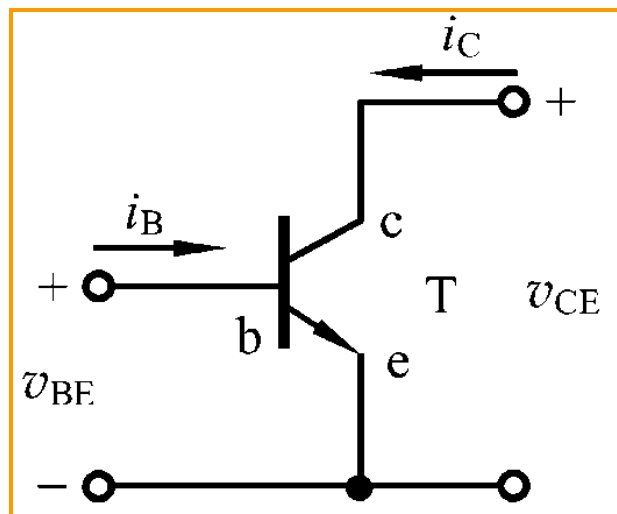
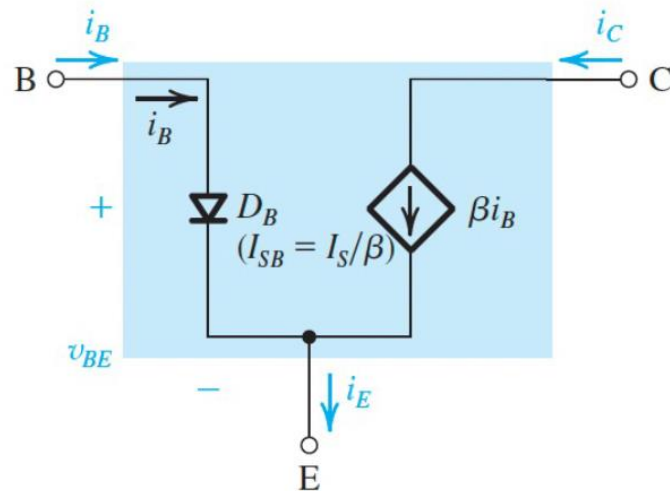
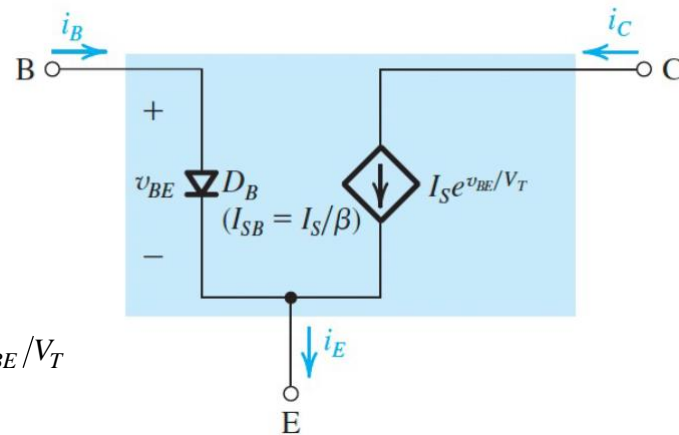


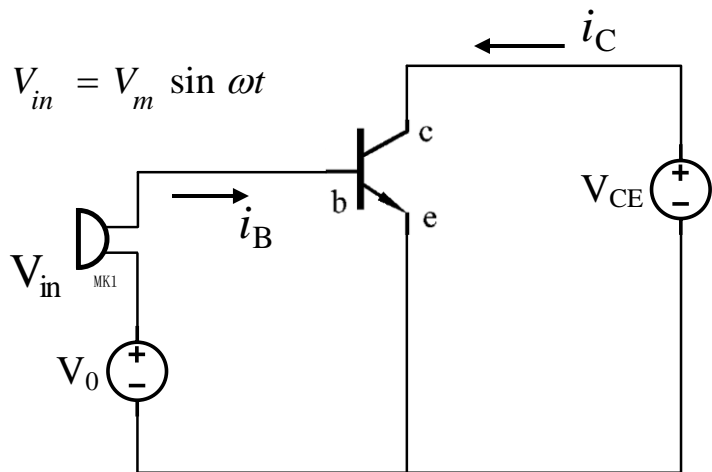


Simple bipolar transistor model

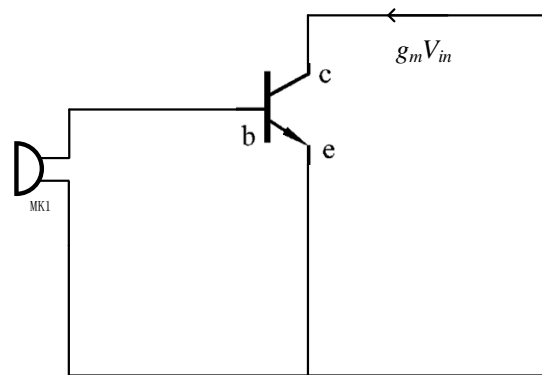
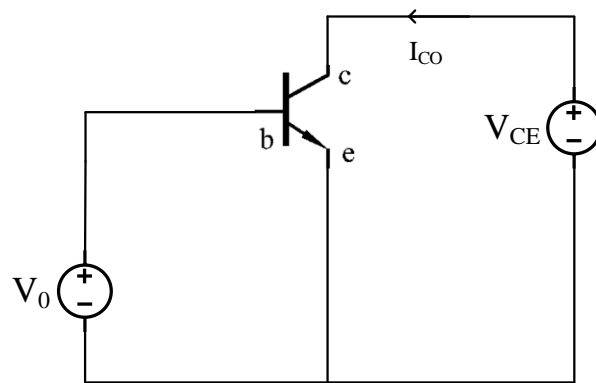


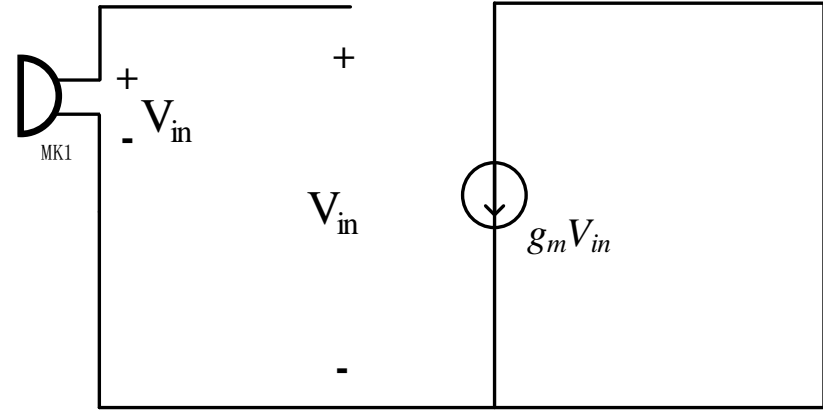
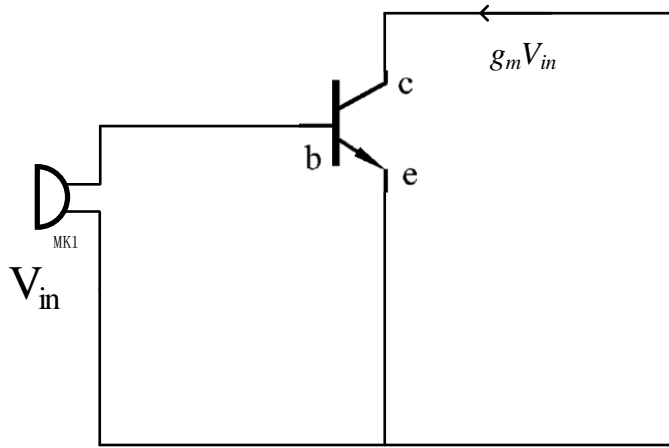
$$i_B = \frac{i_C}{\beta} = \frac{i_S}{\beta} e^{v_{BE}/V_T}$$



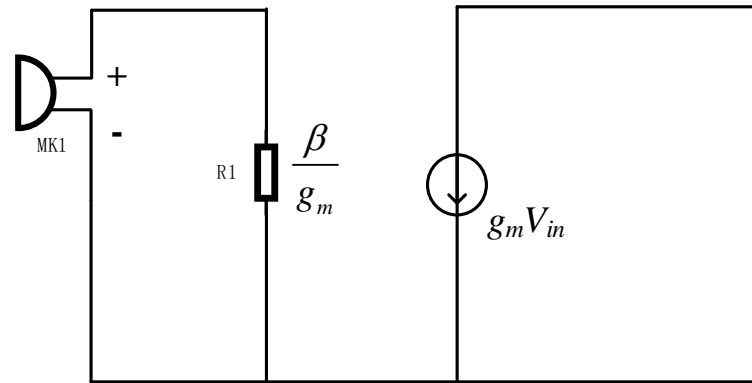


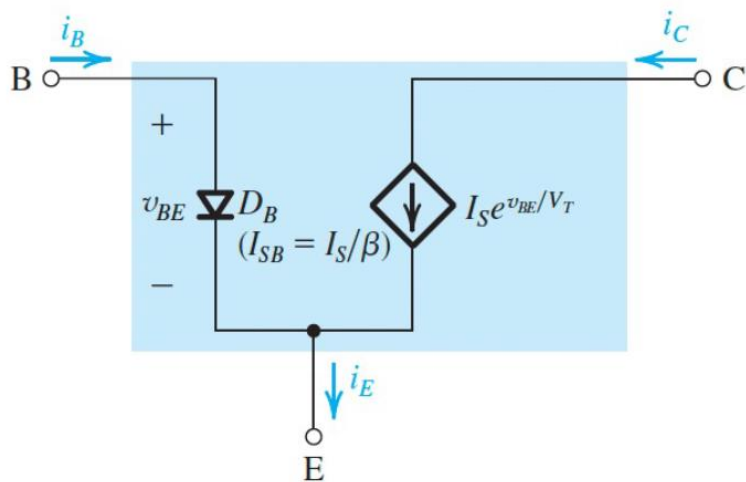
$$\begin{aligned} i_C &= I_S e^{\left(\frac{V_0 + V_{in}}{V_T}\right)} = I_S e^{\left(\frac{V_0}{V_T}\right)} \cdot e^{\left(\frac{V_m \sin \omega t}{V_T}\right)} \\ &= I_{CO} \cdot e^{\left(\frac{V_m \sin \omega t}{V_T}\right)} = I_{CO} \cdot \left(1 + \frac{V_m \sin \omega t}{V_T}\right) \\ &= I_{CO} + \frac{I_{CO}}{V_T} V_m \sin \omega t \\ &= I_{CO} + g_m V_m \sin \omega t \end{aligned}$$



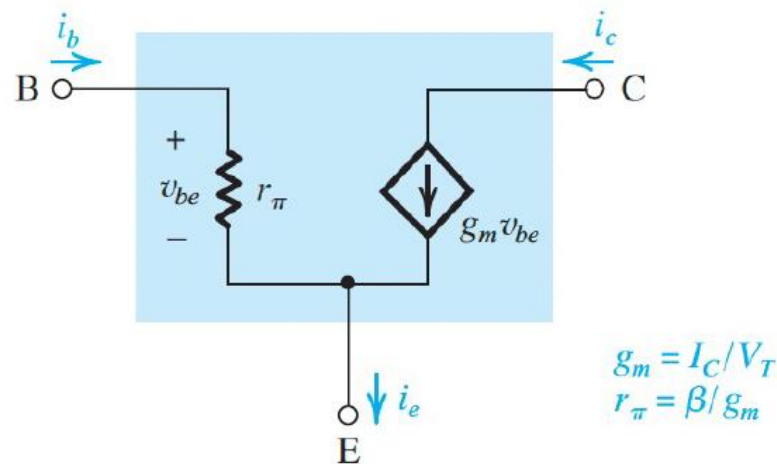


$$i_B = \frac{i_C}{\beta} = \frac{i_{CO}}{\beta} + \frac{g_m V_{in}}{\beta}$$





Large-signal model



Small-signal model

Bipolar Junction Transistors

Peng Mei

Department of Electronic Systems

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AALBORG UNIVERSITY
DENMARK

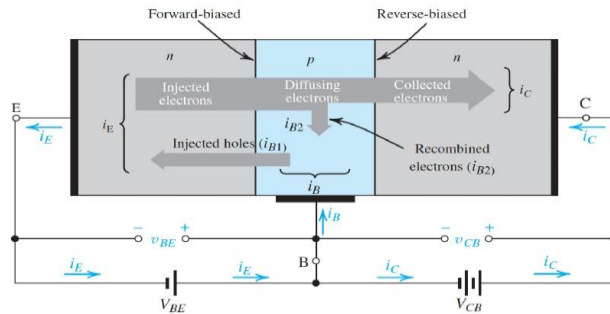
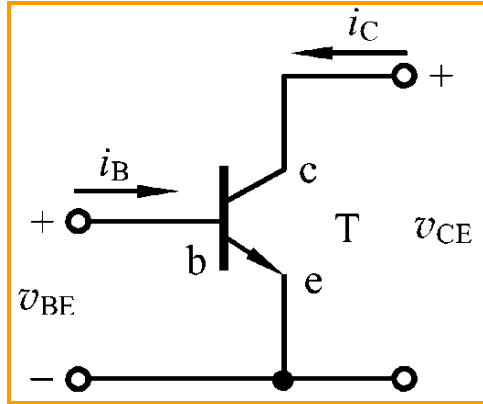


Learning objectives:

- Early effect
- Static operating point in power amplifier design



$i_C \sim v_{CE}$ curve:



i_C :

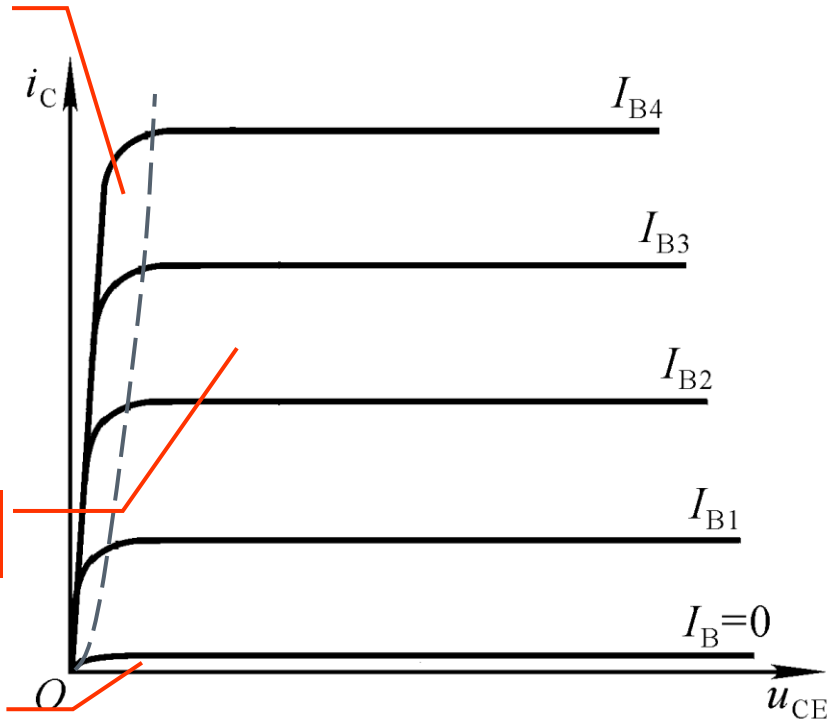
Electrons $E \rightarrow B \rightarrow C$

Saturation

Active

Cutoff

$$i_C = f(u_{CE}) \Big|_{I_B}$$



A big i_B results in a big i_C .



Mode	EBJ	CBJ
Cutoff	Reverse	Reverse
Active	Forward	Reverse
Saturation	Forward	Forward

Saturation region: i_c is mainly controlled by v_{ce} , $\beta i_b > i_c$

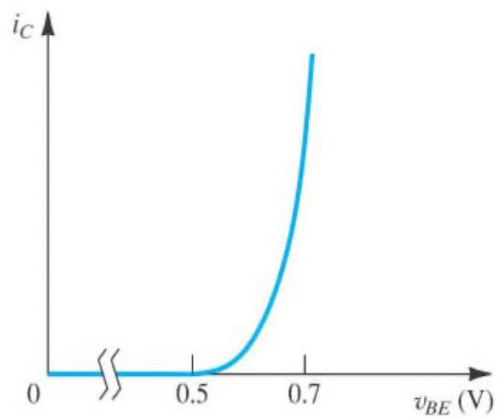
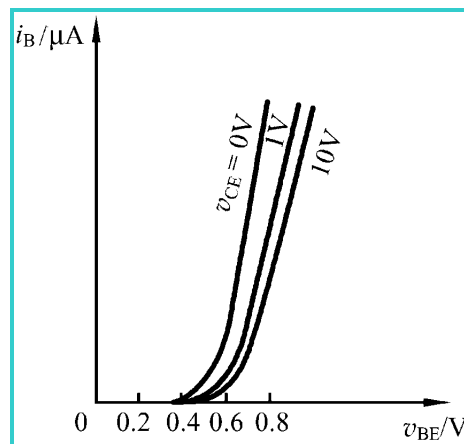
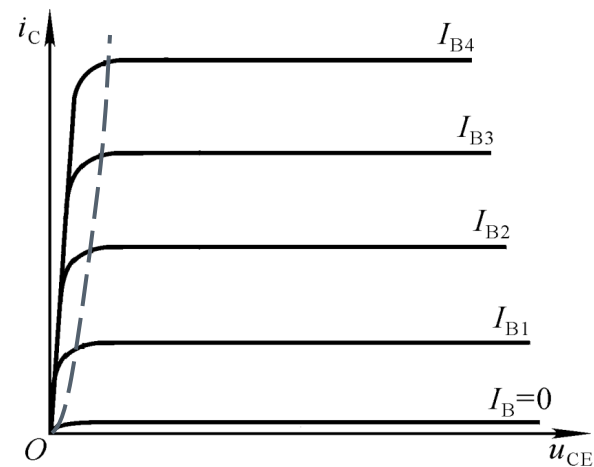
$$V_{BE} = 0.7V, V_{CE} < 1V$$

Active region: i_c is basically parallel with v_{ce} , $\beta i_b = i_c$

$$V_{BE} = 0.7V, V_{CE} > 1V$$

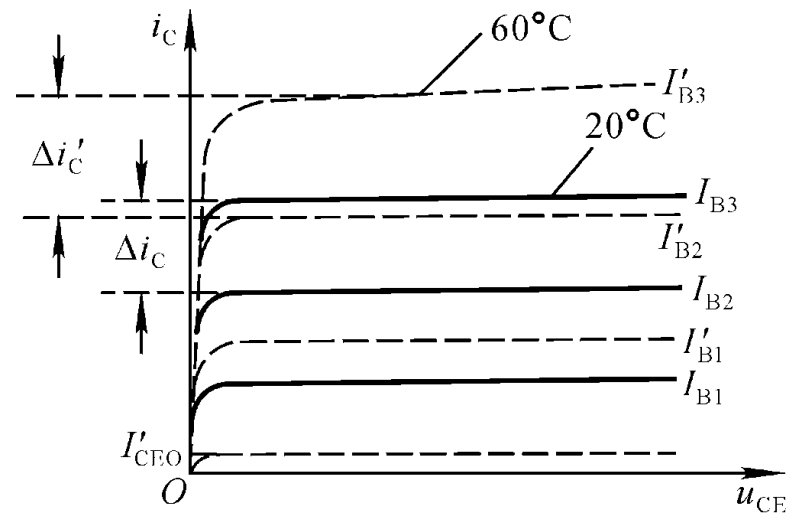
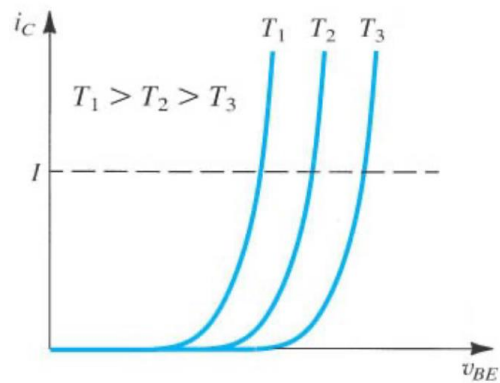
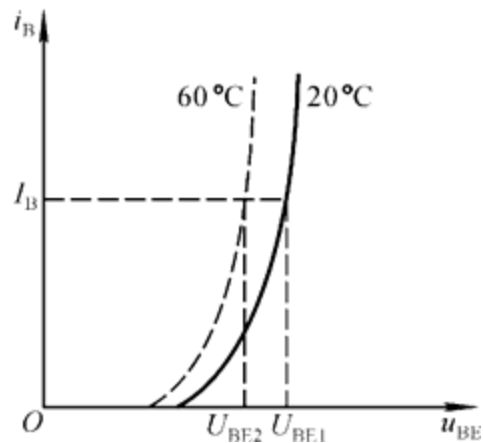
Cutoff region: i_c is approaching to 0, $i_b \approx i_c \approx 0$

$$V_{BE} < 0.5V$$

 $u_{BE} - i_C$  $u_{BE} - i_B$  $u_{CE} - i_C$

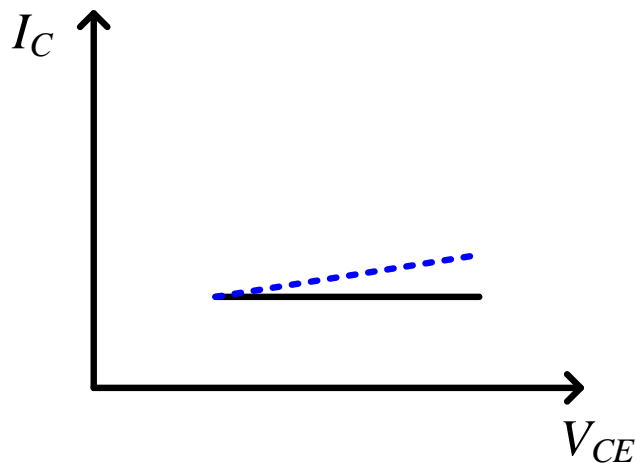


Effects of temperature:





Early effects:



The effects of early voltage on transconductance:

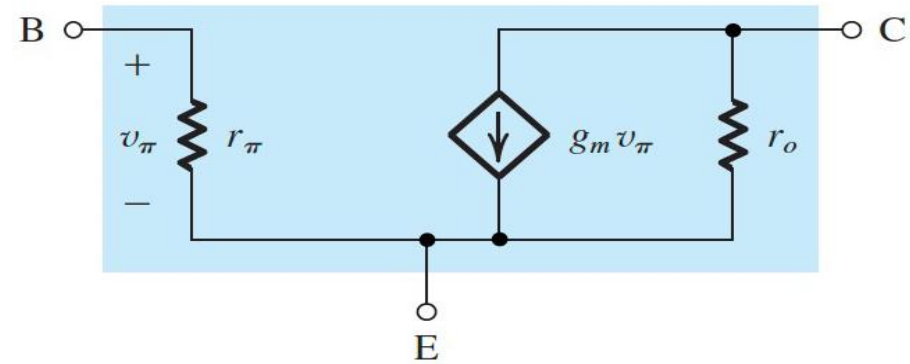
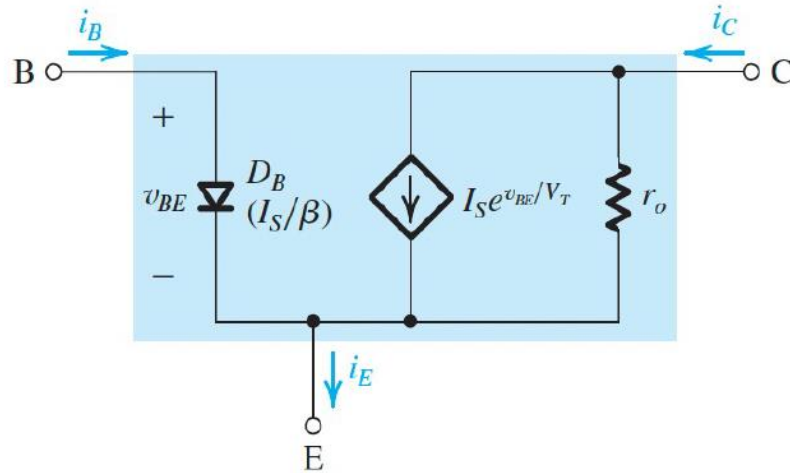
$$g_m = \frac{dI_C}{dV_{BE}} = \frac{I_S}{V_T} e^{\frac{V_{BE}}{V_T}} \left(1 + \frac{V_{CE}}{V_A} \right) = \frac{I_C}{V_T}$$

Not change

$$I_C = I_S e^{\frac{V_{BE}}{V_T}} \left(1 + \frac{V_{CE}}{V_A} \right) \quad V_A \text{ is early voltage}$$



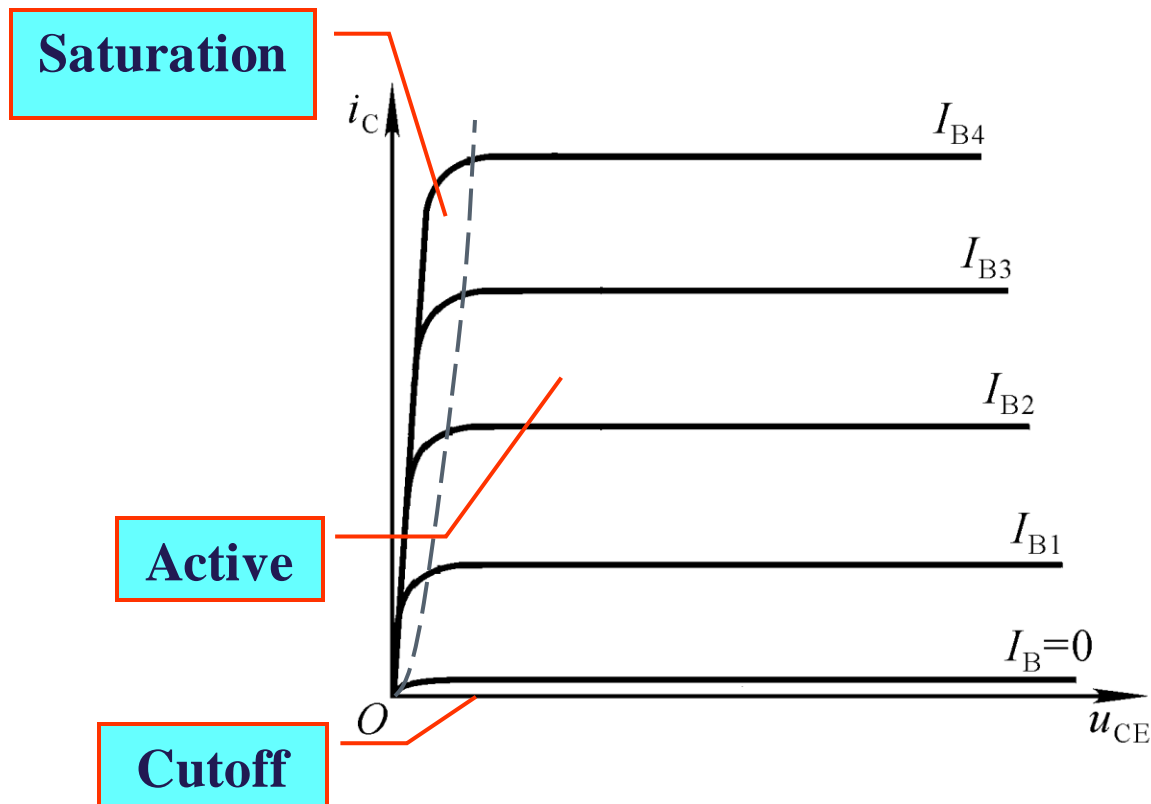
Inclusion of early effect in large-signal and small-signal models:



$$r_o = \frac{V_A}{I_S e^{\frac{v_{BE}}{V_T}}} \approx \frac{V_A}{I_C}$$



Power amplifier:





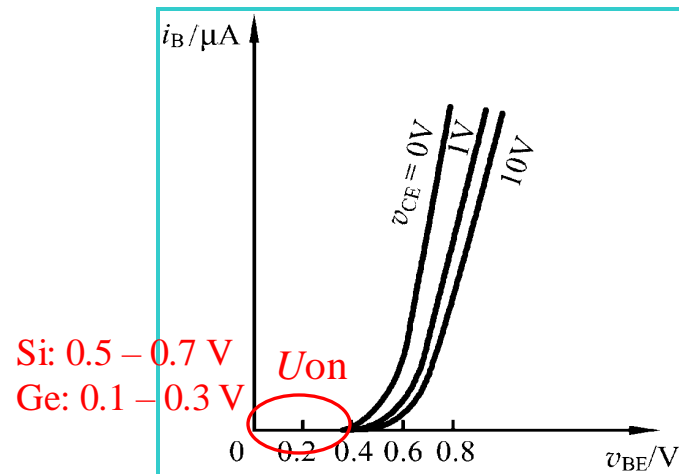
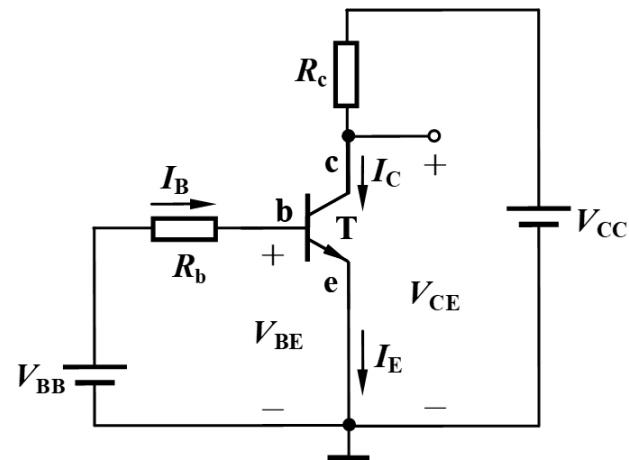
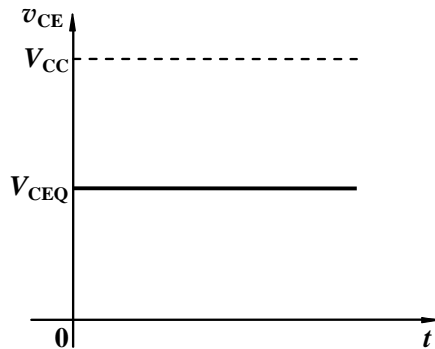
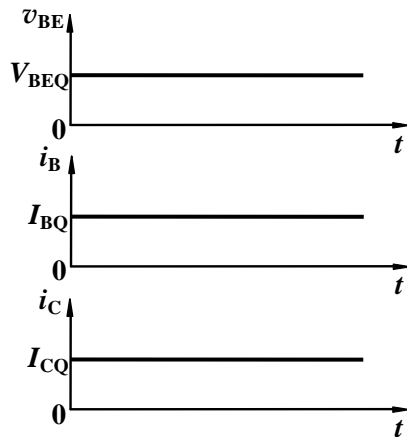
DC biasing (Static operating point (Q point)):

$$I_{BQ} = \frac{V_{BB} - V_{BEQ}}{R_b}$$

$$I_{CQ} \approx \beta \cdot I_{BQ}$$

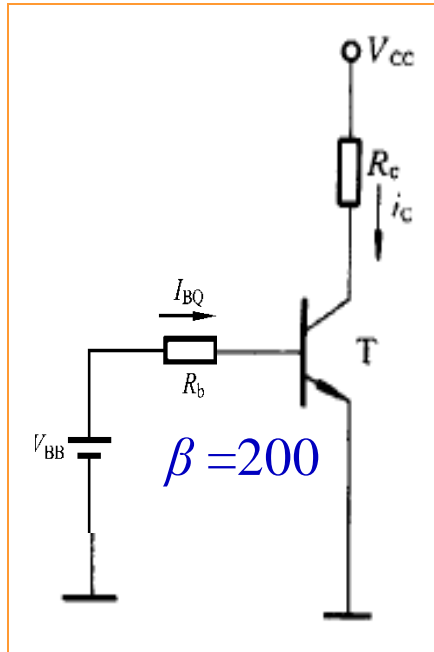
$$V_{CEQ} = V_{CC} - I_{CQ}R_c$$

$$Q(I_{BQ}, I_{CQ}, V_{CEQ})$$





Calculate Q point:



$$V_{CC}=15\text{V}, R_C=1.5\text{k}\Omega, i_B=20\mu\text{A}$$

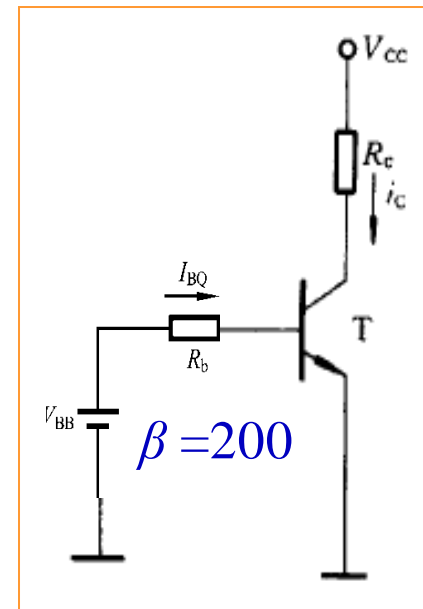
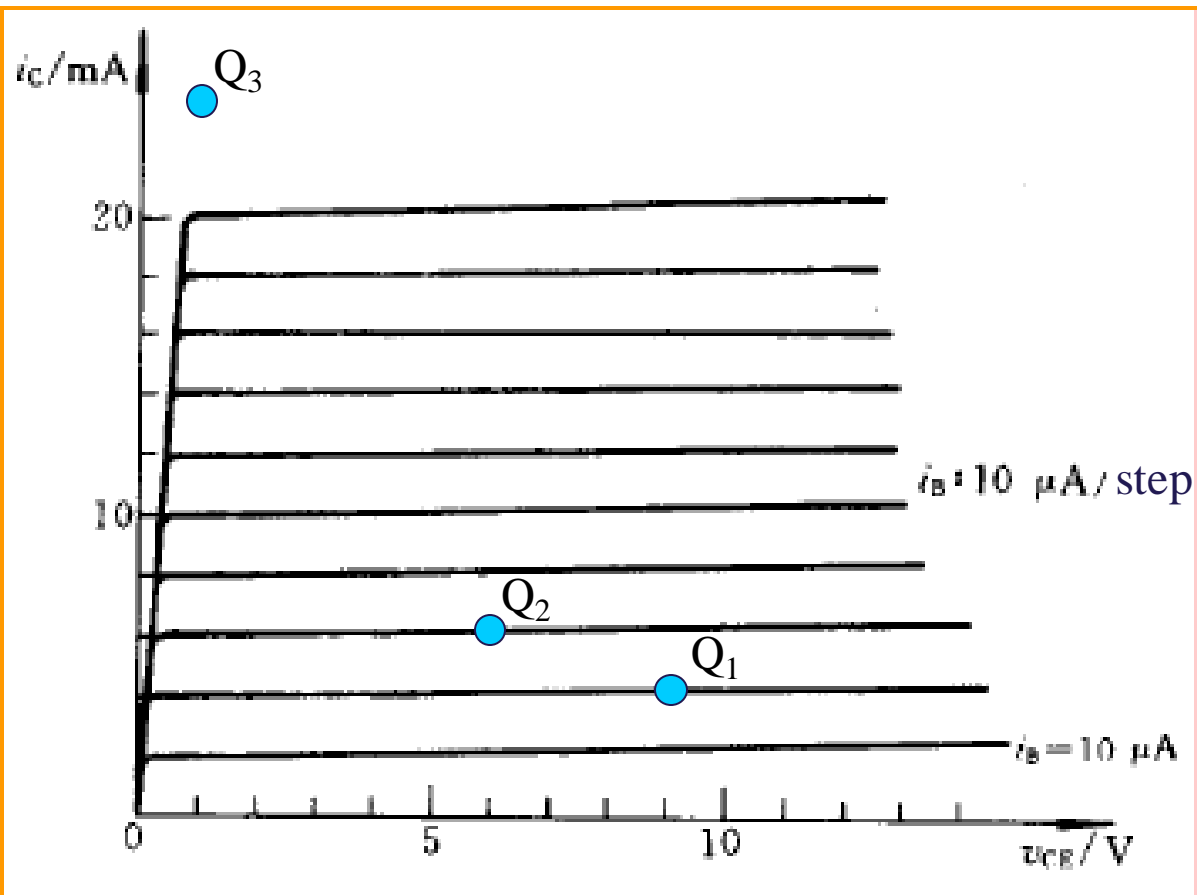
$$Q(20\mu\text{A}, 4\text{mA}, 9\text{V})$$

$$V_{CC}=12\text{V}, R_C=1\text{k}\Omega, V_{BB}=2.2\text{V}, R_b=50\text{k}\Omega, V_{BEQ}=0.7\text{V}$$

$$Q(30\mu\text{A}, 6\text{mA}, 6\text{V})$$

$$V_{CC}=6\text{V}, R_C=200\Omega, V_{BB}=3.2\text{V}, R_b=20\text{k}\Omega, V_{BEQ}=0.7\text{V}$$

$$Q(125\mu\text{A}, 25\text{mA}, 1\text{V})$$



$Q_1(20\mu\text{A}, 4 \text{ mA}, 9 \text{ V})$

$Q_2(30\mu\text{A}, 6 \text{ mA}, 6 \text{ V})$

$Q_3(125\mu\text{A}, 25 \text{ mA}, 1 \text{ V})$

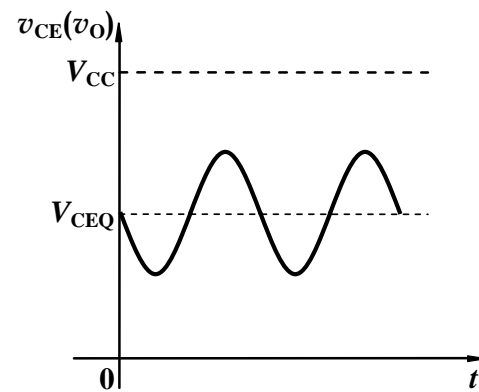
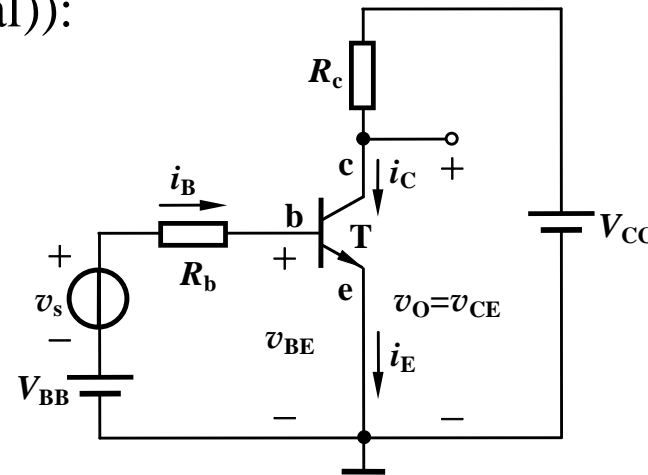
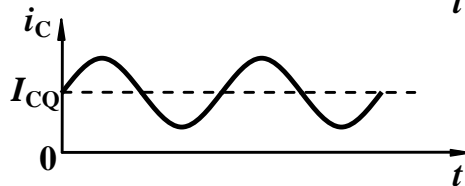
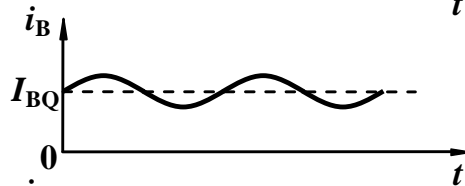
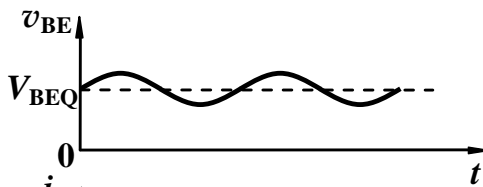


With a perturbation (a sinusoidal signal (alternating signal)):

$$i_B = \frac{V_{BB} + v_s - V_{BEQ}}{R_b}$$

$$i_C = \beta \cdot i_B$$

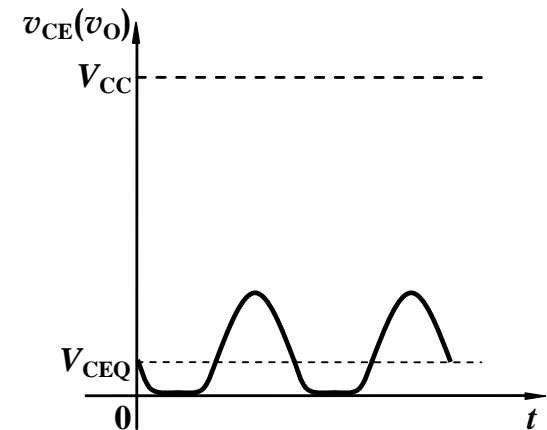
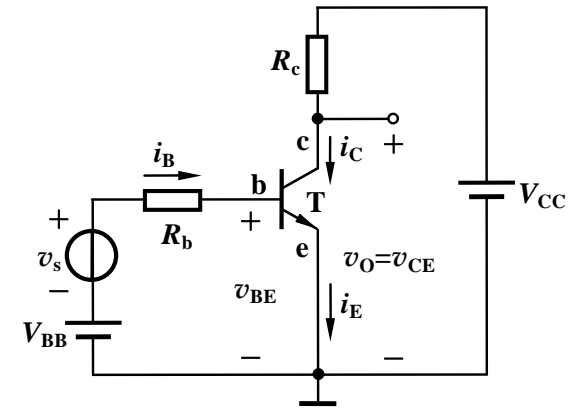
$$v_{CE} = V_{CC} - i_C R_c$$





The effects of static operating point on output voltage

- $I_{BQ} \uparrow \longrightarrow I_{CQ} \uparrow \longrightarrow \text{the voltage on } R_c \uparrow$
 $\longrightarrow V_{CEQ} \downarrow$
- $R_c \uparrow \longrightarrow \text{the voltage on } R_c \uparrow \longrightarrow V_{CEQ} \downarrow$



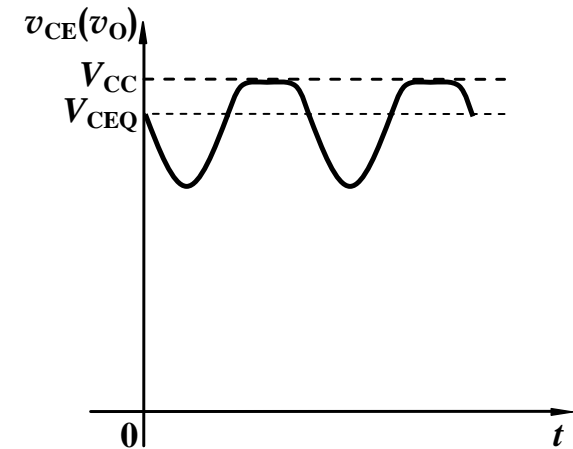
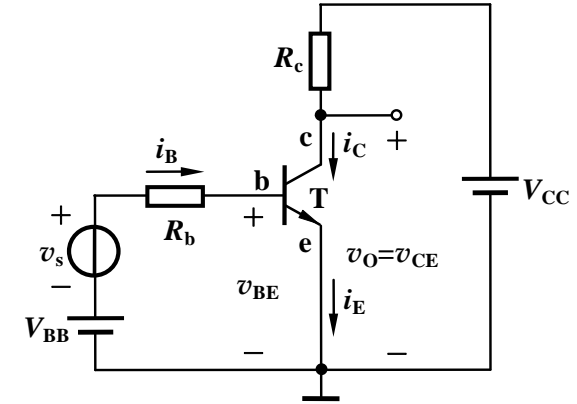


The effects of static operating point on amplification

- $I_{BQ} \downarrow \longrightarrow I_{CQ} \downarrow \longrightarrow \text{the voltage on } R_c \downarrow$
 $\longrightarrow V_{CEQ} \uparrow$

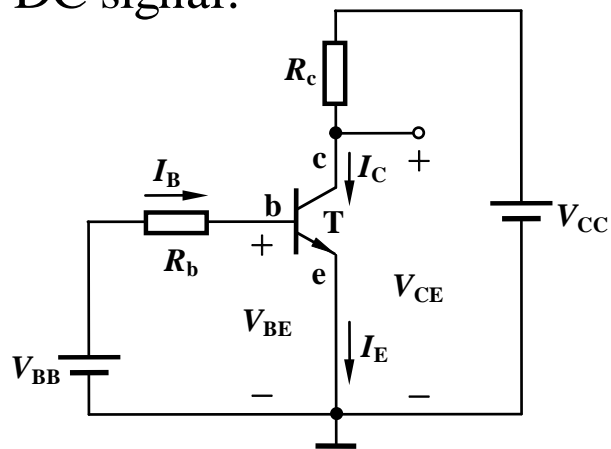
A proper static operating point should be provided to make the transistor operate at the active mode (amplification region).

The amplitude of output signal is limited by V_{CC} .

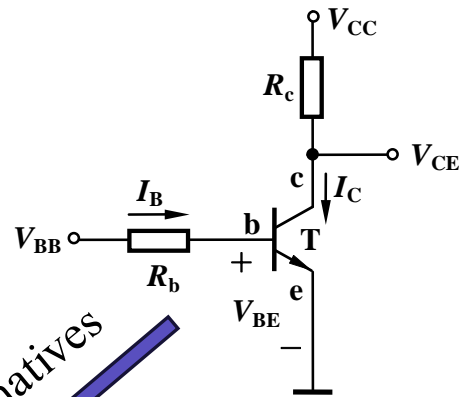




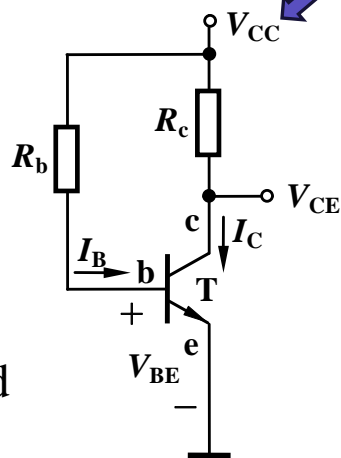
For DC signal:



Simplified



Alternatives



Only one DC
power is involved

Q point:

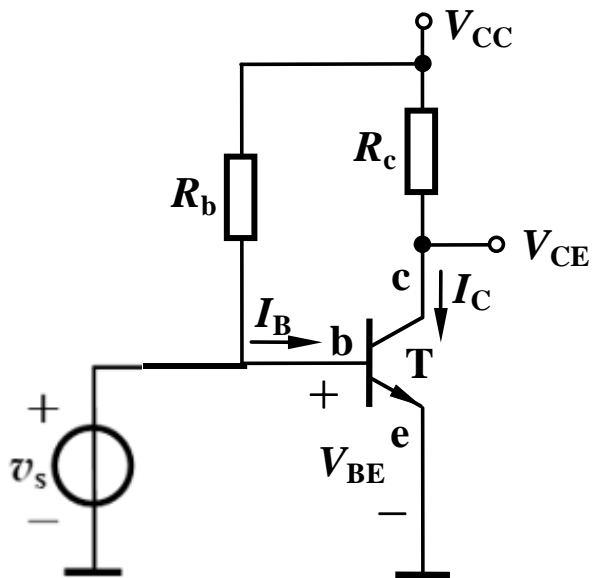
$$I_{BQ} = \frac{V_{CC} - V_{BEQ}}{R_b}$$

$$I_{CQ} = \beta \cdot I_{BQ}$$

$$V_{CEQ} = V_{CC} - I_{CQ} R_c$$



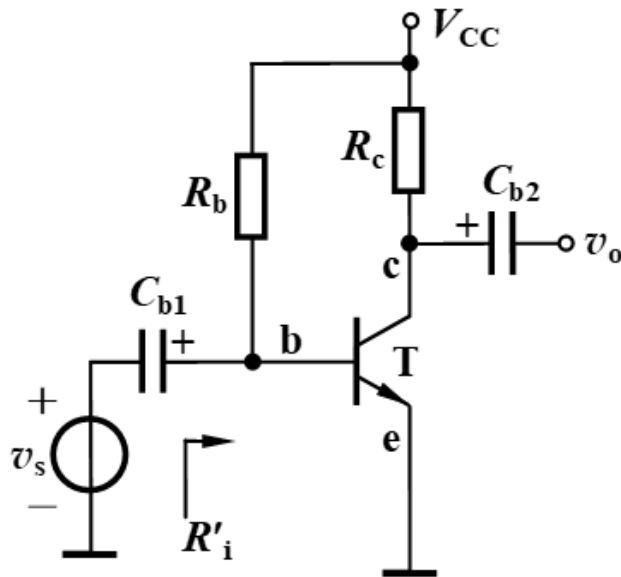
When AC signal is added directly:



What will happen when $v_s = 0$?



When AC signal is added with capacitors:



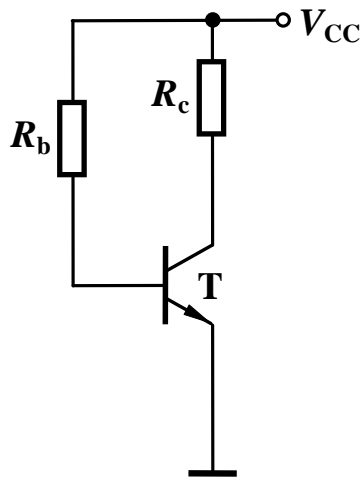
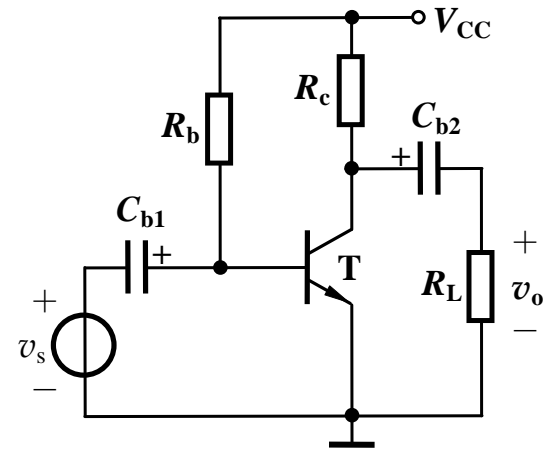
Two capacitors are added at input and output ends to isolate DC and AC signals.

The involvements of v_s and v_o do not affect the Q point of the circuit.

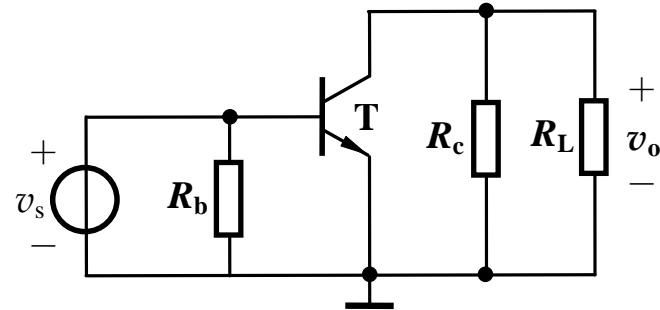
The frequency of v_s can not be too small.



DC circuit and AC circuit:



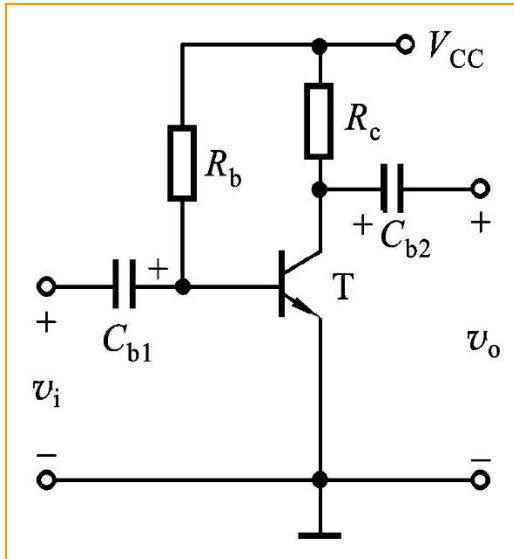
DC circuit



AC circuit

DC circuit: capacitor is open, AC source is open;

AC circuit: capacitor is short, DC source is short;



$$\beta = 80, R_b = 300\text{k}\Omega, R_c = 2\text{k}\Omega, V_{CC} = +12\text{V}$$

V_{BEQ} is assumed to be 0

Calculate Q point, which region does the BJT operate?

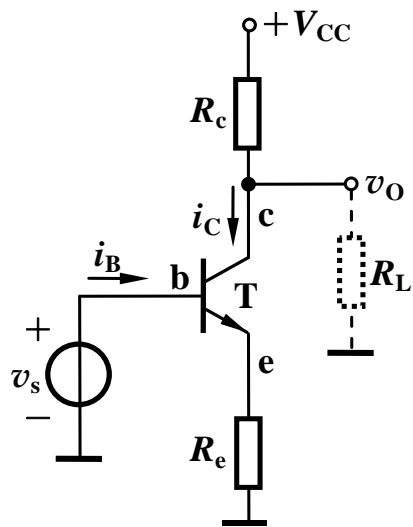
Q ($40\mu\text{A}$, 3.2mA , 5.6V) Active region

If $R_b = 100\text{k}\Omega$,

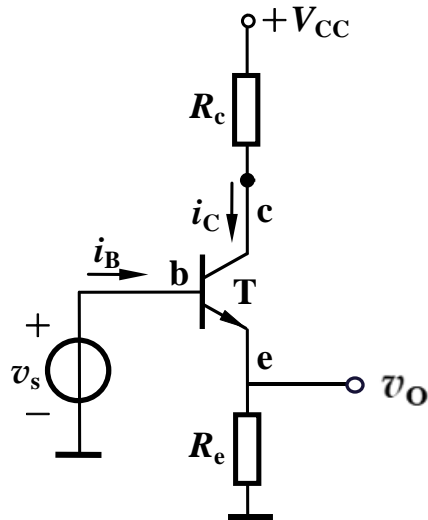
Q ($120\mu\text{A}$, 6.0mA , 0V) Saturation region

If $R_b = 300\text{k}\Omega$, $R_c = 5\text{k}\Omega$

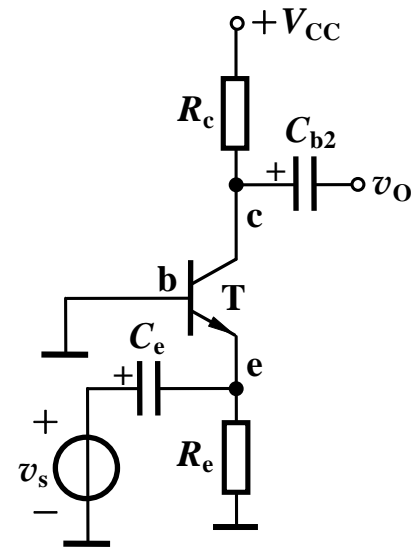
Q ($40\mu\text{A}$, 2.4mA , 0V) Saturation region



Common emitter



Common collector



Common base

Common emitter: signal is input from the base, and output from the collector;

Common collector: signal is input from the base, and output from the emitter;

Common base: signal is input from the emitter, and output from the collector;



Thanks