

# Analog electronics

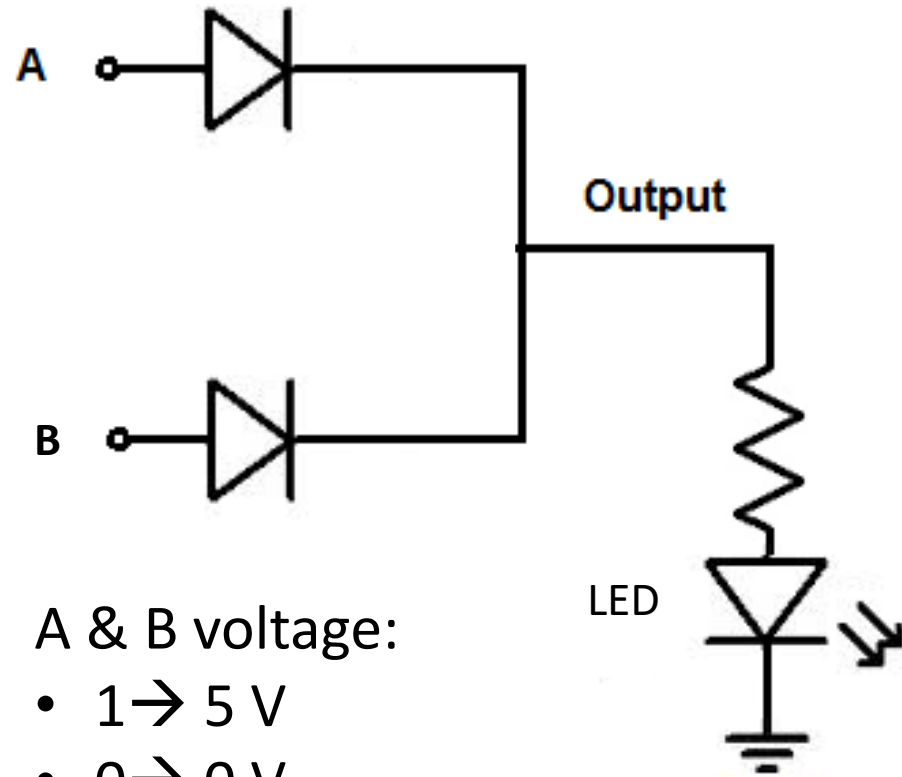
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# Agenda

- Diode
  - Recap diode circuit analysis principle, practical diode circuits, solutions to assignments
  - Practical diode circuits:
    - Clipper or limiter
    - Voltage doubler/multiplier
  - Small signal model

# Recap: application example: OR logic gate



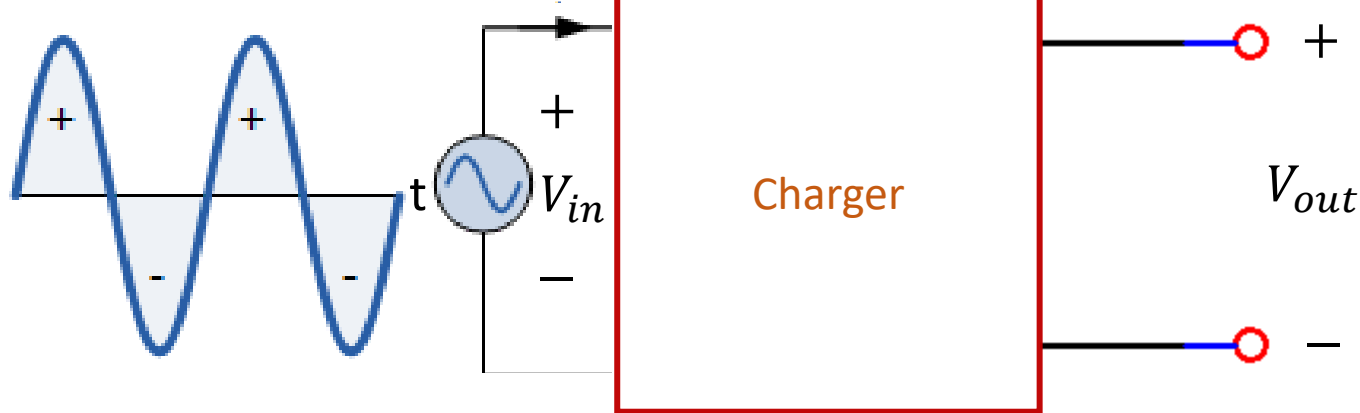
A	B	LED
0	0	0 (off)
0	1	1 (on)
1	0	1 (on)
1	1	1 (on)

The LED forward voltage drop is 2 V.

# PN junction diode application example: charger/adaptor

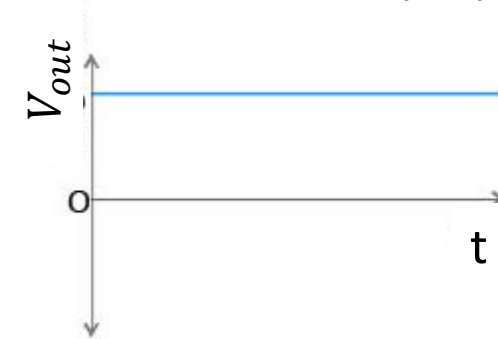


$$V_{in}(t) = 230\sin(2\pi 50t)$$



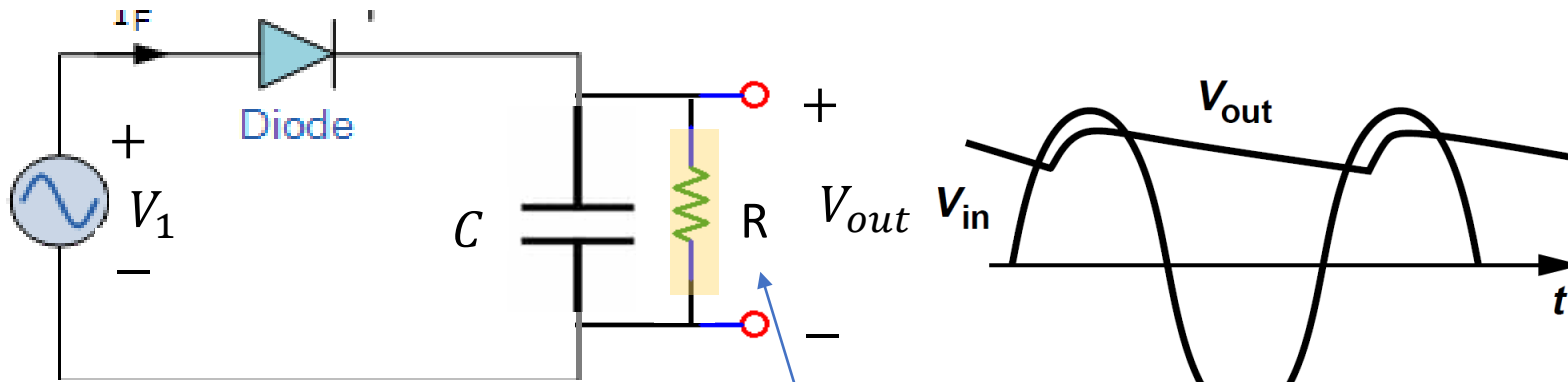
$V_{out}$ :

- 5 V for cellphone
- 20 V for laptop



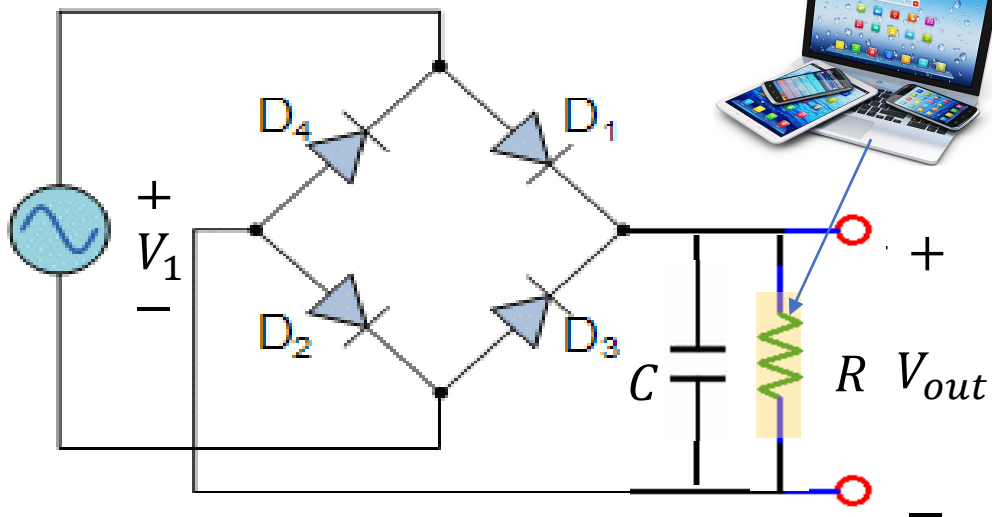
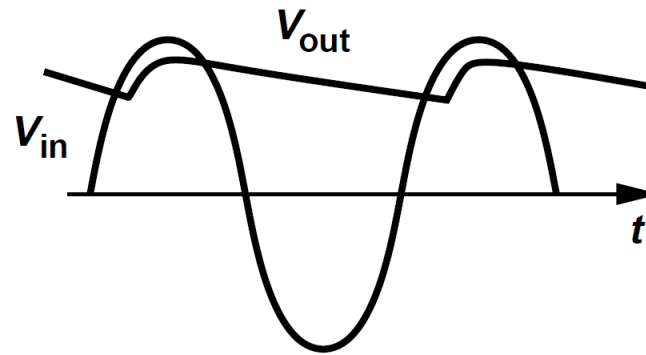
Alternating Current (AC)  
Direct Current (DC)  
Rectifier: convert AC to DC

# Recap: Half-wave rectifier Vs. Full-wave rectifier with capacitor and load



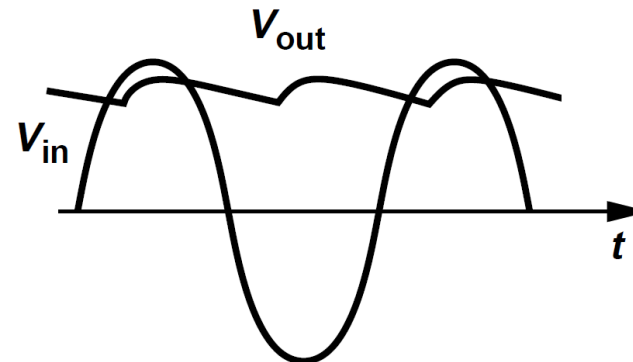
$$\text{Ripple amplitude} = \frac{V_o - V_{D,on}}{fRC}$$

$$\text{Max reverse voltage} = 2V_o - V_{D,on}$$



$$\text{Ripple amplitude} = \frac{V_o - 2V_{D,on}}{2fRC}$$

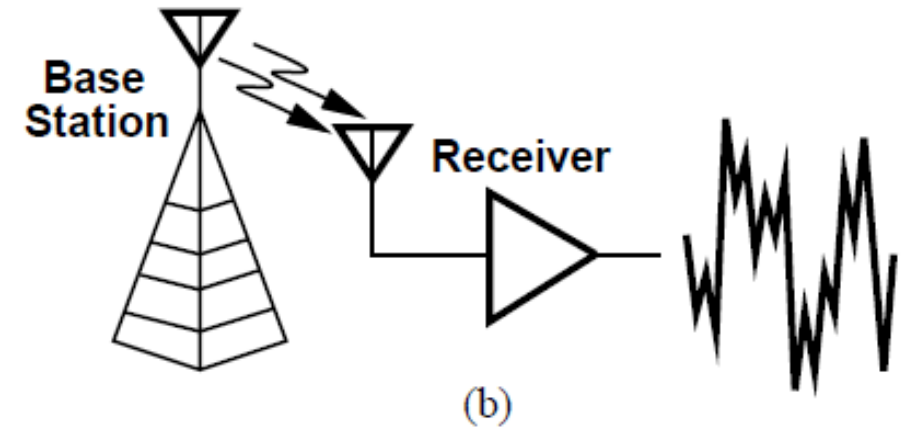
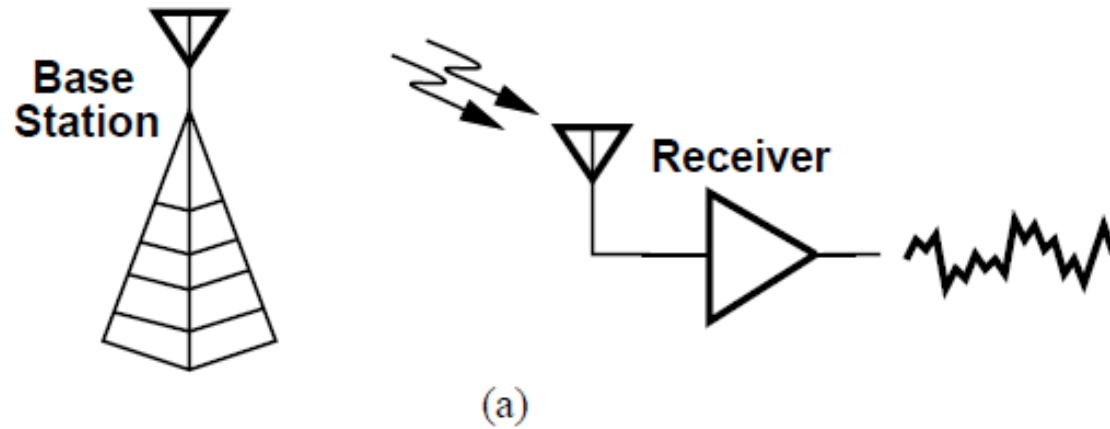
$$\text{Max reverse voltage} = V_o - V_{D,on}$$



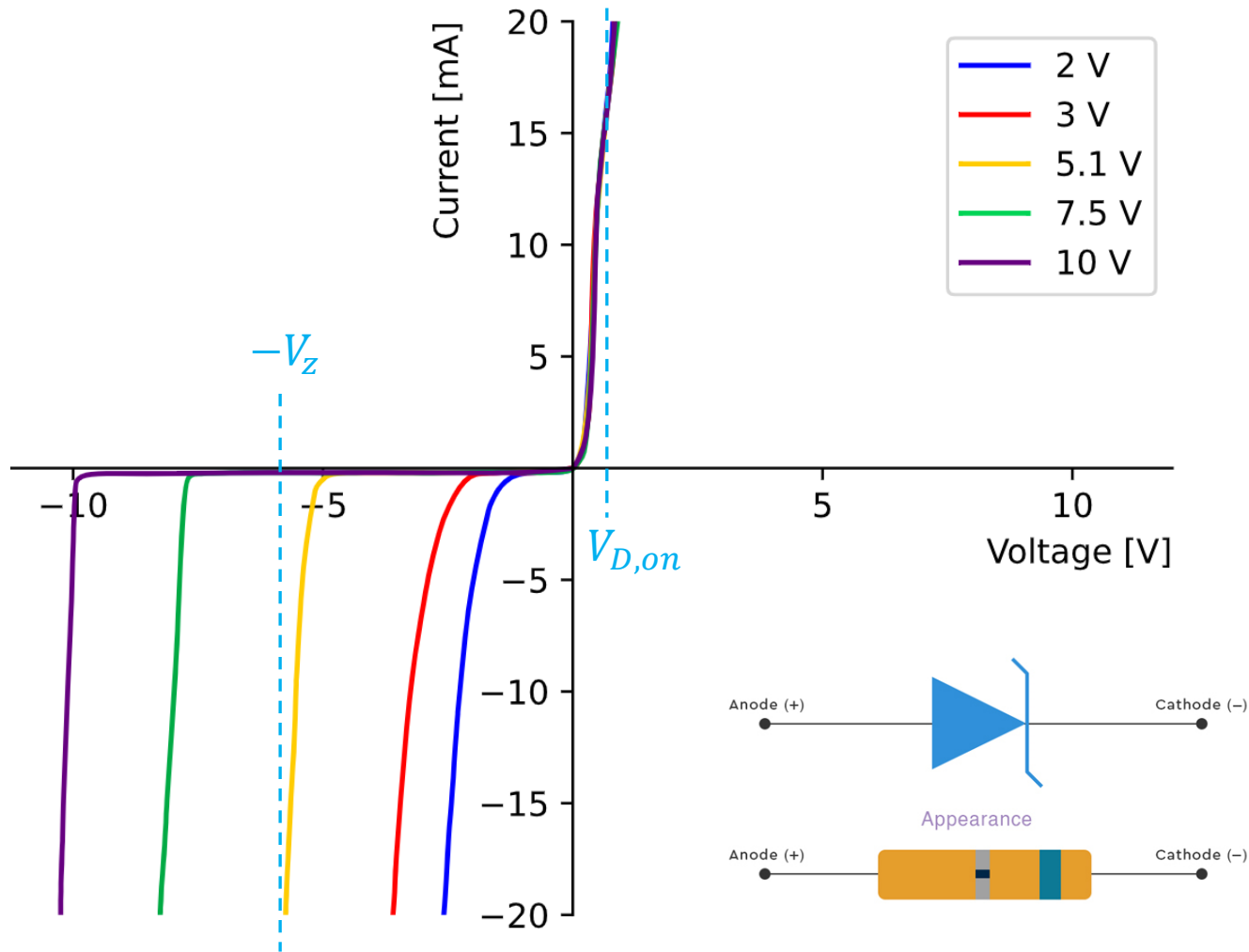
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  - Small signal model

# Clipper/limiting circuits



# Zener diode

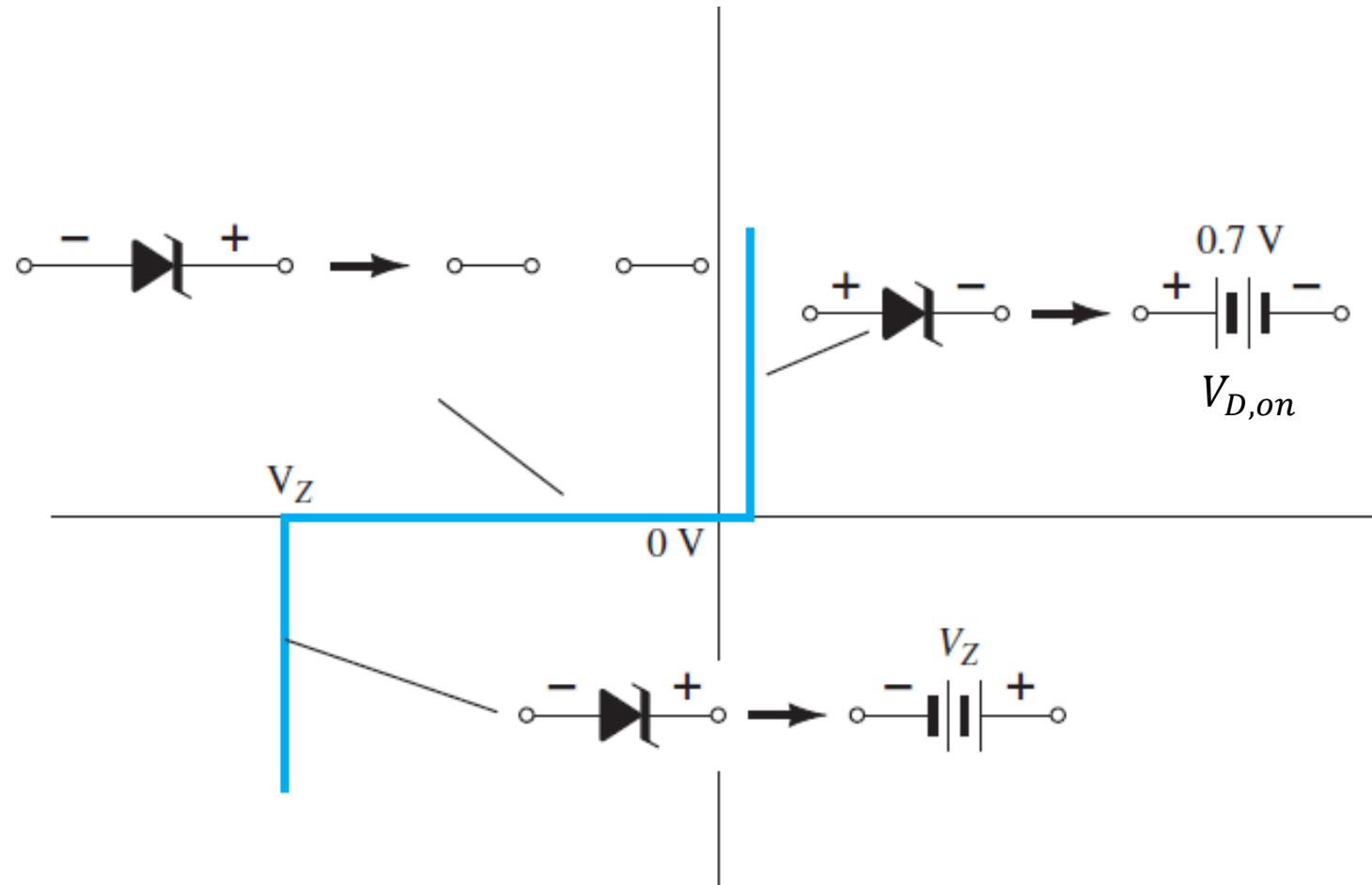


- Designed to work in the reverse breakdown region.
- Stable and predicable voltage drop.
- Often used for clipper and limiter circuits.

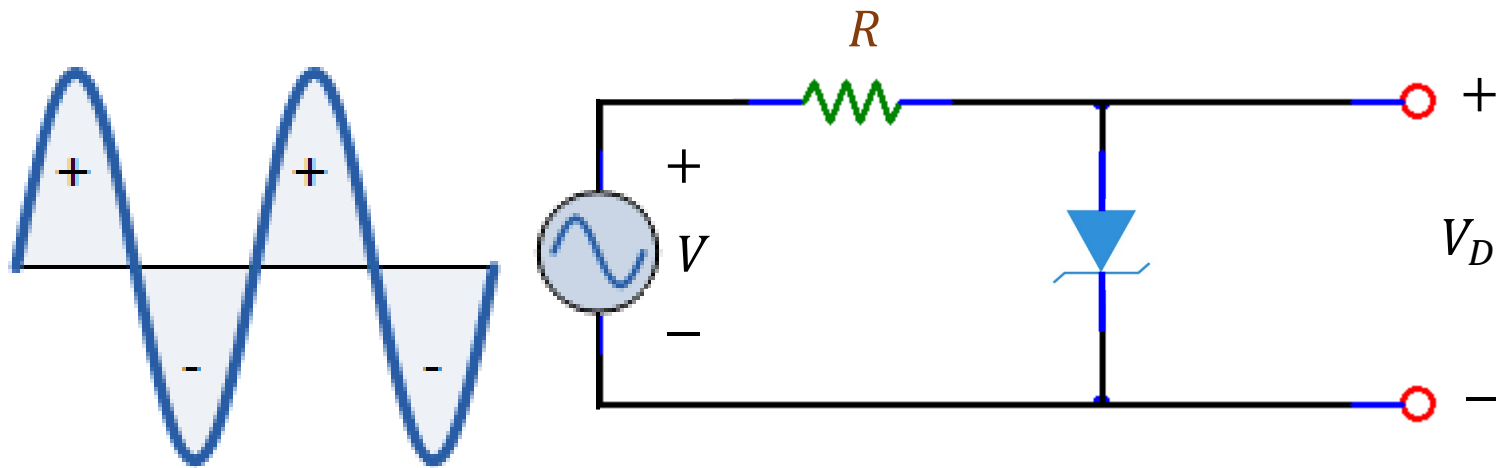
Device	Zener Voltage	
	Min.	Max.
BZX79C2V4	2.2	2.6
BZX79C2V7	2.5	2.9
BZX79C3V0	2.8	3.2
BZX79C3V3	3.1	3.5
BZX79C3V6	3.4	3.8
BZX79C3V9	3.7	4.1
BZX79C4V3	4	4.6
BZX79C4V7	4.4	5
BZX79C5V1	4.8	5.4
BZX79C5V6	5.2	6
BZX79C6V2	5.8	6.6
BZX79C6V8	6.4	7.2
BZX79C7V5	7	7.9
BZX79C8V2	7.7	8.7
BZX79C9V1	8.5	9.6
BZX79C10	9.4	10.6
BZX79C11	10.4	11.6
BZX79C12	11.4	12.7
BZX79C13	12.4	14.1
BZX79C15	13.8	15.6
BZX79C16	15.3	17.1
BZX79C18	16.8	19.1
BZX79C20	18.8	21.2
BZX79C22	20.8	23.3
BZX79C24	22.8	25.6



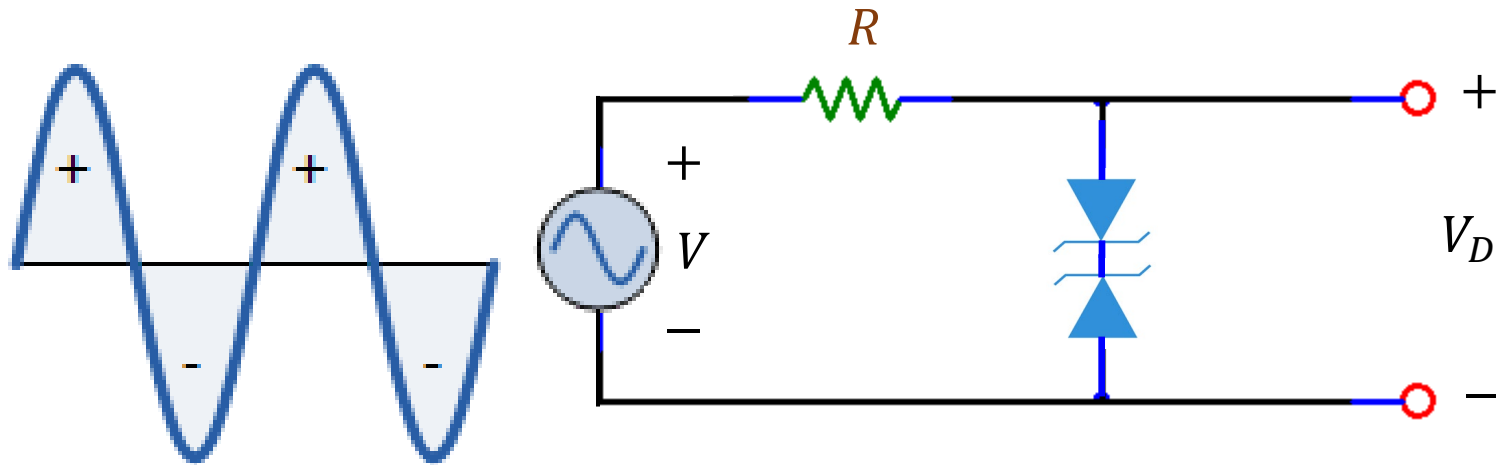
# Zener diode—constant voltage drop model



# Quiz: Clipper/limiting circuits



# Clipper/limiting circuits



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# Voltage doubler circuits

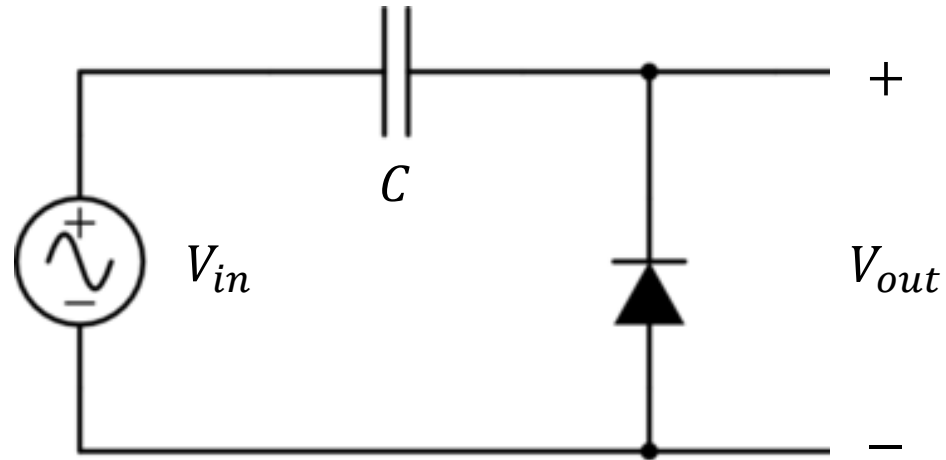
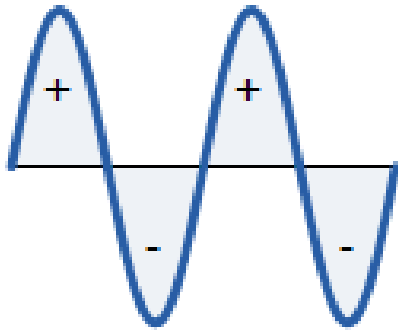


Passports with RFID (Radio-Frequency Identification) chips do not have batteries.

The reader emits radio waves that power the passive RFID chip in the passport.

# Voltage doubler circuits

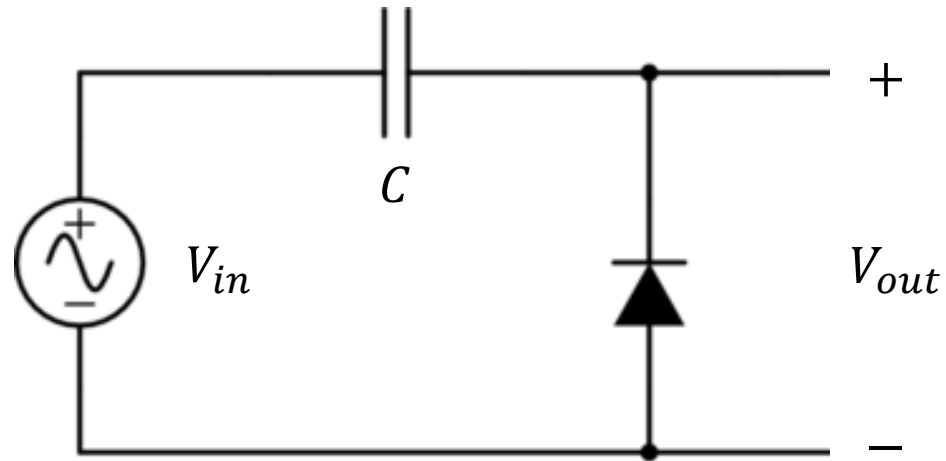
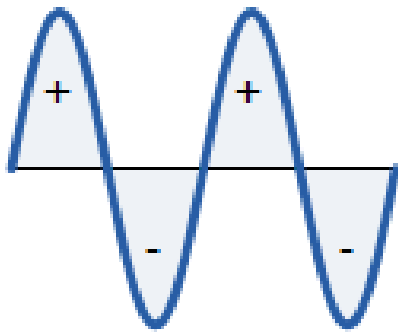
$$V_{in}(t) = V_o \sin(2\pi f t)$$



Assume ideal diode model

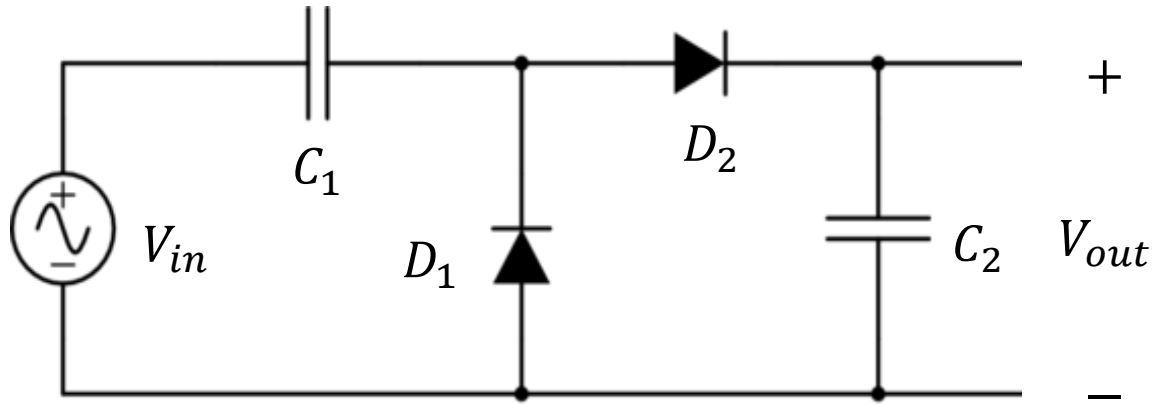
# Quiz

$$V_{in}(t) = V_o \sin(2\pi f t)$$



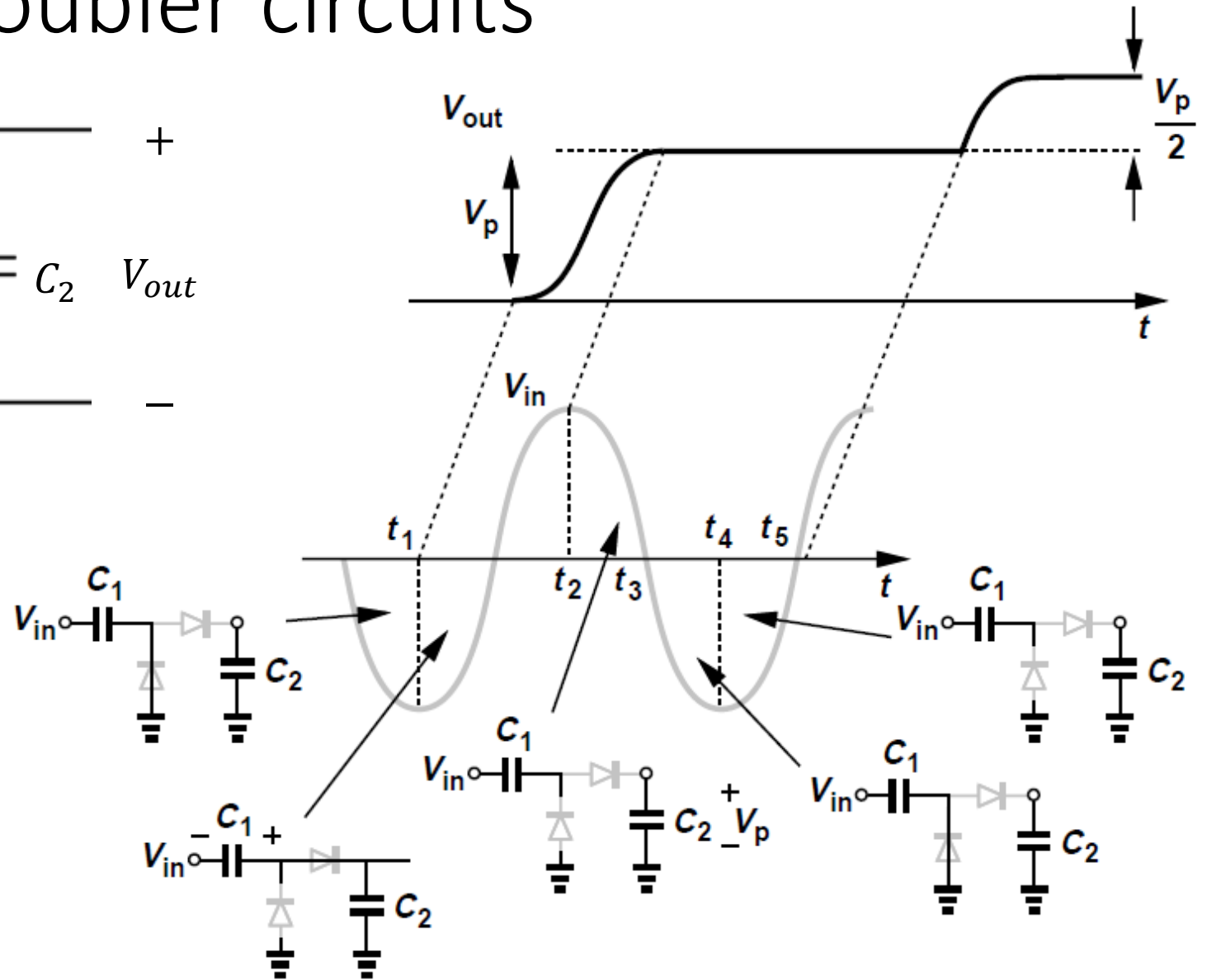
Assume constant voltage drop model

# Actual voltage doubler circuits



$$V_{in}(t) = V_p \sin(2\pi f t)$$

Assume ideal diode model





# LTspice simulation: voltage doubler

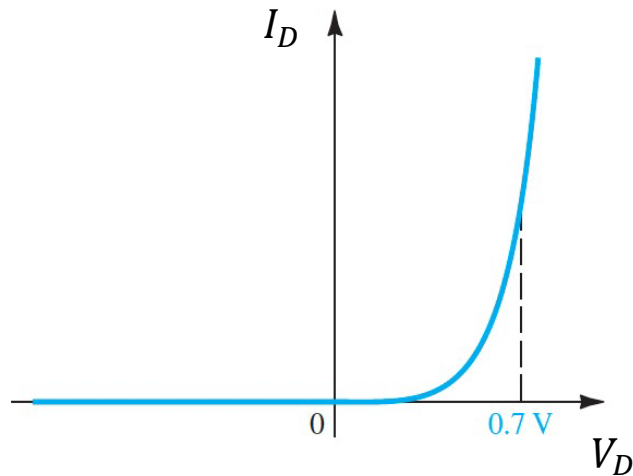
- $V = 3 \sin(2\pi 50t + \pi)$
- $C1 = C2 = 0.0001 \text{ F}$
- Diodes: 1N4007

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# PN diode models

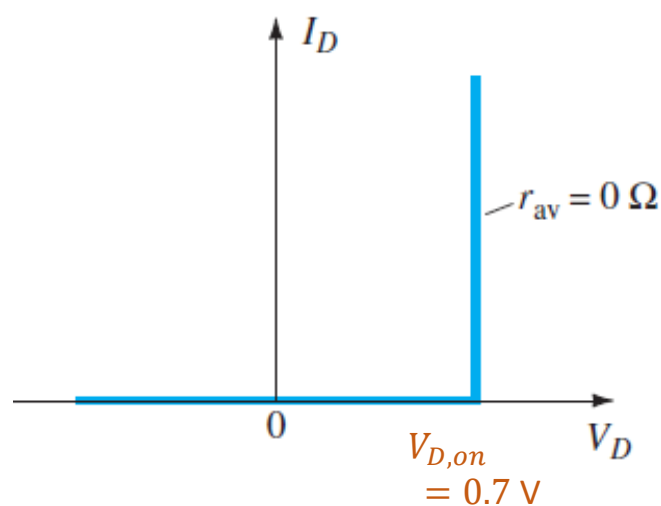
Exponential model  
(usage rate = 10-20%)



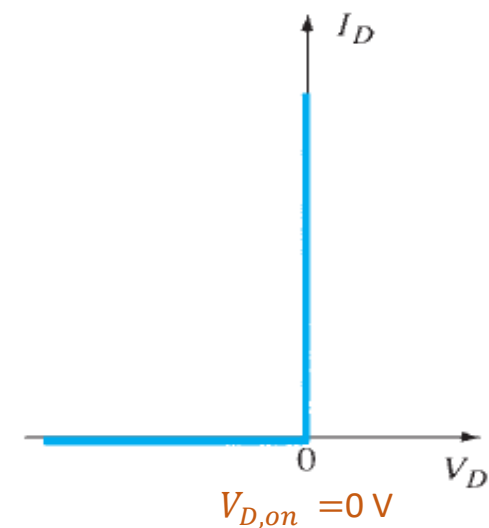
$$I_D \approx I_S e^{\frac{V_D}{V_T}}$$

Simplify calculation  
Approximate results

Constant voltage model  
(usage rate = 70-80%)

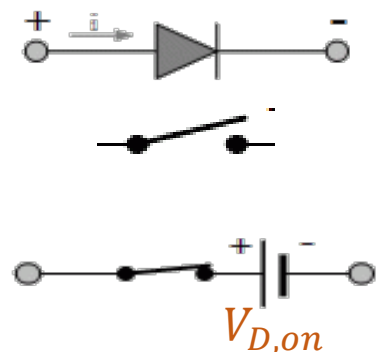


Ideal model  
(usage rate = 10-20%)

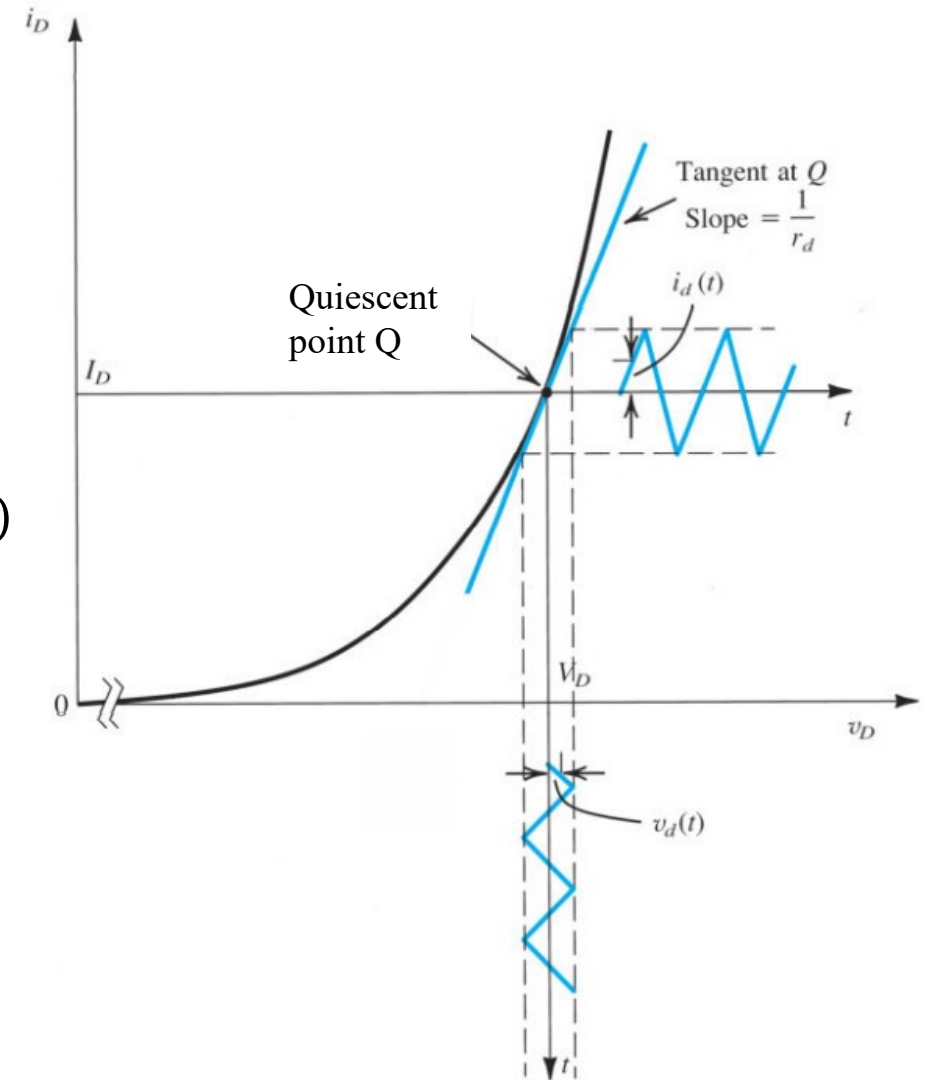
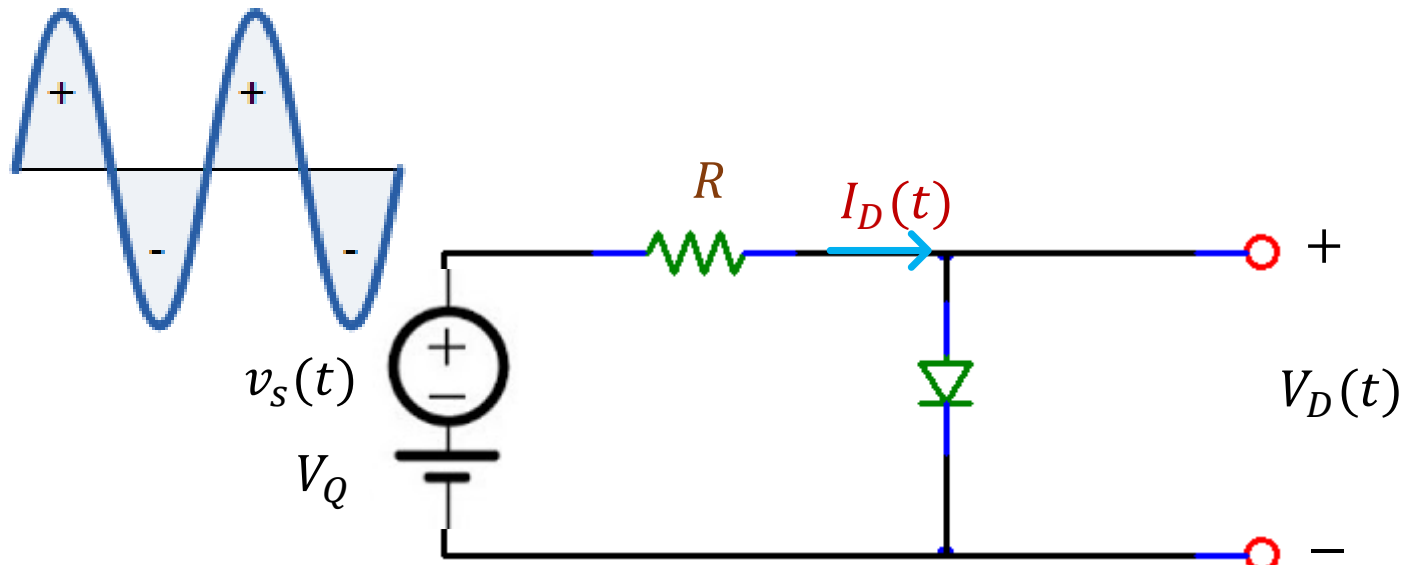


The diode has two states:

- $V_D < V_{D,on} \rightarrow$  diode is off  $\rightarrow$  open circuit
- $V_D \geq V_{D,on} \rightarrow$  diode is on  $\rightarrow$  a voltage drop

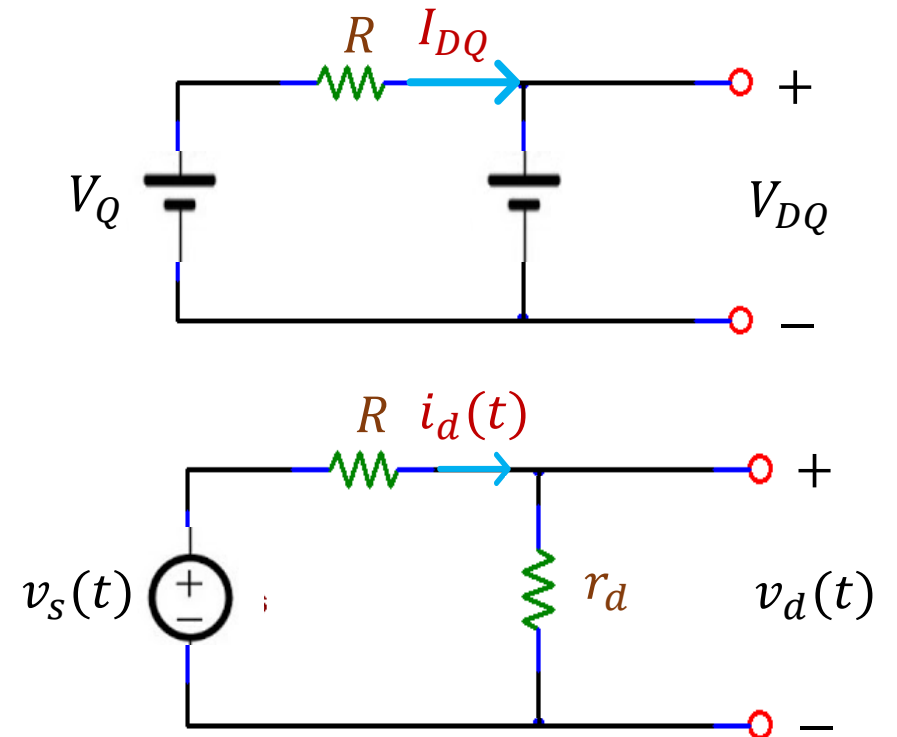
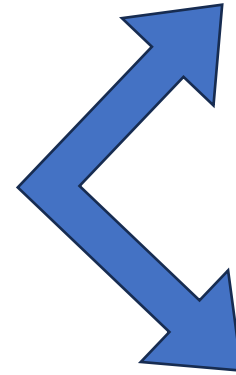
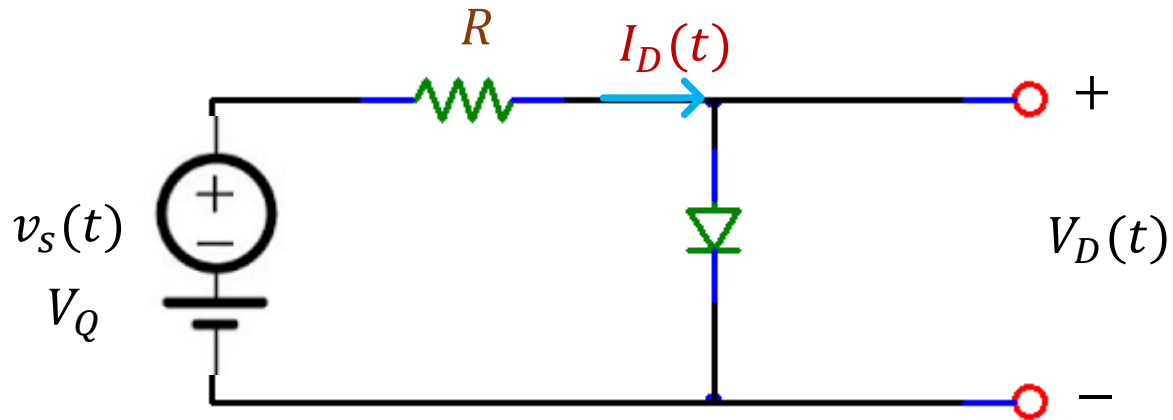


# Small-signal model



# Procedure

- DC analysis to get  $I_{DQ}$ .
- Calculate the diode small-signal resistance  $r_d = \frac{V_T}{I_{DQ}} \big|_{V_{DQ}}$ .
- $v_d(t) = \frac{v_s(t)r_d}{r_d+R}$

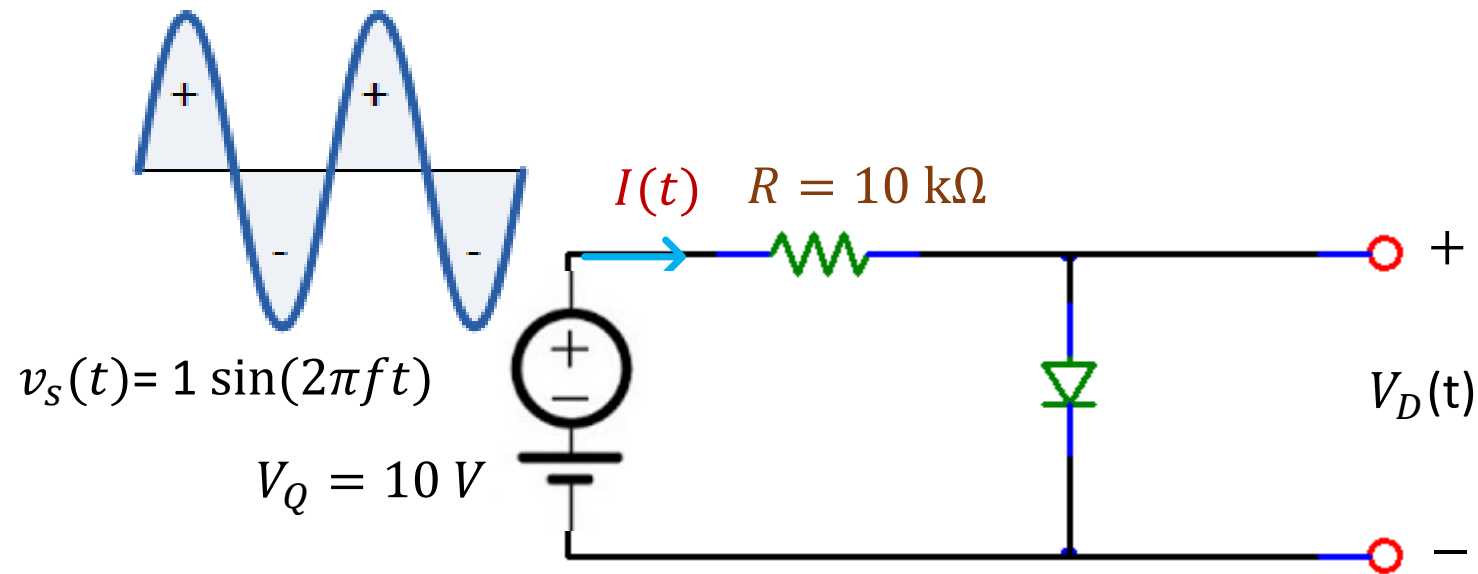


# Quiz: Small-signal model

The DC current of a diode is 1 mA.

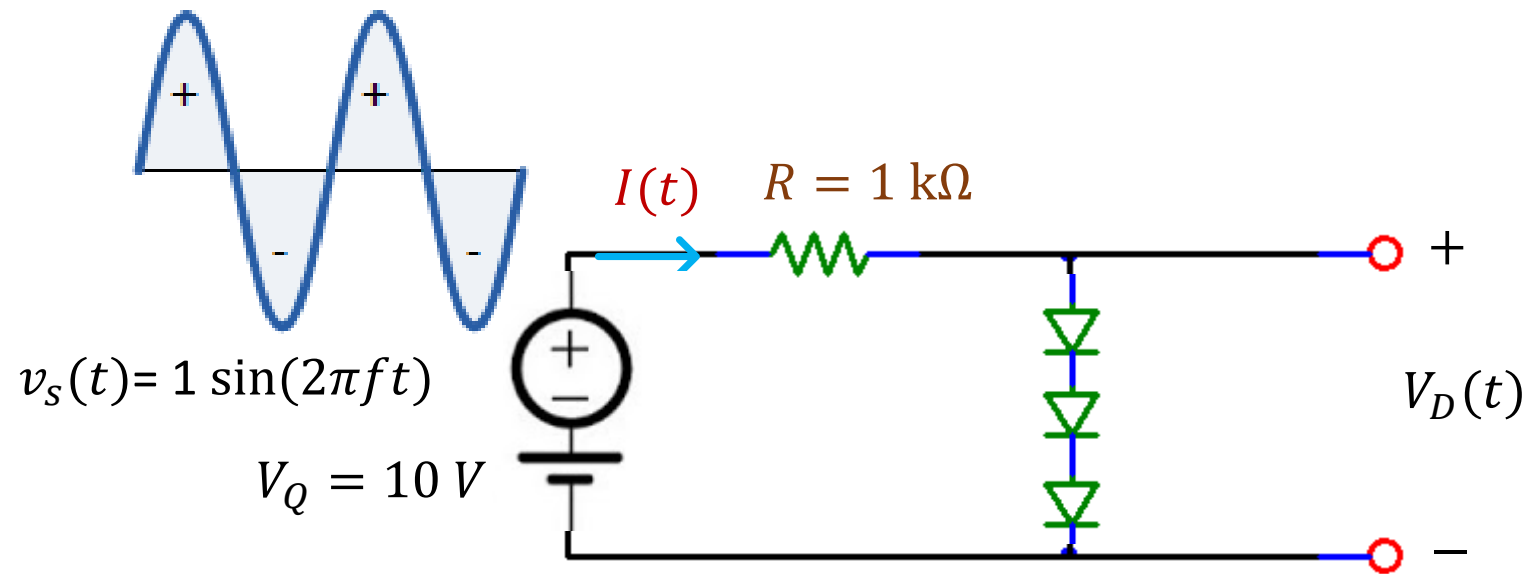
- (a) Determine the current change if  $V_D$  changes by 1 mV.
- (b) Determine the voltage change if  $I_D$  changes by 10%.

# example: small signal model



The voltage drop across the diode  $V_{DQ} = 0.7\text{ V}$  when only the DC voltage is applied.

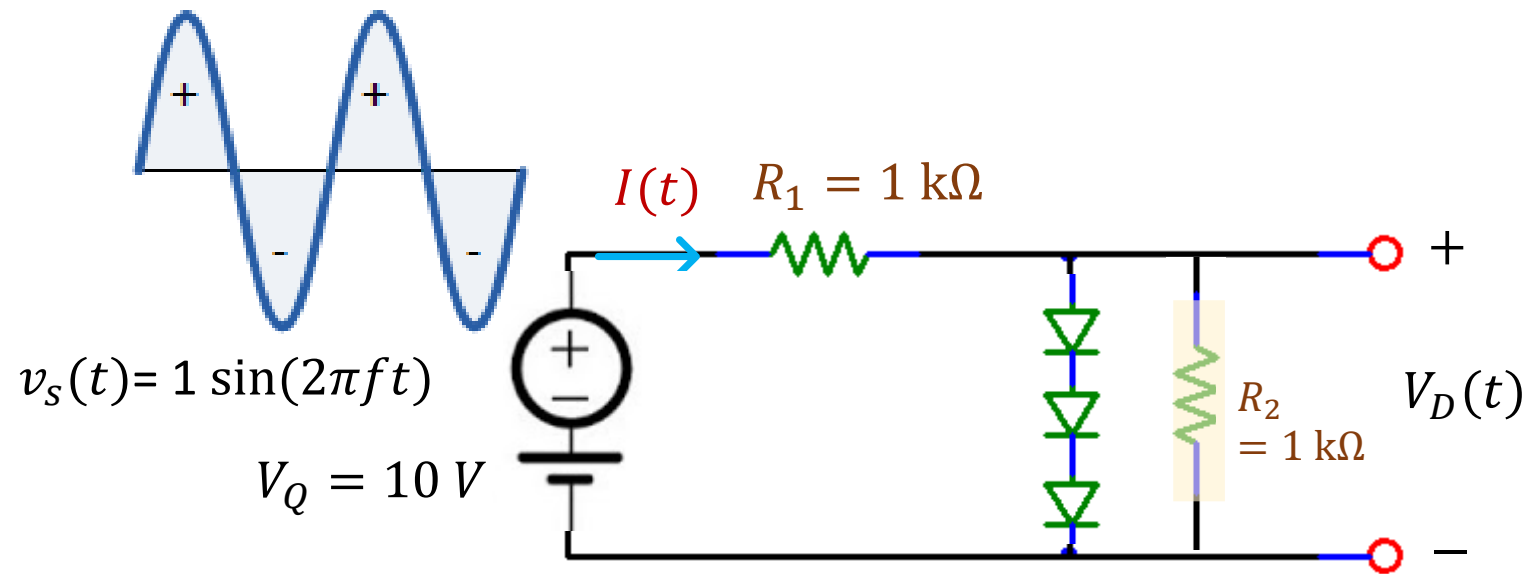
# exercise: small signal model



The voltage drop across each diode is  $V_{DQ} = 0.7 \text{ V}$  when only the DC voltage is applied.



# exercise: small signal model



The voltage drop across each diode is  $V_{DQ} = 0.7$  V when only the DC voltage is applied.

# Small-signal model approximation error

$$I_D(t) = I_s e^{[V_{DQ} + v_d(t)]/nV_T} = I_s e^{V_{DQ}/nV_T} e^{v_d(t)/nV_T} = I_{DQ} e^{v_d(t)/nV_T}$$

$$I_D(t) = I_{DQ} + i_d(t)$$

$$\rightarrow i_d(t) = I_D(t) - I_{DQ} = I_{DQ} (e^{v_d(t)/nV_T} - 1) \quad \text{actual } i_d(t)$$

$$\text{Small-signal approximated } i_d(t): \hat{i}_d(t) = I_{DQ} v_d(t)/nV_T$$

$$\rightarrow \frac{i_d(t)}{\hat{i}_d(t)} = \frac{e^{v_d(t)/nV_T} - 1}{v_d(t)/nV_T}$$

$v_d(t)/nV_T$	0.1	0.2	0.3	0.4	0.5	0.6	0.7
$\frac{i_d(t)}{\hat{i}_d(t)}$	1.05	1.11	1.17	1.23	1.30	1.37	1.45