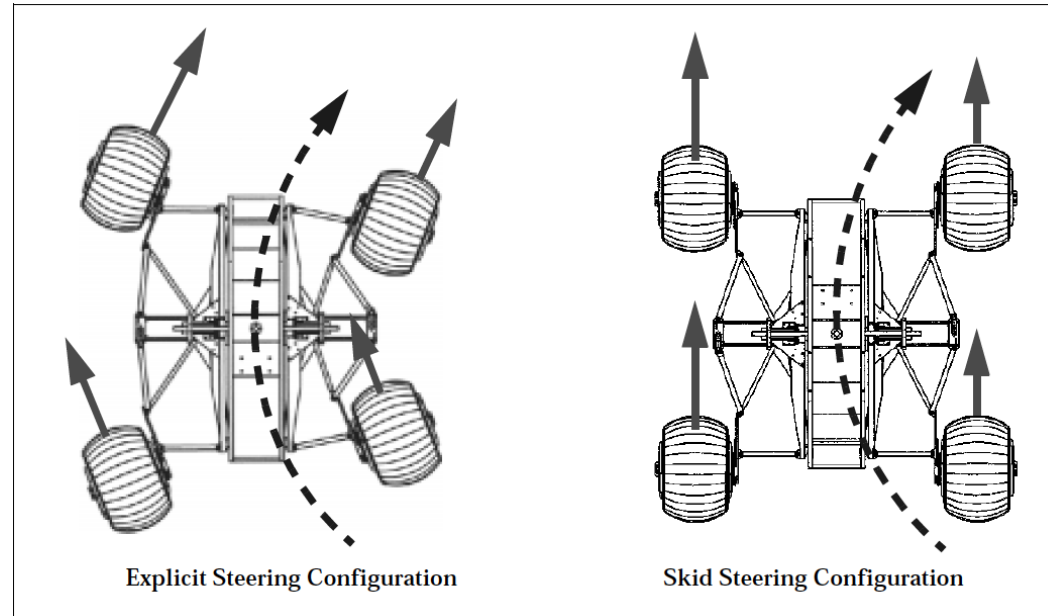


EBS 289K: Topics in Agricultural Robotics and Automation

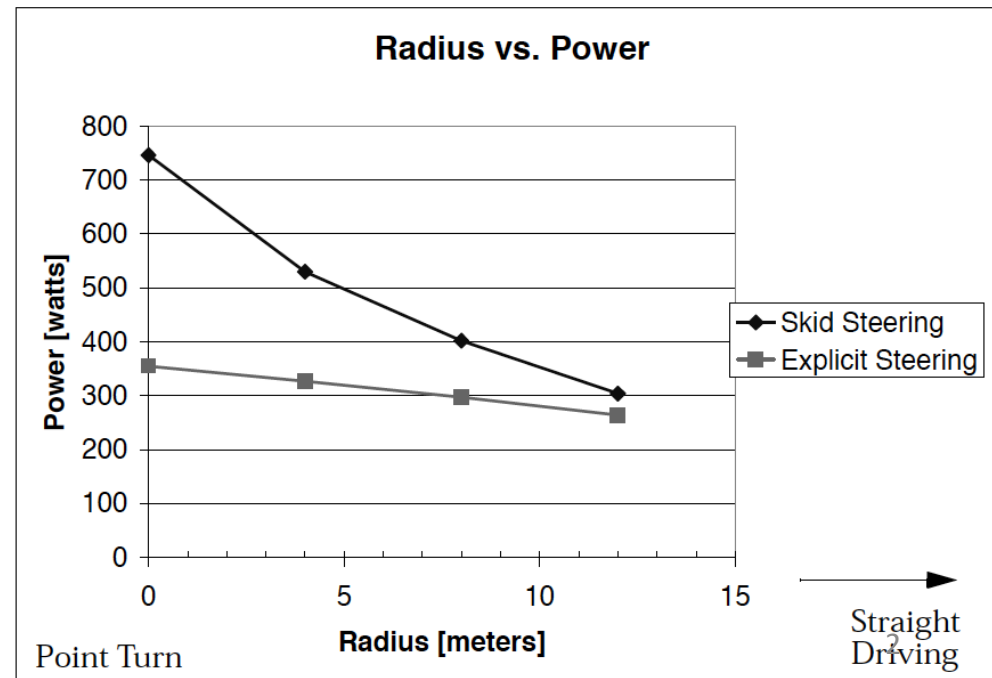
Stavros G. Vougioukas

UC Davis

Energy expenditure



- Skid-steering spends more energy



Ackermann Steering

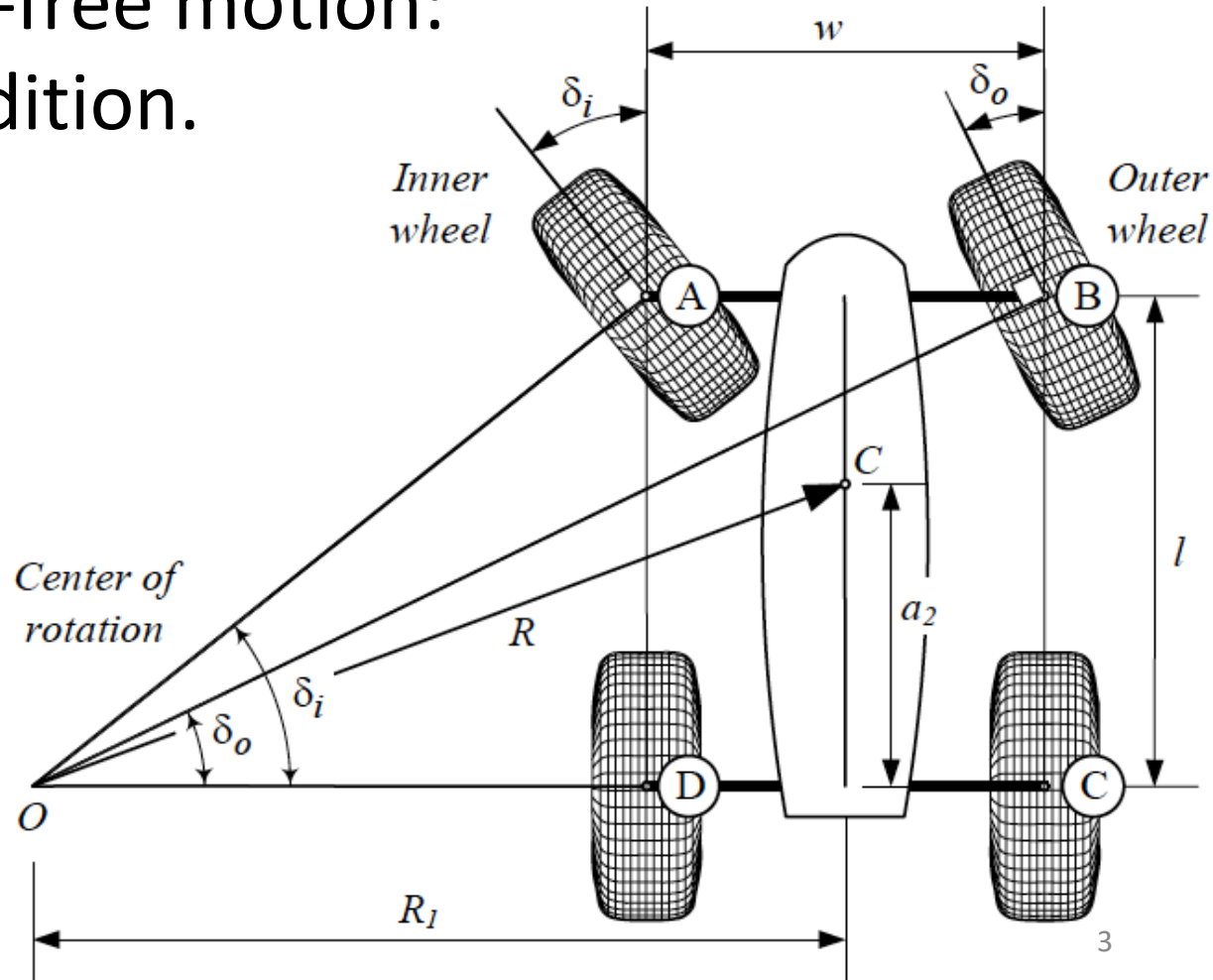
- Front-wheel steering.
- Slow speed, slip-free motion: Ackermann condition.

$$\cot \delta_o - \cot \delta_i = \frac{w}{l}$$

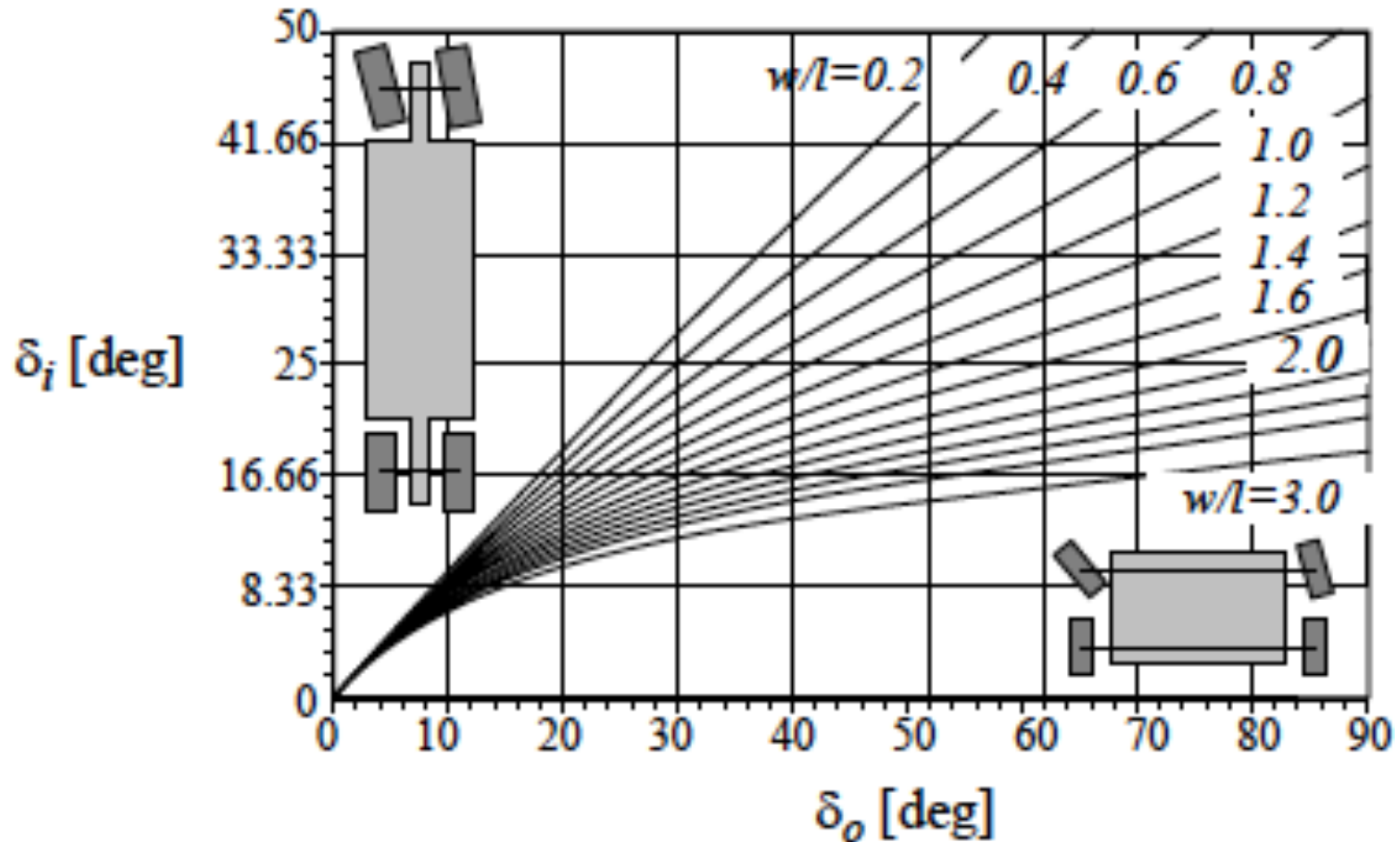
- Prove it!

$$\tan \delta_i = \frac{l}{R_1 - \frac{w}{2}}$$

$$\tan \delta_o = \frac{l}{R_1 + \frac{w}{2}}$$

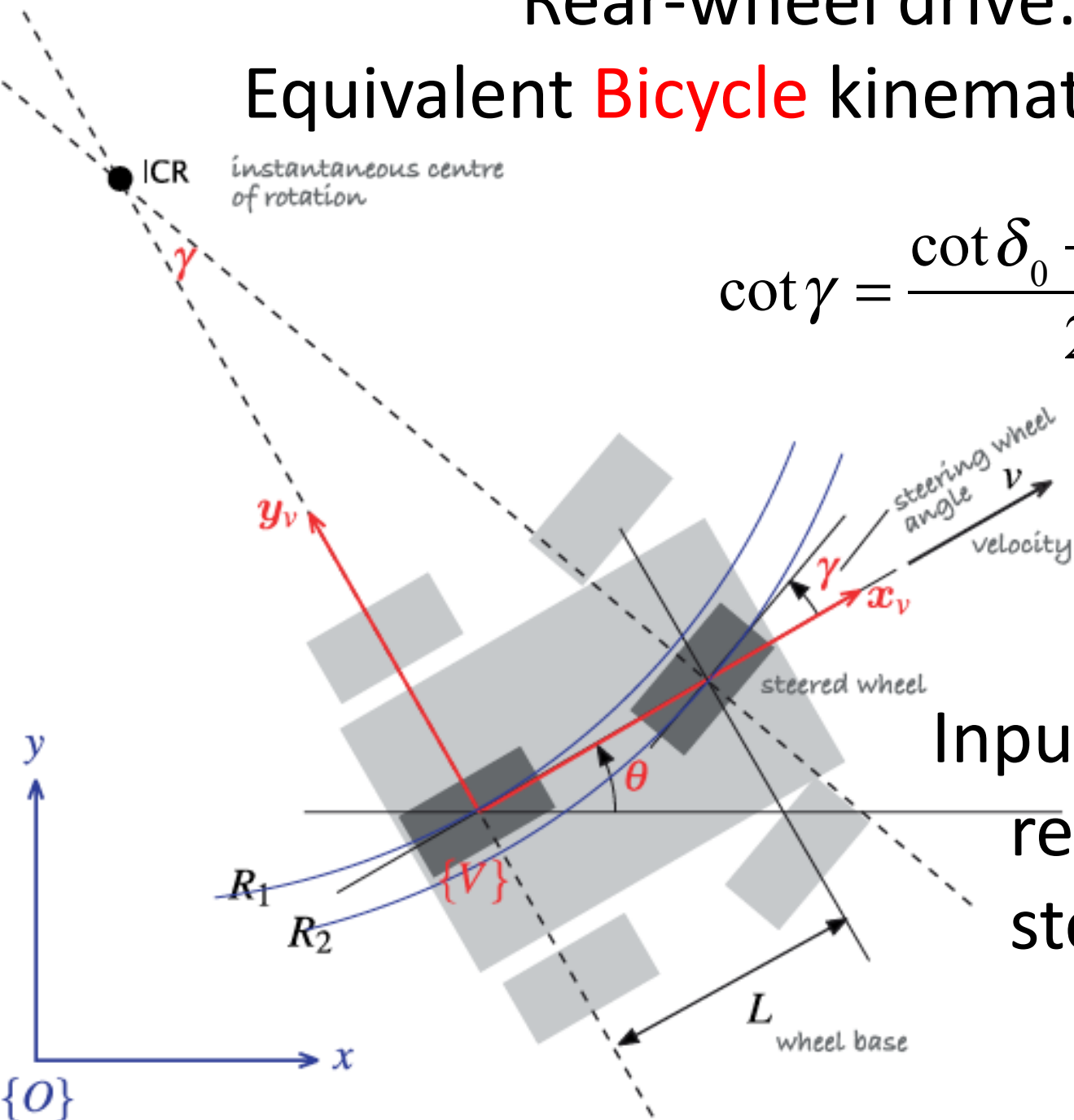


Effect of w/l on the Ackerman condition for front-wheel-steering vehicles



Rear-wheel drive: Equivalent **Bicycle** kinematic model

$$\cot \gamma = \frac{\cot \delta_0 + \cot \delta_i}{2}$$



Inputs:

rear wheel v ,
steering angle γ .

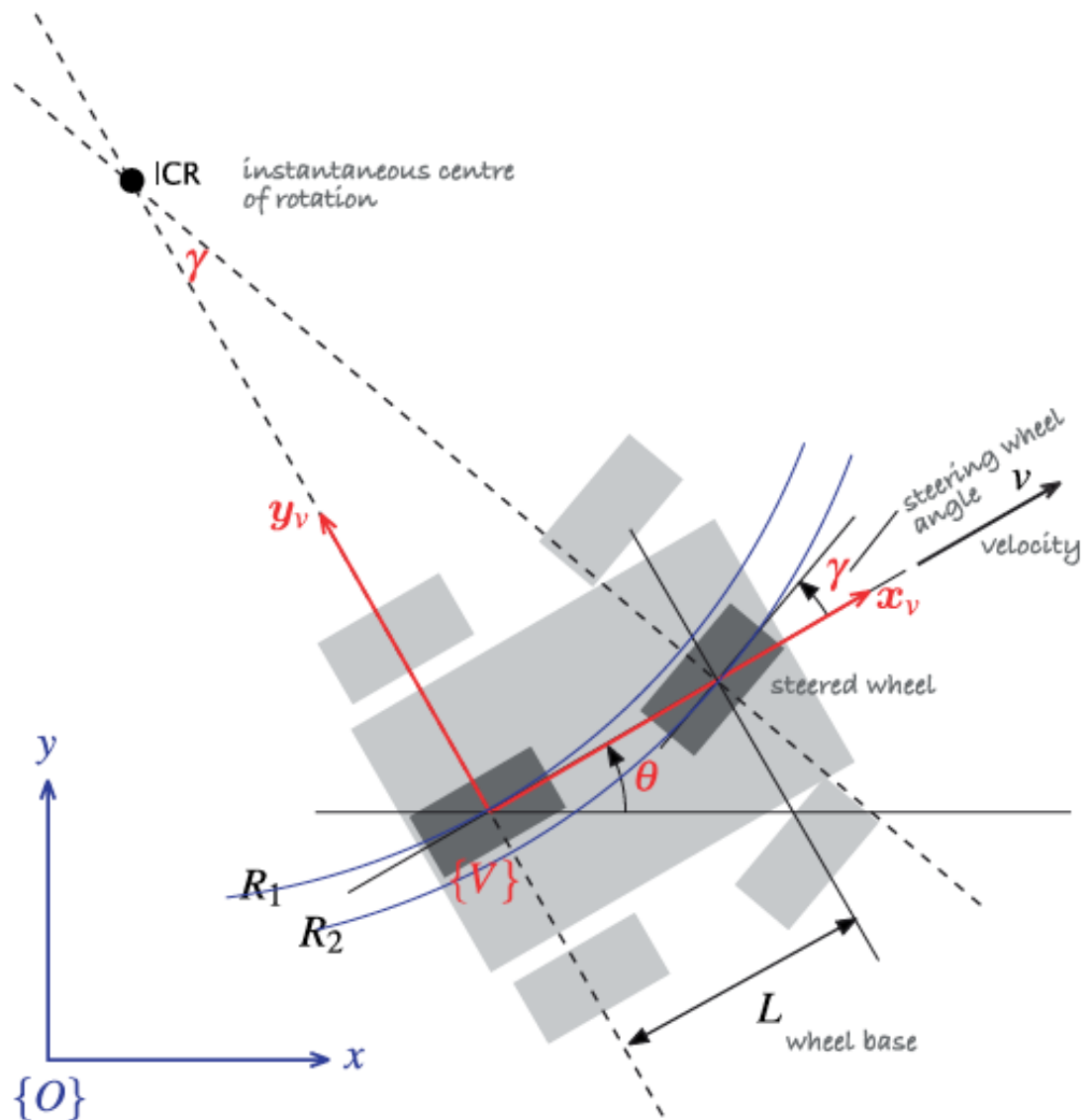
Bicycle model kinematic equations

$$\dot{x} = v \cos \theta$$

$$\dot{y} = v \sin \theta$$

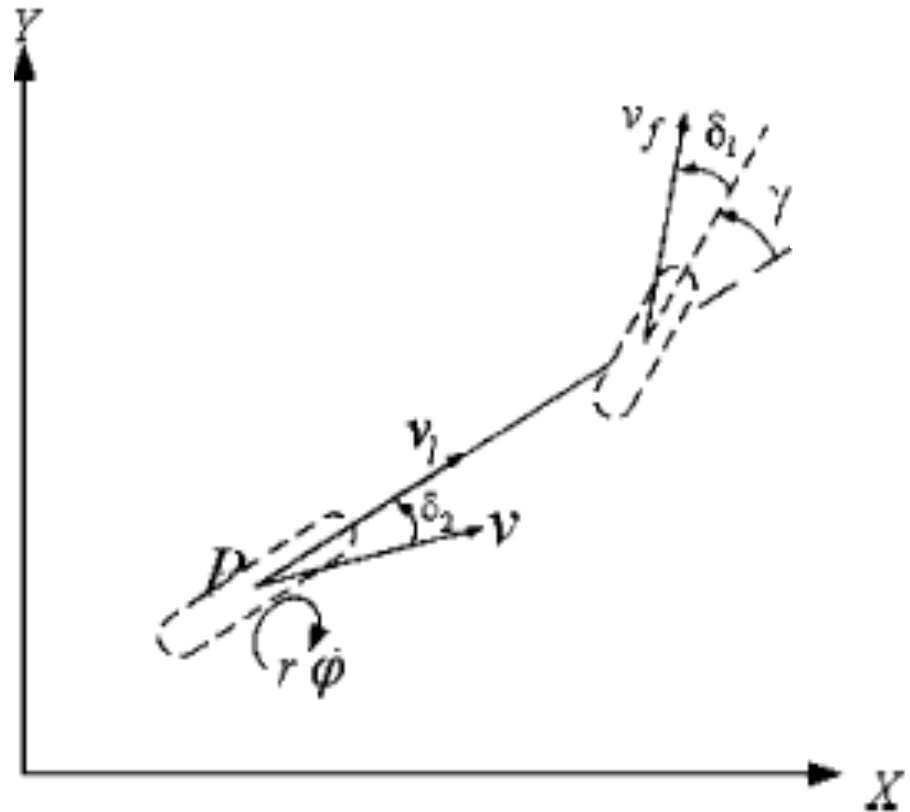
$$\dot{\theta} = v \frac{\tan \gamma}{L}$$

- Hint:
Vehicle rotates about ICR.



Skidding and slipping

- Front wheel:
 - ☐ Skidding with slip angle δ_1 .
- Rear (driven) wheel:
 - ☐ Longitudinal slip, s .
 - ☐ Skidding with slip angle δ_2 .



Skidding and slipping

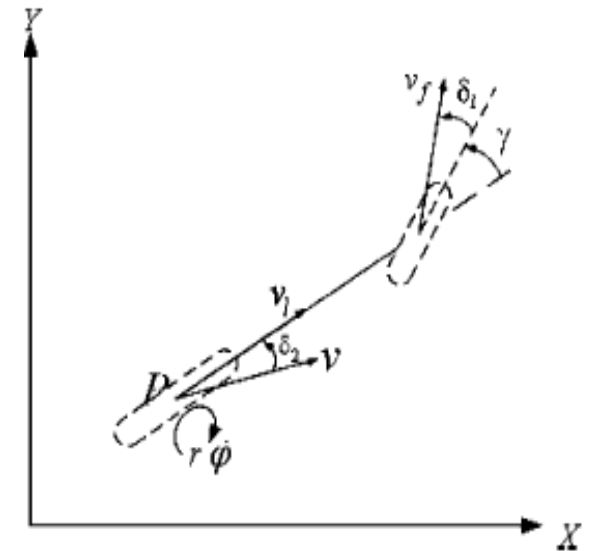
- Kinematic model:

- Same approach as with differential drive.

$$v_l = \begin{cases} (1-s) v & \text{if driving} \\ v / (1+s) & \text{if braking} \end{cases}$$

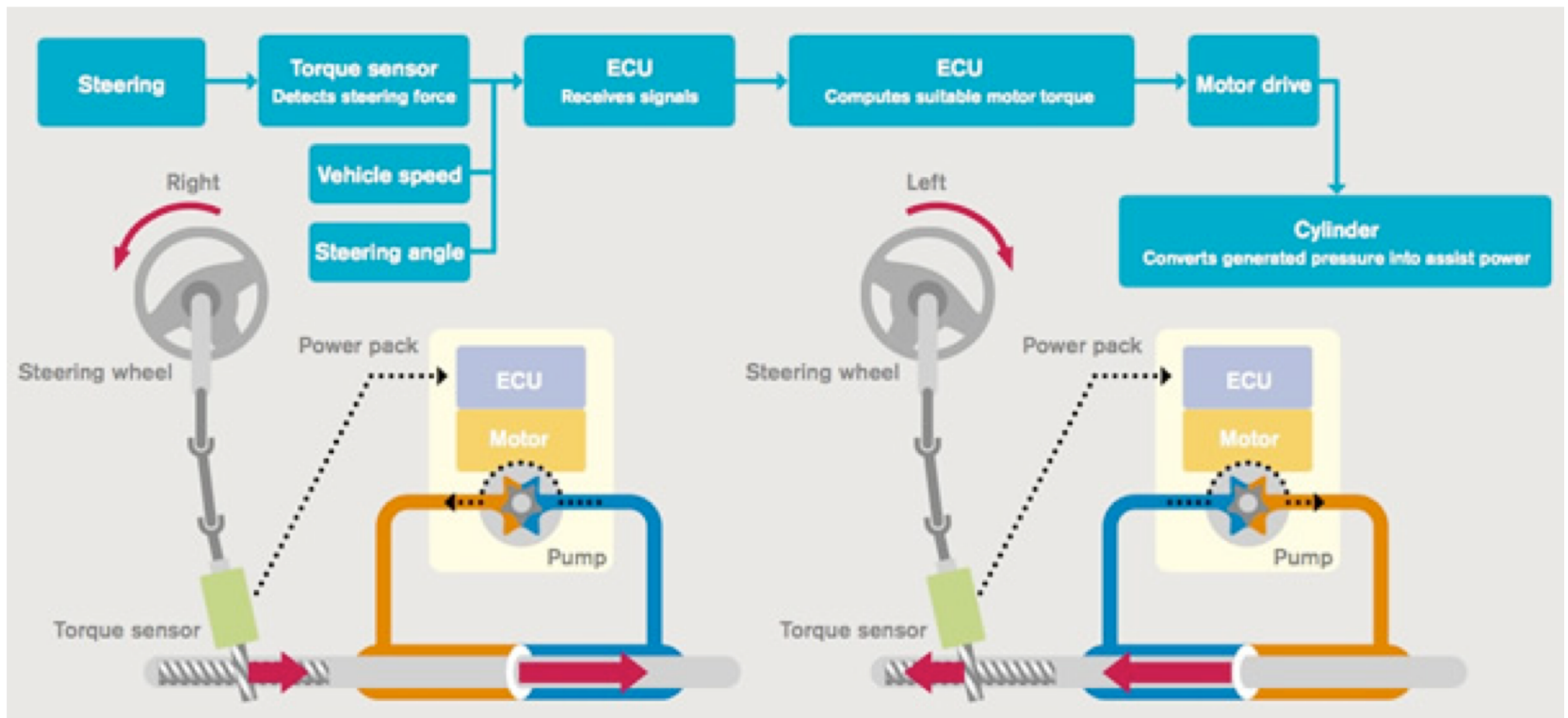
$$v_y = v_l \tan(\delta_2)$$

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} v_l \cos \theta - v_y \sin \theta \\ v_l \sin \theta + v_y \cos \theta \\ \frac{v_l}{L} \tan(\gamma + \delta_1) - \frac{v_y}{L} \end{bmatrix}$$



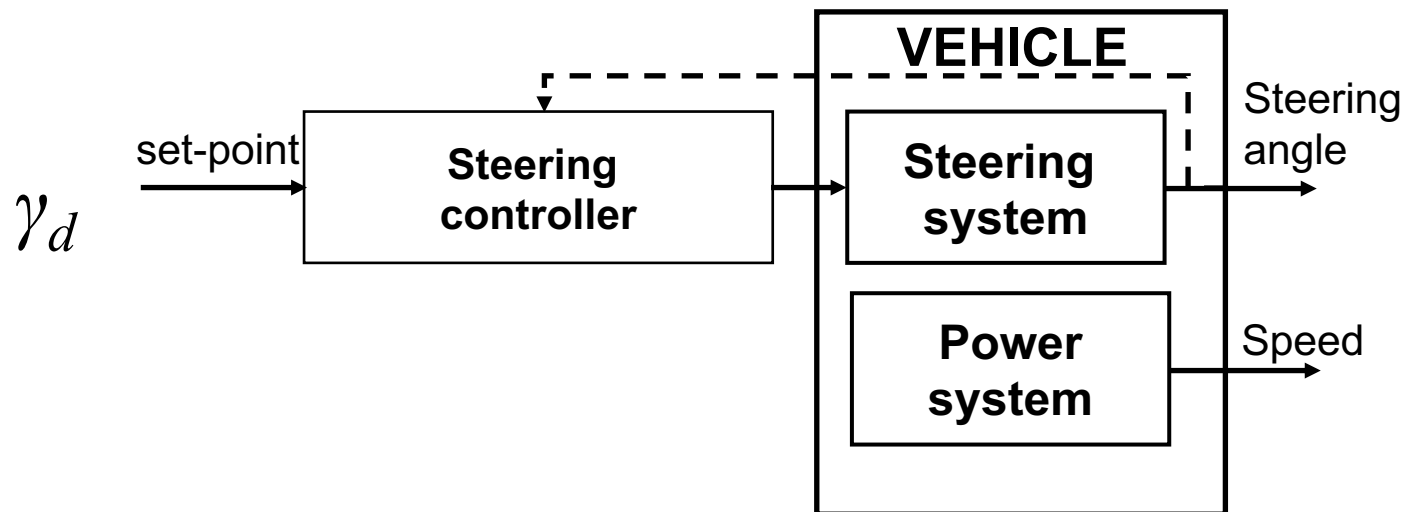
Steering dynamics

- If we want to change steering angle from γ_1 to γ_2 can it happen instantaneously?
- Tractors and off-road vehicles typically feature electro-hydraulic steering systems.
- Smaller vehicles involve gearing or chains.
- Linkages and tires have mass.



Steering dynamics

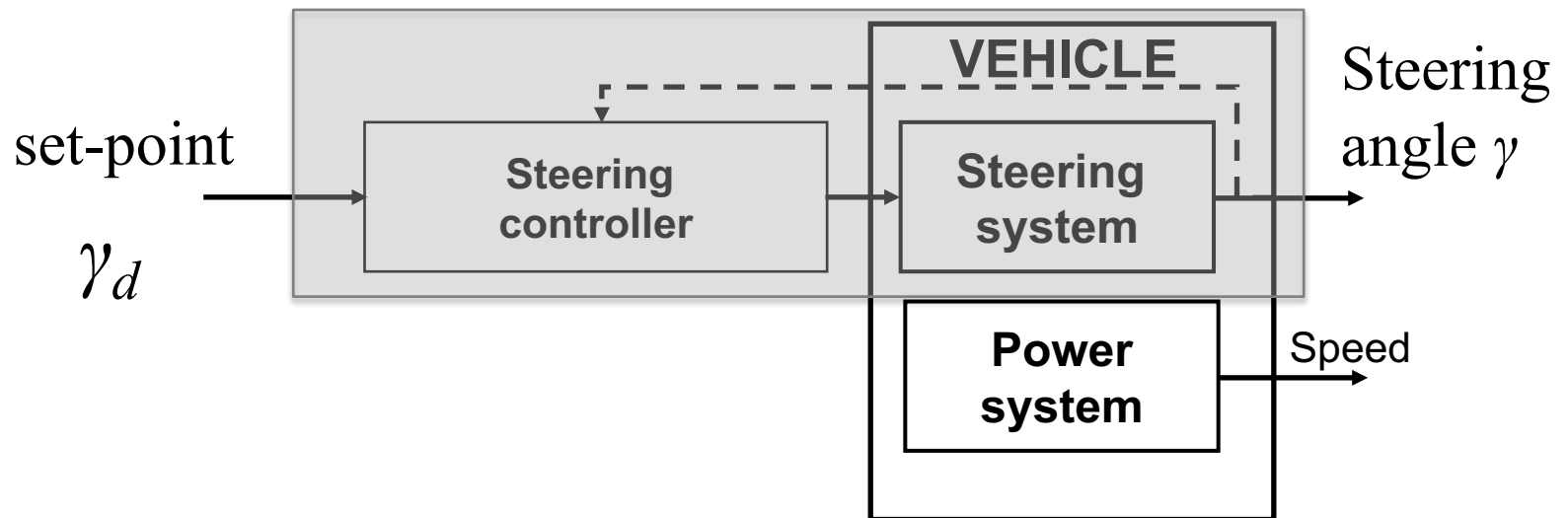
- Electro-hydraulics and wheel-soil interaction are very complex to model, and parameters are unknown.
- Computer-controlled vehicles feature a low-level steering controller.



Steering dynamics

- The steering system closed loop transfer function can be approximated as a first order system.

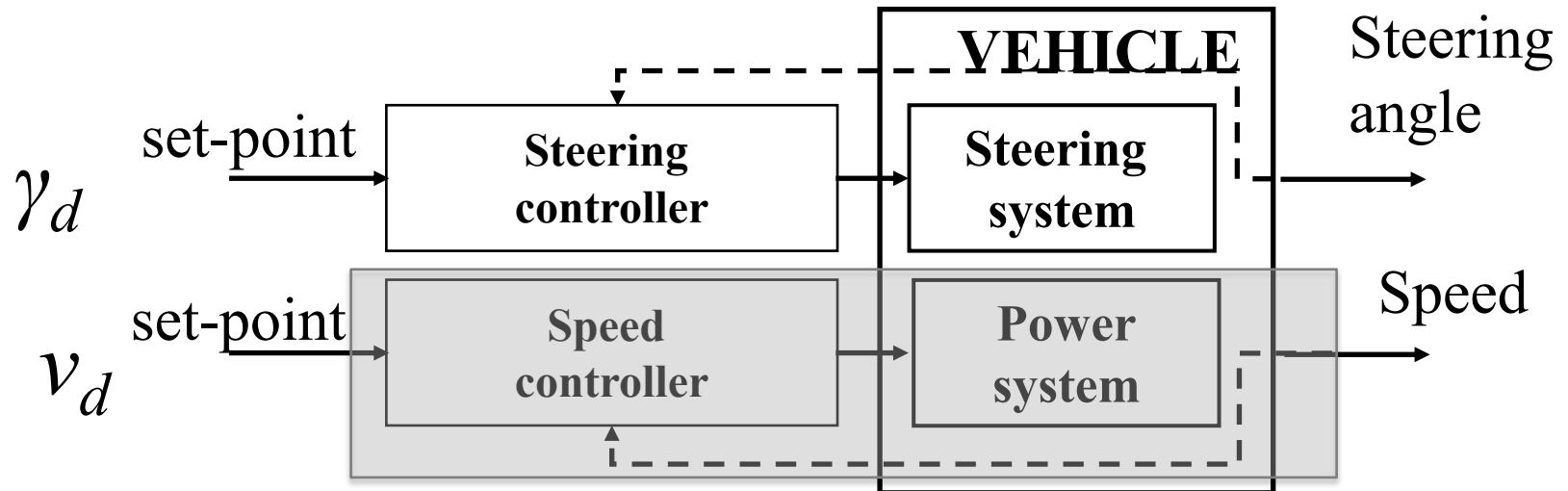
$$\dot{\gamma} = -\frac{1}{\tau_{\gamma}}\gamma + \frac{1}{\tau_{\gamma}}\gamma_d$$



Longitudinal velocity

- Does it change instantly?
- Same concept can be applied to a low-level speed controller.
- In the presence of slip, the steady state is $(1-s)v_d$.

$$\dot{v}_l = -\frac{1}{\tau_v} v_l + \frac{1}{\tau_v} (1-s)v_d$$



Discretization

- Euler discretization

$$\gamma_{k+1} - \gamma_k = dt \left(-\frac{1}{\tau_\gamma} \gamma_k + \frac{1}{\tau_\gamma} \gamma_d \right) \Rightarrow$$

$$\gamma_{k+1} = \gamma_k \left(1 - \frac{dt}{\tau_\gamma} \right) + \frac{dt}{\tau_\gamma} \gamma_d$$

- Similarly for speed.

Kinematic + simple dynamic model for driving: Updated equations

- Inputs: γ_d and v_d
- Remember:

$v_y = v_l \tan(\delta_2)$ (skidding).

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{v}_l \\ \dot{\gamma} \end{bmatrix} = \begin{bmatrix} v_l \cos\theta - v_y \sin\theta \\ v_l \sin\theta + v_y \cos\theta \\ (v_l \tan(\gamma + \delta_1) - v_y)/L \\ (-v_l + (1 - s)v_d)/\tau_v \\ (-\gamma + \gamma_d)/\tau_\gamma \end{bmatrix}$$

These equations must be integrated via Euler.

Integration vs. controller sampling

- The kinematic model integration step dt must be small (e.g., 1-10 ms) to achieve high accuracy when integrating the motion model with the Euler method.
- However, the controller's sampling interval DT is typically much longer, in the order of 100 ms (10 Hz) or slower.
- Therefore, we must implement our models with two distinct sampling intervals.
 - Two nested loops.

Kinematic + simple dynamic model:

Updated equations

$$\mathbf{q} = \begin{bmatrix} x \\ y \\ \theta \\ v \\ \gamma \end{bmatrix}$$

- Attention:
 - You need to pass input $\mathbf{u} = [\gamma_d \ v_d]$ and state (\mathbf{q}) constraints to your model.
 - $\mathbf{U}_{min} \leq \mathbf{u} \leq \mathbf{U}_{max}$ (2 x 1 vectors)
 - $\mathbf{q}_{min} \leq \mathbf{q} \leq \mathbf{q}_{max}$ (5 x 1 vectors)
 - The state constraints must be enforced inside the Euler loop because the state changes during integration
 - For example, the steering angle γ is now a component of the state vector \mathbf{q} , and it changes inside the loop.
 - The input constraints need only be enforced once, before the beginning of the loop, since \mathbf{u} is constant from step k to $k+1$ (during DT).

Assignment 2 Part 1

- Implement the bicycle model in Matlab, with skid-slip and with two distinct sampling intervals (Euler integration dt & controller DT).
- Input: control vector $\mathbf{u} = [\gamma_d \ v_d]$, state vector \mathbf{q} , and all parameters (e.g., dt , DT , L , s , δ_1 , δ_2), control and state constraints.
 - Note: input for turning could also be ω , or R .
- **Assume zero slip and skid**
- Tractor wheel radius = 0.5m;
Wheelbase = 2.5 m; $|\gamma_{\max}| \leq 45^\circ$; $|v_{\max}| \leq 5 \text{ m/s}$
- Assume $dt=DT=0.01 \text{ s}$.
- Apply input to turn at headland from one row to the next; row-center distance = 2 m.
- Does it work? Why? Try row-center distance = 3 m. Show traces.

Assignment 2 Part 2

- **Non zero slip and skid**
- Use same parameters as before.
- Add small slip angles δ_1 and δ_2 (e.g., 4°)
- Apply input to turn at headland from one row to the next; row-center distance = 3 m.
- What happens as slip angles δ_1 and δ_2 (skidding) increase? (Assume zero slip, s , for rear driven wheel).
- What if skidding is zero ($\delta_1 = \delta_2 = 0$) and only slipping affects the rear wheel?

Assignment 2 Part 3

- Augment bicycle model with 1st order closed-loop steering and speed dynamics.
- Plot vehicle path for γ_d step function (0 to γ_{\max}) and:
 - 1. Speed lag:
 $\tau_v = 0$ s; τ_γ from 0 to 2 s (same plot).
– (How will you implement τ_v or $\tau_\gamma = 0$?)
 - 2. Speed lag:
 $\tau_v = 1$ s; τ_γ from 0 to 2 s (same plot).
- Comment on these plots.