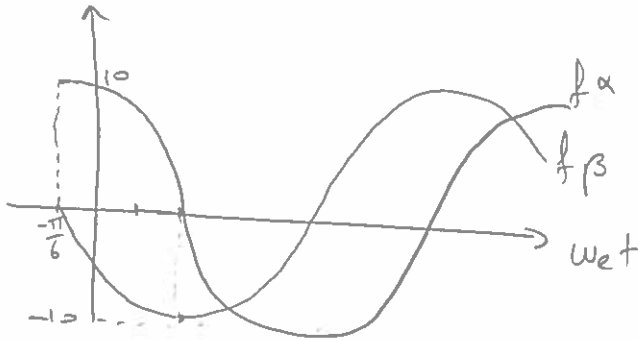


Problem 1)

(1) knowing $\overline{f_{\alpha\beta}} = f_{\alpha} - j f_{\beta}$ (the definition)

now $\overline{f} = 10 e^{-j(\omega_e t + \frac{\pi}{6})} = f_{\alpha\beta}$

therefore $f_{\alpha\beta} = 10^{-j(\omega_e t + \frac{\pi}{6})} = 10 \left[\cos(\omega_e t + \frac{\pi}{6}) - j \sin(\omega_e t + \frac{\pi}{6}) \right]$



$$= \frac{\pi}{6} - \frac{\pi}{6}$$

$$= \frac{\pi}{6}$$

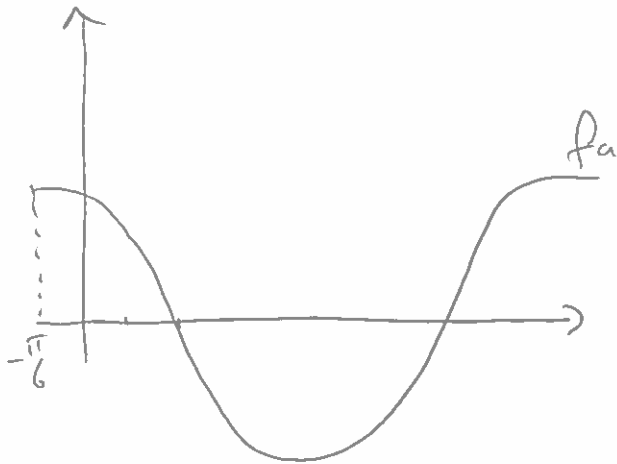
(2) Using the "vector protection method"

$$f_a = \operatorname{Re} \left(\frac{\overline{f_{\alpha\beta}}}{e^{j0^\circ}} \right) = 10 \cos(\omega_e t + \frac{\pi}{6}) \quad f_b = \operatorname{Re} \left(\frac{\overline{f_{\alpha\beta}}}{e^{j120^\circ}} \right) = 10 \cos(\omega_e t + \frac{\pi}{6} + 120^\circ)$$

↑
Real part taken

↑
location of phase axis

$$f_c = \operatorname{Re} \left(\frac{\overline{f_{\alpha\beta}}}{e^{j120^\circ}} \right) = 10 \cos(\omega_e t + \frac{\pi}{6} - 120^\circ)$$



(3) $f_b = 10 \cos(\omega_e t + \frac{\pi}{6} + 120^\circ) \Rightarrow \cos(\omega_e t + \frac{\pi}{6} + 120^\circ) = 1$

$$T = \frac{1}{f} = \frac{1}{50} = 0,02 \text{ s}$$

$$\Rightarrow \omega_e t + \frac{\pi}{6} + 120^\circ = 0$$

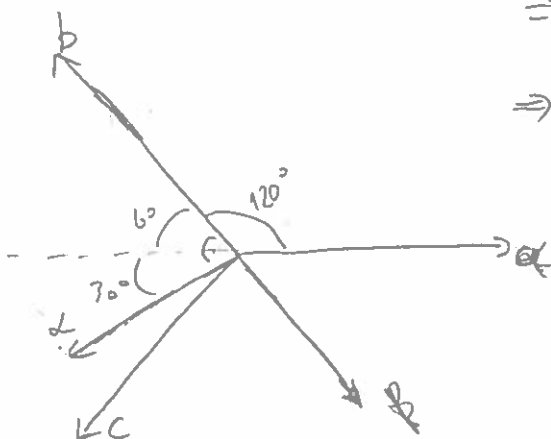
$$\Rightarrow 2\pi \cdot 50 t + \frac{\pi}{6} + \frac{2\pi}{3} = 0$$

$$+ 2\pi \cdot \frac{10}{50} = -\frac{5\pi}{6} \Rightarrow t = -\frac{1}{120} \text{ s}$$

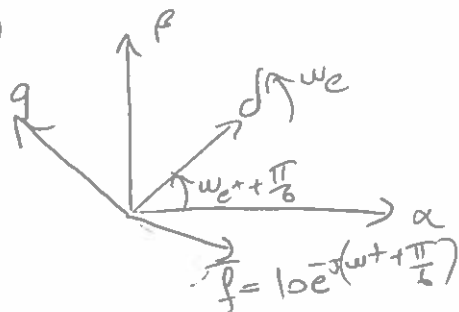
$$t = -\frac{1}{120} \text{ s} \Rightarrow$$

$$t = -\frac{1}{120} + 0,02 = 0,0166 \text{ s}$$

$$\theta = 360 \cdot \frac{t}{T} = 210^\circ$$



(4)



This is how the reference frames may be defined
It can be seen that at $t=0$, $\omega_e t + \frac{\pi}{6} = \frac{\pi}{6}$ and
d-axis has $+\frac{\pi}{6}$ degree difference between phase-α
axis (and α-axis).

Some vector projection method used and if " t " increases $\bar{f} = 10e^{-j(\omega_e t + \frac{\pi}{6})}$
will rotate CCW respectively.

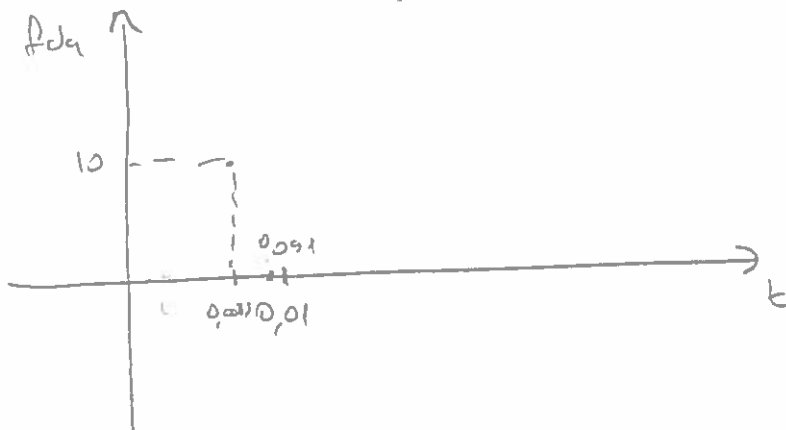
According to vector projection method

$$f_d = \text{Re} \left(\frac{\bar{f}_{\alpha\beta}}{e^{j(\omega_e t + \frac{\pi}{6})}} \right) = 10 \cos \left(2\omega_e t + \frac{\pi}{3} \right) \quad (\text{Note } \bar{f}_{\alpha\beta} = \bar{f} = 10e^{-j(\omega_e t + \frac{\pi}{6})})$$

↑
location of the d-axis

$$f_q = \text{Re} \left(\frac{\bar{f}_{\alpha\beta}}{e^{j(\omega_e t + \frac{\pi}{6}) + \frac{\pi}{2}}} \right) = -10 \sin \left(2\omega_e t + \frac{\pi}{3} \right)$$

It can be drawn for $f = 2\omega_e t \Rightarrow 100 \text{ Hz}$



for f_d
 $\frac{\text{max}}{2\omega_e t + \frac{\pi}{3}} = 0$

$$2.2\pi \cdot 50 \cdot t = -\frac{\pi}{3}$$

$$t = -\frac{1}{600} + 0.01 = 0.0083 \text{ ms}$$

$$2\omega_e t + \frac{\pi}{3} = \frac{\pi}{2}$$

$$2.2\pi \cdot 50 \cdot t = \frac{\pi}{2} - \frac{\pi}{3} = \frac{\pi}{6}$$

$$\frac{\pi}{6} - \frac{\pi}{3} = \frac{\pi}{6}$$

Q1) (3) $t = 0,05$

$$\omega_e t = 2\pi \times 0,05 = 5\pi = 180^\circ$$

$$\theta = \underbrace{180}_{\text{time}} + \underbrace{30}_{\text{beginning}} + \underbrace{90}_{\text{difference}} = 300^\circ$$

\vec{I} for current

$$\vec{I} = 10 (e^{j\omega_e t})$$

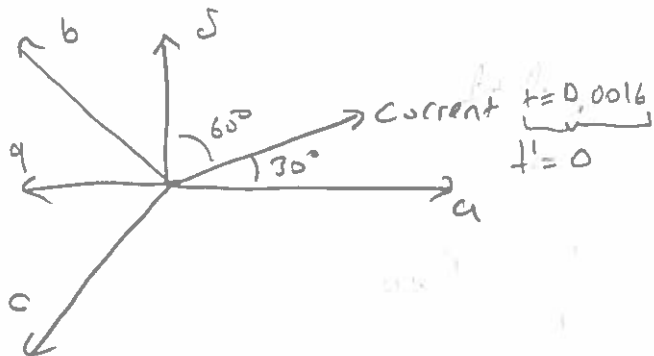
$$\vec{f_d} = \Re \left(\frac{\vec{I}}{e^{j300}} \right) = \Re (10 e^{j\omega_e t} \cdot e^{-j300})$$

$$= 10 \cos (\omega_e t - 300)$$

$$\vec{f_q} = \Re \left(\frac{\vec{I}}{e^{j30}} \right) = \Re (10 e^{j\omega_e t} \cdot e^{-j30})$$

$$= 10 \cos (\omega_e t - 30)$$

Case 1



$$\theta_{d1} = 90^\circ$$

$$\theta_{c1} = 30^\circ$$

d frame is always leading current frame

$$0,05 \text{ s} \Rightarrow \frac{0,05}{0,02} = 2,5 \text{ rotation}$$

$$\theta_{\text{lead}} = \Delta d - \Delta c = (300 - 90) - (210 - 30) = 30^\circ \text{ in } 2,5 \text{ rotation}$$

$$\Delta \omega_e \cdot t = \theta_{\text{lead}}$$

$$2\pi (f_{dq} - f_c) \cdot t = \theta_{\text{lead}}$$

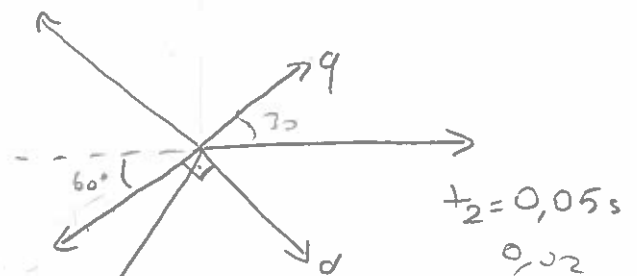
$$2\pi (f_{dq} - 50) \cdot t = 12$$

$$f_{dq} - 50 = 1,66$$

$$f_{dq} = 51,66$$

$$\omega_e = 2\pi \cdot 51,66 \text{ rad/s}$$

case 2



$$\theta_{d2} = 300^\circ$$

$$\theta_{c2} = 210^\circ$$

Q2)

(1) Determine mutual inductance between stator b and stator c

$$M_{bscsm} = L_{ad} \operatorname{Re} \left(\frac{e^{j\theta}}{e^{j120}} \right) \operatorname{Re} \left(\frac{e^{j\theta}}{e^{-j120}} \right) + L_{aq} \operatorname{Re} \left(\frac{e^{j\theta+90}}{e^{j120}} \right) \operatorname{Re} \left(\frac{e^{j\theta+90}}{e^{-j120}} \right)$$

$$M_{bscsm} = L_{ad} \cos(\theta-120) \cos(\theta+120) + L_{aq} \cos(\theta+90-120) \cos(\theta+90+120)$$

$$= L_{ad} \cos(\theta-120) \cos(\theta+120) + L_{aq} \sin(\theta-120) \sin(\theta+120)$$

(2) When d-axis on phase a it gives out the maximum inductances and they are together when $\theta = 0$

$$M_{bscsm} = L_{ad} \cos(\theta-120) \cos(\theta+120) + L_{aq} \sin(\theta-120) \sin(\theta+120)$$

$$= 0,25 L_{ad} - 0,75 L_{aq}$$

from Lecture 4 notes $\Rightarrow -\frac{1}{2} L_1 - L_2 \cos(2\theta)$

$$= -\frac{1}{2} L_1 - L_2$$

$$L_{ad} = L_1 - L_2$$

$$L_{aq} = L_1 + L_2$$

Minimum when $\theta = \frac{\pi}{2}$

$$M_{bscsm} = L_{ad} \cos(90-120) \cos(90+120) + L_{aq} \sin(90-120) \sin(90+120)$$

$$= 0,75 L_{ad} + 0,25 L_{aq}$$

(3) $I_{pm, a} = I_{mpm} \cos(\theta)$ $\overline{I_{abc}} = \overline{I_d} = \overline{I_q} = \overline{I_{\alpha\beta}}$

Phase-a: $I_a = -I_m \sin(3\theta)$

Instantaneous Torque \nearrow electrical rotor angle

$$\tau = p \cdot I_a \cdot I_{mpm} (-\sin \theta)$$

$$= +p I_m \sin(3\theta) \sin \theta \cdot I_{mpm} \cos(\theta)$$

$$= 2 \underbrace{I_m I_{mpm}}_{\text{constant} = x} \sin(3\theta) \sin(\theta) \cos(\theta)$$

At $\theta = 0 \text{ and } 90^\circ \Rightarrow I_m I_{mpm} = x$

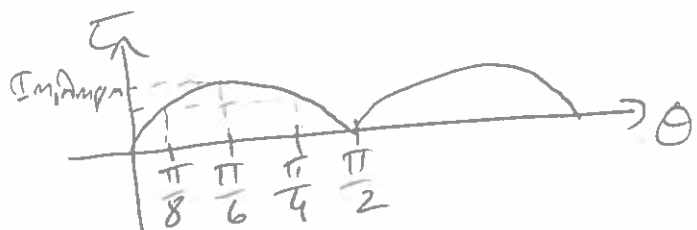
$$\tau = 2x \sin(0) \cdot \sin(0) \cdot \cos(0) \quad \tau = 0$$

$$\tau = 2x \sin(90) \cdot \sin(90) \cdot \cos(90) \quad \tau = 0$$

$$\theta = \frac{\pi}{2} \quad \tau = 2x \cdot 0,353$$

$$\theta = \frac{\pi}{6} \quad \tau = 2x \cdot 0,473$$

$$\theta = \frac{\pi}{4} \quad \tau = 2x \cdot 0,31$$



(4) Yes

(5) 3 φ

Q3) (1)

The second row $"-J"$ and then plus the first row.

We have

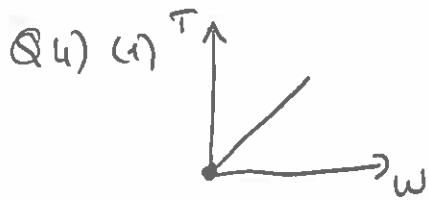
$$U_{qs} - J U_{ds} = R_s (I_{qs} - J I_{ds}) + p (\dot{\lambda}_{qs} - J \dot{\lambda}_{ds}) + \omega_s \dot{\lambda}_{ds} + J \omega_s \dot{\lambda}_{qs}$$

$$(2) \int \alpha \beta = \int d\alpha e^{j\theta}$$

$$\vec{U}_\alpha = \text{Re} \left(\frac{\vec{U}_{qds}}{e^{j\theta}} \right) = R_s I_{qds} + p \dot{\lambda}_{qds} + J \omega_s \dot{\lambda}_{qds}$$

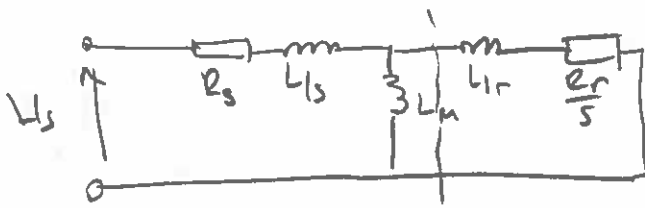
$$\vec{U}_\beta = \text{Re} \left(\frac{\vec{U}_{qds}}{e^{j\theta}} \right) = R_s I_{qds} \cos \theta + p \dot{\lambda}_{qds} \cos \theta + J \omega_s \dot{\lambda}_{qds} \sin \theta$$

$$\begin{aligned} \vec{U}_{\alpha\beta} = U_\alpha + j U_\beta &= R_s I_{qds} + p \dot{\lambda}_{qds} + J \omega_s \dot{\lambda}_{qds} - J \omega_s \dot{\lambda}_{qds} \\ &= R_s I_{qds} + p \dot{\lambda}_{qds} \end{aligned}$$



If $T=0$ $\omega_{slip}=0$ that means $\frac{\omega_s}{p} = \omega_m$

$$n_s = \omega_s \cdot \frac{60}{\pi} \cdot \frac{1}{2p} = 2\pi \cdot f \cdot \frac{60}{\pi} \cdot \frac{1}{2 \cdot 2} = 1500 \text{ rpm} = n_m$$



$s=0$ rotor side is neglected

$$L_{ls} = I_s (R_s + (2\pi f (L_{ls} + L_m)))$$

$$\frac{880}{\sqrt{3}} = I_s (2,5 + (2\pi f (0,281)))$$

$$I_s = 2,43 \text{ A}$$

$$\Rightarrow U_x = I_s \cdot X_{TOTAL} = 2,43 \times 8 = 213,75 \text{ V}$$

(2) Voltage drop compensation

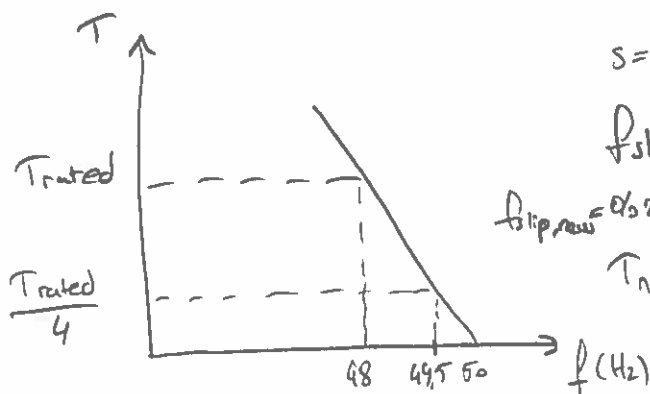
$$U_s = R_s I_s + j\omega_s L_s I_s$$

$\rightarrow R_s$ and I_s must be known

To obtain a constant flux linkage $L_s I_s$ needs to be taken into account, and added to the input voltage.

$$(3) V_{rated} = \frac{V_{l-l}}{\sqrt{3}} = 220 \quad I_{rated} = \frac{1,9 \text{ kW}}{3 \times 220} \approx 4,1 \text{ A}$$

$$I_{act,rated} = I_{rated} \times \sqrt{2} \times \cos \phi = 4,1 \times \sqrt{2} \times 0,8 = 4,638$$



$$s = \frac{n_s - n_{rated}}{n_s} = 0,04$$

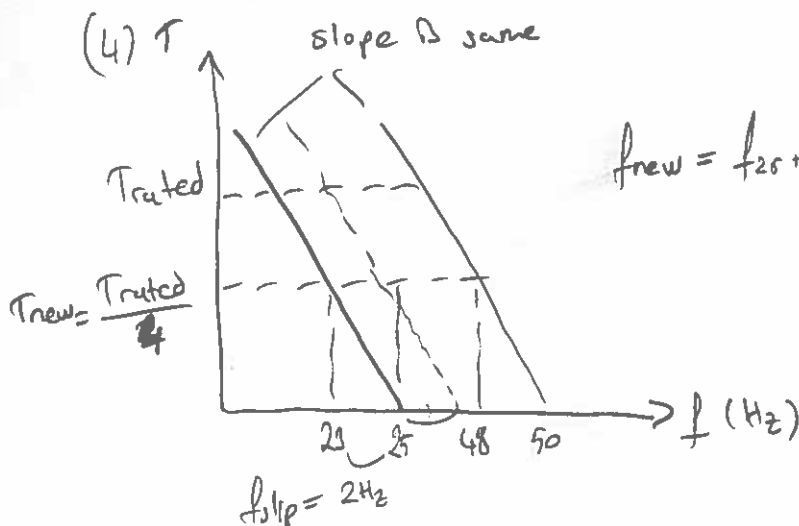
$$f_{slip} = f_s \cdot s = 50 \cdot 0,04 = 2 \text{ Hz}$$

$$f_{slip,new} = 0,25 \times f_{slip} = 0,5 \text{ Hz}$$

$$T_{new} = 0,25 \text{ of } T_{rated}$$

$$\frac{I_{sd,new}}{I_{sd}} = \frac{T_{new}}{T_{rated}} = \frac{I_{sd,new}}{4,63} = \frac{1}{4}$$

$$I_{sd,new} = 1,157 \text{ A}$$



$$f_{new} = f_{25} + f_{slip} = 25 + 2 = 27 \text{ Hz}$$

Q(5)

(1) Yes, Lecture 5 exercise answer p 1-2-3

$$(2) f = \frac{n \cdot p}{60} = \frac{1200 \cdot 4}{60} = 80 \text{ Hz}$$

$$(3) \omega_r = 2\pi \cdot p \left(\frac{n}{60} \right) = 502,65 \text{ rad/s}$$

$$V_{ph, peak} = \frac{120}{\sqrt{3}} \times \sqrt{2} = 98 \text{ V}$$

from equations it can be seen that $I_{mpm} = \frac{V_{ph, peak}}{\omega_r} = \frac{98}{502,65} = 0,195$

$$(4) L_{mq} = L_{md}$$

$$d\text{-axis current} = 2 \text{ A}$$

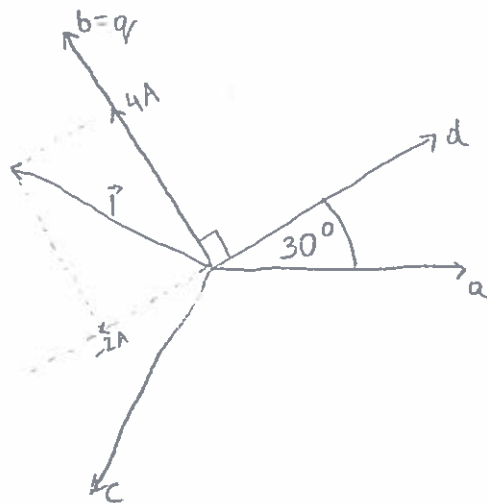
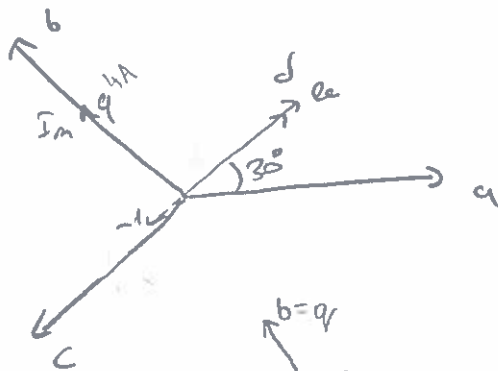
$$q\text{-axis current} = -1 \text{ A}$$

$$T = ?$$

$$T_e = \frac{3}{2} p (I_{mpm} \cdot i_q + (L_d - L_q) i_d \cdot i_q)$$

$$T_e = \frac{3}{2} \cdot 4 (0,195 \times 2 + 0) = 2,34 \text{ Nm}$$

(5)



As b-axis is aligned with q-axis, the initial value is $i_q = 4 \text{ A}$.

We can calculate current peak value as the length of current vector:

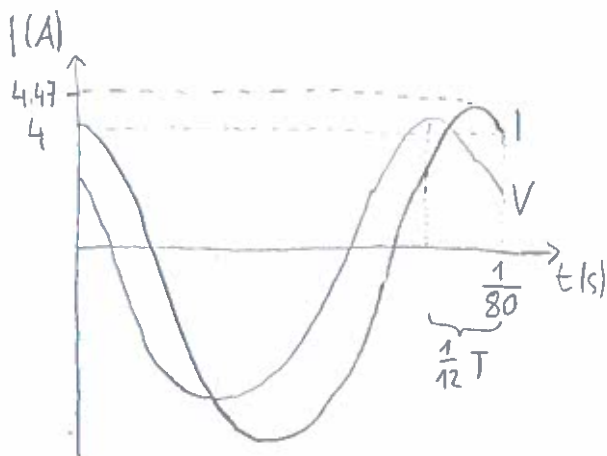
$$|\vec{I}| = \sqrt{4^2 + (-1)^2} = \sqrt{16+1} = \sqrt{17}$$

$$|\vec{I}| = 4.12 \text{ A}$$

$$f_{me} = 1200 \text{ rpm} = \frac{1200}{60} \text{ Hz} = 20 \text{ Hz}$$

This is mechanical frequency. In order to obtain electrical frequency, we need to multiply it by number of pole pairs:

$$f_{el} = p \cdot f_{me} \quad f_{el} = 4 \cdot 20 \text{ Hz} = 80 \text{ Hz}$$



$$\cos \phi = 0.866$$

$$\phi = 30^\circ$$

$$30^\circ = \frac{360^\circ}{12}$$

Peak voltage:

$$V_{peak} = V_{rms} \cdot \sqrt{2} = 100\sqrt{2} \text{ V}$$