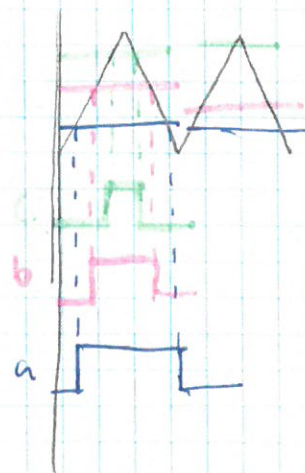
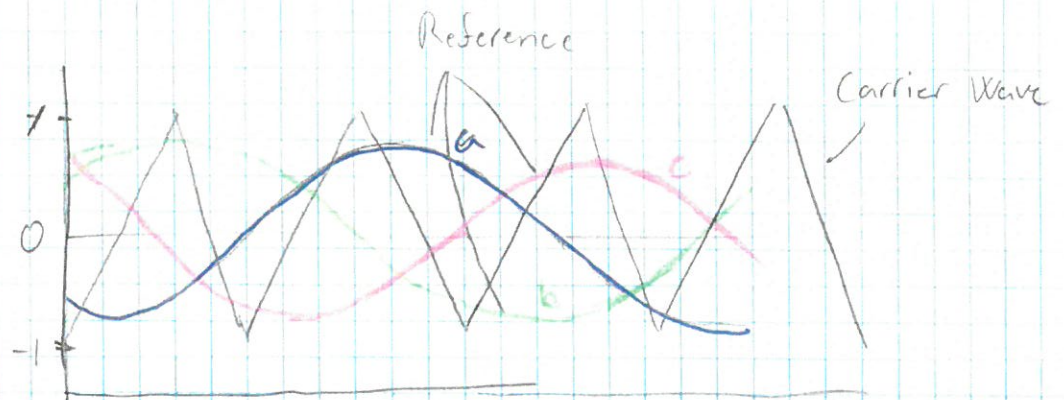


Sac - Exam B

Part 1

1 - 3-phase PWM:

- Three reference is generated from a sine function where each are 120° apart. This is then compared with the carrier wave:

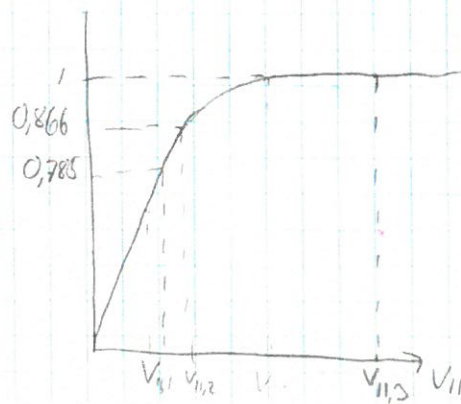


The frequency of the carrier wave much larger than the fundamental frequency.

- The ranges of the modulation index:

$$M = \frac{V_0}{\frac{2}{\pi} V_{dc}}$$

V_0 : Amplitude of the fundamental voltage.



V_{n1} - End of linear range for Sine PWM

V_{n2} - End of linear range for SVM, THH PWM

V_{n3} - End of Over modulation

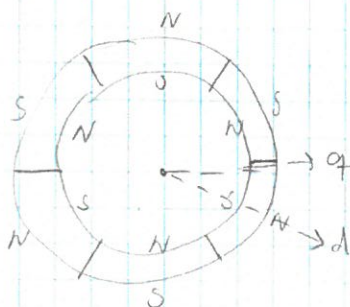
$> V_{n3}$ - Square wave

CoEDSAC - Exam 13

Part 2 - PMSM

- A 6-pole surface mounted Permanent Magnet machine in a synchronously rotating reference frame,

1 - dq - reference frame



2 - Torque

By inserting the expressions for λ_q & λ_d into T_e , it yields:

$$T_e = \frac{3}{2} p ((L_d i_d + \lambda_{mpm}) i_q - L_q i_q i_q)$$

$$= \frac{3}{2} p i_q ((L_d i_d + \lambda_{mpm}) - L_q i_q)$$

$$= \frac{3}{2} p (\lambda_{mpm} i_q + (L_d - L_q) i_d i_q)$$

\Downarrow For a surface mounted PMSM, $L_d = L_q$

$$T_e = \frac{3}{2} p (\lambda_{mpm} i_q)$$

CoEDS a C - Exam 13

- d and q-axes current references for

FOC:

$i_{d,ref}^* = 0$, used to flux, however the flux comes from PM

$i_{q,ref}^*$ can be found through a torque reference:

$$i_{q,ref}^* = \frac{2}{3} \frac{T_{e,ref}^*}{p \lambda_{mpm}}$$

3 - Rotor Electric Speed:

$$\begin{aligned} \omega_{rel} &= p \omega_{shaft} \Rightarrow \omega_{shaft} = \omega_{rel} / p \\ &= 377 \text{ rad/s} / 3 \cdot \frac{60}{2\pi} = 1200 \text{ rpm} \end{aligned}$$

- 4 - Tuning the current loop PI at zero speed:
At zero speed, the system becomes decouple, hence no back-EMF, thus an LTI model arises.

5 - Control Block Diagram:

