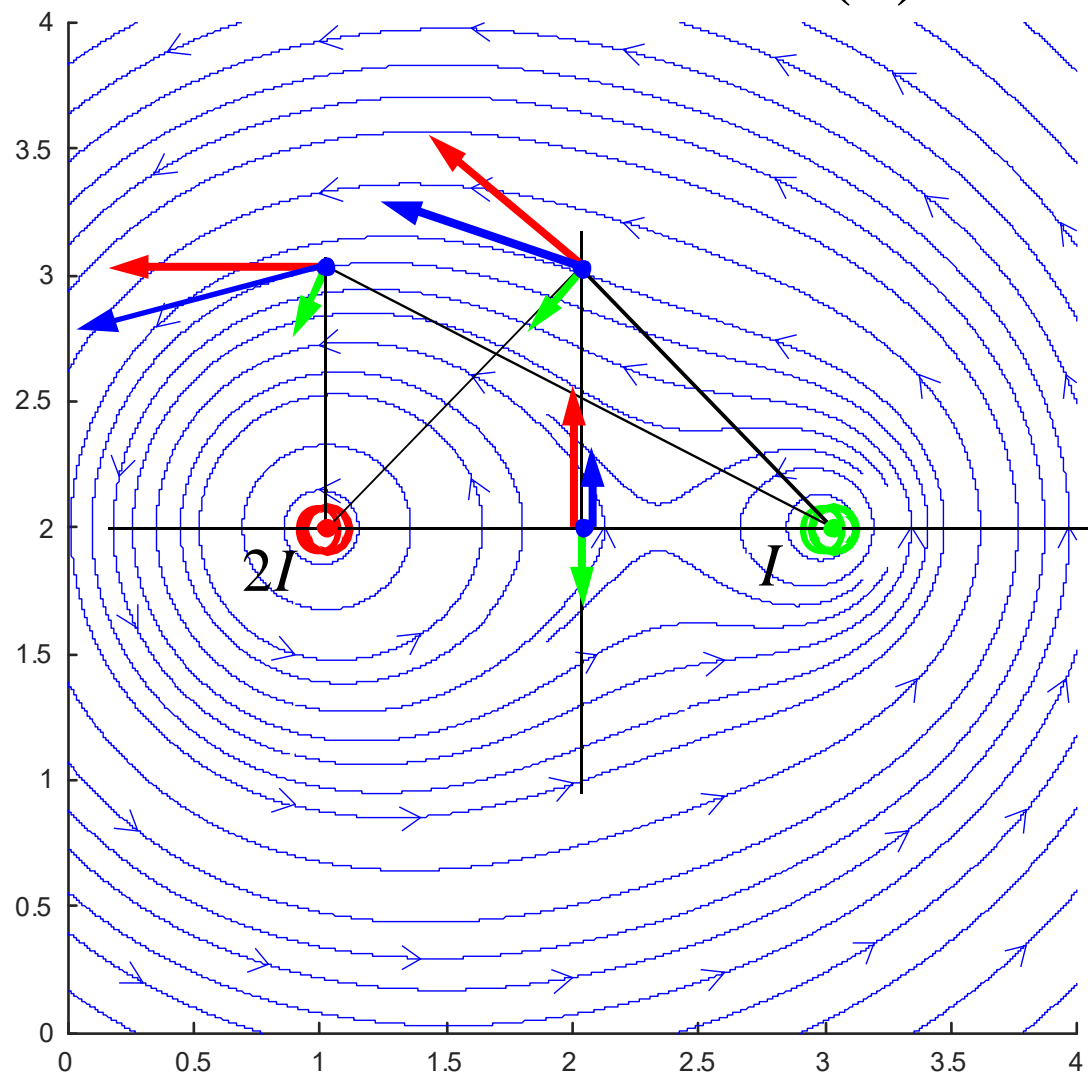
$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi$$



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## Biot – Savart Law (8)

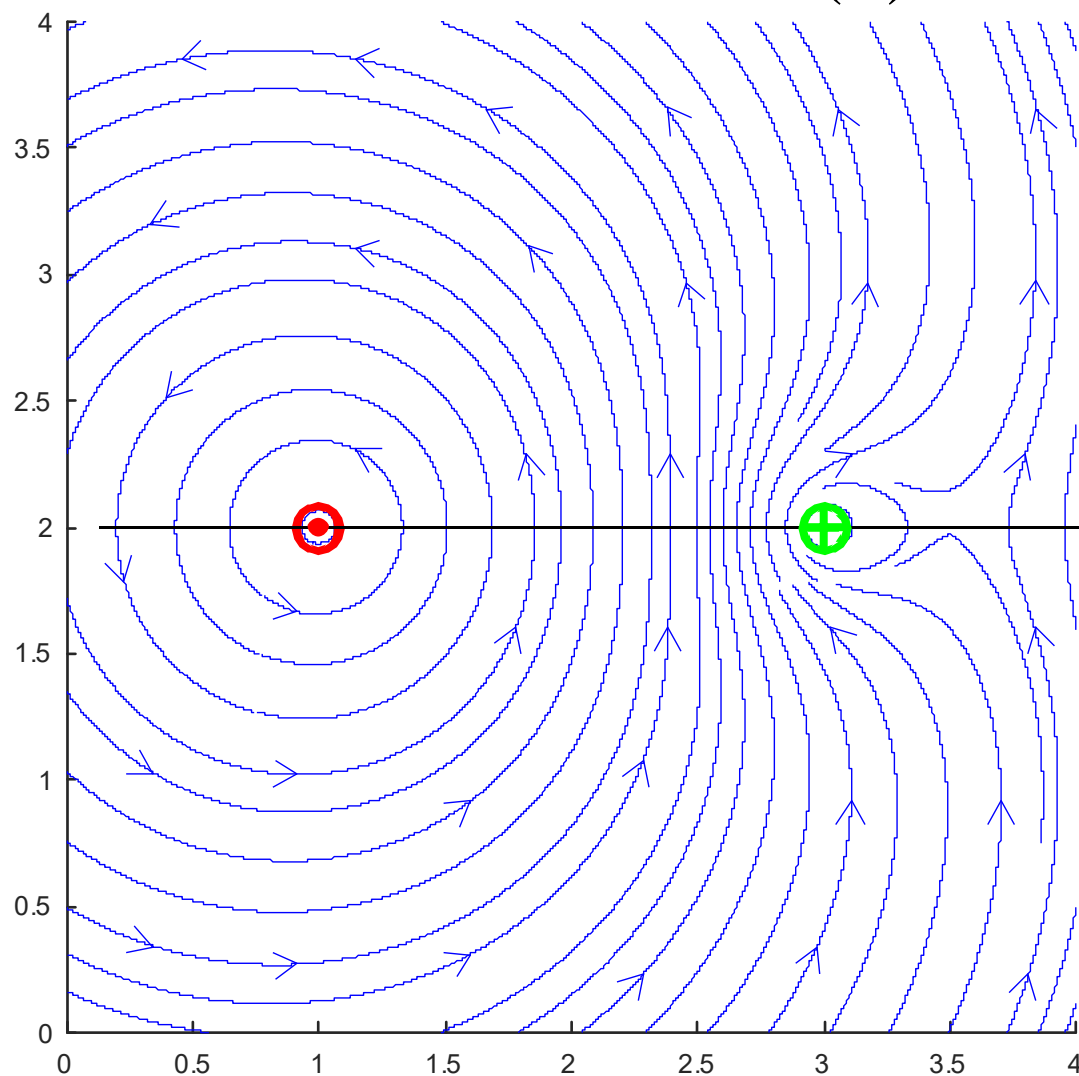
$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi$$



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## Biot – Savart Law (9)

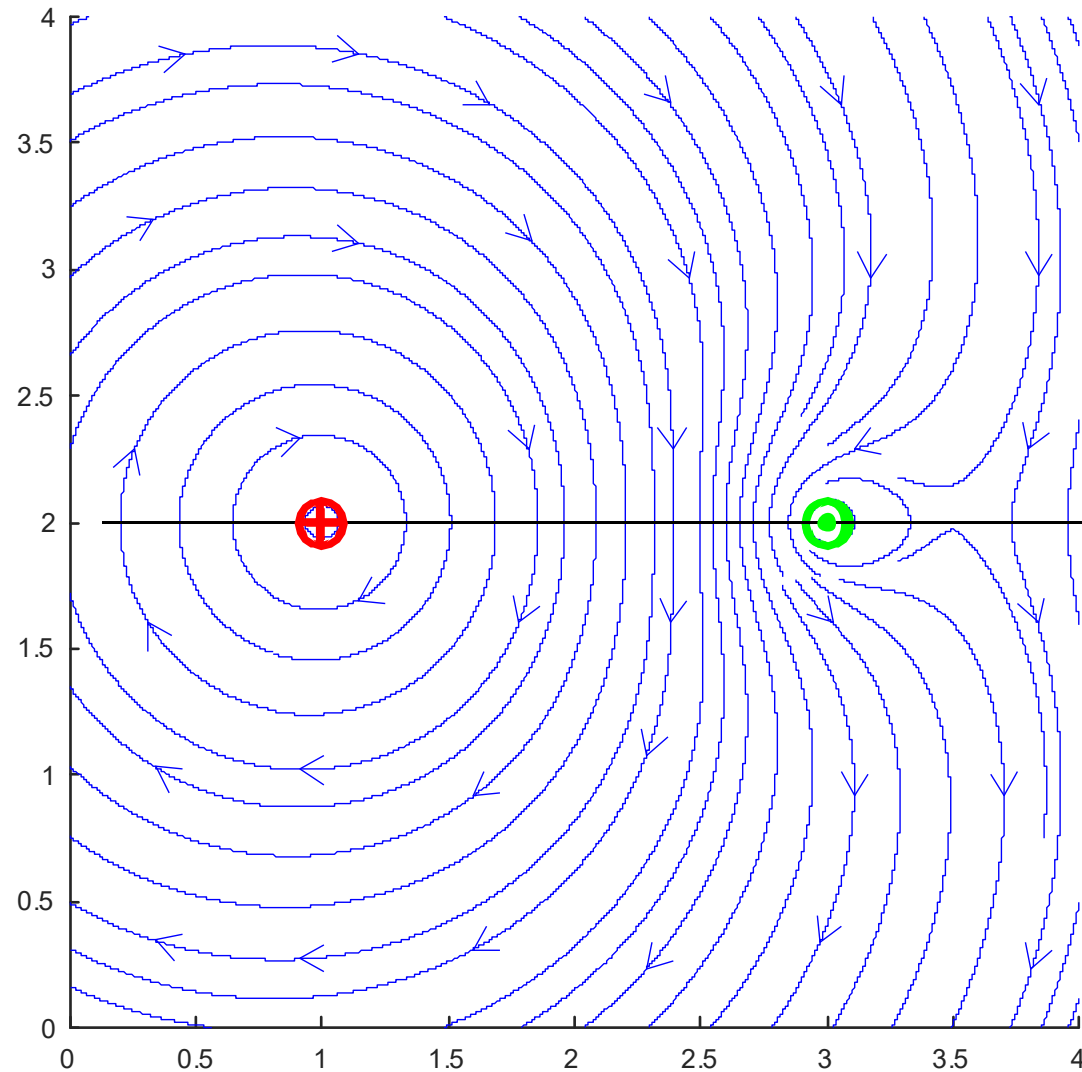
$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi$$



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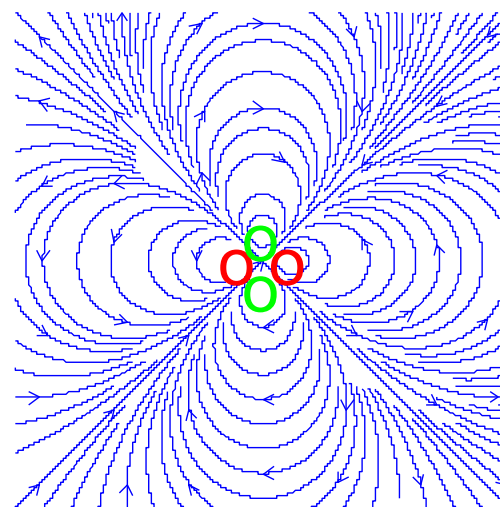
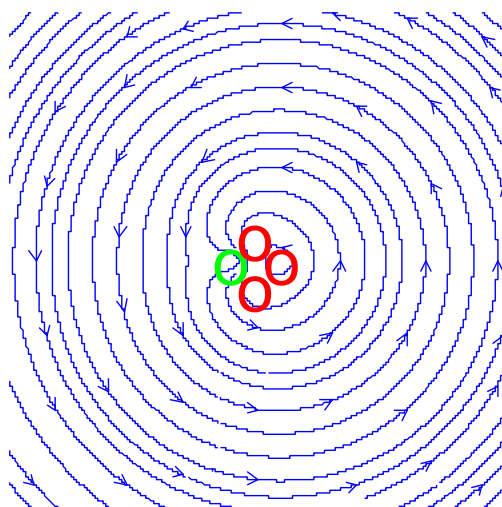
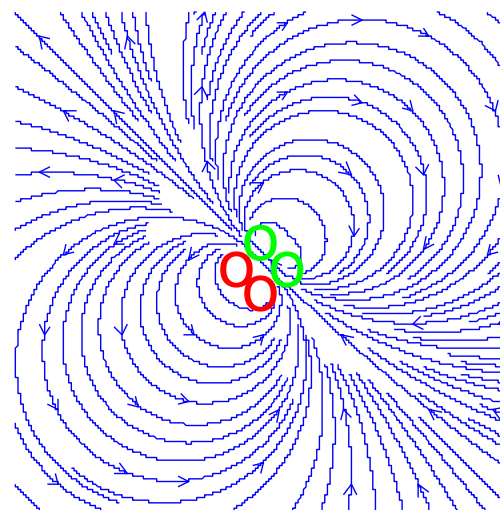
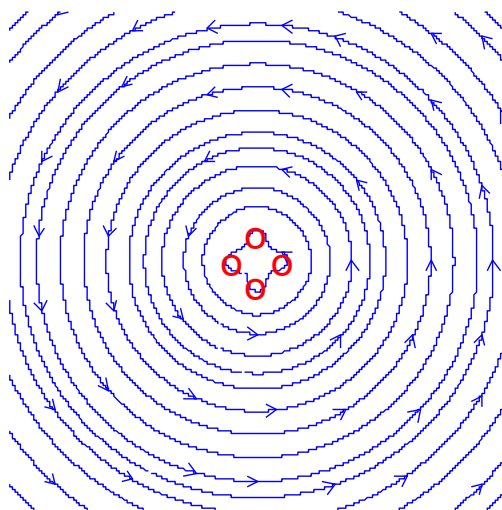
## Biot – Savart Law (10)

$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi$$



The Steady Magnetic Field - [sites.google.com/site/ncpdhbkhn](https://sites.google.com/site/ncpdhbkhn)

## Biot – Savart Law (11)





## Biot – Savart Law (12)

$$\mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2}$$

$$\mathbf{H} = \int_S \frac{\mathbf{K} \times \mathbf{a}_R dS}{4\pi R^2}$$

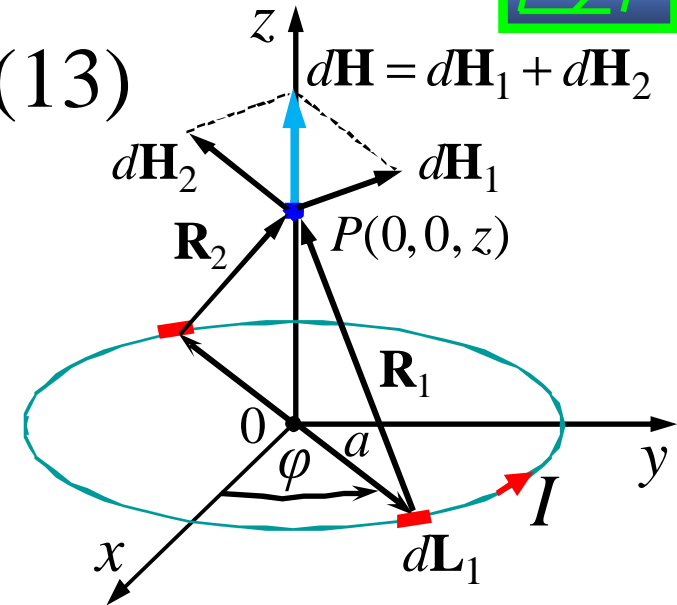
$$\mathbf{H} = \int_V \frac{\mathbf{J} \times \mathbf{a}_R dV}{4\pi R^2}$$



### Ex. 1

## Biot – Savart Law (13)

Given a circular hoop of radius  $a$  centered about the origin in the  $xy$  plane carries a constant current  $I$ . Find MFI at  $P$ ?



$$\left. \begin{aligned} d\mathbf{H}_1 &= \frac{Id\mathbf{L}_1 \times \mathbf{a}_{R1}}{4\pi R_1^2} \\ d\mathbf{L}_1 &= ad\varphi \mathbf{a}_\varphi \\ \mathbf{R}_1 &= -a\mathbf{a}_\rho + z\mathbf{a}_z \\ R_1 &= \sqrt{z^2 + a^2} \\ \mathbf{a}_{R1} &= \frac{-a\mathbf{a}_\rho + z\mathbf{a}_z}{\sqrt{z^2 + a^2}} \end{aligned} \right\}$$

$$\rightarrow \left. \begin{aligned} d\mathbf{H}_1 &= \frac{Iad\varphi}{4\pi(z^2 + a^2)^{3/2}} (a\mathbf{a}_z + z\mathbf{a}_\rho) \\ d\mathbf{H}_2 &= \frac{Iad\varphi}{4\pi(z^2 + a^2)^{3/2}} (a\mathbf{a}_z - z\mathbf{a}_\rho) \end{aligned} \right\}$$

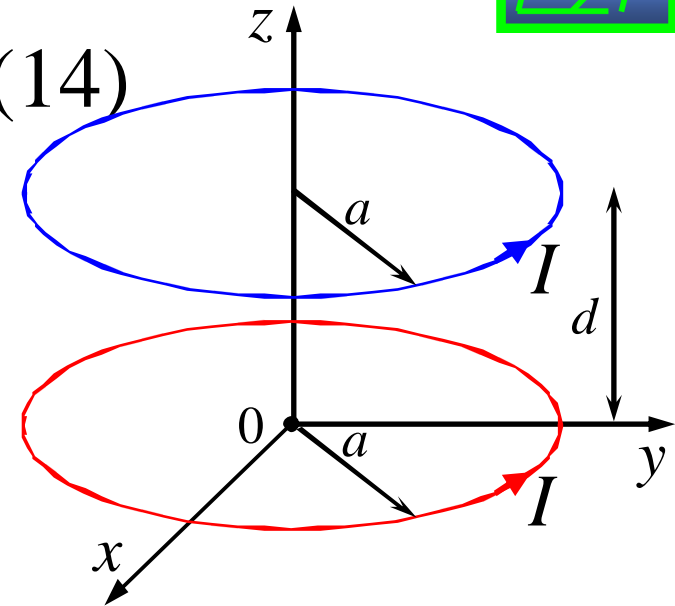
$$\rightarrow d\mathbf{H} = \frac{2Ia^2 d\varphi}{4\pi(z^2 + a^2)^{3/2}} \mathbf{a}_z \rightarrow \mathbf{H} = \int_0^\pi \frac{2Ia^2 d\varphi}{4\pi(z^2 + a^2)^{3/2}} \mathbf{a}_z = \frac{Ia^2}{2(z^2 + a^2)^{3/2}} \mathbf{a}_z$$

**Ex. 2**

**Biot – Savart Law (14)**

Find MFI on the  $z$  axis?

$$\left. \begin{aligned} H_{z, red} &= \frac{Ia^2}{2(z^2 + a^2)^{3/2}} \\ H_{z, blue} &= \frac{Ia^2}{2[(z-d)^2 + a^2]^{3/2}} \end{aligned} \right\}$$



$$\rightarrow H_z = \frac{Ia^2}{2} \left( \frac{1}{(z^2 + a^2)^{3/2}} + \frac{1}{[(z-d)^2 + a^2]^{3/2}} \right)$$

$$\left. \frac{\partial H_z}{\partial z} \right|_{z=d/2} = 0 \qquad \left. \frac{\partial^2 H_z}{\partial z^2} \right|_{z=d/2, d=a} = 0$$

**Ex. 3**

# Biot – Savart Law (15)

Find MFI on the  $z$  axis?

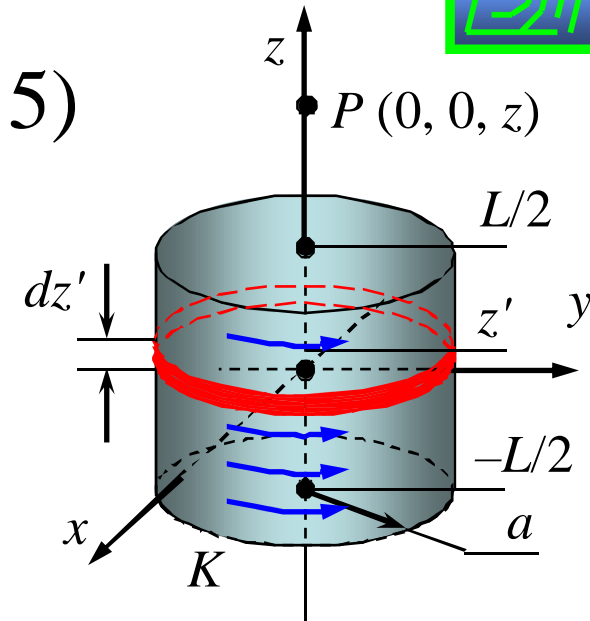
$$\left. \begin{aligned} \mathbf{H} &= \frac{Ia^2}{2(z^2 + a^2)^{3/2}} \mathbf{a}_z \\ z &= z - z', I = Kdz' \end{aligned} \right\}$$

$$\rightarrow dH_z = \frac{a^2 K dz'}{2[(z - z')^2 + a^2]^{3/2}}$$

$$\rightarrow H_z = \int_{z'=-L/2}^{L/2} \frac{a^2 K dz'}{2[(z - z')^2 + a^2]^{3/2}}$$

$$= \frac{K}{2} \left( \frac{-z + L/2}{\sqrt{(z - L/2)^2 + a^2}} + \frac{z + L/2}{\sqrt{(z + L/2)^2 + a^2}} \right)$$

$$\lim_{L \rightarrow \infty} H_z = K$$

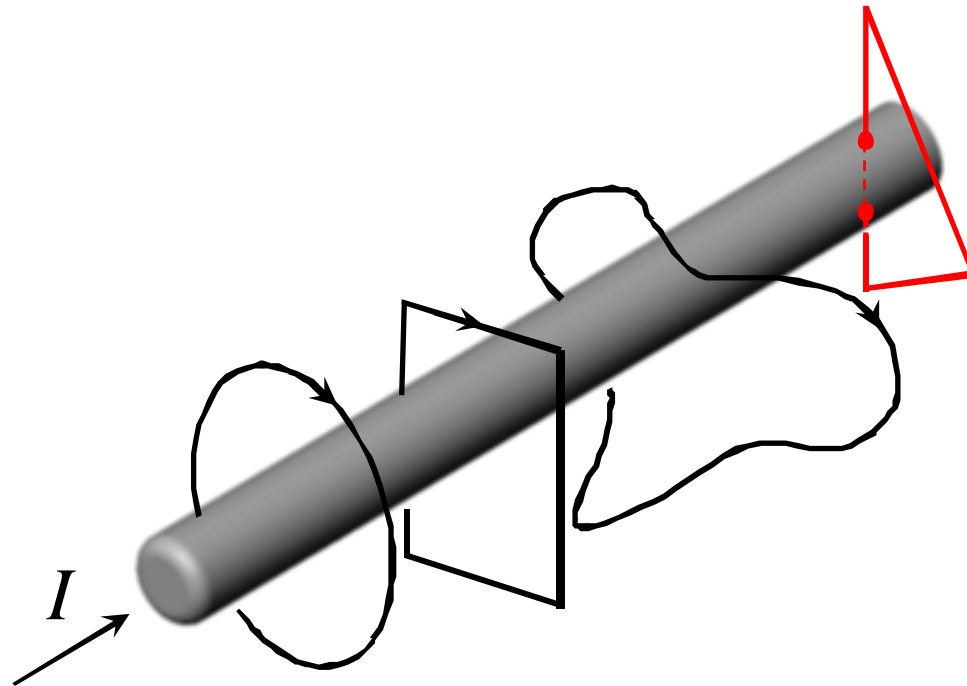


# The Steady Magnetic Field

1. Biot – Savart Law
- 2. Ampere's Circuital Law**
3. Curl
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7. Derivation of the Steady – Magnetic – Field Law

## Ampere's Circuital Law (1)

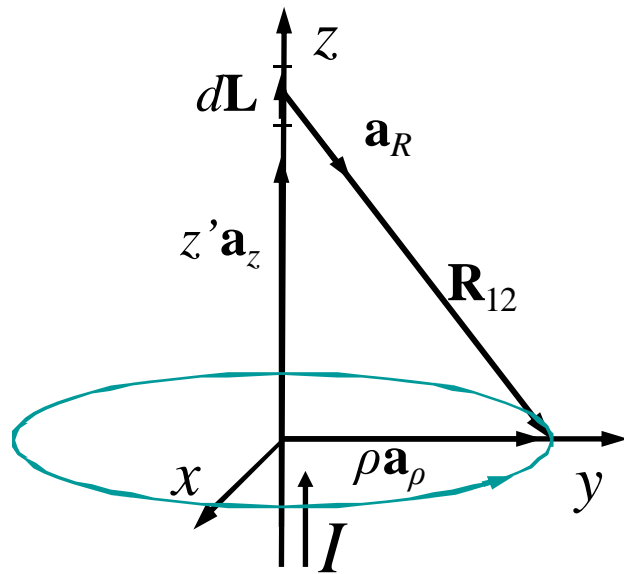
$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$



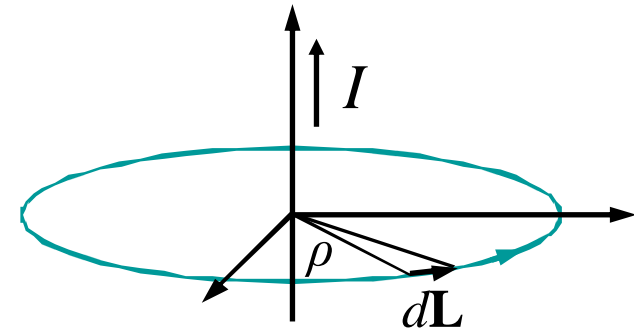
## Ampere's Circuital Law (2)

**Ex. 1**

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$



$$\mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi$$



$$\left. \begin{aligned} \mathbf{H} &= H_\phi \mathbf{a}_\phi \\ d\mathbf{L} &= \rho \tan(d\phi) \mathbf{a}_\phi \approx \rho d\phi \mathbf{a}_\phi \end{aligned} \right\}$$

$$\begin{aligned} \rightarrow \oint \mathbf{H} \cdot d\mathbf{L} &= \int_0^{2\pi} H_\phi \rho d\phi \\ &= H_\phi \rho \int_0^{2\pi} d\phi \end{aligned}$$

$$= H_\phi 2\pi\rho = I \rightarrow H_\phi = \frac{I}{2\pi\rho}$$

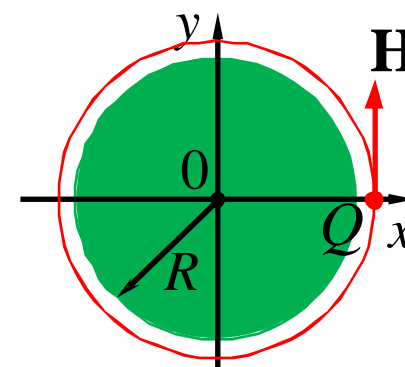
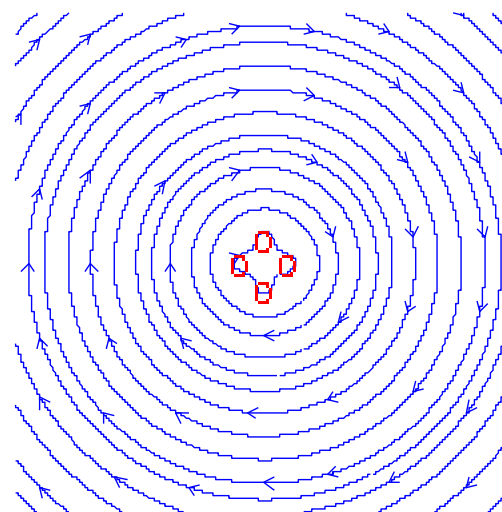
**Ex. 2**

## Ampere's Circuital Law (3)

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\rightarrow H(2\pi\rho) = J(\pi R^2)$$

$$\rightarrow \mathbf{H} = \frac{JR^2}{2\rho} \mathbf{a}_\phi, \quad \rho > R$$



**Ex. 2**

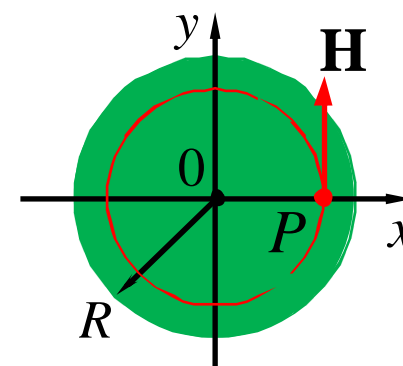
## Ampere's Circuital Law (4)

$$\mathbf{H} = \frac{JR^2}{2\rho} \mathbf{a}_\varphi, \quad \rho > R$$

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\rightarrow H(2\pi\rho) = J(\pi\rho^2)$$

$$\rightarrow \mathbf{H} = \frac{J\rho}{2} \mathbf{a}_\varphi, \quad \rho < R$$





## Ampere's Circuital Law (5)

### Ex. 3

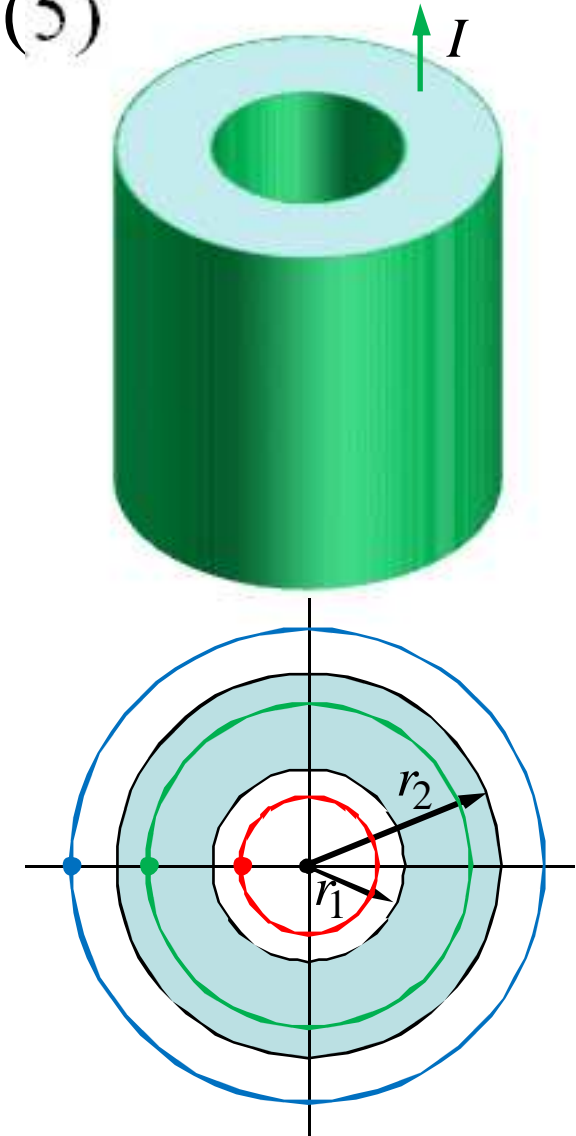
$$\oint \mathbf{H}_r \cdot d\mathbf{L} = I_r = 0 \quad \rightarrow H_r = 0$$

$$\oint \mathbf{H}_b \cdot d\mathbf{L} = I_b = I$$

$$\rightarrow H_b(2\pi r_b) = I \quad \rightarrow H_b = \frac{I}{2\pi r_b} \quad \rightarrow \mathbf{H}_b = \frac{I}{2\pi r_b} \mathbf{a}_\varphi$$

$$\left. \begin{aligned} \oint \mathbf{H}_g \cdot d\mathbf{L} &= I_g = JS_g \\ J &= \frac{I}{\pi r_2^2 - \pi r_1^2} \\ S_g &= \pi r_g^2 - \pi r_1^2 \end{aligned} \right\} \rightarrow I_g = I \frac{r_g^2 - r_1^2}{r_2^2 - r_1^2}$$

$$\rightarrow H_g(2\pi r_g) = I \frac{r_g^2 - r_1^2}{r_2^2 - r_1^2} \quad \rightarrow \mathbf{H}_g = \frac{I}{2\pi r_g} \cdot \frac{r_g^2 - r_1^2}{r_2^2 - r_1^2} \mathbf{a}_\varphi$$



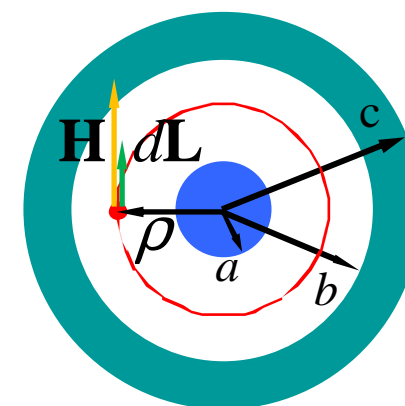
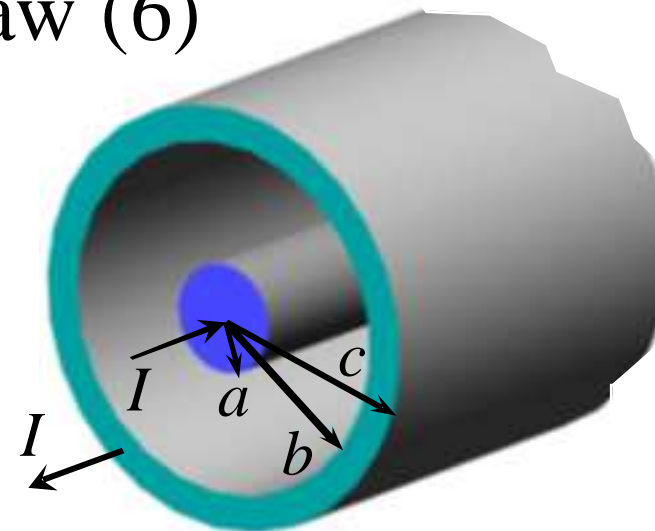
**Ex. 4**

## Ampere's Circuital Law (6)

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\rightarrow H(2\pi\rho) = I$$

$$\rightarrow H(\rho) = \frac{I}{2\pi\rho}, \quad a < \rho < b$$



**Ex. 4**

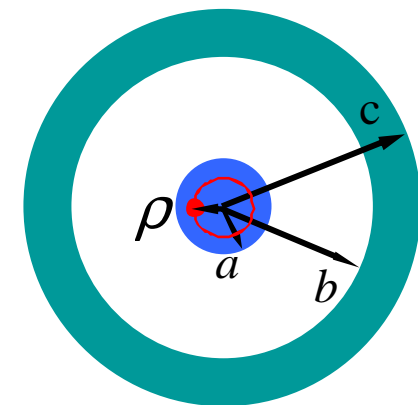
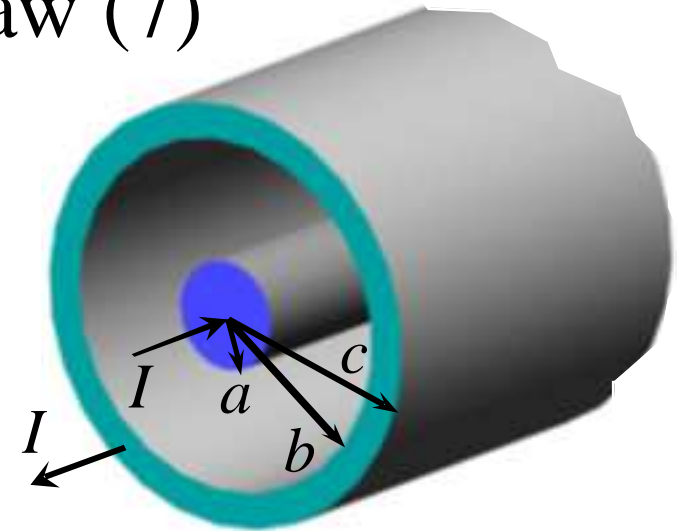
# Ampere's Circuital Law (7)

$$\oint \mathbf{H} \cdot d\mathbf{L} = I'$$

$$\left. \begin{aligned} \rightarrow H(2\pi\rho) &= JS' \\ J &= \frac{I}{\pi a^2} \\ S' &= \pi\rho^2 \end{aligned} \right\}$$

$$\rightarrow H(2\pi\rho) = \frac{I}{\pi a^2} \pi\rho^2$$

$$\rightarrow H = \frac{I}{2\pi a^2} \rho, \quad \rho < a$$



**Ex. 4**

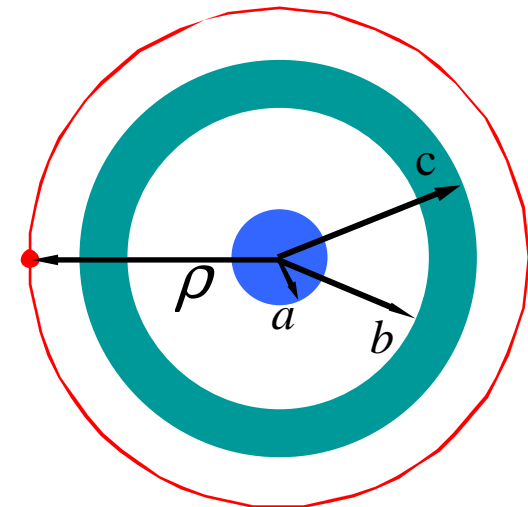
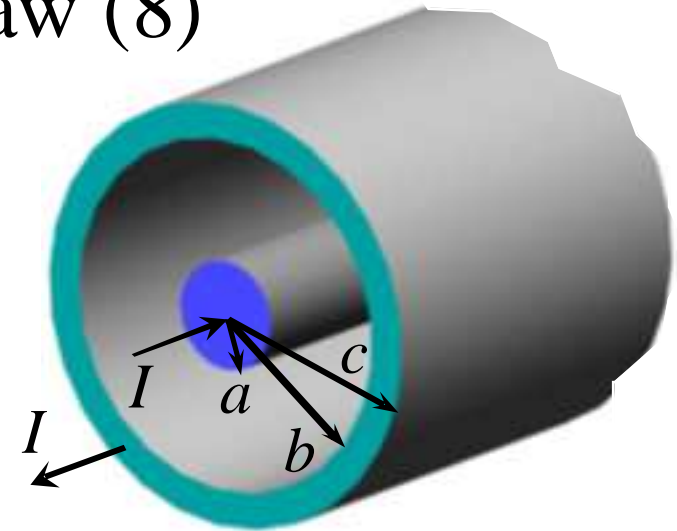
## Ampere's Circuital Law (8)

$$\oint \mathbf{H} \cdot d\mathbf{L} = \sum I$$

$$\sum I = I_{\text{inner conductor}} + I_{\text{outer conductor}} = I - I = 0$$

$$\rightarrow H(2\pi\rho) = 0$$

$$\rightarrow H(\rho) = 0, \quad \rho > c$$



## Ampere's Circuital Law (9)

**Ex. 4**

$$\oint \mathbf{H} \cdot d\mathbf{L} = \sum I$$

$$\sum I = I_{\text{inner conductor}} + I_{\text{partial outer conductor}}$$

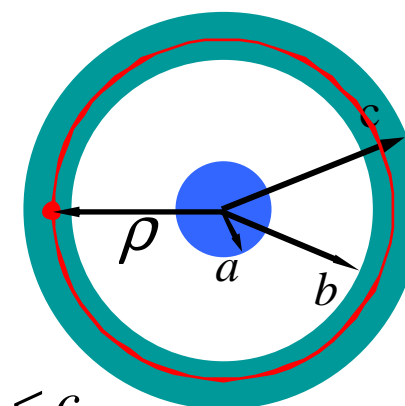
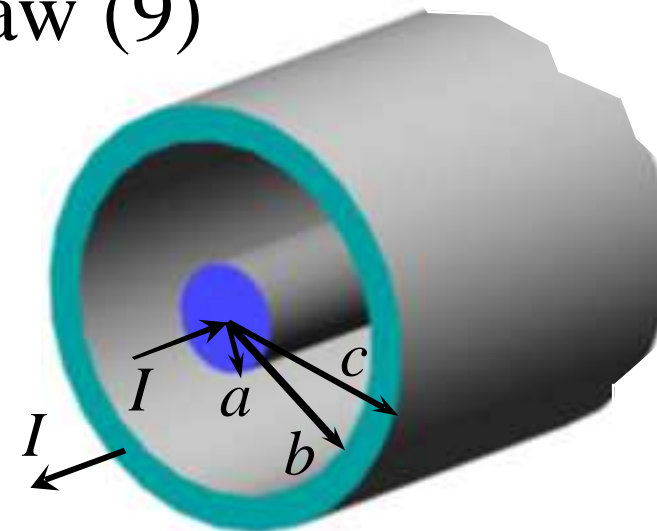
$$I_{\text{partial outer conductor}} = JS''$$

$$J = \frac{I}{\pi c^2 - \pi b^2}$$

$$S'' = \pi \rho^2 - \pi b^2$$

$$\rightarrow I_{\text{partial outer conductor}} = \frac{I \pi (\rho^2 - b^2)}{\pi (c^2 - b^2)}$$

$$\rightarrow H(2\pi\rho) = I \frac{c^2 - \rho^2}{c^2 - b^2} \rightarrow H(\rho) = \frac{I}{2\pi\rho} \cdot \frac{c^2 - \rho^2}{c^2 - b^2}, \quad b < \rho < c$$

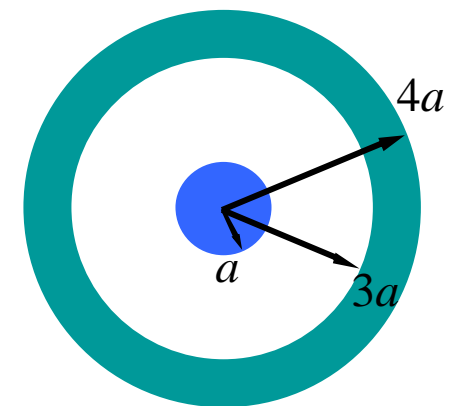
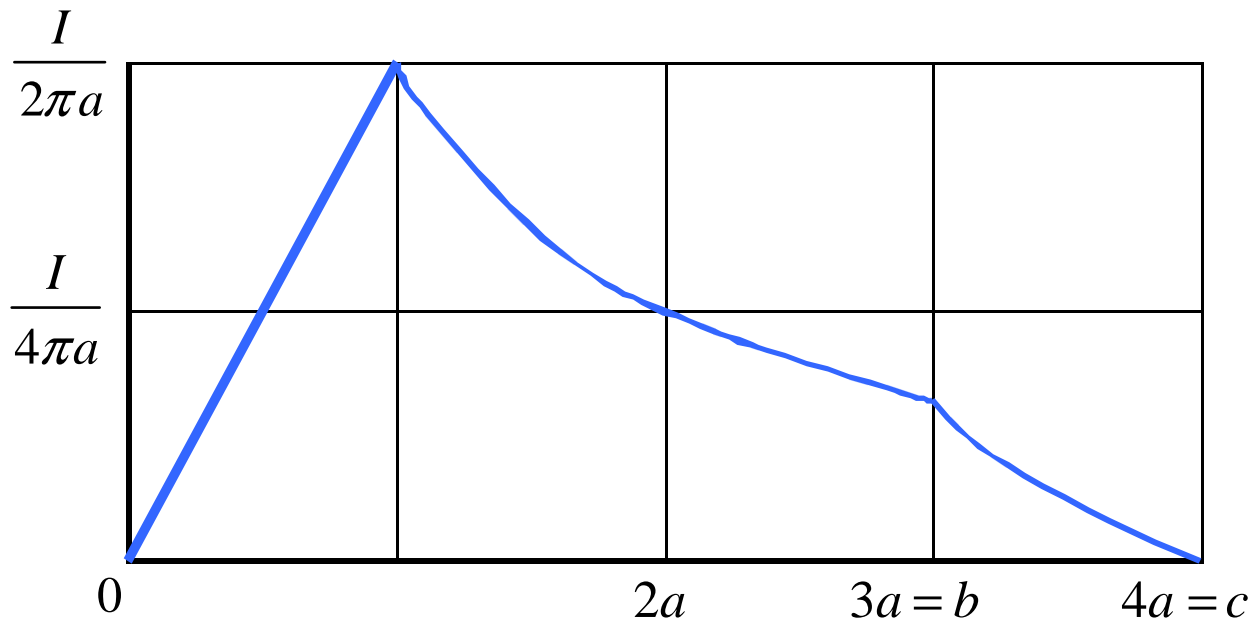
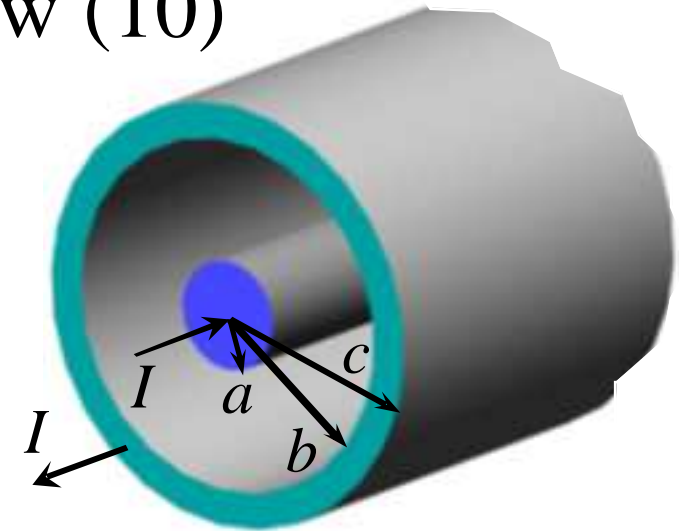


## Ampere's Circuital Law (10)

**Ex. 4**

$$H_{\varphi} = I \frac{\rho}{2\pi a^2} \quad (\rho < a); H_{\varphi} = \frac{I}{2\pi\rho} \quad (a < \rho < b)$$

$$H_{\varphi} = \frac{I}{2\pi\rho} \frac{c^2 - \rho^2}{c^2 - b^2} \quad (b < \rho < c); H_{\varphi} = 0 \quad (\rho > c)$$



## Ampere's Circuital Law (11)

### Ex. 5

$$\mathbf{H} = \mathbf{H}_1 + \mathbf{H}_2$$

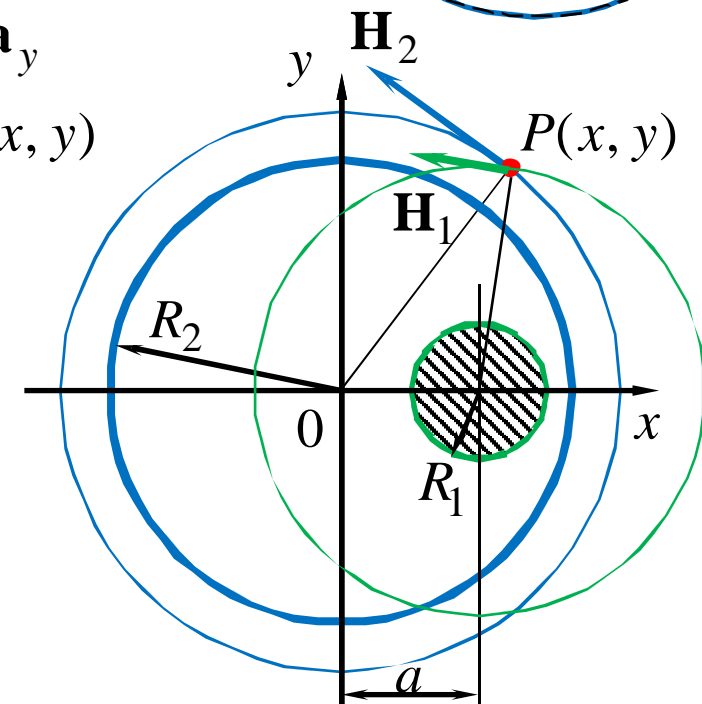
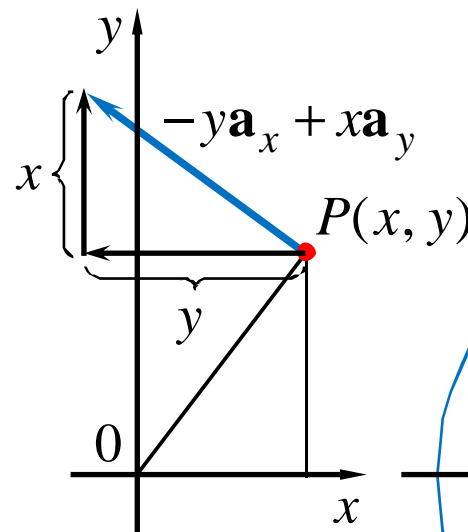
$$\oint \mathbf{H}_2 \cdot d\mathbf{L} = I_2$$

$$\rightarrow H_2(2\pi\sqrt{x^2 + y^2}) = I_2$$

$$\rightarrow H_2 = \frac{I_2}{2\pi\sqrt{x^2 + y^2}}$$

$$\rightarrow \mathbf{H}_2 = \frac{I_2}{2\pi\sqrt{x^2 + y^2}} \cdot \frac{-y\mathbf{a}_x + x\mathbf{a}_y}{\sqrt{x^2 + y^2}}$$

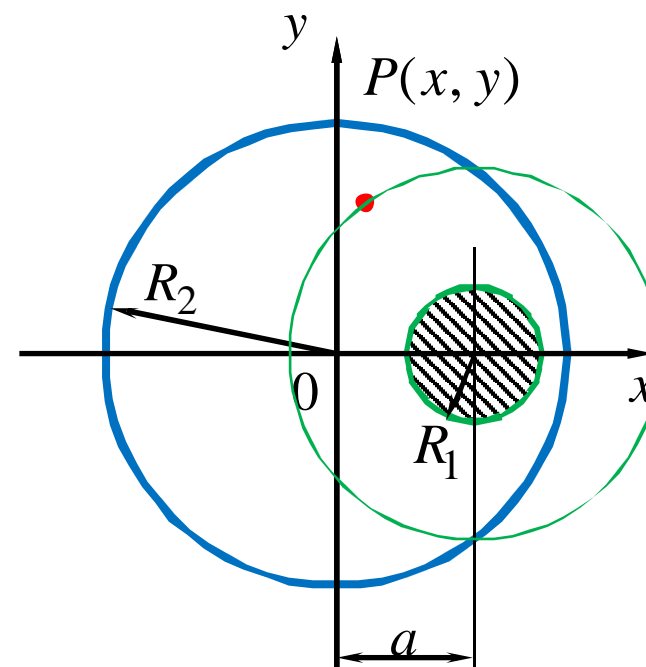
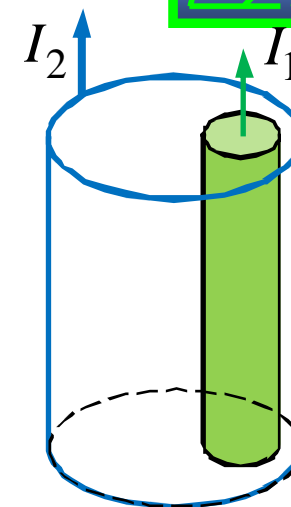
$$\mathbf{H}_1 = \frac{I_1}{2\pi[(x-a)^2 + y^2]} [-y\mathbf{a}_x + (x-a)\mathbf{a}_y]$$





Ex. 5

# Ampere's Circuital Law (12)





## Ampere's Circuital Law (13)

**Ex. 6**

$$\oint \mathbf{H}_{Pg} \cdot d\mathbf{L} = I_{Pb}$$

$$\rightarrow H_{Pg}(2\pi x_P) = J(\pi x_P^2)$$

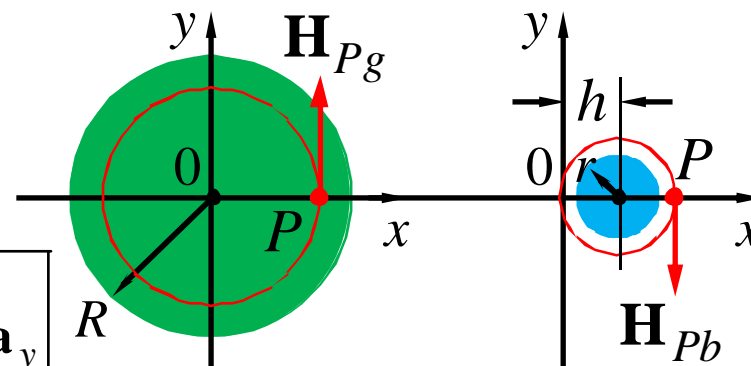
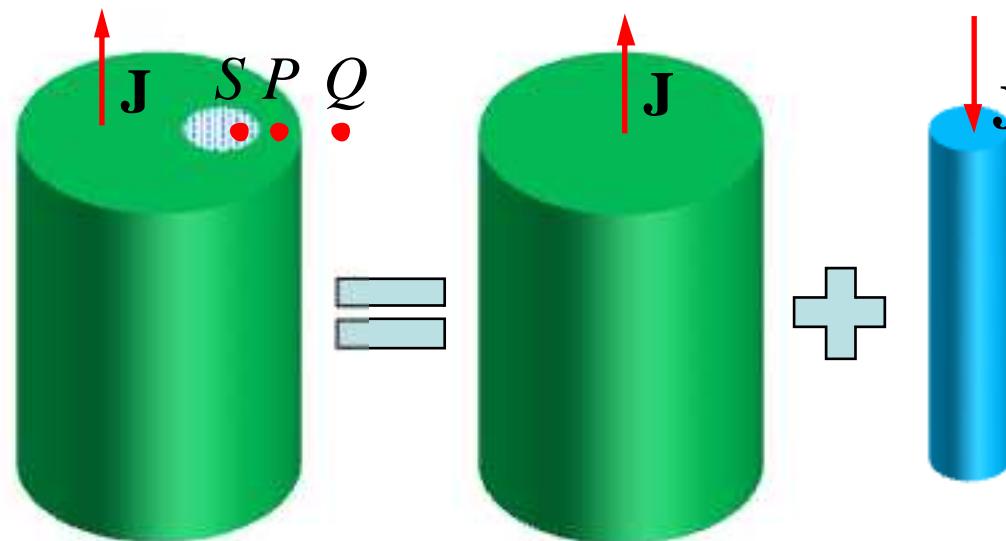
$$\rightarrow \mathbf{H}_{Pg} = \frac{Jx_P}{2} \mathbf{a}_y$$

$$\oint \mathbf{H}_{Pb} \cdot d\mathbf{L} = I_{Pb}$$

$$\rightarrow H_{Pb}[2\pi(x_P - h)] = J(\pi r^2)$$

$$\rightarrow \mathbf{H}_{Pb} = -\frac{Jr^2}{2(x_P - h)} \mathbf{a}_y$$

$$\rightarrow \mathbf{H}_P = \mathbf{H}_{Pg} + \mathbf{H}_{Pb} = \left[ \frac{J}{2} \left( x_P - \frac{r^2}{x_P - h} \right) \right] \mathbf{a}_y$$



## Ampere's Circuital Law (14)

**Ex. 6**

$$\oint \mathbf{H}_{Qg} \cdot d\mathbf{L} = I_{Qb}$$

$$\rightarrow H_{Qg}(2\pi x_Q) = J(\pi R^2)$$

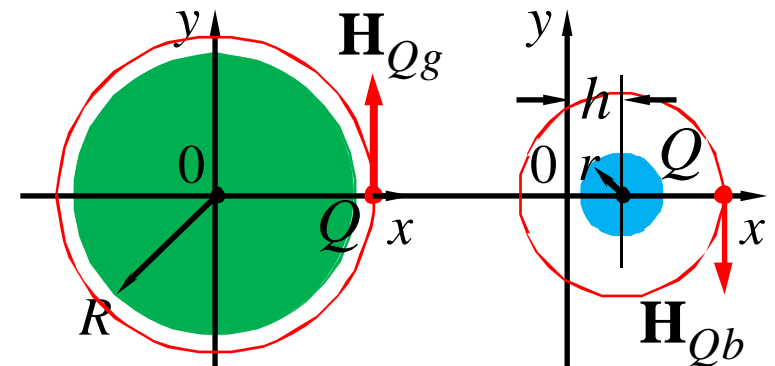
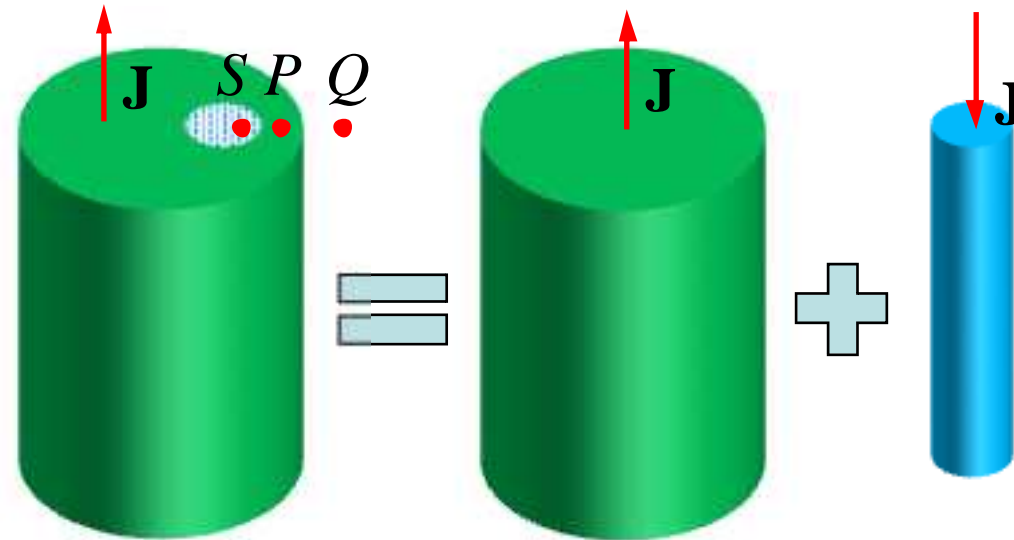
$$\rightarrow \mathbf{H}_{Qg} = \frac{JR^2}{2x_Q} \mathbf{a}_y$$

$$\oint \mathbf{H}_{Qb} \cdot d\mathbf{L} = I_{Qb}$$

$$\rightarrow H_{Qb}[2\pi(x_Q - h)] = J(\pi r^2)$$

$$\rightarrow \mathbf{H}_{Qb} = -\frac{Jr^2}{2(x_Q - h)} \mathbf{a}_y$$

$$\rightarrow \mathbf{H}_P = \mathbf{H}_{Pg} + \mathbf{H}_{Pb} = \left[ \frac{J}{2} \left( \frac{R^2}{x_Q} - \frac{r^2}{x_Q - h} \right) \right] \mathbf{a}_y$$



## Ampere's Circuital Law (15)

**Ex. 7**

$$\oint_{abcd} \mathbf{H} \cdot d\mathbf{L} = I = K_y L$$

$$\rightarrow \int_a^b \mathbf{H} \cdot d\mathbf{L} + \int_b^c \mathbf{H} \cdot d\mathbf{L} + \int_c^d \mathbf{H} \cdot d\mathbf{L} + \int_d^a \mathbf{H} \cdot d\mathbf{L} = KL$$

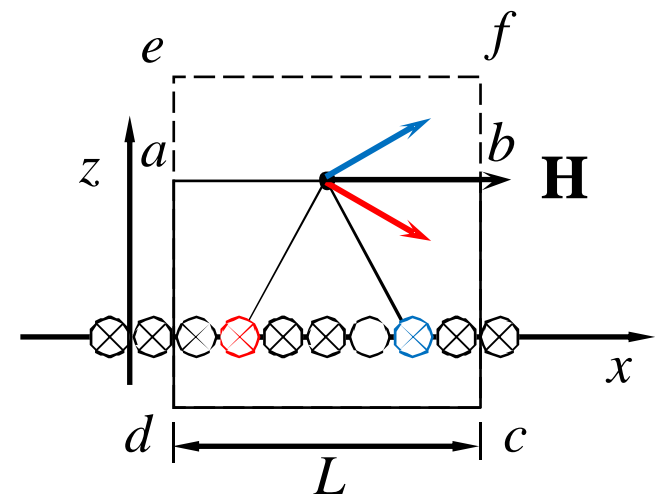
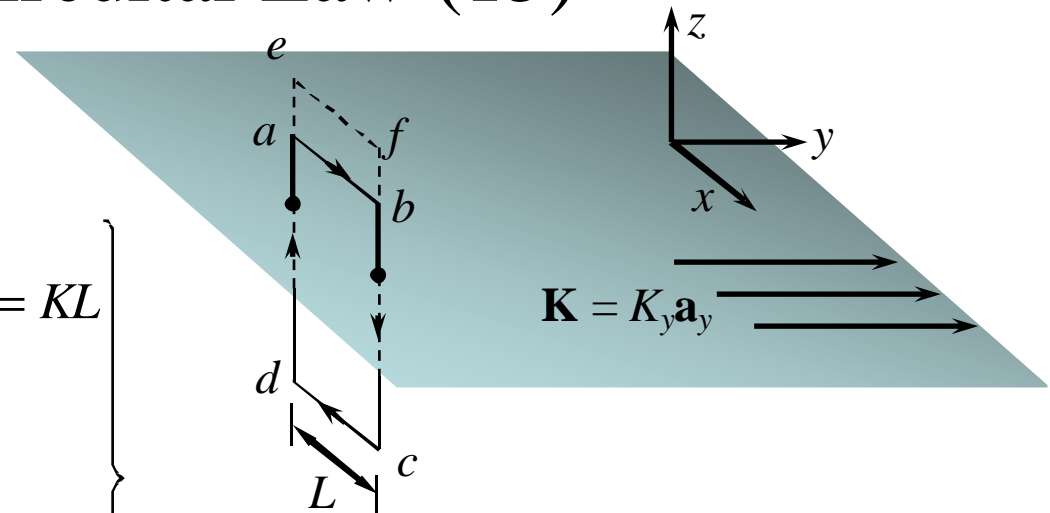
$$\int_b^c \mathbf{H} \cdot d\mathbf{L} = 0, \quad \int_d^a \mathbf{H} \cdot d\mathbf{L} = 0$$

$$\int_a^b \mathbf{H} \cdot d\mathbf{L} = H_{ab}L, \quad \int_c^d \mathbf{H} \cdot d\mathbf{L} = -H_{cd}L$$

$$\rightarrow H_{ab}L - H_{cd}L = K_y L$$

$$\rightarrow H_{ab} - H_{cd} = K_y$$

$$\oint_{efcd} \mathbf{H} \cdot d\mathbf{L} = I = K_y L \quad \rightarrow H_{ef} - H_{cd} = K_y$$



## Ampere's Circuital Law (16)

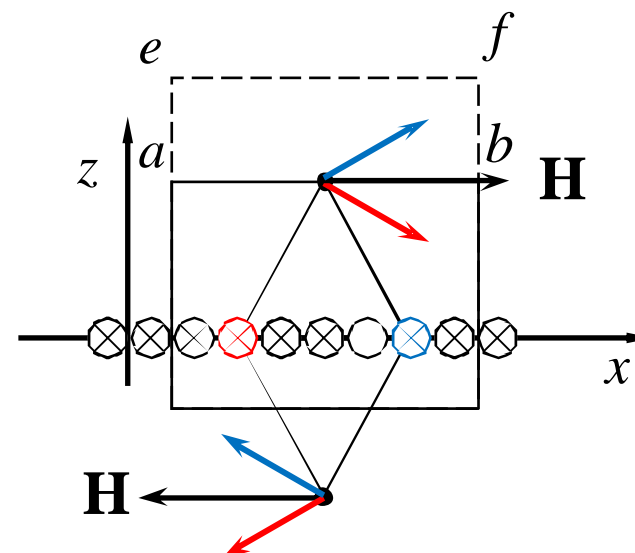
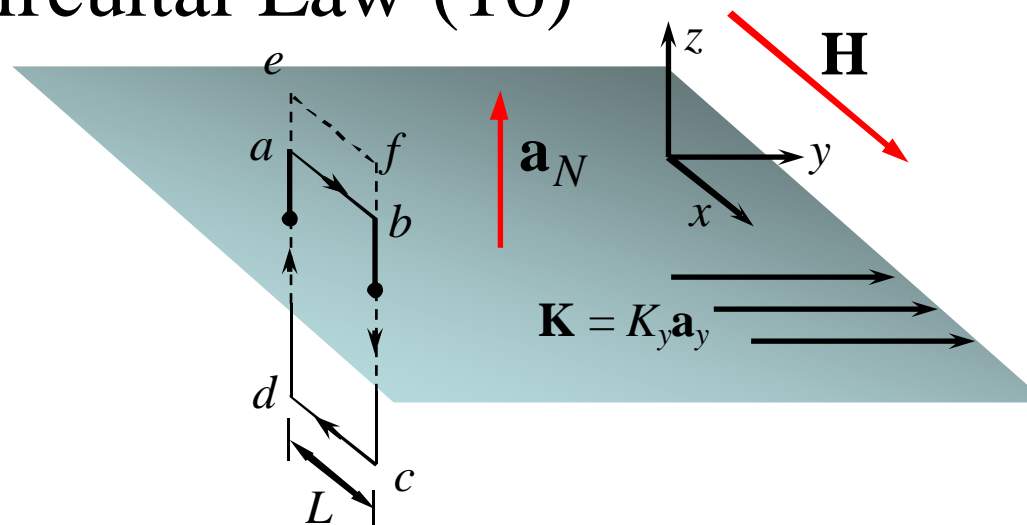
**Ex. 7**

$$\left. \begin{aligned} H_{ab} - H_{cd} &= K_y \\ H_{ef} - H_{cd} &= K_y \end{aligned} \right\}$$

$$\rightarrow H_{ab} = H_{ef}$$

$$\rightarrow \begin{cases} H_x = \frac{1}{2} K_y & (z > 0) \\ H_x = -\frac{1}{2} K_y & (z < 0) \end{cases}$$

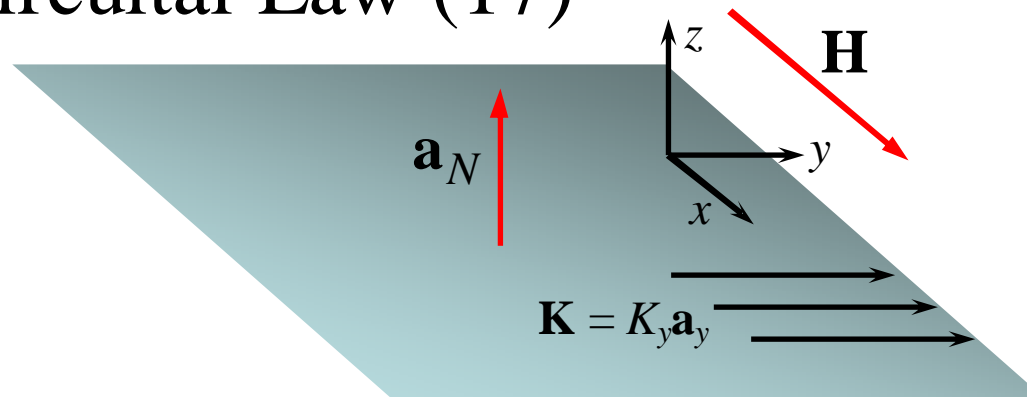
$$\rightarrow \mathbf{H} = \frac{1}{2} \mathbf{K} \times \mathbf{a}_N$$



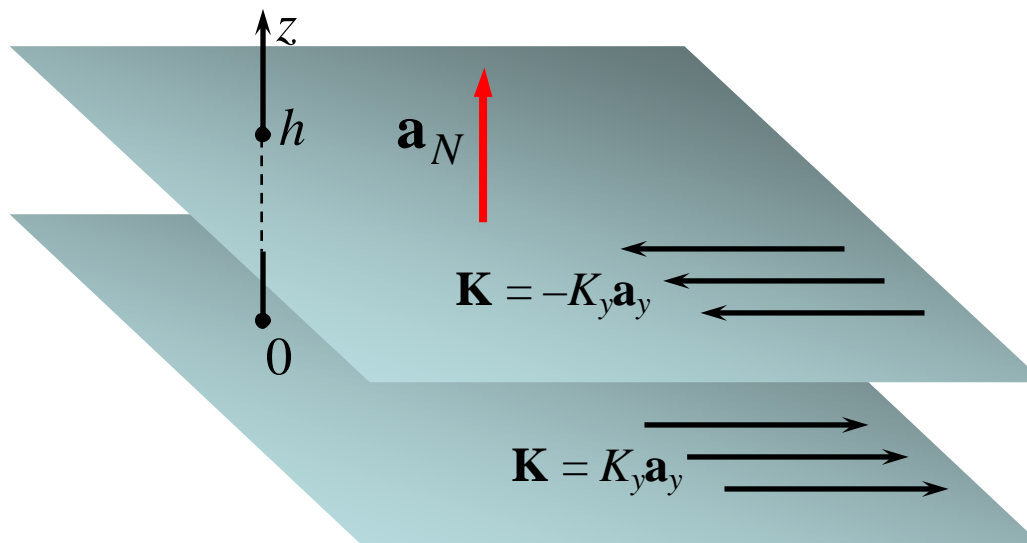
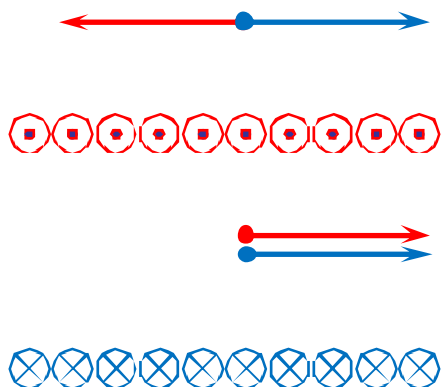
**Ex. 8**

## Ampere's Circuital Law (17)

$$\mathbf{H} = \frac{1}{2} \mathbf{K} \times \mathbf{a}_N$$



$$\begin{cases} \mathbf{H} = \mathbf{K} \times \mathbf{a}_N & (0 < z < h) \\ \mathbf{H} = 0 & (z < 0, z > h) \end{cases}$$



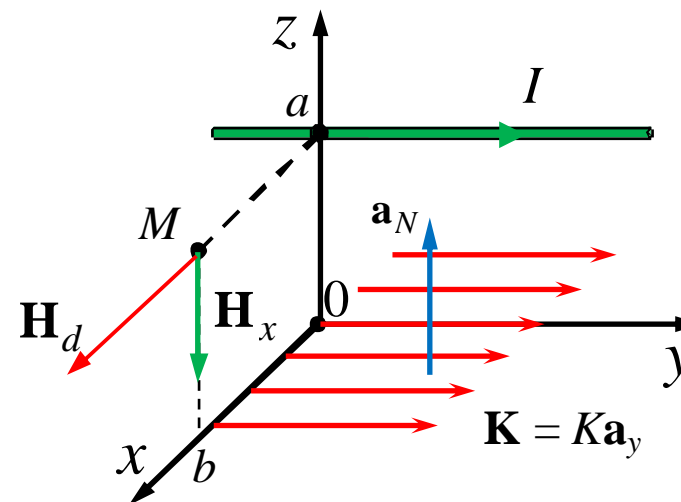
## Ampere's Circuital Law (18)

**Ex. 9**

$$\mathbf{H}_x = \frac{I}{2\pi\rho} \mathbf{a}_\rho = \frac{I}{2\pi b} (-\mathbf{a}_z)$$

$$\mathbf{H}_d = \frac{1}{2} \mathbf{K} \times \mathbf{a}_N = \frac{1}{2} (K\mathbf{a}_y) \times \mathbf{a}_z = \frac{K}{2} \mathbf{a}_x$$

$$\mathbf{H}_M = \mathbf{H}_d + \mathbf{H}_x = \frac{K}{2} \mathbf{a}_x - \frac{I}{2\pi b} \mathbf{a}_z$$



## Ampere's Circuital Law (19)

### Ex. 10

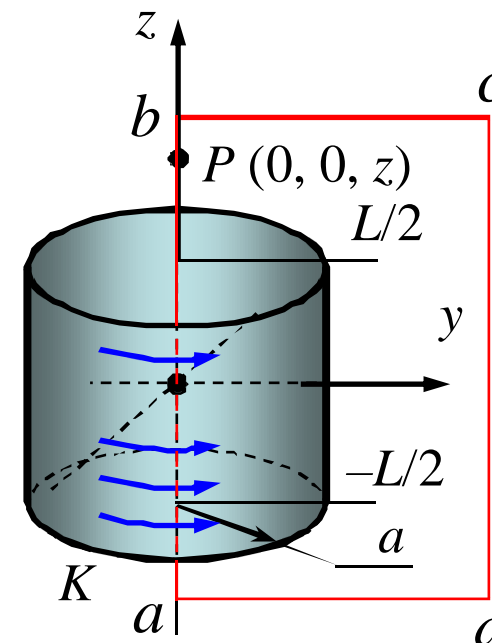
A hollow cylinder with a surface current density of  $K$ . Find MFI on the  $z$ -axis?

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\rightarrow \int_a^b \mathbf{H} \cdot d\mathbf{L} + \int_b^c \mathbf{H} \cdot d\mathbf{L} + \int_c^d \mathbf{H} \cdot d\mathbf{L} + \int_d^a \mathbf{H} \cdot d\mathbf{L} = KL$$

$$\rightarrow H_{ab}L = KL$$

$$\rightarrow H_{ab} = K$$



**Ex. 11**

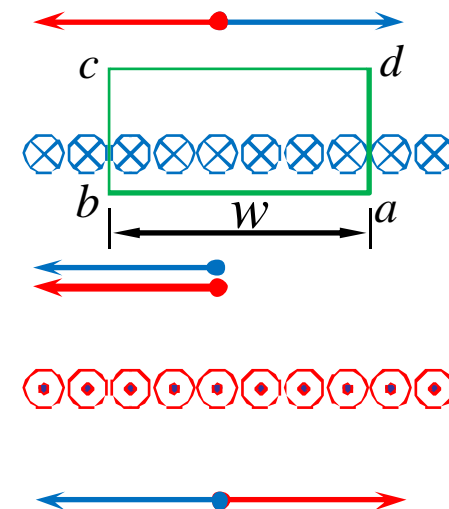
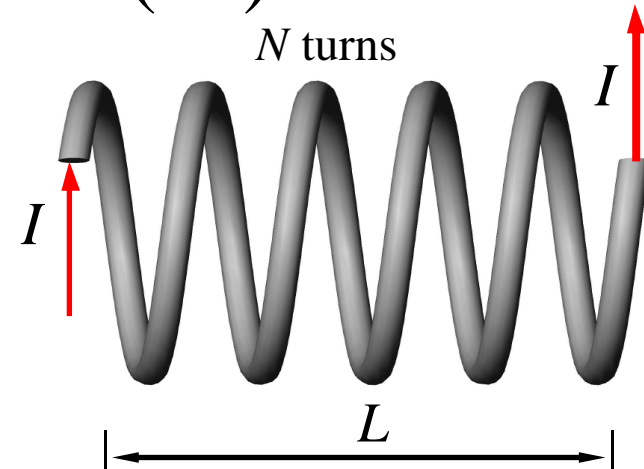
## Ampere's Circuital Law (20)

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\rightarrow \int_a^b \mathbf{H} \cdot d\mathbf{L} + \int_b^c \mathbf{H} \cdot d\mathbf{L} + \int_c^d \mathbf{H} \cdot d\mathbf{L} + \int_d^a \mathbf{H} \cdot d\mathbf{L} = K_w$$

$$\rightarrow H_{ab} w = I \frac{N}{L} w$$

$$\rightarrow H_{ab} = \frac{NI}{L}$$





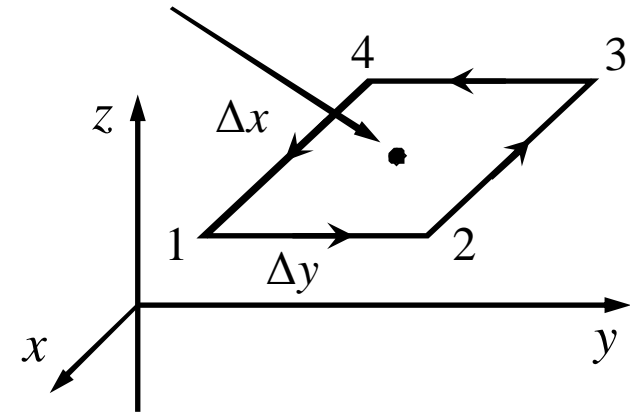
# The Steady Magnetic Field

1. Biot – Savart Law
2. Ampere's Circuital Law
- 3. Curl**
4. Stokes' Theorem
5. Magnetic Flux & Magnetic Flux Density
6. Magnetic Potential
7. Derivation of the Steady – Magnetic – Field Law

Curl (1)

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\mathbf{H} = \mathbf{H}_0 = H_{x0}\mathbf{a}_x + H_{y0}\mathbf{a}_y + H_{z0}\mathbf{a}_z$$



$$\left. \begin{aligned} (\mathbf{H} \cdot \Delta\mathbf{L})_{1-2} &= H_{y,1-2} \Delta y \\ H_{y,1-2} &\approx H_{y0} + \frac{\partial H_y}{\partial x} \left( \frac{1}{2} \Delta x \right) \end{aligned} \right\}$$

$$\rightarrow (\mathbf{H} \cdot \Delta\mathbf{L})_{1-2} \approx \left( H_{y0} + \frac{1}{2} \frac{\partial H_y}{\partial x} \Delta x \right) \Delta y$$

$$(\mathbf{H} \cdot \Delta\mathbf{L})_{2-3} \approx H_{x,2-3} (-\Delta x) \approx - \left( H_{x0} + \frac{1}{2} \frac{\partial H_x}{\partial y} \Delta y \right) \Delta x$$

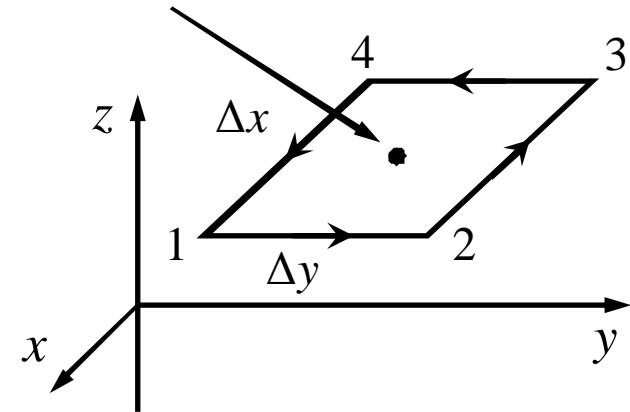
$$(\mathbf{H} \cdot \Delta\mathbf{L})_{3-4} \approx - \left( H_{y0} - \frac{1}{2} \frac{\partial H_y}{\partial x} \Delta x \right) \Delta y$$

$$(\mathbf{H} \cdot \Delta\mathbf{L})_{4-1} \approx \left( H_{x0} - \frac{1}{2} \frac{\partial H_x}{\partial y} \Delta y \right) \Delta x$$

## Curl (2)

$$\oint \mathbf{H} \cdot d\mathbf{L} = I$$

$$\mathbf{H} = \mathbf{H}_0 = H_{x0}\mathbf{a}_x + H_{y0}\mathbf{a}_y + H_{z0}\mathbf{a}_z$$



$$\left. \begin{aligned} (\mathbf{H} \cdot \Delta\mathbf{L})_{1-2} &\approx \left( H_{y0} + \frac{1}{2} \frac{\partial H_y}{\partial x} \Delta x \right) \Delta y \\ (\mathbf{H} \cdot \Delta\mathbf{L})_{2-3} &\approx - \left( H_{x0} + \frac{1}{2} \frac{\partial H_x}{\partial y} \Delta y \right) \Delta x \\ (\mathbf{H} \cdot \Delta\mathbf{L})_{3-4} &\approx - \left( H_{y0} - \frac{1}{2} \frac{\partial H_y}{\partial x} \Delta x \right) \Delta y \\ (\mathbf{H} \cdot \Delta\mathbf{L})_{4-1} &\approx \left( H_{x0} - \frac{1}{2} \frac{\partial H_x}{\partial y} \Delta y \right) \Delta x \end{aligned} \right\} \rightarrow \oint \mathbf{H} \cdot d\mathbf{L} \approx \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \Delta x \Delta y$$

$$\oint \mathbf{H} \cdot d\mathbf{L} \approx (\mathbf{H} \cdot \Delta\mathbf{L})_{1-2} + (\mathbf{H} \cdot \Delta\mathbf{L})_{2-3} + (\mathbf{H} \cdot \Delta\mathbf{L})_{3-4} + (\mathbf{H} \cdot \Delta\mathbf{L})_{4-1}$$

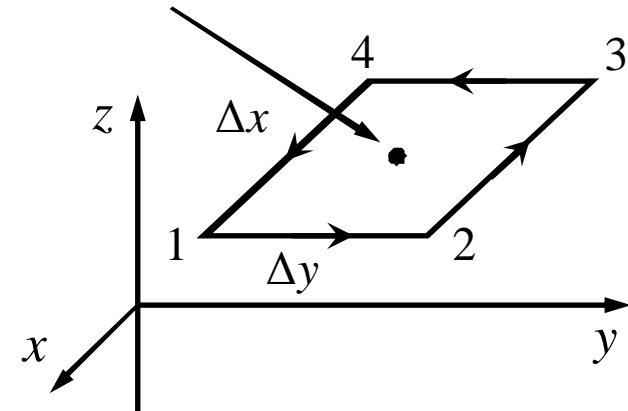
## Curl (3)

$$\mathbf{H} = \mathbf{H}_0 = H_{x0}\mathbf{a}_x + H_{y0}\mathbf{a}_y + H_{z0}\mathbf{a}_z$$

$$\oint \mathbf{H} \cdot d\mathbf{L} \approx \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \Delta x \Delta y$$

$$\oint \mathbf{H} \cdot d\mathbf{L} = \Delta I$$

$$\Delta I \approx J_z \Delta x \Delta y$$



$$\rightarrow \oint \mathbf{H} \cdot d\mathbf{L} \approx \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \Delta x \Delta y \approx J_z \Delta x \Delta y$$

$$\rightarrow \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta x \Delta y} \approx \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \approx J_z \quad \rightarrow \quad \lim_{\Delta x, \Delta y \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta x \Delta y} = \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = J_z$$

$$\lim_{\Delta y, \Delta z \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta y \Delta z} = \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = J_x$$

$$\lim_{\Delta z, \Delta x \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta z \Delta x} = \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = J_y$$

## Curl (4)

$$\lim_{\Delta x, \Delta y \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta x \Delta y} = \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = J_z$$

$$\lim_{\Delta y, \Delta z \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta y \Delta z} = \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = J_x$$

$$\lim_{\Delta z, \Delta x \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta z \Delta x} = \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = J_y$$

Define  $\boxed{(\text{rot } \mathbf{H})_N = \lim_{\Delta S_N \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta S_N}}$

- $S_N$  : planar area enclosed by the closed line integral
- $(\text{rot} \mathbf{H})_N$  : the component (of  $\text{rot} \mathbf{H}$ ) perpendicular to  $S_N$

## Curl (5)

$$(\text{rot } \mathbf{H})_N = \lim_{\Delta S_N \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta S_N}$$

$$\text{rot } \mathbf{H} = \left( \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \mathbf{a}_z$$

$$\text{rot } \mathbf{H} = \begin{vmatrix} \mathbf{a}_x & \mathbf{a}_y & \mathbf{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ H_x & H_y & H_z \end{vmatrix}$$

$$\text{rot } \mathbf{H} = \nabla \times \mathbf{H}$$

## Curl (6)

$$\text{rot } \mathbf{H} = \nabla \times \mathbf{H} = \left( \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \mathbf{a}_z$$

$$\nabla \times \mathbf{H} = \left( \frac{1}{\rho} \frac{\partial H_z}{\partial \varphi} - \frac{\partial H_\varphi}{\partial z} \right) \mathbf{a}_\rho + \left( \frac{\partial H_\rho}{\partial z} - \frac{\partial H_z}{\partial \rho} \right) \mathbf{a}_\varphi + \left( \frac{1}{\rho} \frac{\partial(\rho H_\varphi)}{\partial \rho} - \frac{1}{\rho} \frac{\partial H_\rho}{\partial \varphi} \right) \mathbf{a}_z$$

$$\begin{aligned} \nabla \times \mathbf{H} = & \frac{1}{r \sin \theta} \left( \frac{\partial(H_\varphi \sin \theta)}{\partial \theta} - \frac{\partial H_\theta}{\partial \varphi} \right) \mathbf{a}_r + \frac{1}{r} \left( \frac{1}{\sin \theta} \frac{\partial H_r}{\partial \varphi} - \frac{\partial(r H_\varphi)}{\partial r} \right) \mathbf{a}_\theta \\ & + \frac{1}{r} \left( \frac{\partial(r H_\theta)}{\partial r} - \frac{\partial H_r}{\partial \theta} \right) \mathbf{a}_\varphi \end{aligned}$$

**Ex.**

## Curl (7)

Find the curl of the following vectors:

a)  $\mathbf{A} = x^2 y \mathbf{a}_x + y^2 z \mathbf{a}_y + x y \mathbf{a}_z$

b)  $\mathbf{B} = \rho \cos \varphi \mathbf{a}_z + \frac{z \sin \varphi}{\rho} \mathbf{a}_\rho$

c)  $\mathbf{C} = r^2 \sin \theta \cos \varphi \mathbf{a}_r + \frac{\cos \theta \sin \varphi}{r^2} \mathbf{a}_\theta$



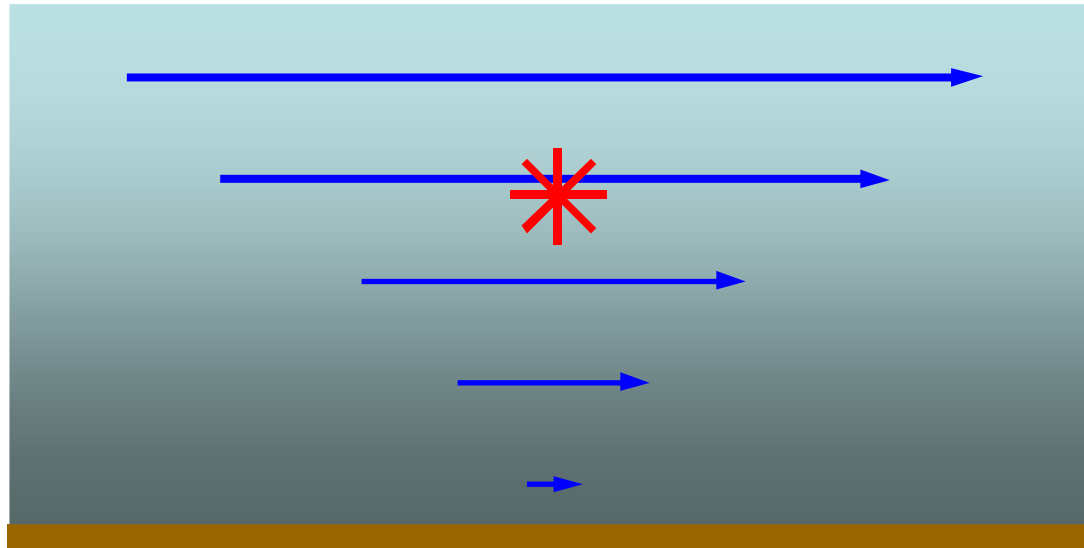
## Curl (8)

$$\text{Curl: } \text{rot } \mathbf{H} = \nabla \times \mathbf{H} = \left( \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \mathbf{a}_z$$

$$\text{Gradient: } \nabla V = \frac{\partial V}{\partial x} \mathbf{a}_x + \frac{\partial V}{\partial y} \mathbf{a}_y + \frac{\partial V}{\partial z} \mathbf{a}_z$$

$$\text{Divergence: } \nabla \cdot \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$

## Curl (9)



$$\text{rot } \mathbf{H} = \nabla \times \mathbf{H} = \left( \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \mathbf{a}_z$$

## Curl (10)

$$\text{rot } \mathbf{H} = \nabla \times \mathbf{H} = \left( \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \mathbf{a}_z$$

$$\left. \begin{aligned} \lim_{\Delta x, \Delta y \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta x \Delta y} &= \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = J_z \\ \lim_{\Delta y, \Delta z \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta y \Delta z} &= \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = J_x \\ \lim_{\Delta z, \Delta x \rightarrow 0} \frac{\oint \mathbf{H} \cdot d\mathbf{L}}{\Delta z \Delta x} &= \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = J_y \end{aligned} \right\}$$

$$\longrightarrow \boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

(the second of Maxwell's four equations)

# The Steady Magnetic Field

1. Biot – Savart Law
2. Ampere's Circuital Law
3. Curl
- 4. Stokes' Theorem**
5. Magnetic Flux & Magnetic Flux Density
6. Magnetic Potential
7. Derivation of the Steady – Magnetic – Field Law

## Stokes' Theorem (1)

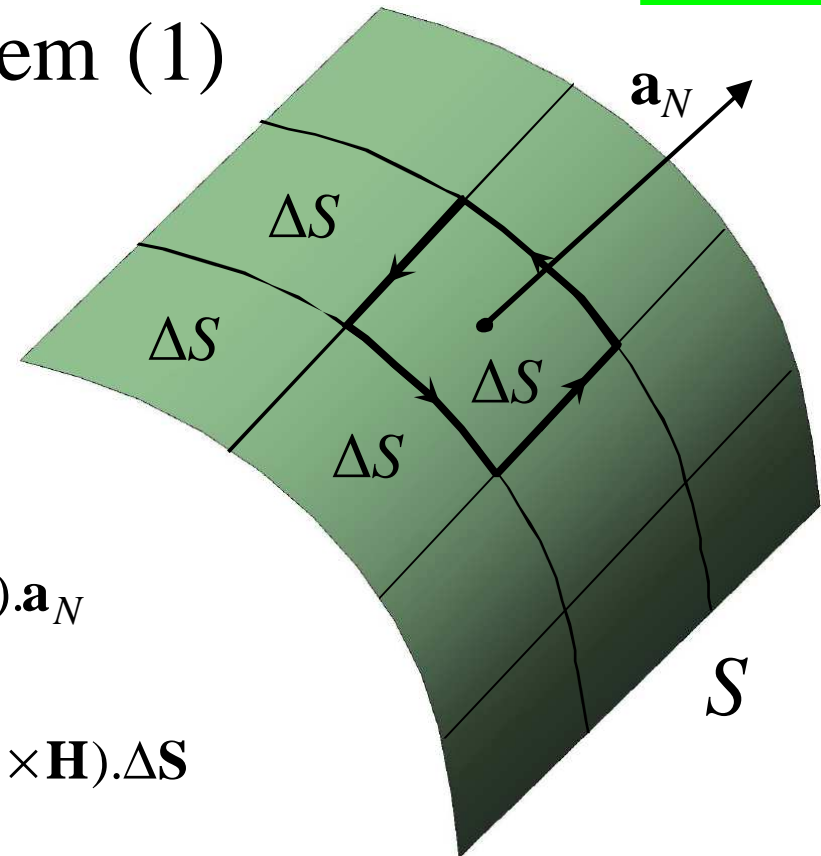
$$\left. \begin{aligned} \mathbf{J}_N &\approx \frac{\mathbf{I}_N}{\Delta S} \\ \mathbf{I}_N &= \oint \mathbf{H} \cdot d\mathbf{L}_{\Delta S} \end{aligned} \right\} \rightarrow \mathbf{J}_N \approx \frac{\oint \mathbf{H} \cdot d\mathbf{L}_{\Delta S}}{\Delta S}$$

$$\mathbf{J}_N = (\nabla \times \mathbf{H})_N$$

$$\rightarrow \frac{\oint \mathbf{H} \cdot d\mathbf{L}_{\Delta S}}{\Delta S} \approx (\nabla \times \mathbf{H})_N = (\nabla \times \mathbf{H}) \cdot \mathbf{a}_N$$

$$\rightarrow \oint \mathbf{H} \cdot d\mathbf{L}_{\Delta S} \approx (\nabla \times \mathbf{H}) \cdot \mathbf{a}_N \Delta S = (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$\rightarrow \boxed{\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}}$$

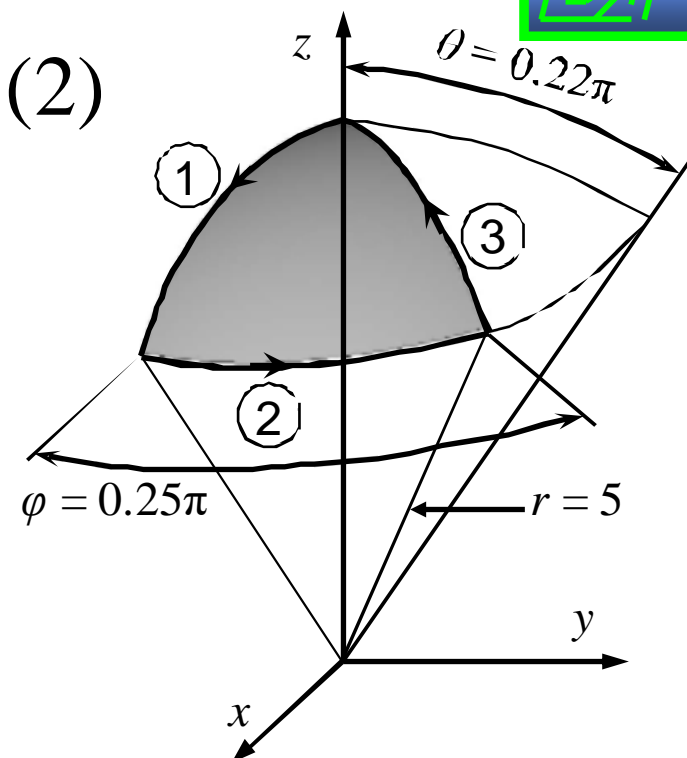
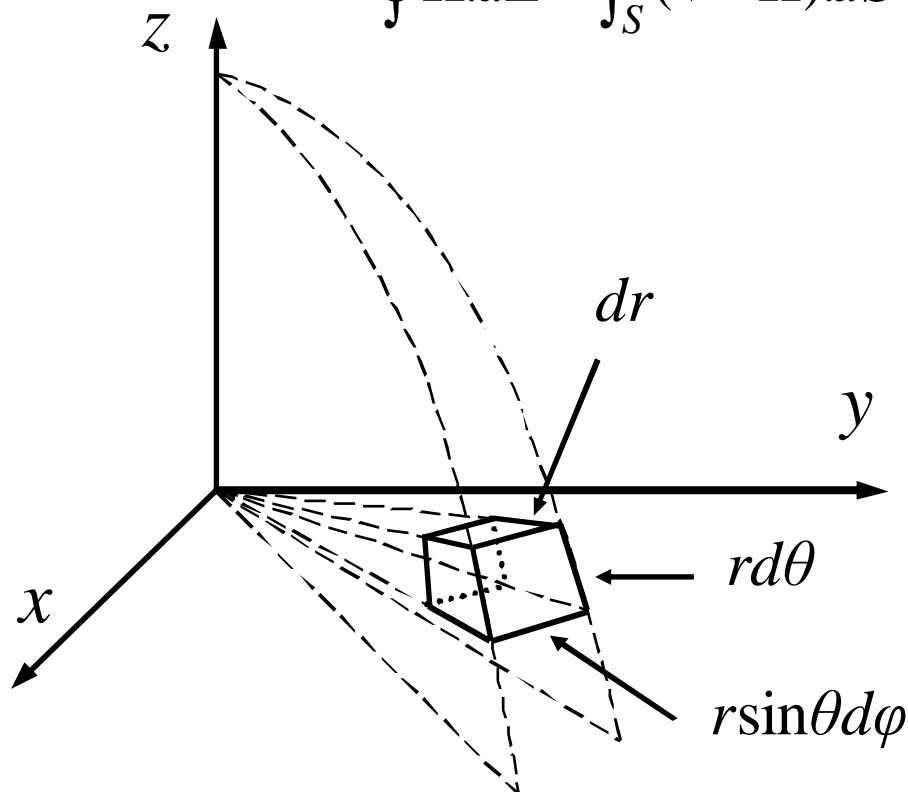


## Ex. 1

## Stokes' Theorem (2)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$



$$d\mathbf{L} = dr\mathbf{a}_r + r d\theta\mathbf{a}_\theta + r \sin \theta d\varphi\mathbf{a}_\varphi$$

### Ex. 1

## Stokes' Theorem (3)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

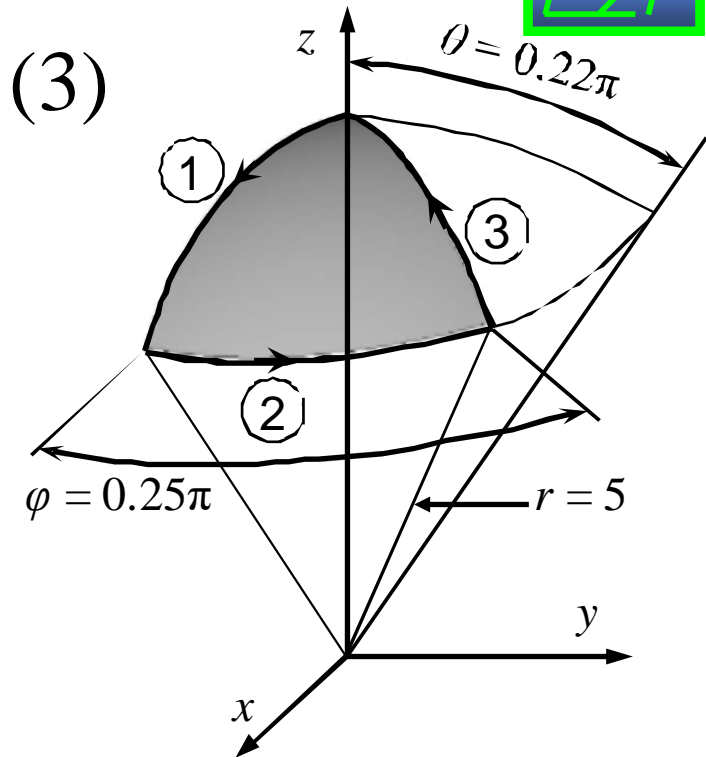
$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$d\mathbf{L} = dr\mathbf{a}_r + r d\theta\mathbf{a}_\theta + r \sin\theta d\varphi\mathbf{a}_\varphi$$

$$\begin{aligned} \rightarrow \oint \mathbf{H} \cdot d\mathbf{L} &= \oint \mathbf{H} \cdot (dr\mathbf{a}_r + r d\theta\mathbf{a}_\theta + r \sin\theta d\varphi\mathbf{a}_\varphi) \\ &= \oint H_r dr + \oint H_\theta r d\theta + \oint H_\varphi r \sin\theta d\varphi \end{aligned}$$

$$\left. \begin{aligned} \oint H_r dr &= \int_1 H_r dr + \int_2 H_r dr + \int_3 H_r dr \\ 1, 2, 3: r &= 5 \rightarrow dr|_{1,2,3} = 0 \end{aligned} \right\} \rightarrow \oint H_r dr = 0$$

$$\left. \begin{aligned} \oint H_\theta r d\theta \\ H_\theta &= 0 \end{aligned} \right\} \rightarrow \oint H_\theta r d\theta = 0$$



## Ex. 1

## Stokes' Theorem (4)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

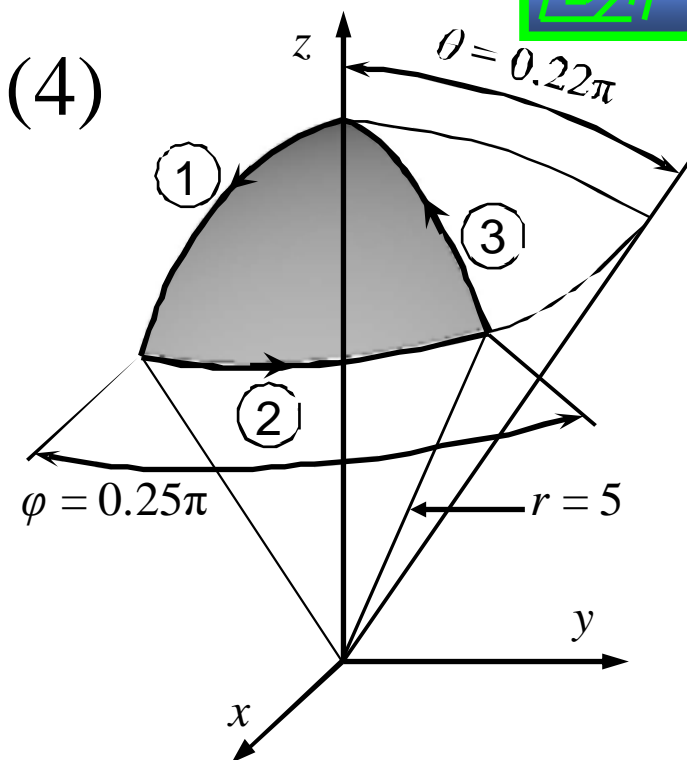
$$\oint \mathbf{H} \cdot d\mathbf{L} = \oint H_r dr + \oint H_\theta r d\theta + \oint H_\varphi r \sin\theta d\varphi$$

$$\oint H_r dr = 0$$

$$\oint H_\theta r d\theta = 0$$

$$\oint H_\varphi r \sin\theta d\varphi = \int_1 H_\varphi r \sin\theta d\varphi + \int_2 H_\varphi r \sin\theta d\varphi + \int_3 H_\varphi r \sin\theta d\varphi \left\{ \begin{array}{l} 1, 3: \varphi = \text{const} \rightarrow d\varphi|_{1,3} = 0 \end{array} \right\}$$

$$\rightarrow \oint H_\varphi r \sin\theta d\varphi = \int_2 H_\varphi r \sin\theta d\varphi$$





## Ex. 1

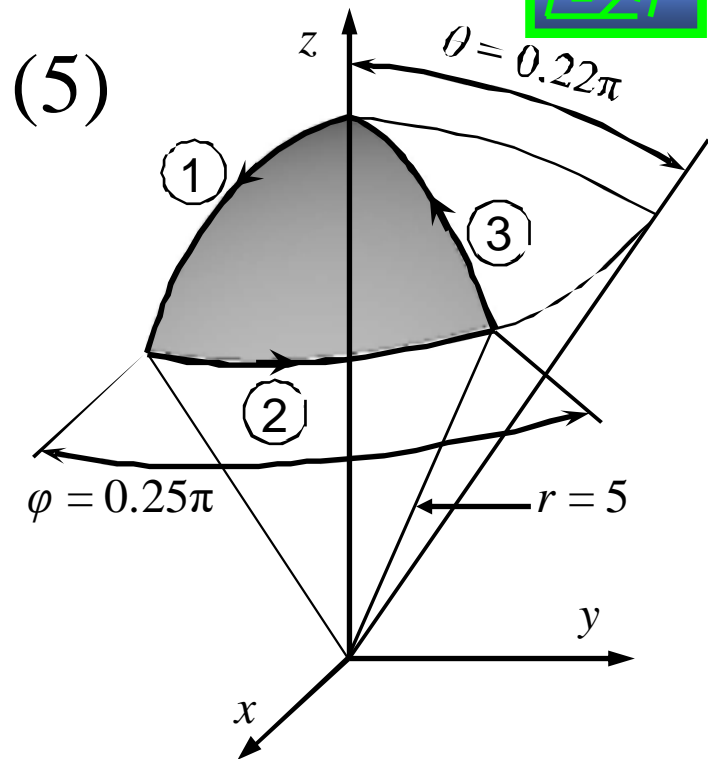
## Stokes' Theorem (5)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$\left. \begin{aligned} \oint \mathbf{H} \cdot d\mathbf{L} &= \oint H_r dr + \oint H_\theta r d\theta + \oint H_\varphi r \sin\theta d\varphi \\ \oint H_r dr &= 0 \\ \oint H_\theta r d\theta &= 0 \\ \oint H_\varphi r \sin\theta d\varphi &= \int_2 H_\varphi r \sin\theta d\varphi \end{aligned} \right\}$$

$$\begin{aligned} \rightarrow \oint \mathbf{H} \cdot d\mathbf{L} &= \int_2 H_\varphi r \sin\theta d\varphi = \int_0^{0.25\pi} H_\varphi r \sin\theta d\varphi = \int_0^{0.25\pi} H_\varphi|_2 5 \sin(0.22\pi) d\varphi \\ &= \int_0^{0.25\pi} 3.19 H_\varphi|_2 d\varphi \end{aligned}$$



## Ex. 1

## Stokes' Theorem (6)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

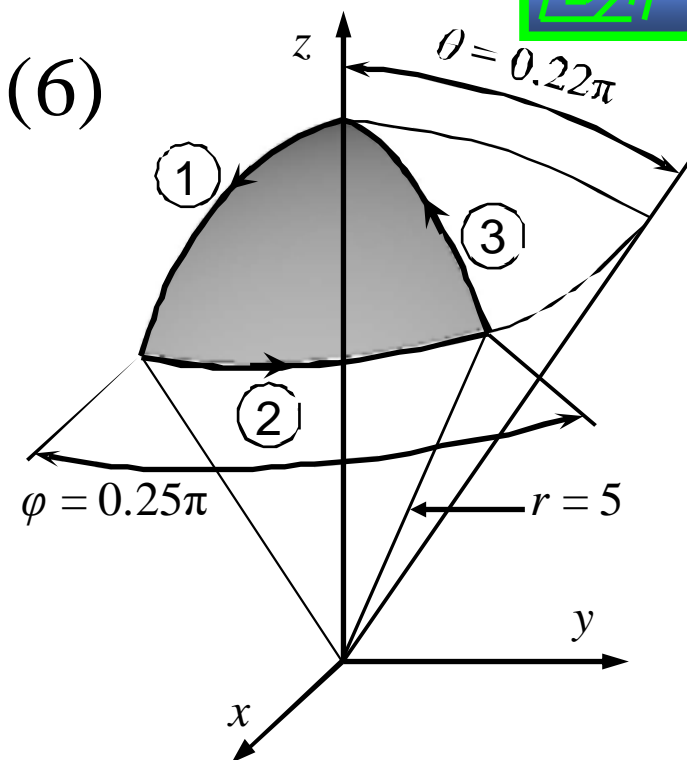
$$\oint \mathbf{H} \cdot d\mathbf{L} = \oint H_r dr + \oint H_\theta r d\theta + \oint H_\varphi r \sin\theta d\varphi$$

$$= \int_0^{0.25\pi} 3.19 H_\varphi|_2 d\varphi$$

$$H_\varphi|_2 = 18 \times 5 \sin(0.22\pi) \cos\varphi = 57.37 \cos\varphi$$

$$\rightarrow \oint \mathbf{H} \cdot d\mathbf{L} = \int_0^{0.25\pi} 3.19 \times 57.37 \cos\varphi d\varphi = \int_0^{0.25\pi} 182.84 \cos\varphi d\varphi$$

$$= 182.84 \sin\varphi \Big|_0^{0.25\pi} = 182.84 \sin(0.25\pi) = 129.27 \text{ A}$$



## Ex. 1

## Stokes' Theorem (7)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

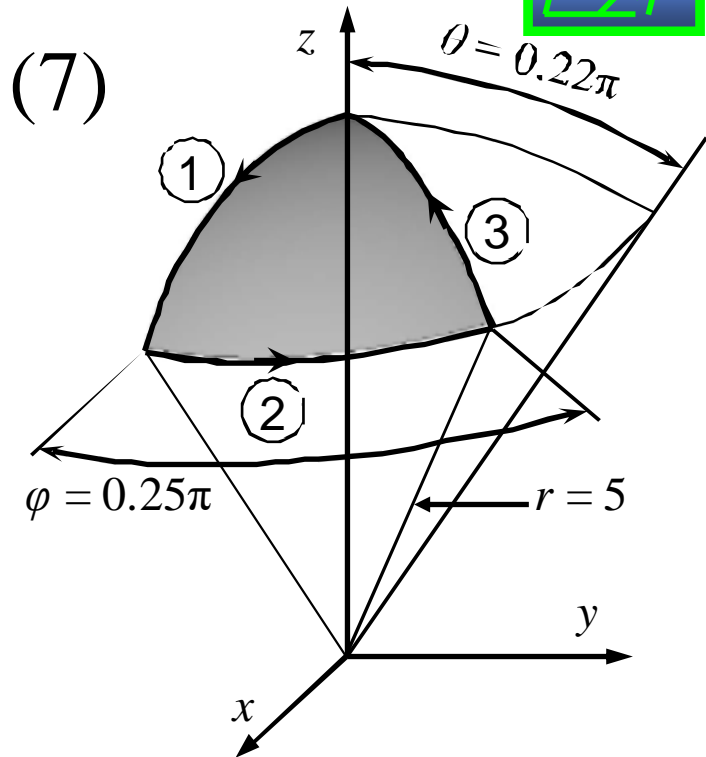
$$\oint \mathbf{H} \cdot d\mathbf{L} = 129.27 \text{ A}$$

$$\int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$\nabla \times \mathbf{H} = \frac{1}{r \sin \theta} \left( \frac{\partial(H_\varphi \sin \theta)}{\partial \theta} - \frac{\partial H_\theta}{\partial \varphi} \right) \mathbf{a}_r$$

$$+ \frac{1}{r} \left( \frac{1}{\sin \theta} \frac{\partial H_r}{\partial \varphi} - \frac{\partial(r H_\varphi)}{\partial r} \right) \mathbf{a}_\theta + \frac{1}{r} \left( \frac{\partial(r H_\theta)}{\partial r} - \frac{\partial H_r}{\partial \theta} \right) \mathbf{a}_\varphi$$

$$= \frac{1}{r \sin \theta} (36r \sin \theta \cos \theta \cos \varphi) \mathbf{a}_r + \frac{1}{r} \left( \frac{1}{\sin \theta} 6r \cos \varphi - 36r \sin \theta \cos \varphi \right) \mathbf{a}_\theta$$



## Ex. 1

## Stokes' Theorem (8)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

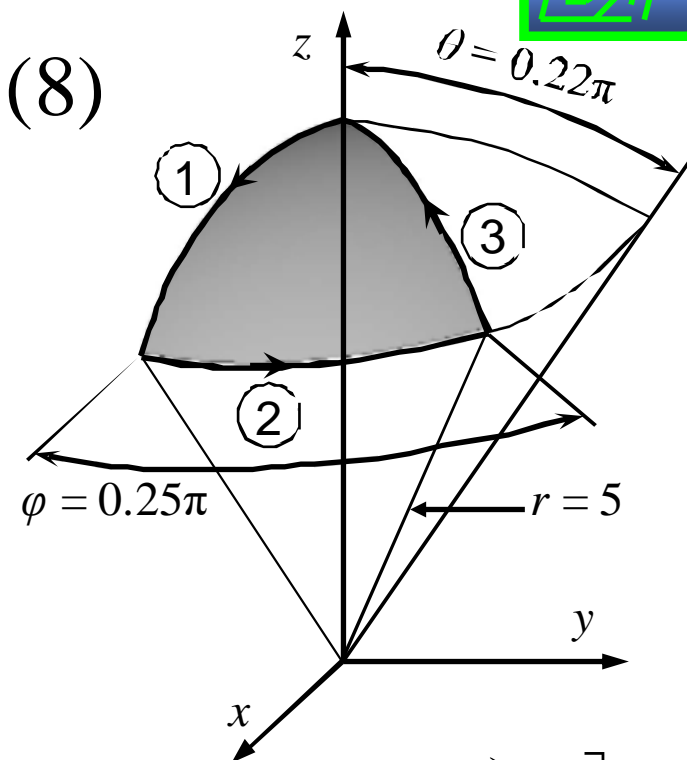
$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$\oint \mathbf{H} \cdot d\mathbf{L} = 129.27 \text{ A}$$

$$\int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$= \int_S \left[ \frac{1}{r\sin\theta} (36r\sin\theta\cos\theta\cos\varphi)\mathbf{a}_r + \frac{1}{r} \left( \frac{1}{\sin\theta} 6r\cos\varphi - 36r\sin\theta\cos\varphi \right) \mathbf{a}_\theta \right] d\mathbf{S}$$

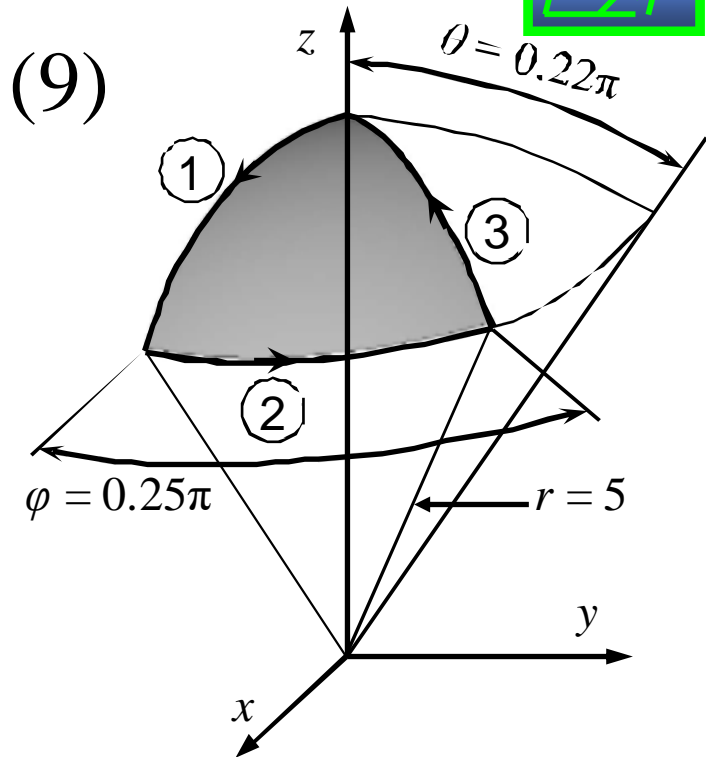
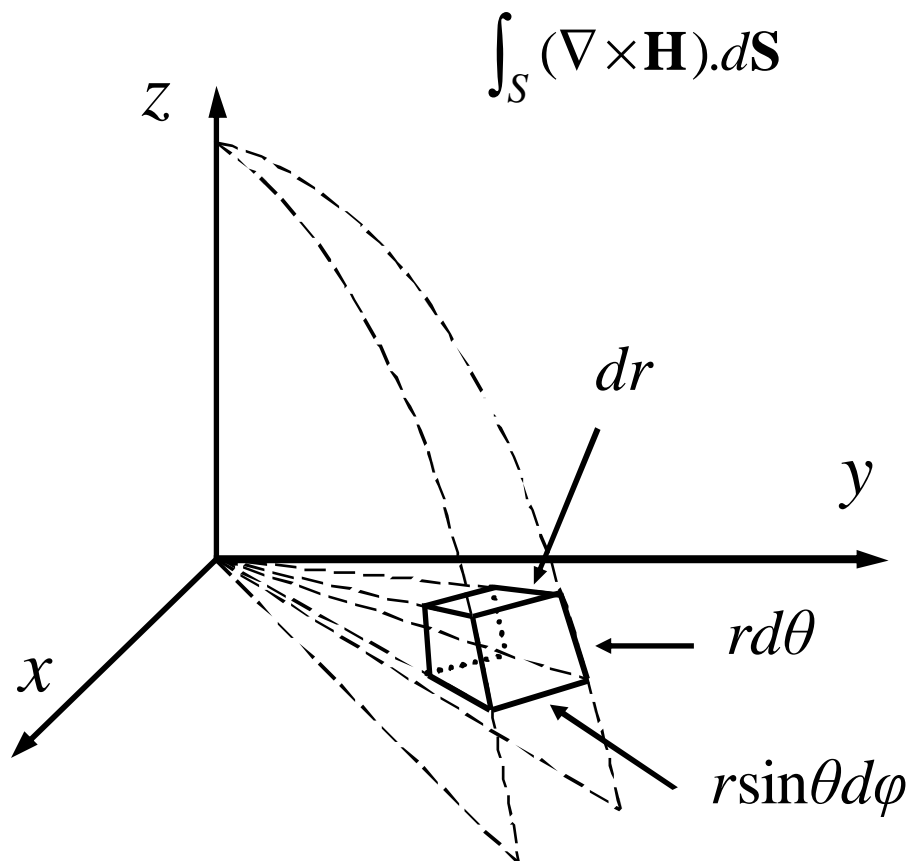
$$= \int_S \left[ (36\cos\theta\cos\varphi)\mathbf{a}_r + \left( \frac{1}{\sin\theta} 6\cos\varphi - 36\sin\theta\cos\varphi \right) \mathbf{a}_\theta \right] d\mathbf{S}$$



## Ex. 1

## Stokes' Theorem (9)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.



$$d\mathbf{S} = r^2 \sin \theta d\theta d\varphi \mathbf{a}_r$$

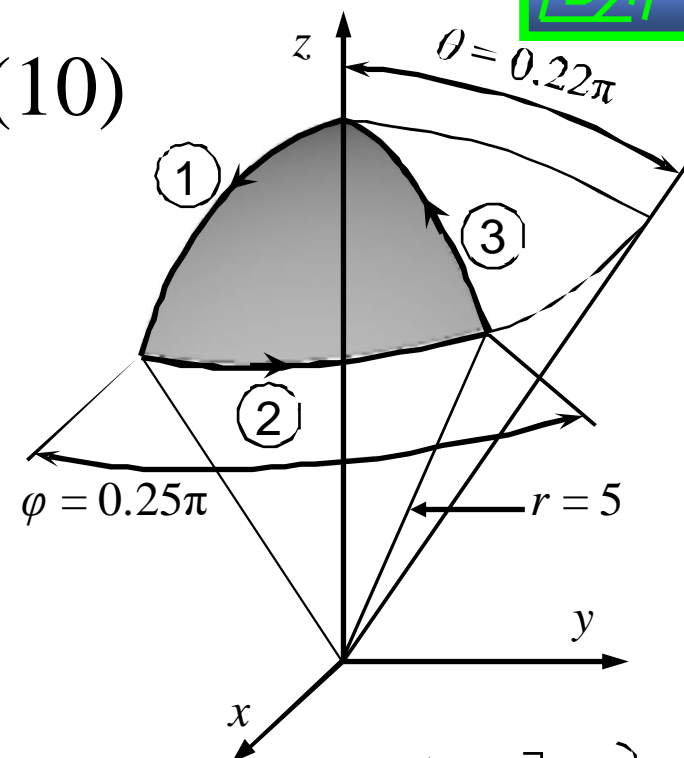
## Ex. 1

## Stokes' Theorem (10)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

$$\oint \mathbf{H} \cdot d\mathbf{L} = 129.27 \text{ A}$$



$$\int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} = \int_S \left[ (36 \cos \theta \cos \varphi) \mathbf{a}_r + \left( \frac{1}{\sin \theta} 6 \cos \varphi - 36 \sin \theta \cos \varphi \right) \mathbf{a}_\theta \right] d\mathbf{S} \left. \vphantom{\int_S} \right\} d\mathbf{S} = r^2 \sin \theta d\theta d\varphi \mathbf{a}_r$$

$$\rightarrow \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} = \int_S 36 \cos \theta \cos \varphi \mathbf{a}_r d\mathbf{S} = \int_S (36 \cos \theta \cos \varphi) (5)^2 \sin \theta d\theta d\varphi$$

## Ex. 1

## Stokes' Theorem (11)

Given  $\mathbf{H} = 6r\sin\varphi\mathbf{a}_r + 18r\sin\theta\cos\varphi\mathbf{a}_\varphi$  A/m.  
Verify Stokes' theorem.

$$\oint \mathbf{H} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S}$$

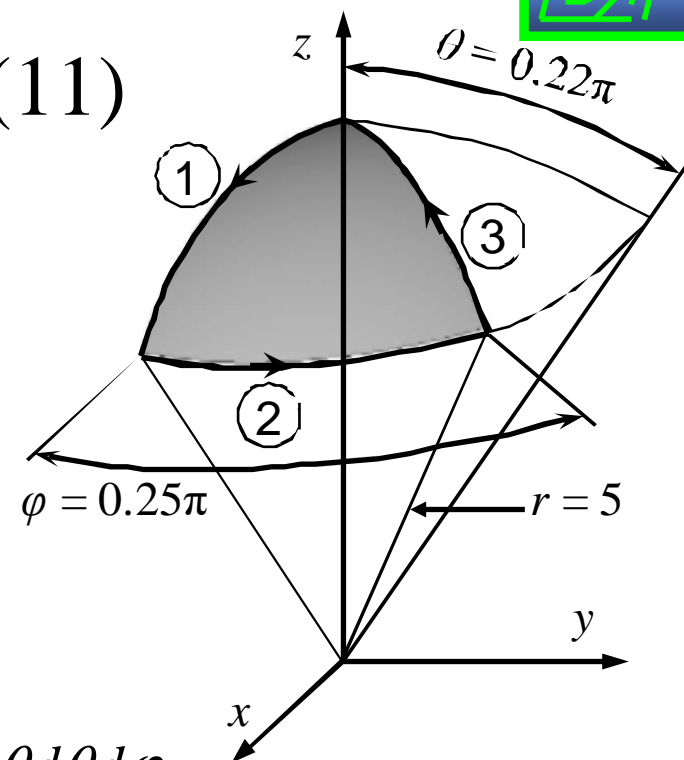
$$\oint \mathbf{H} \cdot d\mathbf{L} = 129.27 \text{ A}$$

$$\int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} = \int_S (36 \cos \theta \cos \varphi)(5)^2 \sin \theta d\theta d\varphi$$

$$= \int_0^{0.25\pi} \int_0^{0.22\pi} (36 \cos \theta \cos \varphi)(5)^2 \sin \theta d\theta d\varphi$$

$$= \int_0^{0.25\pi} 900 \left( \frac{1}{2} \sin^2 \theta \right) \Big|_0^{0.22\pi} \cos \varphi d\varphi = \int_0^{0.25\pi} 182.84 \cos \varphi d\varphi$$

$$= \int_0^{0.25\pi} 182.84 \cos \varphi d\varphi = 182.84 \sin \varphi \Big|_0^{0.25\pi} = 129.27 \text{ A}$$





**Ex. 2****Stokes' Theorem (12)**

Extract  $\oint \mathbf{H} \cdot d\mathbf{L} = I$  from  $\nabla \times \mathbf{H} = \mathbf{J}$

$$\nabla \times \mathbf{H} = \mathbf{J}$$

$$\rightarrow (\nabla \times \mathbf{H}) \cdot d\mathbf{S} = \mathbf{J} \cdot d\mathbf{S}$$

$$\left. \begin{aligned} \rightarrow \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} &= \int_S \mathbf{J} \cdot d\mathbf{S} = I \\ \oint \mathbf{H} \cdot d\mathbf{L} &= \int_S (\nabla \times \mathbf{H}) \cdot d\mathbf{S} \end{aligned} \right\}$$

$$\rightarrow \oint \mathbf{H} \cdot d\mathbf{L} = I$$

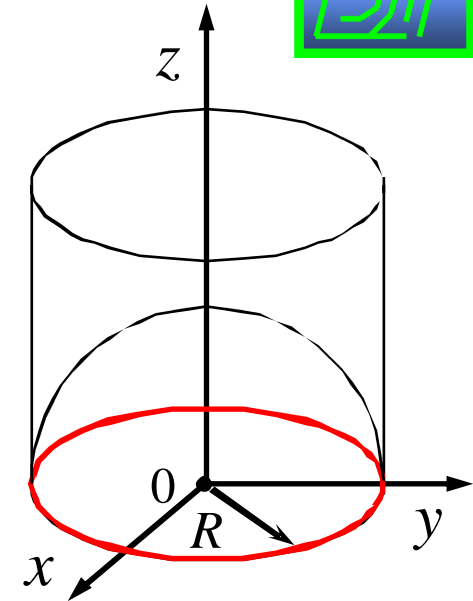


### Ex. 3

## Stokes' Theorem (13)

Given  $\mathbf{A} = -y\mathbf{a}_x + x\mathbf{a}_y - z\mathbf{a}_z = \rho\mathbf{a}_\phi - z\mathbf{a}_z$ . Verify Stokes' theorem for the circular bounding contour in the  $xy$  plane; check the result for:

- The flat circular surface in the  $xy$  plane,
- The hemispherical surface bounded by the contour,
- The cylindrical surface bounded by the contour.



$$\oint \mathbf{A} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{A}) \cdot d\mathbf{S}$$

$$d\mathbf{L} = R d\phi \mathbf{a}_\phi \rightarrow \mathbf{A} \cdot d\mathbf{L} = R^2 d\phi \rightarrow \oint \mathbf{A} \cdot d\mathbf{L} = \int_0^{2\pi} R^2 d\phi = \boxed{2\pi R^2}$$

$$\nabla \times \mathbf{A} = \left( \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \mathbf{a}_z = 2\mathbf{a}_z$$

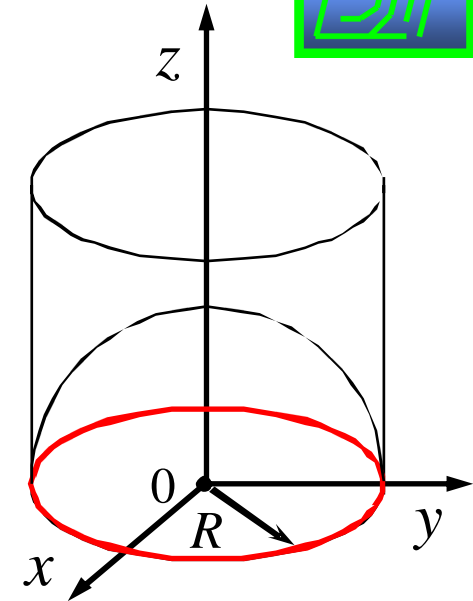
$$\int_{flat} (\nabla \times \mathbf{A}) \cdot d\mathbf{S} = \int_{flat} (2\mathbf{a}_z) \cdot dS \mathbf{a}_z = 2 \int_{flat} dS = \boxed{2\pi R^2}$$

### Ex. 3

## Stokes' Theorem (14)

Given  $\mathbf{A} = -y\mathbf{a}_x + x\mathbf{a}_y - z\mathbf{a}_z = \rho\mathbf{a}_\phi - z\mathbf{a}_z$ . Verify Stokes' theorem for the circular bounding contour in the  $xy$  plane; check the result for:

- The flat circular surface in the  $xy$  plane,
- The hemispherical surface bounded by the contour,
- The cylindrical surface bounded by the contour.



$$\boxed{2\pi R^2} = \oint \mathbf{A} \cdot d\mathbf{L} = \int_S (\nabla \times \mathbf{A}) \cdot d\mathbf{S}$$

$$\left. \begin{aligned} \int_{hemi} (\nabla \times \mathbf{A}) \cdot d\mathbf{S} &= \int_{hemi} (2\mathbf{a}_z) \cdot (R^2 \sin \theta d\theta d\phi) \mathbf{a}_r \\ \mathbf{a}_z \cdot \mathbf{a}_r &= \cos \theta \end{aligned} \right\}$$

$$\rightarrow \int_{hemi} (\nabla \times \mathbf{A}) \cdot d\mathbf{S} = \int_{\theta=0}^{\pi/2} \int_{\phi=0}^{2\pi} R^2 \sin 2\theta d\theta d\phi = -2\pi R^2 \frac{\cos 2\theta}{2} \Big|_{\theta=0}^{\pi/2} = \boxed{2\pi R^2}$$

$$\int_{cy} (\nabla \times \mathbf{A}) \cdot d\mathbf{S} = ?$$

# The Steady Magnetic Field

1. Biot – Savart Law
2. Ampere's Circuital Law
3. Curl
4. Stokes' Theorem
- 5. Magnetic Flux & Magnetic Flux Density**
6. Magnetic Potential
7. Derivation of the Steady – Magnetic – Field Law

# Magnetic Flux & Magnetic Flux Density (1)

- The magnetic flux density  $\mathbf{B}$  is defined in free space:

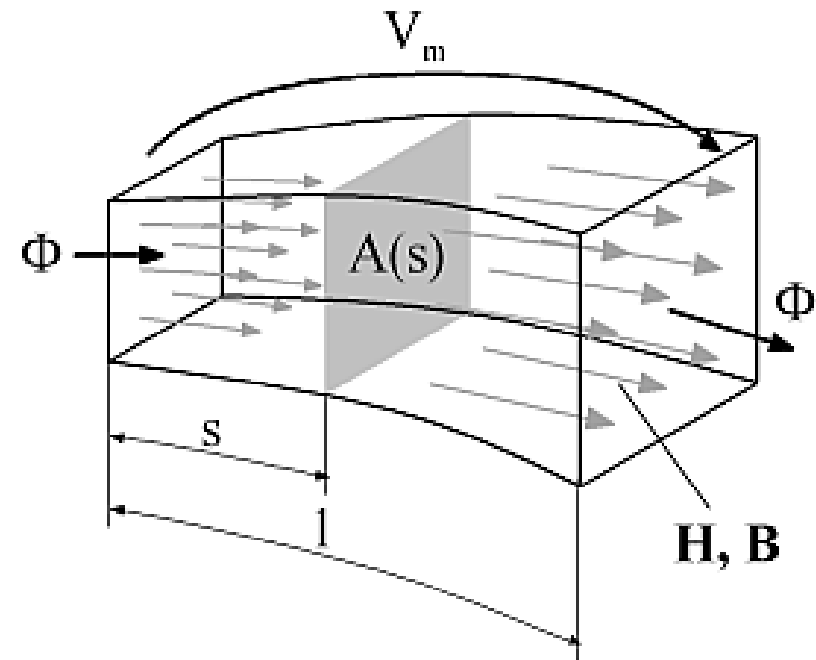
$$\mathbf{B} = \mu_0 \mathbf{H}$$

- Unit: Wb/m<sup>2</sup> or T or G  
(1T = 10000G)
- Permeability  $\mu_0 = 4\pi \times 10^{-7}$  H/m
- Definition of magnetic flux:

$$\Phi = \int_S \mathbf{B} \cdot d\mathbf{S}$$

- Electric flux:

$$\Psi = \oint_S \mathbf{D} \cdot d\mathbf{S} = Q$$



[https://www.maplesoft.com/documentation\\_center/online\\_manuals/modelica/Modelica\\_Magnetic\\_FluxTubes\\_UsersGuide.html](https://www.maplesoft.com/documentation_center/online_manuals/modelica/Modelica_Magnetic_FluxTubes_UsersGuide.html)



## Magnetic Flux & Magnetic Flux Density (2)

- Gauss' law for the magnetic field:

$$\oint_S \mathbf{B} \cdot d\mathbf{S} = 0$$

- The last of Maxwell's four equations:

$$\nabla \cdot \mathbf{B} = 0$$

- Maxwell's four equations:

$$\begin{aligned}\nabla \cdot \mathbf{D} &= \rho_v \\ \nabla \times \mathbf{E} &= 0 \\ \nabla \times \mathbf{H} &= \mathbf{J} \\ \nabla \cdot \mathbf{B} &= 0\end{aligned}$$



$$\begin{aligned}\oint_S \mathbf{D} \cdot d\mathbf{S} &= Q = \int_V \rho_v dv \\ \oint \mathbf{E} \cdot d\mathbf{L} &= 0 \\ \oint \mathbf{H} \cdot d\mathbf{L} &= I = \oint_S \mathbf{J} \cdot d\mathbf{S} \\ \oint_S \mathbf{B} \cdot d\mathbf{S} &= 0\end{aligned}$$

## Ex. 1 Magnetic Flux & Magnetic Flux Density (3)

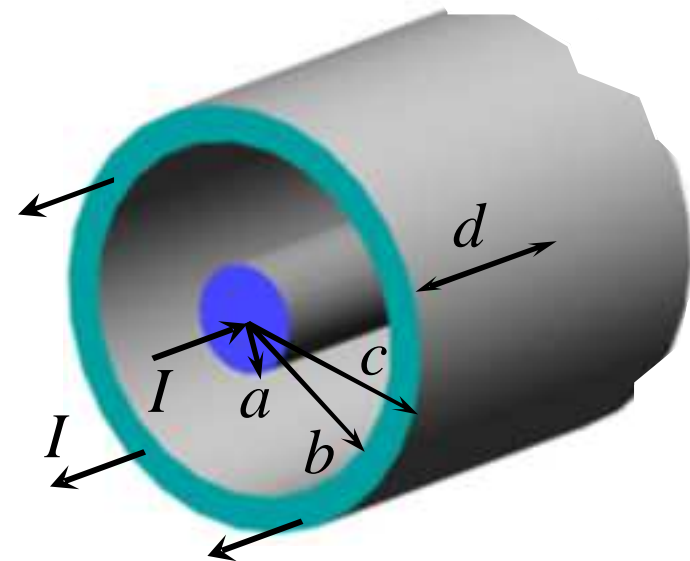
Given the magnetic field  $\mathbf{B} = 3xy^2\mathbf{a}_z$  Wb/m<sup>2</sup>. Determine the magnetic flux crossing the portion of the  $xy$  plane lying between  $x = 0$ ,  $x = 1$ ,  $y = 0$ , &  $y = 1$ .

$$\left. \begin{array}{l} \Phi = \int_S \mathbf{B} \cdot d\mathbf{S} \\ \mathbf{B} = 3xy^2\mathbf{a}_z \\ d\mathbf{S} = dxdy\mathbf{a}_z \end{array} \right\} \rightarrow \Phi = \int_{x=0}^1 \int_{y=0}^1 3xy^2 dxdy = 0.5 \text{ Wb}$$

## Ex. 2 Magnetic Flux & Magnetic Flux Density (4)

Find the flux between the conductors of the coaxial line.

$$\left. \begin{aligned} H_{\varphi} &= \frac{I}{2\pi\rho} \quad (a < \rho < b) \\ \rightarrow \mathbf{B} &= \mu_0 \mathbf{H} = \frac{\mu_0 I}{2\pi\rho} \mathbf{a}_{\varphi} \\ \Phi &= \int_S \mathbf{B} \cdot d\mathbf{S} \\ d\mathbf{S} &= d\rho dz \mathbf{a}_{\varphi} \end{aligned} \right\}$$



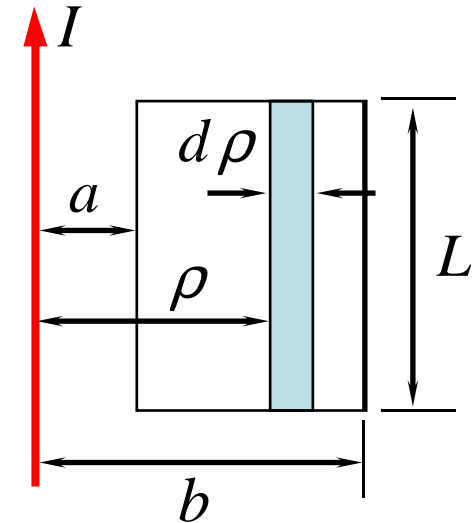
$$\rightarrow \Phi = \int_0^d \int_a^b \frac{\mu_0 I}{2\pi\rho} \mathbf{a}_{\varphi} \cdot d\rho dz \mathbf{a}_{\varphi} = \frac{\mu_0 I d}{2\pi} \ln \frac{b}{a}$$

## Ex. 3 Magnetic Flux & Magnetic Flux Density (5)

Find the total flux through the rectangular circuit.

$$\left. \begin{aligned} \Phi &= \int_S \mathbf{B} \cdot d\mathbf{S} \\ \mathbf{B} &= \mu_0 \mathbf{H} = \frac{\mu_0 I}{2\pi\rho} \mathbf{a}_\phi \\ d\mathbf{S} &= L d\rho \mathbf{a}_\phi \end{aligned} \right\}$$

$$\rightarrow \Phi = \int_{\rho=a}^{\rho=b} \frac{\mu_0 I}{2\pi\rho} L d\rho = \frac{\mu_0 I L}{2\pi} \ln \frac{b}{a}$$





## Ex. 4 Magnetic Flux & Magnetic Flux Density (6)

Find the total flux through the rectangular circuit.

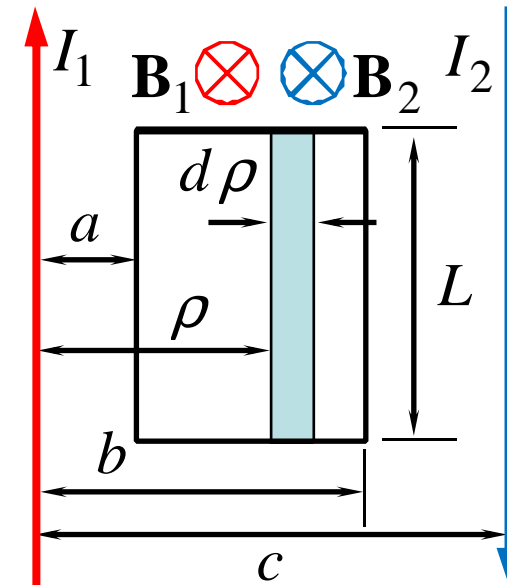
$$\Phi = \int_S \mathbf{B} \cdot d\mathbf{S} = \int_S (\mathbf{B}_1 + \mathbf{B}_2) \cdot d\mathbf{S}$$

$$\mathbf{B}_1 = \mu_0 \mathbf{H}_1 = \frac{\mu_0 I_1}{2\pi\rho} \mathbf{a}_\varphi$$

$$\mathbf{B}_2 = \mu_0 \mathbf{H}_2 = \frac{\mu_0 I_2}{2\pi(c-\rho)} \mathbf{a}_\varphi$$

$$d\mathbf{S} = L d\rho \mathbf{a}_\varphi$$

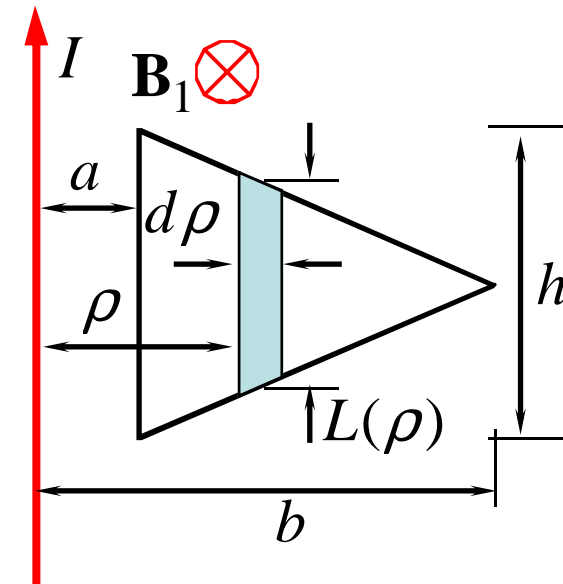
$$\rightarrow \Phi = \int_{\rho=a}^{\rho=b} \left[ \frac{\mu_0 I_1}{2\pi\rho} + \frac{\mu_0 I_2}{2\pi(c-\rho)} \right] L d\rho = \frac{\mu_0 L}{2\pi} \left( I_1 \ln \frac{b}{a} + I_2 \ln \frac{c-a}{c-b} \right)$$



## Ex. 5 Magnetic Flux & Magnetic Flux Density (7)

Find the total flux through the triangular circuit.

$$\left. \begin{aligned} \Phi &= \int_S \mathbf{B} \cdot d\mathbf{S} \\ \mathbf{B} &= \mu_0 \mathbf{H} = \frac{\mu_0 I}{2\pi\rho} \mathbf{a}_\varphi \\ d\mathbf{S} &= L(\rho) d\rho \mathbf{a}_\varphi \\ \frac{h}{b-a} &= \frac{L(\rho)}{b-\rho} \rightarrow L(\rho) = \frac{h(b-\rho)}{b-a} \end{aligned} \right\}$$



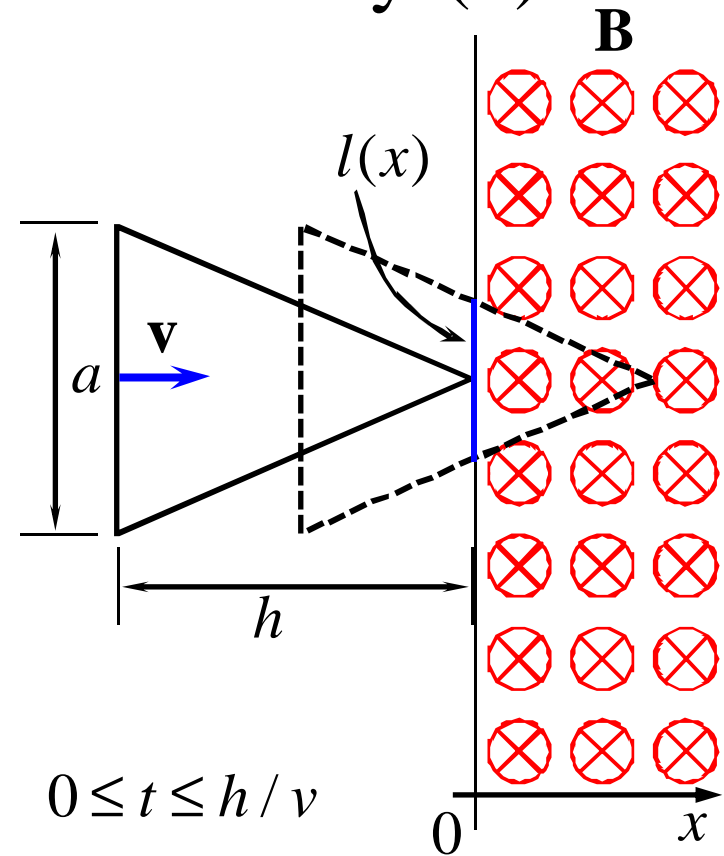
$$\rightarrow \Phi = \int_{\rho=a}^{\rho=b} \left( \frac{\mu_0 I}{2\pi\rho} \right) \left[ \frac{h(b-\rho)}{b-a} d\rho \right]$$

## Ex. 6 Magnetic Flux & Magnetic Flux Density (8)

Find the total flux through the triangular circuit when it enters a uniform field  $\mathbf{B}$  with a speed of  $\mathbf{v}$ ?

$$\left. \begin{aligned} \Phi &= \int_S \mathbf{B} \cdot d\mathbf{S} = BS(x) \\ S(x) &= \frac{1}{2} l(x)x \\ \frac{a}{h} &= \frac{l(x)}{x} \rightarrow l(x) = \frac{a}{h}x \end{aligned} \right\} \rightarrow \Phi = B \frac{a}{2h} x^2 \quad \left. \begin{aligned} & \\ & x = vt \end{aligned} \right\}$$

$$\rightarrow \Phi(t) = \begin{cases} \frac{aBv^2}{2h} t^2, & 0 \leq t \leq h/v \\ \frac{ahB}{2}, & t > h/v \end{cases}$$

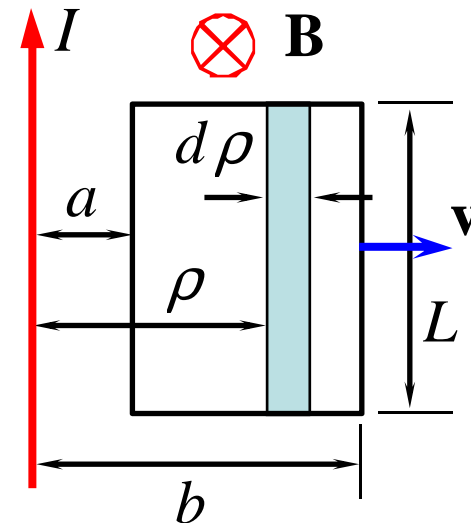


## VD7 Magnetic Flux & Magnetic Flux Density (9)

Find the total flux through the rectangular circuit if it moves with a speed of  $v$ ?

$$\left. \begin{aligned} \Phi &= \frac{\mu_0 I L}{2\pi} \ln \frac{b}{a} \\ a &= a_0 + vt \\ b &= b_0 + vt \end{aligned} \right\}$$

$$\rightarrow \Phi(t) = \frac{\mu_0 I L}{2\pi} \ln \frac{b_0 + vt}{a_0 + vt}$$



## Ex. 8 Magnetic Flux & Magnetic Flux Density (10)

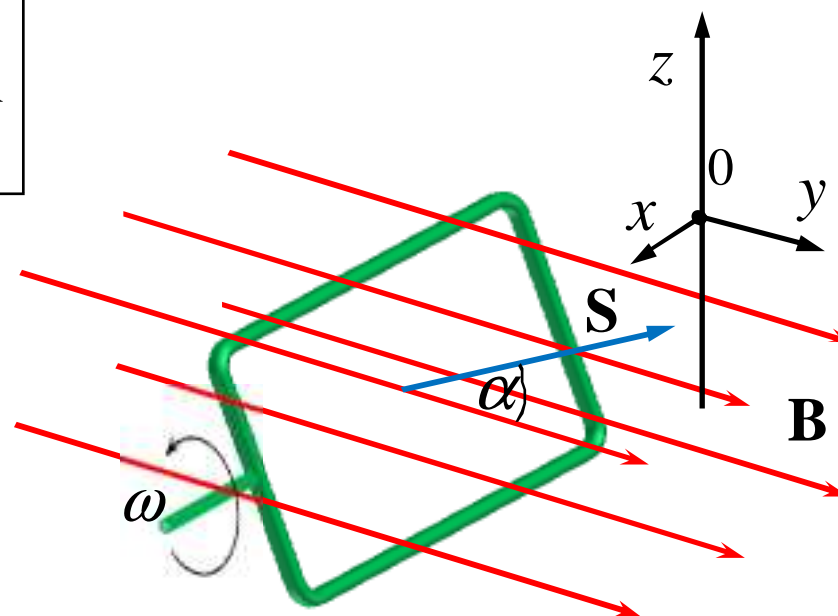
Find the total flux through the rectangular circuit having an area of  $S$  when it rotates with an angular speed of  $\omega$  in a uniform field  $\mathbf{B}$ ?

$$\Phi = \int_S \mathbf{B} \cdot d\mathbf{S} = \mathbf{B} \cdot \mathbf{S}$$

$$= BS \cos \alpha$$

$$\alpha = \omega t$$

$$\rightarrow \Phi = BS \cos \omega t$$



# The Steady Magnetic Field

1. Biot – Savart Law
2. Ampere's Circuital Law
3. Curl
4. Stokes' Theorem
5. Magnetic Flux & Magnetic Flux Density
- 6. Magnetic Potential**
7. Derivation of the Steady – Magnetic – Field Law

## Magnetic Potential (1)

- The scalar magnetic potential  $V_m$  is defined by:

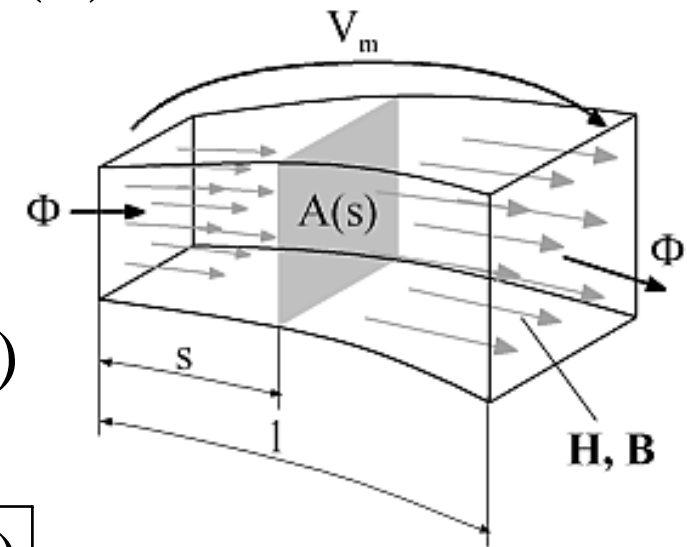
$$\mathbf{H} = -\nabla V_m$$

- $\nabla \times \mathbf{H} = \mathbf{J} \rightarrow \nabla \times \mathbf{H} = \mathbf{J} = \nabla \times (-\nabla V_m)$
- Curl of gradient of a scalar field is zero, therefore:  $\mathbf{H} = -\nabla V_m \quad (\mathbf{J} = 0)$

$$\nabla \cdot \mathbf{B} = 0 \rightarrow \nabla \cdot \mathbf{B} = \mu_0 \nabla \cdot \mathbf{H} = 0$$

$$\rightarrow \mu_0 \nabla \cdot (-\nabla V_m) = 0 \rightarrow \nabla^2 V_m = 0 \quad (\mathbf{J} = 0)$$

$$V_{m,ab} = -\int_b^a \mathbf{H} \cdot d\mathbf{L}$$



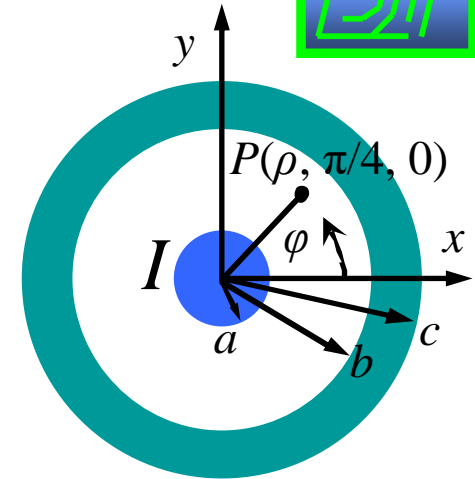
[https://www.maplesoft.com/documentation\\_center/online\\_manuals/modelica/Modelica\\_Magnetic\\_FluxTubes\\_UsersGuide.html](https://www.maplesoft.com/documentation_center/online_manuals/modelica/Modelica_Magnetic_FluxTubes_UsersGuide.html)

## Magnetic Potential (2)

$$a < \rho < b: \mathbf{J} = 0$$

$$\left. \begin{aligned} \mathbf{H} &= \frac{I}{2\pi\rho} \mathbf{a}_\varphi \quad (a < \rho < b) \\ \mathbf{H} &= -\nabla V_m \quad (\mathbf{J} = 0) \end{aligned} \right\} \rightarrow \frac{I}{2\pi\rho} = -\nabla V_m|_\varphi = -\frac{1}{\rho} \frac{\partial V_m}{\partial \varphi}$$

$$\rightarrow \frac{\partial V_m}{\partial \varphi} = -\frac{I}{2\pi} \rightarrow V_m = -\frac{I}{2\pi} \varphi$$



$$\text{Assume } V_m|_{\varphi=0} = 0 \rightarrow V_{mP} = \frac{I}{2\pi} \left( 2n - \frac{1}{4} \right) \pi \quad (n = 0, \pm 1, \pm 2, \dots)$$

$$= I \left( n - \frac{1}{8} \right) \quad (n = 0, \pm 1, \pm 2, \dots)$$



## Magnetic Potential (3)

- Definition of a vector magnetic potential  $\mathbf{A}$ :

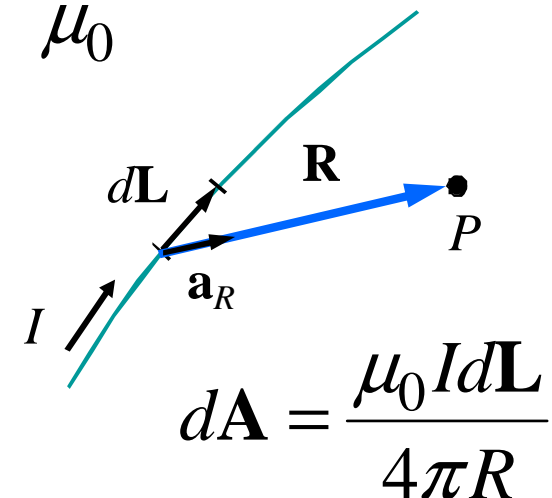
$$\mathbf{B} = \nabla \times \mathbf{A}$$

- Unit: Wb/m

$$\mathbf{H} = \frac{1}{\mu_0} \mathbf{B} = \frac{1}{\mu_0} \nabla \times \mathbf{A} \quad \rightarrow \quad \nabla \times \mathbf{H} = \mathbf{J} = \frac{1}{\mu_0} \nabla \times \nabla \times \mathbf{A}$$

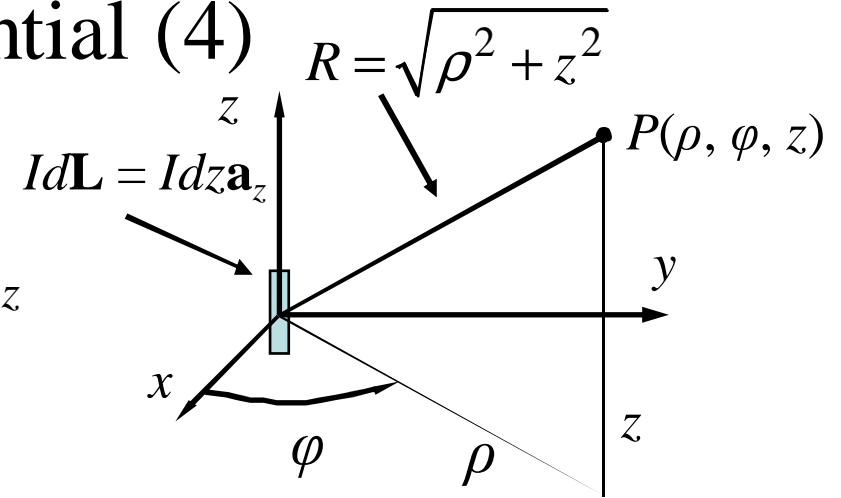
- $\mathbf{A}$  may be determined by:

$$\mathbf{A} = \oint \frac{\mu_0 I d\mathbf{L}}{4\pi R}$$



## Magnetic Potential (4)

$$\left. \begin{aligned} d\mathbf{A} &= \frac{\mu_0 Id\mathbf{L}}{4\pi R} \\ d\mathbf{L} &= dz\mathbf{a}_z \\ R &= \sqrt{\rho^2 + z^2} \end{aligned} \right\} \rightarrow d\mathbf{A} = \frac{\mu_0 Idz}{4\pi\sqrt{\rho^2 + z^2}} \mathbf{a}_z$$



$$\left. \begin{aligned} \rightarrow d\mathbf{A}_z &= \frac{\mu_0 Idz\mathbf{a}_z}{4\pi\sqrt{\rho^2 + z^2}} & d\mathbf{A}_\varphi &= 0 & d\mathbf{A}_\rho &= 0 \\ \mathbf{H} &= \frac{1}{\mu_0} \nabla \times \mathbf{A} \end{aligned} \right\} \rightarrow d\mathbf{H} = \frac{1}{\mu_0} \nabla \times d\mathbf{A} = \frac{1}{\mu_0} \left( -\frac{\partial dA_z}{\partial \rho} \right) \mathbf{a}_\varphi$$

$$\rightarrow d\mathbf{H} = \frac{Idz}{4\pi} \frac{\rho}{(\rho^2 + z^2)^{3/2}} \mathbf{a}_\varphi$$

## Magnetic Potential (5)

$$d\mathbf{A} = \frac{\mu_0 I d\mathbf{L}}{4\pi R}$$

- In the case of current flow throughout a volume with a density  $\mathbf{J}$ , then:

$$I d\mathbf{L} = \mathbf{J} dv$$

$$\rightarrow \mathbf{A} = \int_V \frac{\mu_0 \mathbf{J} dv}{4\pi R}$$

## Ex. 1 Magnetic Potential (6)

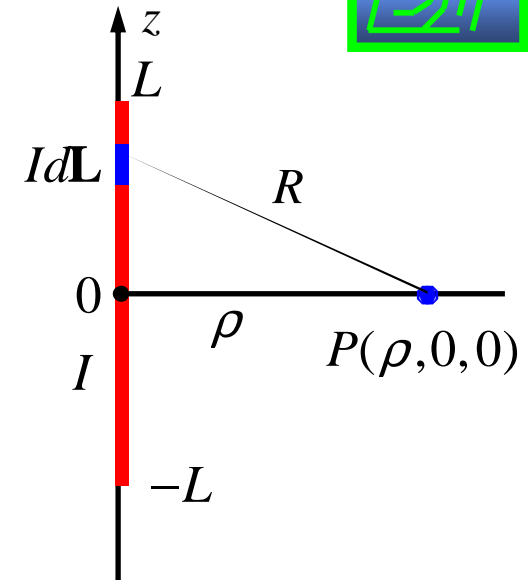
A very long, straight conductor lies along the  $z$  axis, carrying a uniform current  $I$  in the  $z$  direction. Find the magnetic potential difference between two points in space?

$$\left. \begin{aligned} V_{m,ab} &= -\int_b^a \mathbf{H} \cdot d\mathbf{L} \\ d\mathbf{L} &= d\rho \mathbf{a}_\rho + \rho d\varphi \mathbf{a}_\varphi + dz \mathbf{a}_z \\ \mathbf{H} &= \frac{I}{2\pi\rho} \mathbf{a}_\varphi \end{aligned} \right\} \rightarrow V_{m,ab} = -\int_b^a \frac{I}{2\pi} d\varphi = \frac{I}{2\pi} (\varphi_b - \varphi_a)$$

## Ex. 2

## Magnetic Potential (7)

Find the vector magnetic potential in the plane bisecting a straight piece of thin wire of finite length  $2L$  in free space.



$$\left. \begin{aligned} d\mathbf{A} &= \frac{\mu_0 I d\mathbf{L}}{4\pi R} \\ Id\mathbf{L} &= Idz' \mathbf{a}_z \\ R &= \sqrt{\rho^2 + (z')^2} \end{aligned} \right\}$$

$$\rightarrow \mathbf{A}(\rho, 0, 0) = \int_{z'=-L}^L \frac{\mu_0 I dz'}{4\pi \sqrt{\rho^2 + (z')^2}} \mathbf{a}_z = \frac{\mu_0 I}{4\pi} \ln \frac{\sqrt{L^2 + \rho^2} + L}{\sqrt{L^2 + \rho^2} - L} \mathbf{a}_z$$

# The Steady Magnetic Field

1. Biot – Savart Law
2. Ampere's Circuital Law
3. Curl
4. Stokes' Theorem
5. Magnetic Flux & Magnetic Flux Density
6. Magnetic Potential
- 7. Derivation of the Steady – Magnetic – Field Law**

(1)

- Use formulae/definitions:

$$\mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2} \quad \mathbf{B} = \mu_0 \mathbf{H} \quad \mathbf{B} = \nabla \times \mathbf{A}$$

- to show that

$$\mathbf{A} = \int_V \frac{\mu_0 \mathbf{J} dv}{4\pi R}$$

$$\boxed{\mathbf{A} = \int_V \frac{\mu_0 \mathbf{J} dv}{4\pi R} \rightarrow \mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2}}$$

(2)

$$\mathbf{A} = \int_V \frac{\mu_0 \mathbf{J} dv}{4\pi R} \rightarrow \mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2}$$

Current element at  $(x_1, y_1, z_1)$ ,  $\mathbf{A}$  at  $(x_2, y_2, z_2) \rightarrow \mathbf{A}_2 = \int_V \frac{\mu_0 \mathbf{J}_1 dv_1}{4\pi R_{12}} \left\{ \begin{array}{l} \mathbf{B} = \mu_0 \mathbf{H} \\ \mathbf{B} = \nabla \times \mathbf{A} \end{array} \right\} \rightarrow \mathbf{H} = \frac{\mathbf{B}}{\mu_0} = \frac{\nabla \times \mathbf{A}}{\mu_0}$

$$\rightarrow \mathbf{H}_2 = \frac{\nabla_2 \times \mathbf{A}_2}{\mu_0} = \frac{\nabla_2}{\mu_0} \times \int_V \frac{\mu_0 \mathbf{J}_1 dv_1}{4\pi R_{12}} = \frac{1}{4\pi} \int_V \nabla_2 \times \frac{\mathbf{J}_1 dv_1}{R_{12}} = \frac{1}{4\pi} \int_V \left( \nabla_2 \times \frac{\mathbf{J}_1}{R_{12}} \right) dv_1 \left\{ \begin{array}{l} \nabla \times (S\mathbf{V}) = (\nabla S) \times \mathbf{V} + S(\nabla \times \mathbf{V}) \end{array} \right\}$$

$$\rightarrow H_2 = \frac{1}{4\pi} \int_V \left[ \left( \nabla_2 \frac{1}{R_{12}} \right) \times \mathbf{J}_1 + \frac{1}{R_{12}} (\nabla_2 \times \mathbf{J}_1) \right] dv_1$$





(3)

$$\mathbf{A} = \int_V \frac{\mu_0 \mathbf{J} dv}{4\pi R} \rightarrow \mathbf{H} = \oint \frac{Id\mathbf{L} \times \mathbf{a}_R}{4\pi R^2}$$

Current element at  $(x_1, y_1, z_1)$ ,  $\mathbf{A}$  at  $(x_2, y_2, z_2)$

$$\rightarrow H_2 = \frac{1}{4\pi} \int_V \left[ \left( \nabla_2 \frac{1}{R_{12}} \right) \times \mathbf{J}_1 + \frac{1}{R_{12}} (\nabla_2 \times \mathbf{J}_1) \right] dv_1 \left. \vphantom{\int_V} \right\} \nabla_2 \times \mathbf{J}_1 = 0$$

$$\rightarrow H_2 = \frac{1}{4\pi} \int_V \left[ \left( \nabla_2 \frac{1}{R_{12}} \right) \times \mathbf{J}_1 \right] dv_1 \left. \vphantom{\int_V} \right\}$$

$$R_{12} = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2} \rightarrow \nabla_2 \frac{1}{R_{12}} = -\frac{\mathbf{R}_{12}}{R_{12}^3} = -\frac{\mathbf{a}_{R12}}{R_{12}^2} \left. \vphantom{\int_V} \right\}$$

$$\rightarrow \mathbf{H}_2 = \frac{1}{4\pi} \int_V \frac{\mathbf{a}_{R12} \times \mathbf{J}_1}{R_{12}^2} dv_1 = \frac{1}{4\pi} \int_V \frac{\mathbf{J}_1 \times \mathbf{a}_{R12}}{R_{12}^2} dv_1$$



(4)

$$\mathbf{A} = \int_V \frac{\mu_0 \mathbf{J} dv}{4\pi R} \rightarrow \mathbf{H} = \oint \frac{I d\mathbf{L} \times \mathbf{a}_R}{4\pi R^2}$$

Current element at  $(x_1, y_1, z_1)$ ,  $\mathbf{A}$  at  $(x_2, y_2, z_2)$

$$\left. \begin{aligned} \rightarrow \mathbf{H}_2 &= \frac{1}{4\pi} \int_V \frac{\mathbf{J}_1 \times \mathbf{a}_{R12}}{R_{12}^2} dv_1 \\ \mathbf{J}_1 dv_1 &= I_1 d\mathbf{L}_1 \end{aligned} \right\}$$

$$\rightarrow \mathbf{H}_2 = \oint \frac{I_1 d\mathbf{L}_1 \times \mathbf{a}_{R12}}{4\pi R_{12}^2}$$

(5)

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

$$\left. \begin{array}{l} \nabla \times \mathbf{H} = \mathbf{J} \\ \mathbf{B} = \mu_0 \mathbf{H} \\ \mathbf{B} = \nabla \times \mathbf{A} \end{array} \right\} \rightarrow \nabla \times \mathbf{H} = \nabla \times \frac{\mathbf{B}}{\mu_0} = \frac{1}{\mu_0} \nabla \times \nabla \times \mathbf{A}$$
$$\left. \begin{array}{l} \nabla \times \nabla \times \mathbf{A} = \nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A} \\ \nabla^2 \mathbf{A} = \nabla^2 A_x \mathbf{a}_x + \nabla^2 A_y \mathbf{a}_y + \nabla^2 A_z \mathbf{a}_z \end{array} \right\}$$

$$\rightarrow \nabla \times \mathbf{H} = \frac{\nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}}{\mu_0}$$

(6)

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

$$\begin{aligned} \rightarrow \nabla \times \mathbf{H} &= \frac{\nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}}{\mu_0} \\ \mathbf{A}_2 &= \int_V \frac{\mu_0 \mathbf{J}_1 dv_1}{4\pi R_{12}} \\ \nabla \cdot (S\mathbf{A}) &= \mathbf{A} \cdot (\nabla S) + S(\nabla \cdot \mathbf{A}) \end{aligned} \quad \left. \vphantom{\begin{aligned} \rightarrow \nabla \times \mathbf{H} &= \frac{\nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}}{\mu_0} \\ \mathbf{A}_2 &= \int_V \frac{\mu_0 \mathbf{J}_1 dv_1}{4\pi R_{12}} \\ \nabla \cdot (S\mathbf{A}) &= \mathbf{A} \cdot (\nabla S) + S(\nabla \cdot \mathbf{A}) \end{aligned}} \right\}$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = \frac{\mu_0}{4\pi} \int_V \left[ \mathbf{J}_1 \cdot \left( \nabla_2 \frac{1}{R_{12}} \right) + \frac{1}{R_{12}} (\nabla_2 \cdot \mathbf{J}_1) \right] dv_1$$



(7)

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = \frac{\mu_0}{4\pi} \int_V \left[ \mathbf{J}_1 \cdot \left( \nabla_2 \frac{1}{R_{12}} \right) + \frac{1}{R_{12}} (\nabla_2 \cdot \mathbf{J}_1) \right] dv_1 \left. \begin{array}{l} \int_V \frac{1}{R_{12}} (\nabla_2 \cdot \mathbf{J}_1) dv_1 = 0 \\ \nabla_1 \frac{1}{R_{12}} = \frac{\mathbf{R}_{12}}{R_{12}^3} = -\nabla_2 \frac{1}{R_{12}} \end{array} \right\}$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = \frac{\mu_0}{4\pi} \int_V \left[ -\mathbf{J}_1 \cdot \left( \nabla_1 \frac{1}{R_{12}} \right) \right] dv_1$$



(8)

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = \frac{\mu_0}{4\pi} \int_V \left[ -\mathbf{J}_1 \cdot \left( \nabla_1 \frac{1}{R_{12}} \right) \right] dv_1 \left. \vphantom{\int_V} \right\} \nabla \cdot (S\mathbf{A}) = \mathbf{A} \cdot (\nabla S) + S(\nabla \cdot \mathbf{A})$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = \frac{\mu_0}{4\pi} \int_V \left[ \frac{1}{R_{12}} (\nabla_1 \cdot \mathbf{J}_1) - \nabla_1 \cdot \left( \frac{\mathbf{J}_1}{R_{12}} \right) \right] dv_1$$

(9)

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = \frac{\mu_0}{4\pi} \int_V \left[ \frac{1}{R_{12}} (\nabla_1 \cdot \mathbf{J}_1) - \nabla_1 \cdot \left( \frac{\mathbf{J}_1}{R_{12}} \right) \right] dv_1 \left. \begin{array}{l} \\ \nabla_1 \cdot \mathbf{J}_1 = -\frac{\partial \rho_v}{\partial t} = 0 \\ \oint_S \mathbf{J} \cdot d\mathbf{S} = \int_V \nabla \cdot \mathbf{J} dv \end{array} \right\}$$

$$\rightarrow \nabla_2 \cdot \mathbf{A}_2 = -\frac{\mu_0}{4\pi} \oint_{S_1} \frac{\mathbf{J}_1}{R_{12}} d\mathbf{S}_1 = 0$$

(10)

$$\boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$

$$\rightarrow \nabla \times \mathbf{H} = \frac{\nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}}{\mu_0}$$

$$\nabla \cdot \mathbf{A} = 0$$

$$\left. \begin{aligned} A_x &= \int_V \frac{\mu_0 J_x dv}{4\pi R} \\ V &= \int_V \frac{\rho_v dv}{4\pi \epsilon_0 R} \\ \nabla^2 V &= -\frac{\rho_v}{\epsilon_0} \end{aligned} \right\} \rightarrow \left\{ \begin{aligned} \nabla^2 A_x &= -\mu_0 J_x \\ \nabla^2 A_y &= -\mu_0 J_y \\ \nabla^2 A_z &= -\mu_0 J_z \end{aligned} \right. \rightarrow \nabla^2 \mathbf{A} = -\mu_0 \mathbf{J}$$

$$\rightarrow \boxed{\nabla \times \mathbf{H} = \mathbf{J}}$$



$$\begin{array}{l}
 Q \longrightarrow \mathbf{F} = \frac{Q_1 Q_2}{4\pi\epsilon R^2} \mathbf{a}_R \longrightarrow \mathbf{E} = \frac{Q}{4\pi\epsilon R^2} \mathbf{a}_R \longrightarrow \mathbf{D} = \epsilon \mathbf{E} \\
 \downarrow \\
 W = -Q \int \mathbf{E} \cdot d\mathbf{L} \longrightarrow V = -\int \mathbf{E} \cdot d\mathbf{L} \longrightarrow C = \frac{Q}{V} \\
 \downarrow \\
 I = \frac{dQ}{dt} \longrightarrow R = \frac{V}{I} \\
 \downarrow \\
 \mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_\phi \longrightarrow \mathbf{B} = \mu \mathbf{H} \longrightarrow \Phi = \int \mathbf{B} \cdot d\mathbf{S}
 \end{array}$$