

High Voltage Engineering

Problem 1 (16.66%)

A 1,2/50 μs single stage impulse generator, type b with a maximum output peak impulse voltage $V_{\text{max}} = 100 \text{ kV}$ should be designed. Already chosen components: Discharge capacitance $C_1 = 10 \text{ nF}$, load capacitance $C_2 = 1,5 \text{ nF}$, discharge resistance $R_2 = 9500 \Omega$

Temperature in the HV laboratory is 15°C and air pressure $p = 1027 \text{ hPa}$

a) Draw a graph of the impulse voltage waveform generated by the impulse generator for a charging voltage of $V_0 = 95 \text{ kV}$ using a sufficient number of calculated points (or MATLAB) of the curve $V(t)$. Determine graphically on the basis of this graph front time T_1 , time to half T_2 and the efficiency η . Please show clearly on the graph how you do this! Comment!

b) The students want to measure the impulse voltage from b) by means of a sphere gap. What should be the *precise* distance S between a pair of 12,5 cm spheres for the sphere gap to ignite (i.e. make a spark) for this voltage? State clearly how you do this!

Problem 2 (16.66%)

Test of a HV capacitor with $C = 400 \text{ nF}$ using non-destructive test methods.

a) Explain briefly the most important methods for non-destructive HV testing.

b) A Schering bridge has been used for measuring the loss angle $\tan \delta$ for the capacitor at 42 kV and the result was $\tan \delta = 0,152$. Calculate the current through the capacitor (result as a phasor, i.e. in complex polar coordinates, explain your method) during the measurement and the loss P in the capacitor. What causes such losses?

c) The losses calculated in b) are not acceptable. What should be the loss angle $\tan \delta$ in order to lower the losses to 10 kW?

Problem 3 (16.66%)

A high voltage impulse voltage divider has a unit step response as shown in the figure attached to this set of exercises.

a) Calculate the response time of this voltage divider as explained in Kuffel chapter 3.6.2. Explain carefully your procedure (you can write on the sheet with the figure and hand in). General approximations are of course acceptable.

b) A front chopped 1,2/50 μs is chopped at $T_c = 0,4 \mu\text{s}$ and its peak voltage was recorded to 418 kV using the above question a) voltage divider. What was the actual peak voltage?

EPSH1/PED1/WPS1

CLB/SMN



DEPARTMENT OF ENERGY TECHNOLOGY
AALBORG UNIVERSITY

Written examination in

High Voltage Engineering and Design of Switch Mode Converters

Monday 25th January 2016

09.00 – 13.00 (4 hours)

Please provide sufficient text description and reference to textbook and equations so your method of solution is clear and easy to follow. Statements and results will only give credit if explained thoroughly.

Design of Switch Mode Converters

Problem 4 (20%)

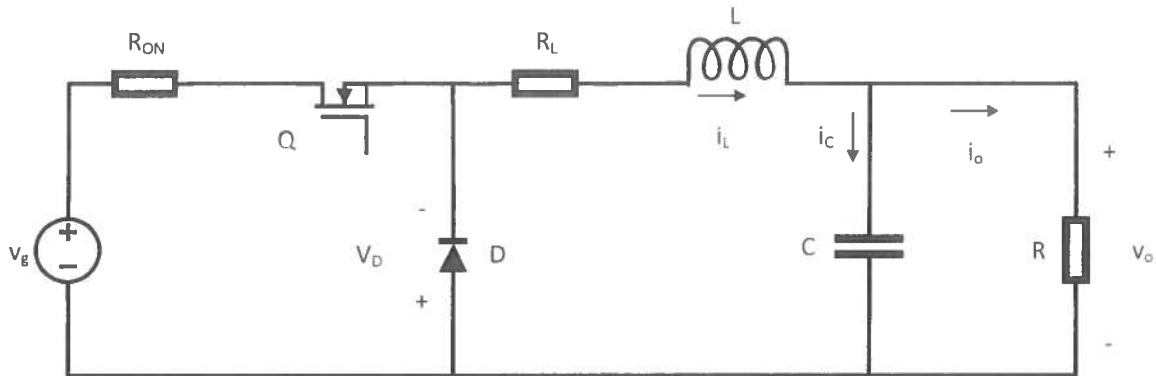


Figure 1: Diagram of the non-ideal buck converter

A non-ideal buck converter from Figure 1 operates in continuous conduction mode, with the values:

- Input voltage $V_g = 15\text{V}$
- Switching frequency $f_{sw} = 250\text{kHz}$
- Inductor $L = 15\mu\text{H}$
- Output capacitor $C = 75\mu\text{F}$
- Load resistance $R = 0.25\Omega$

The desired full-load output is:

- $V_o = 5\text{V}$
- $I_o = 25\text{A}$

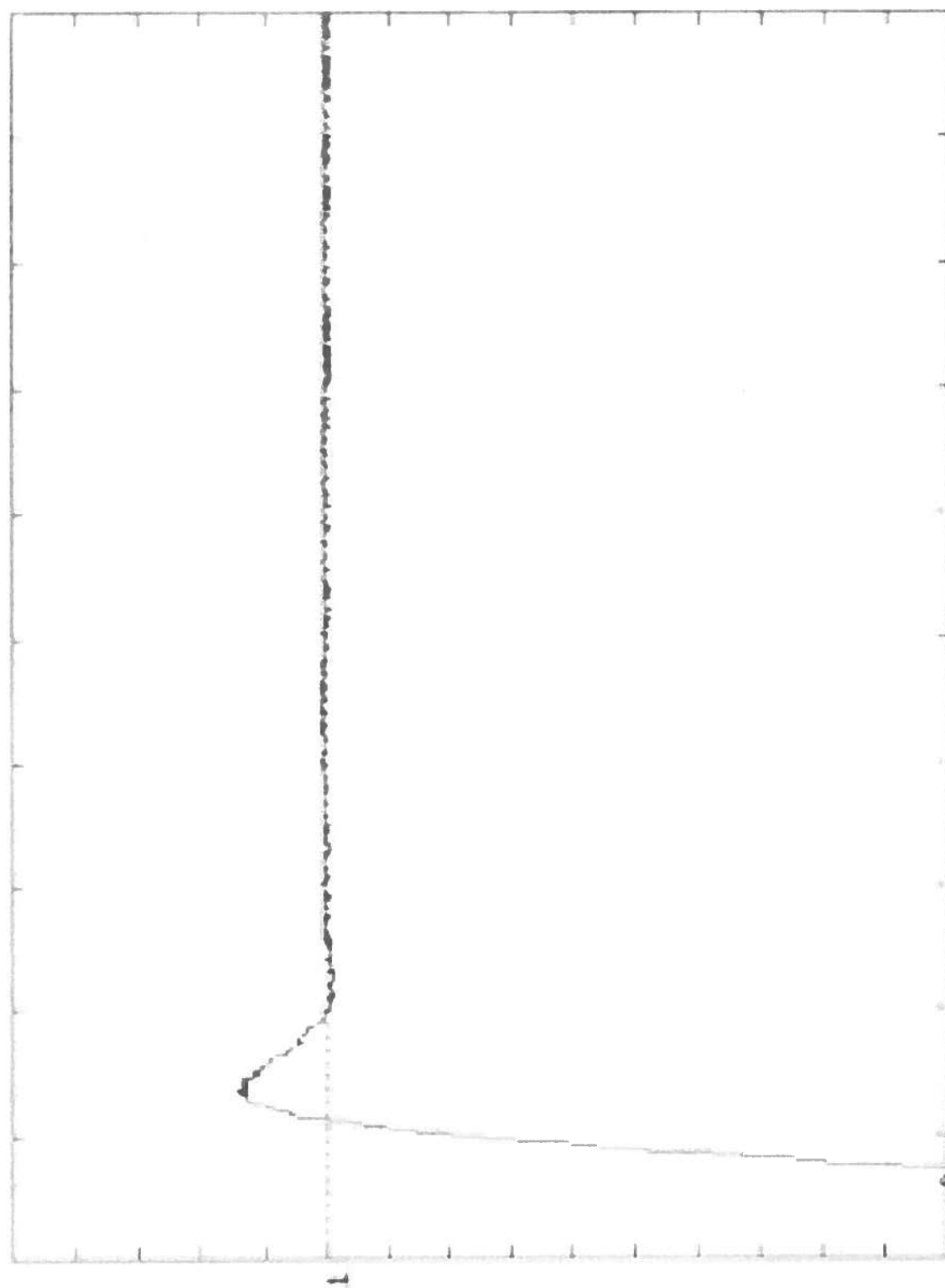
The power stage contains the following loss elements: MOSFET $R_{ON} = 0.1\Omega$, Schottky diode forward voltage drop $V_D = 0.5\text{V}$, inductor winding resistance $R_L = 0.05\Omega$.

Questions:

- A.) Determine the converter steady state duty cycle D , then inductor current ripple slopes m_1 and m_2 .
- B.) Determine the small-signal equations for duty cycle control (AC components of inductor voltage, capacitor current and input current)

A current-programmed controller is implemented for this converter. An artificial ramp is used, having a fixed slope of $M_a = 0.375 \cdot M_2$, where M_2 is the steady state slope m_2 at nominal output.

- C.) Over what range of D is the current programmed control stable for $M_a = 0.375 \cdot M_2$? What about for the case $M_a = 0.5 \cdot M_2$?
- D.) Determine the control-to-output transfer function using the simple approximation $i_L(t) = i_{ctrl}$.

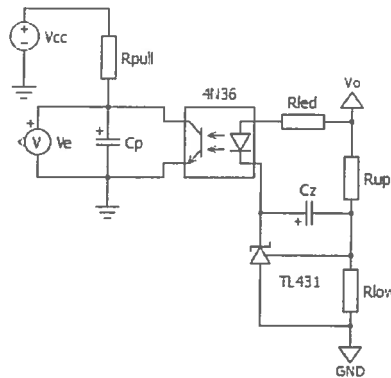


Unit Step Response

5.000us

Problem 6 (20%)

Design a Type II controller, as show on the figure below using analog components (resistors, capacitors, optocoupler and TL431 shunt regulator) for a DC-DC converter having an output voltage $V_o=12V$. The bandwidth of the controller should be $\omega_{cross} = 15000 \text{ rad/s}$.



Tasks:

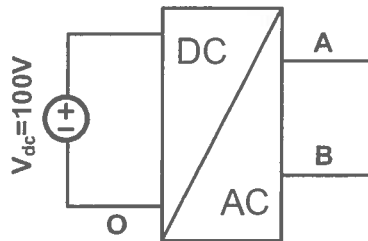
1. Define the desired value of ω_z and ω_p and motivate why did you chose it so?
2. Calculate the G_0 , ω_z , ω_p and ω_0 of the controller (R_{up} , R_{low} , R_{led} , R_{pull} , C_p , C_z respectively) and show the compensator $G_c(s)$ transfer function.

Given are the followings:

- The minimum cathode voltage on the TL431 $V_{Kmin}=2.5 \text{ V}$ and the reference voltage of the TL431 IC is $V_{ref}=2.5 \text{ V}$
- The forward voltage drop of the optocoupler at a minimum forward current $i_{Fmin}=1 \text{ mA}$ is $V_{Fmin}=1.1 \text{ V}$
- The Current Transfer Ration of the optocoupler is $CTR = 0.7$
- The converter gain the cross-over frequency is: $||G_{converter}(\omega_{cross})|| = 3 \text{ dB}$
- $V_{cc} = 3.3 \text{ V}$

Problem 5 (10%)

Calculate and draw the differential mode (V_{AB}) and common mode (V_{CM}) voltages for a PWM converter shown below:



Draw V_{CM} and V_{AB} for the given V_{Ao} and V_{Bo} voltage measurements.

