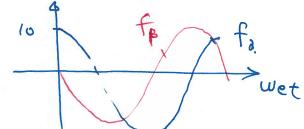
Answers - Exam 2014. Esbjerg. Dynamic modeling of Fl. machines.

Problem 1.



(2) Using the "Vector projection method

$$f_a = Re\left(\frac{f_{op}}{e^{io^*}}\right) = 10 \cdot cos weti.$$

(take the real location of phas-a axis

$$f_b = Re\left(\frac{f_{0}}{e^{j_120^\circ}}\right) = 10.005 (Wet+120^\circ)$$

location of phase-baxis

What we find is that compared to a normal abc sequence, here, phose-b and phase-c are exchanged. this is how the reference frames may be defined.

You can see that at t=0, wet=0, and d-axis is alinged with phase-a axis (and the 2-axis)

We use the same vector projection method. Note for  $\bar{f} = 10 \, \text{e}^{-1} \text{wet}$ , when t increases, it is rotating in a clock-wise (negative) direction.

According to the vector projection method.

$$f_d = Re\left(\frac{f_{ap}}{e^{jwet}}\right) = 10.\cos(2wet)$$
 (Note.  $f_{ap} = f = 10e^{jwet}$ )

$$f_g = Re\left(\frac{f_{op}}{e^{j(wet+90)}}\right) = -losin(2wet).$$

You can now Sketch their waveforms. The frequency is loo Hz.

= 
$$\frac{2}{3}$$
.  $V_{pk}$  [ $\sin(wet) + \sin(wet + \frac{27}{3})e^{\frac{1}{3}} + \sin(wet - \frac{27}{3})e^{\frac{1}{3}}$ ]

The real part. Of this term V

= 
$$\sin (\text{Wet}) + \sin (\text{Wet} + \frac{31}{3}) \cdot (\cos \frac{27}{3} + \sin (\text{Wet} - \frac{27}{3}) \cos \frac{27}{3}$$

$$= \operatorname{Sim}(\operatorname{wet}) - \frac{1}{2} \left[ \operatorname{Sim}(\operatorname{wet} + \frac{27}{3}) + \operatorname{Sim}(\operatorname{wet} - \frac{27}{3}) \right]$$

= 
$$\sin(wet) - \sin(wet) - (os_3^2) = \frac{3}{2} \sin(wet)$$
.

The imaginary park part.

Therefore.

$$\frac{1}{\log x} = \sqrt{\frac{2}{5} \cdot \frac{3}{3} \cdot \frac{3}{2} \cdot \left[ \sin (wet) + \frac{1}{3} \cos (wet) \right]}$$

$$= \sqrt{\frac{3}{5} \cdot \frac{3}{3} \cdot \frac{3}{2} \cdot \left[ \sin (wet) + \frac{1}{3} \cos (wet) \right]}$$

Then you can do the transformation. to other reference frames using the vector projection method.

## Problem 3

(1) The second row x-j, and then plus the first row.

We have .

$$u_{gs} - j u_{ds} = k_s (i_{gs} - j I_{ds}) + \beta (\lambda_{gs} - j \lambda_{gs}) + w_{\theta} \lambda_{ds} + j w_{\theta} \lambda_{gs}.$$

Therefore

Mote. 
$$j w_0 \lambda_{gds} = j w_0 (\lambda_{gs} - j \lambda_{ds})$$

$$= w_0 \lambda_{ds} + j w_0 \lambda_{gs}.$$

(2) in Steady State, differentiation term of the flux linkage will dissappear. Therefore.