

# CONTROL OF ELECTRICAL DRIVE SYSTEMS AND CONVERTERS

## Three-phase modulation

Tamas Kerekes

# Control of electrical drive systems and converters

## Lecture 1. Three phase converters

Sinusoidal modulation, harmonics, square wave operation, dc link current, converter model, dead-time, current control.

Problems: 8-10 and 8-7

*Page: 225-243 in the book 'Power Electronics Converters, Application and Design. N. Mohan, T.M. Undeland and W.P. Robbins, John Wiley ISBN 0-471-58408-8'*

## Lecture 2. Three-phase modulation

Sinusoidal modulation with added 3<sup>rd</sup> harmonic, space vector modulation, 60 deg modulation, discontinuous modulation.

*Papers: The use of harmonic distortion to increase the output voltage, Simple Analytical and Graphical Methods for Carrier-Based PWM-VSI Drives*

## Lecture 3. Utility interface applications of power electronics

Interconnection of energy sources to the grid, control of switch mode interface, improved single and three phase utility interface.

*Page: 475-480, 494 – 502 in the book 'Power Electronics Converters, Application and Design. N. Mohan, T.M. Undeland and W.P. Robbins, John Wiley ISBN 0-471-58408-8'*

## Lecture 4. Variable-frequency converter classifications

PWM-VSI, CSI, electromagnetic braking, speed control, square-wave vsi drive

*Page: 418-432 in the book 'Power Electronics Converters, Application and Design. N. Mohan, T.M. Undeland and W.P. Robbins, John Wiley ISBN 0-471-58408-8'*

## Lecture 5. Soft-switching in PWM – converters

Hard and soft switching, classification of converters, basic resonant circuits, ZVS – VSI converters, phase shifted converters, resonant link inverters.

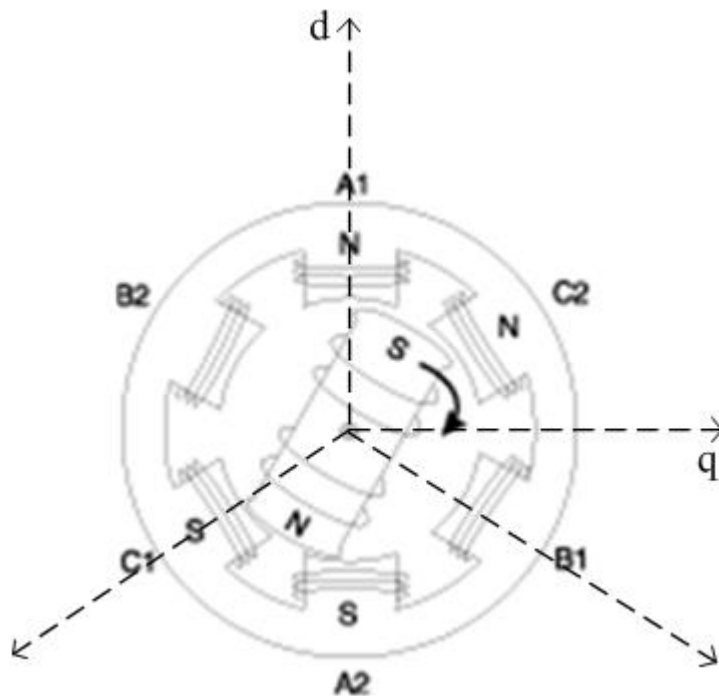
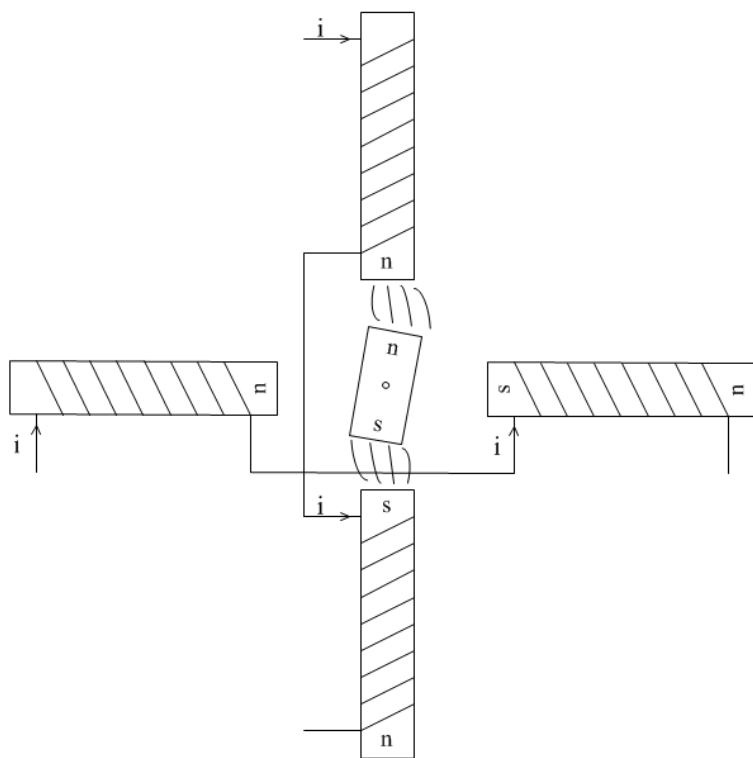
*Page: 249-258,, 280-291 in the book 'Power Electronics Converters, Application and Design. N. Mohan, T.M. Undeland and W.P. Robbins, John Wiley ISBN 0-471-58408-8'*

# Lecture 2: Three-phase modulation

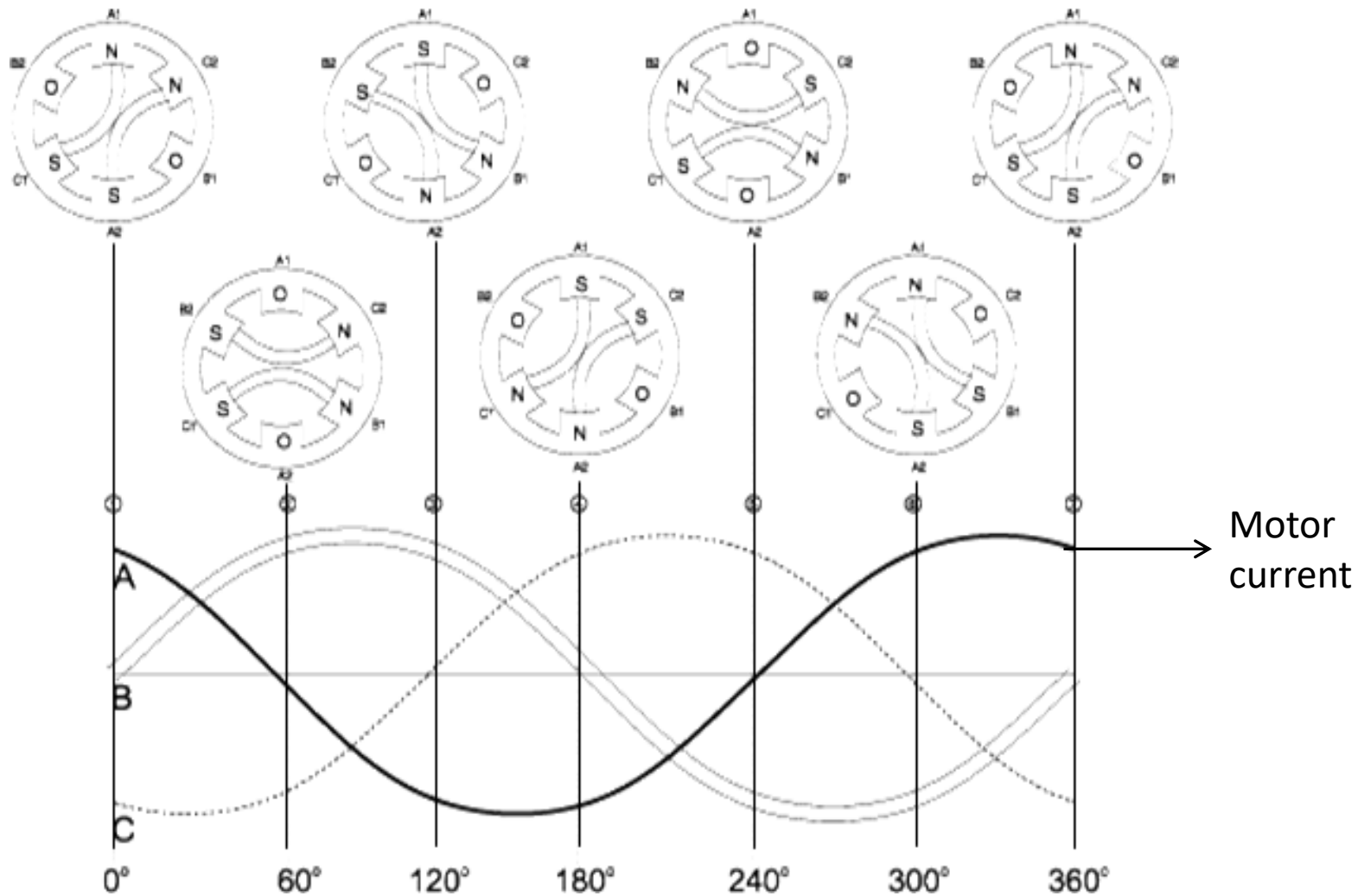
- Magnetomotive force generation in a motor
- ST-PWM with added 3rd harmonic
- SVM
- Discontinuous modulation
- Analytical spectrum calculation
- Current measurement

# Magnetomotive force between a coil and PM

- Passing a current through a coil aligns the magnet; reversing the current will rotate  $180^\circ$  the magnet (direction of rotation is not defined)
- By placing three pair coils,  $120^\circ$  shifted in space, the magnet can take an arbitrary position in the d-q plane



# Rotating field generation



- During one fundamental period one revolution of the rotor can be obtained

# Third harmonic injection

Relation between the phase and line voltages

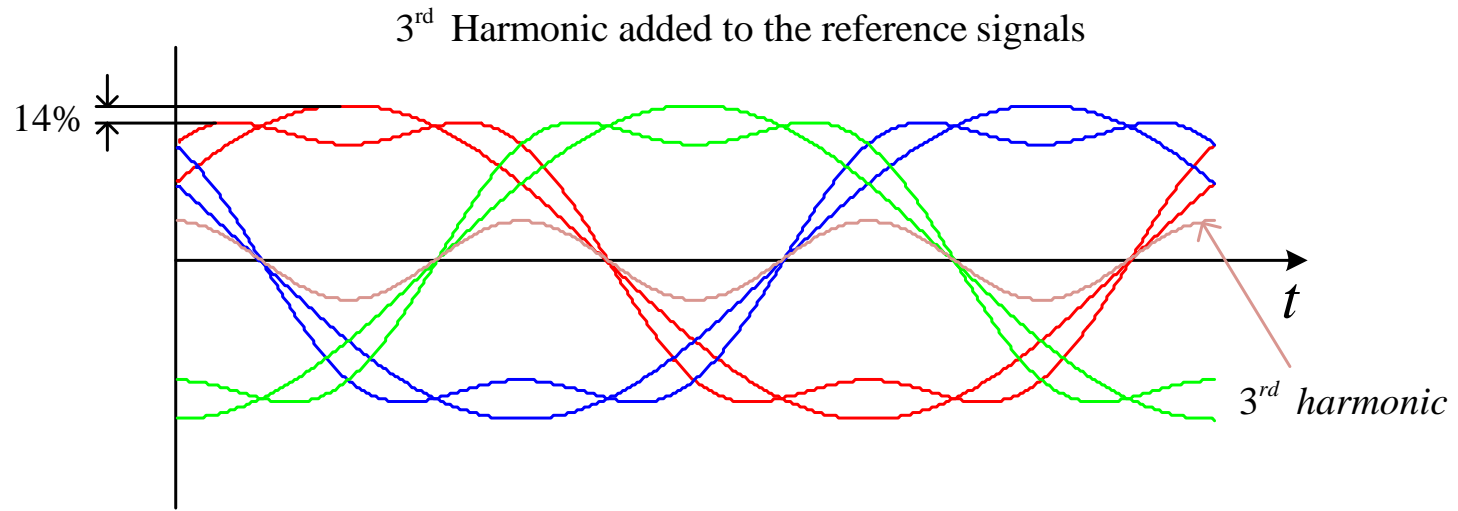
$$v_{AB} = v_{AN} - v_{BN}$$

$$v_{BC} = v_{BN} - v_{CN}$$

$$v_{AC} = v_{AN} - v_{CN}$$

Note: if the same value is added to the phase signals that will not affect the line to line voltage

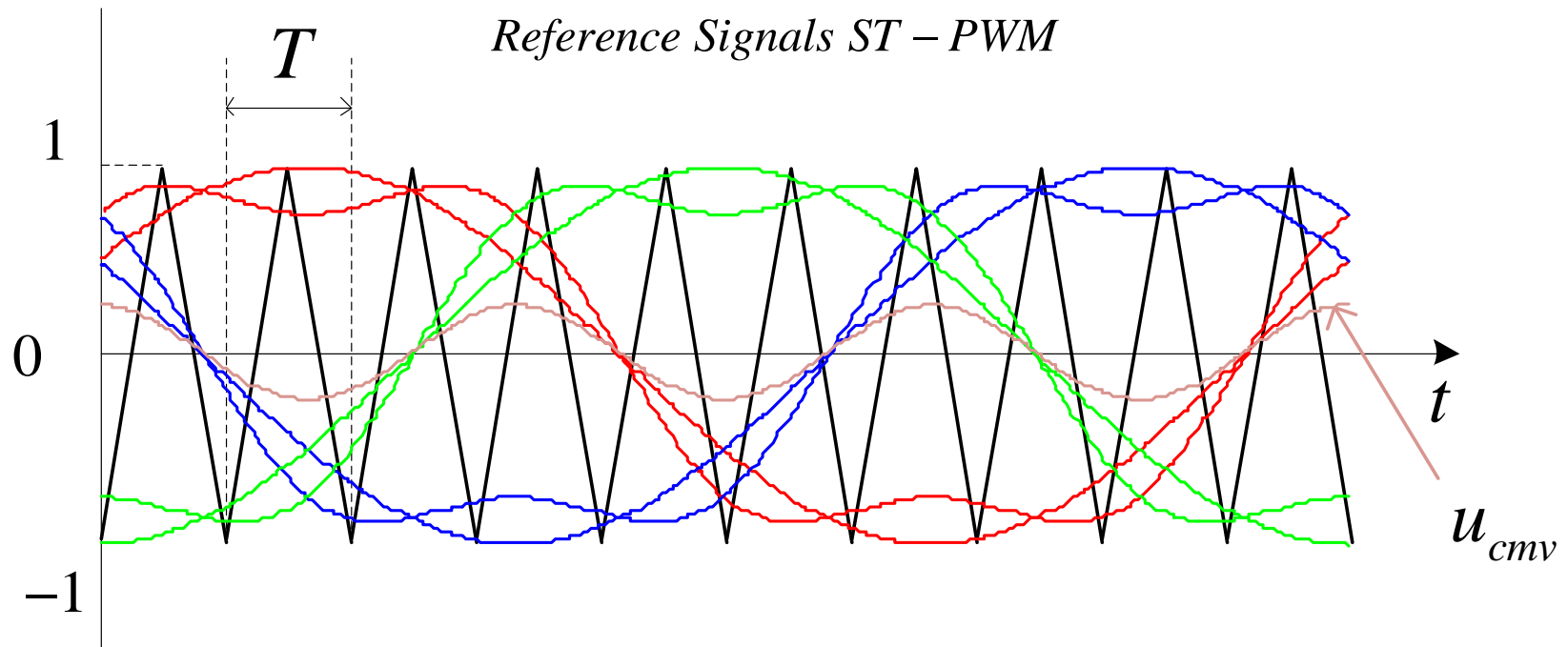
# Third harmonic injection waveform



Note:

- By adding a sinusoidal signal to the phase voltage waveform the line to line voltage is maintained sinusoidal
- The peak of the phase voltage is reduced with around 14%

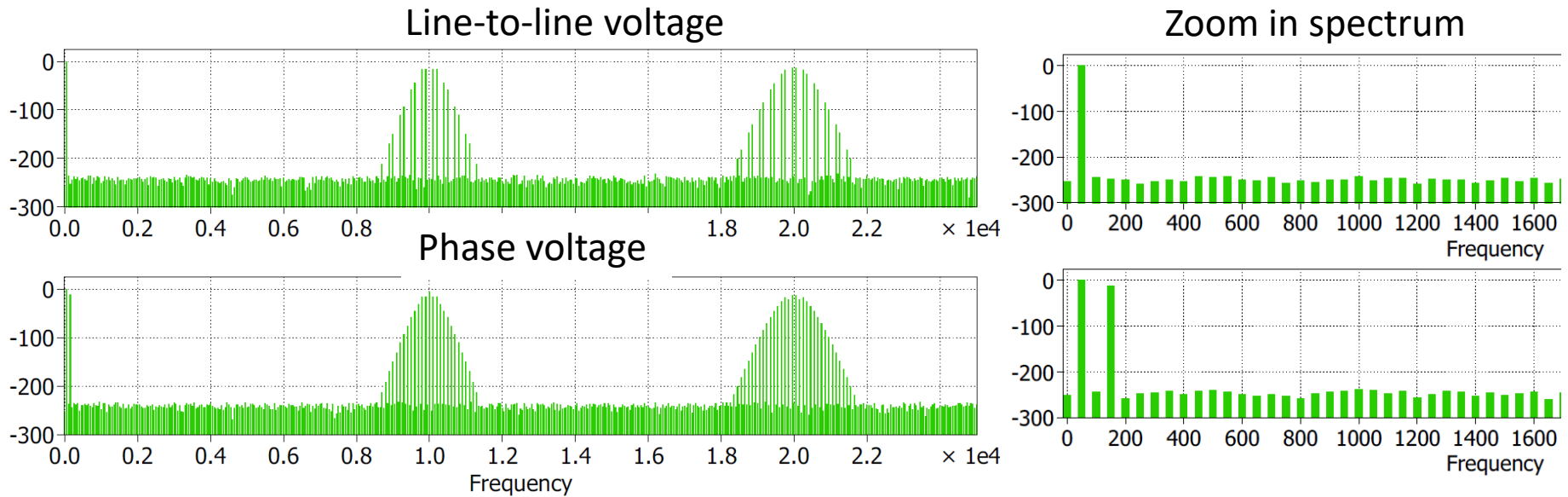
# Modulation of THI-PWM waveforms



- Note: The linear range is extended with around 14%

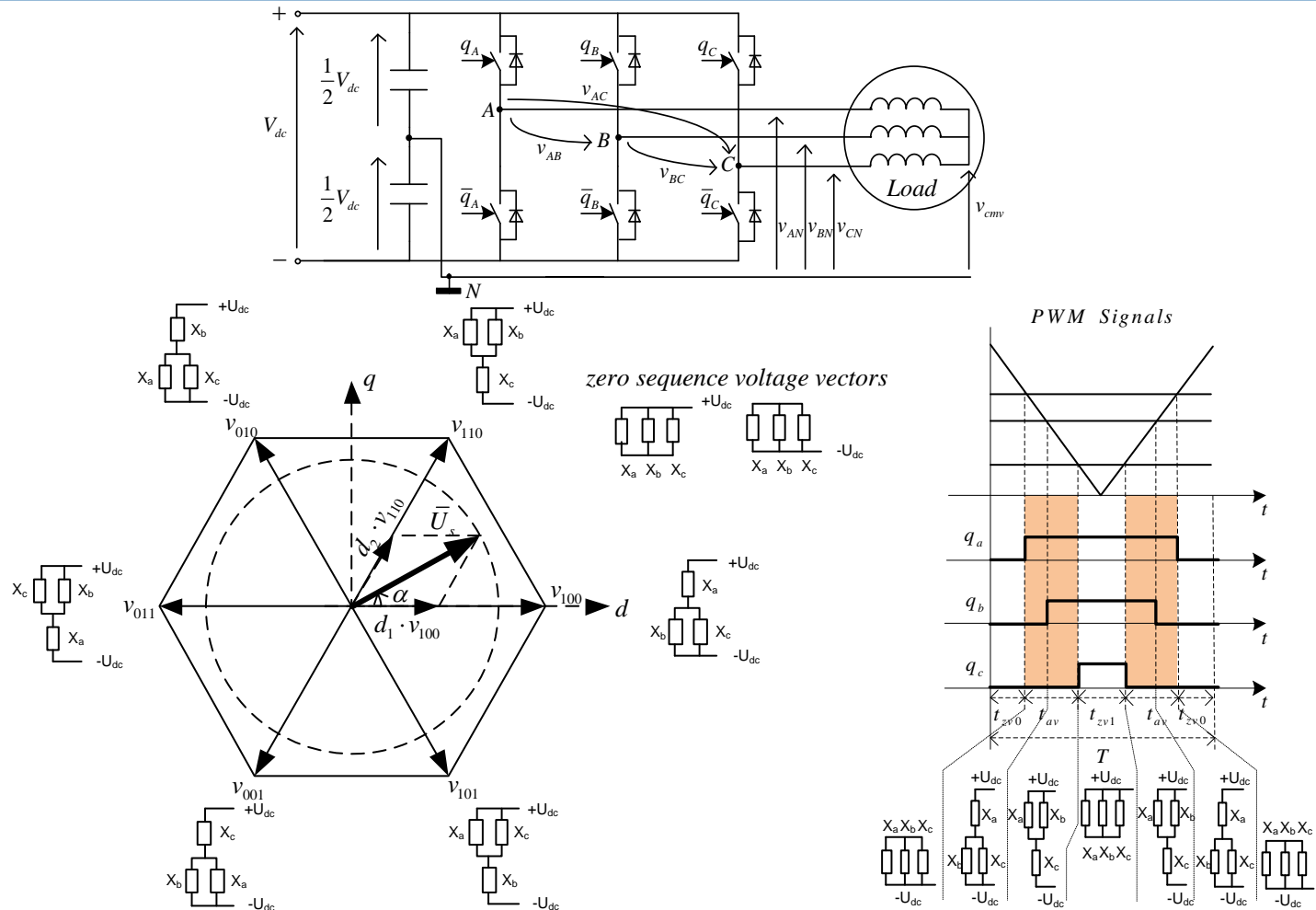


# Spectrum of THI-PWM



- The harmonic content is increased
- At low frequency there is no change in spectrum

# Space vector representation



- With the two level VSI 6 active and 2 zero sequence voltage vectors can be generated

# Timing calculation

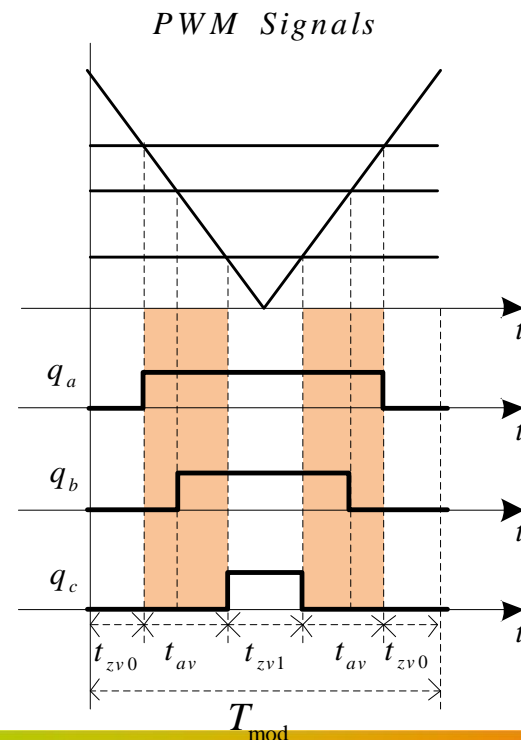
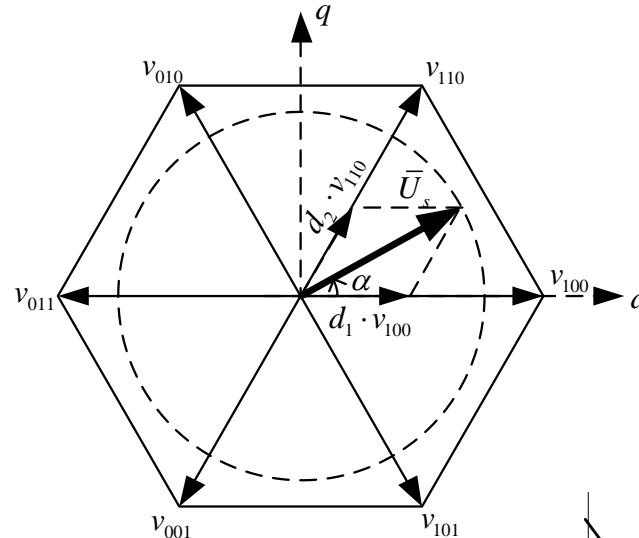
$$\bar{U}_s = d_1 \cdot \bar{v}_x + d_2 \cdot \bar{v}_y$$

$$d_1 = \sqrt{3} \frac{|U_s|}{U_{dc}} \sin(\alpha)$$

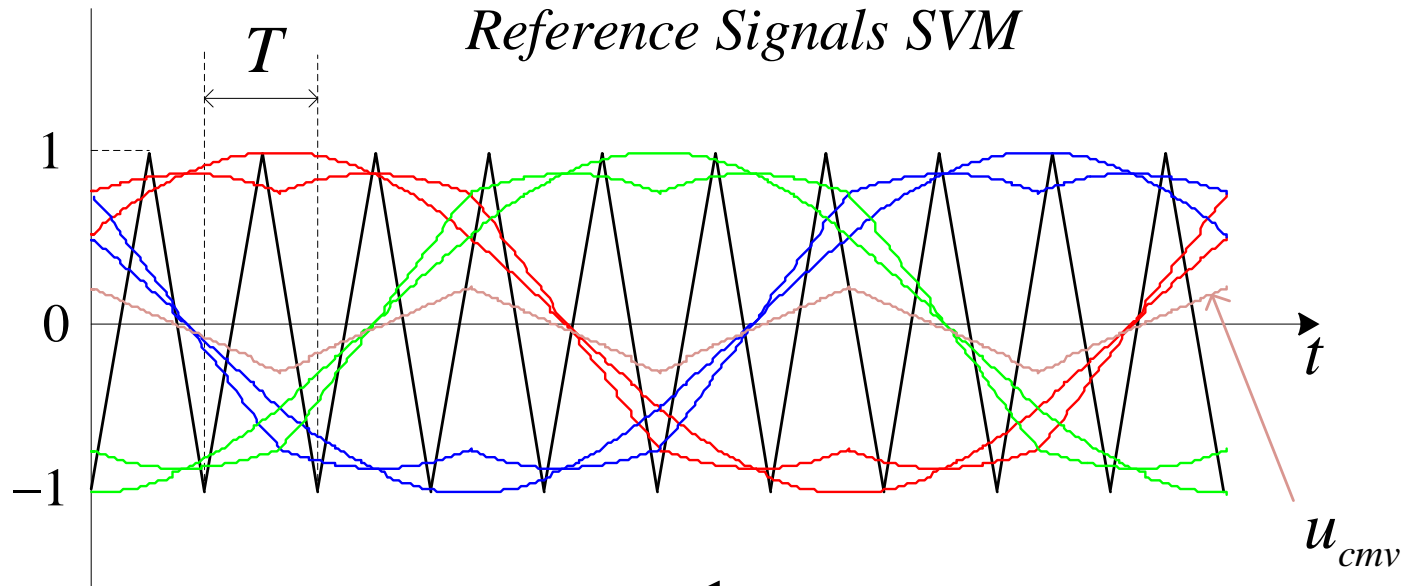
$$d_2 = \sqrt{3} \frac{|U_s|}{U_{dc}} \sin\left(\frac{\pi}{3} - \alpha\right)$$

$$d_{zv} = 1 - (d_1 + d_2)$$

- where  $d$  is the duty cycle



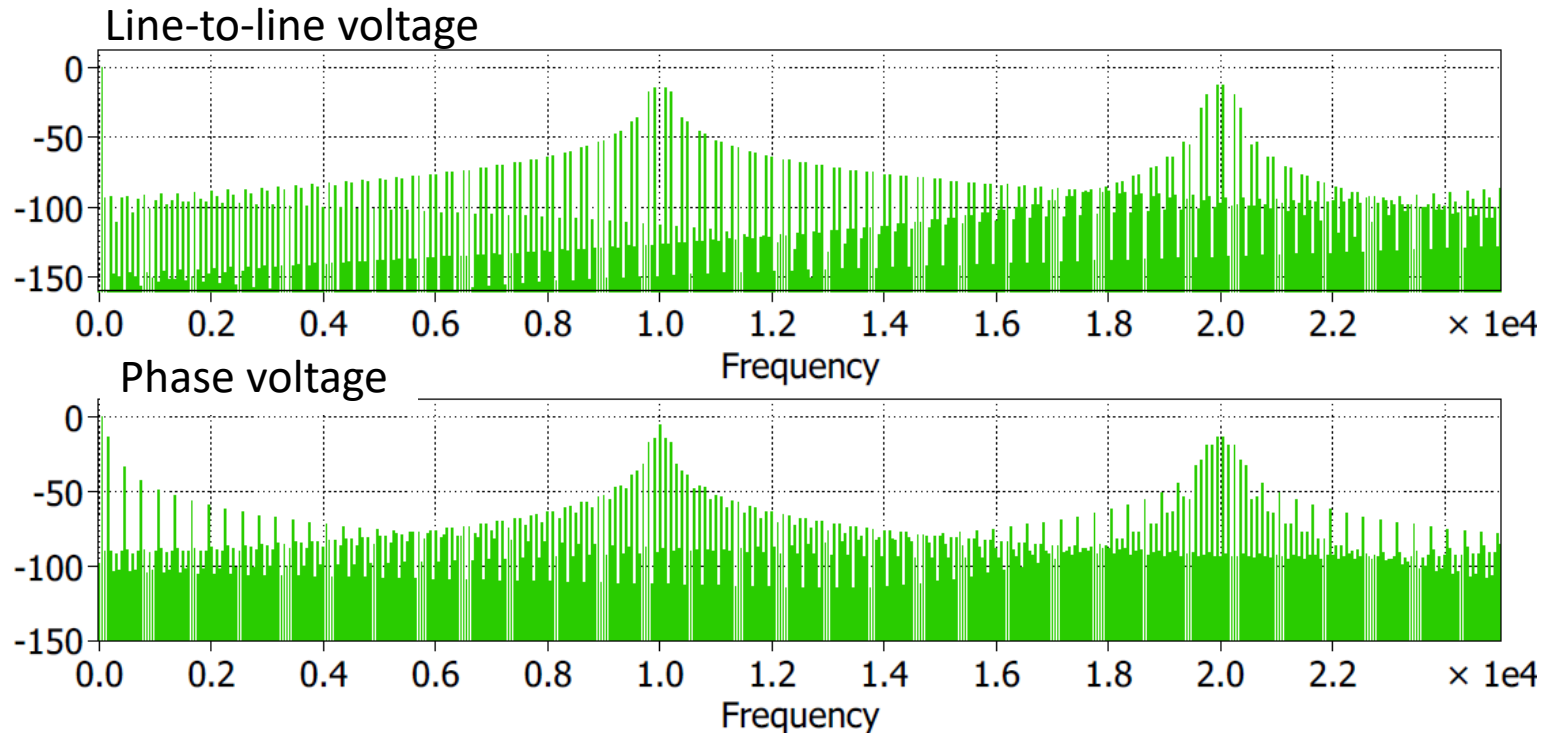
# SVM waveforms



$$t_{zv0} = t_{zv1} = \frac{1}{2} d_{zv} \cdot T_{\text{mod}}$$

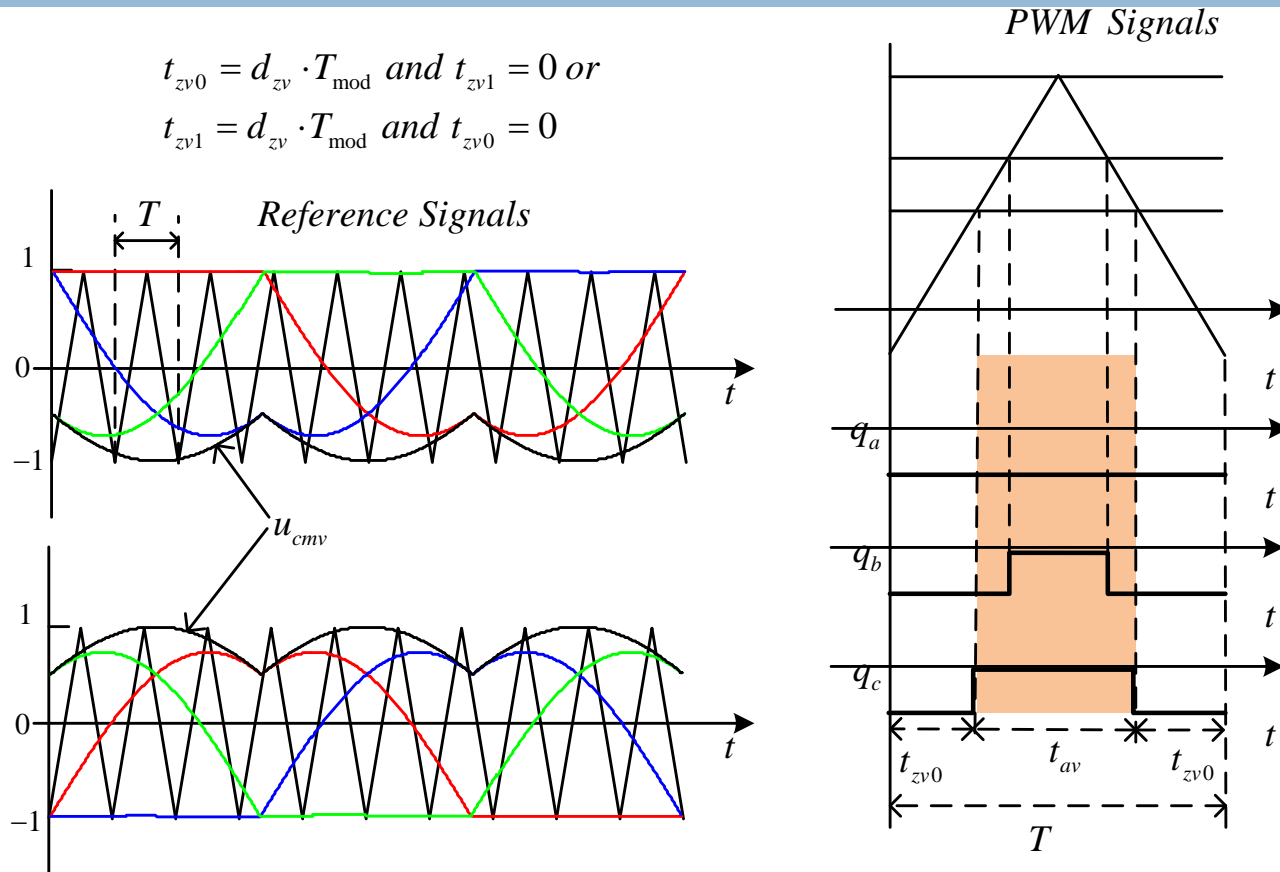
- By making the time spent for the generation of the two zero vectors equal is similar to add a triangular signal is added to the phase voltages

# SVM spectrum



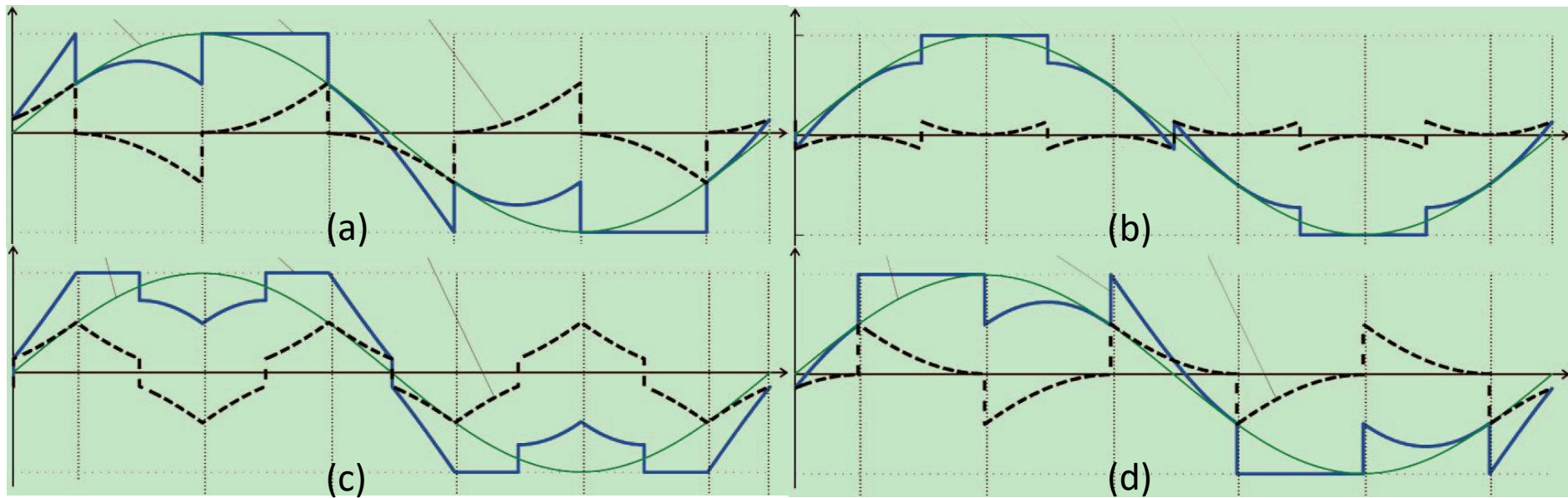
- High frequency region more harmonics are present, the amplitude of the harmonics are reduced with few dB

# 120° PWM



- Only one zero voltage vector is generated
- Number of switching is reduced with 25% (reduced switching losses)
- Increased stress for some of the components

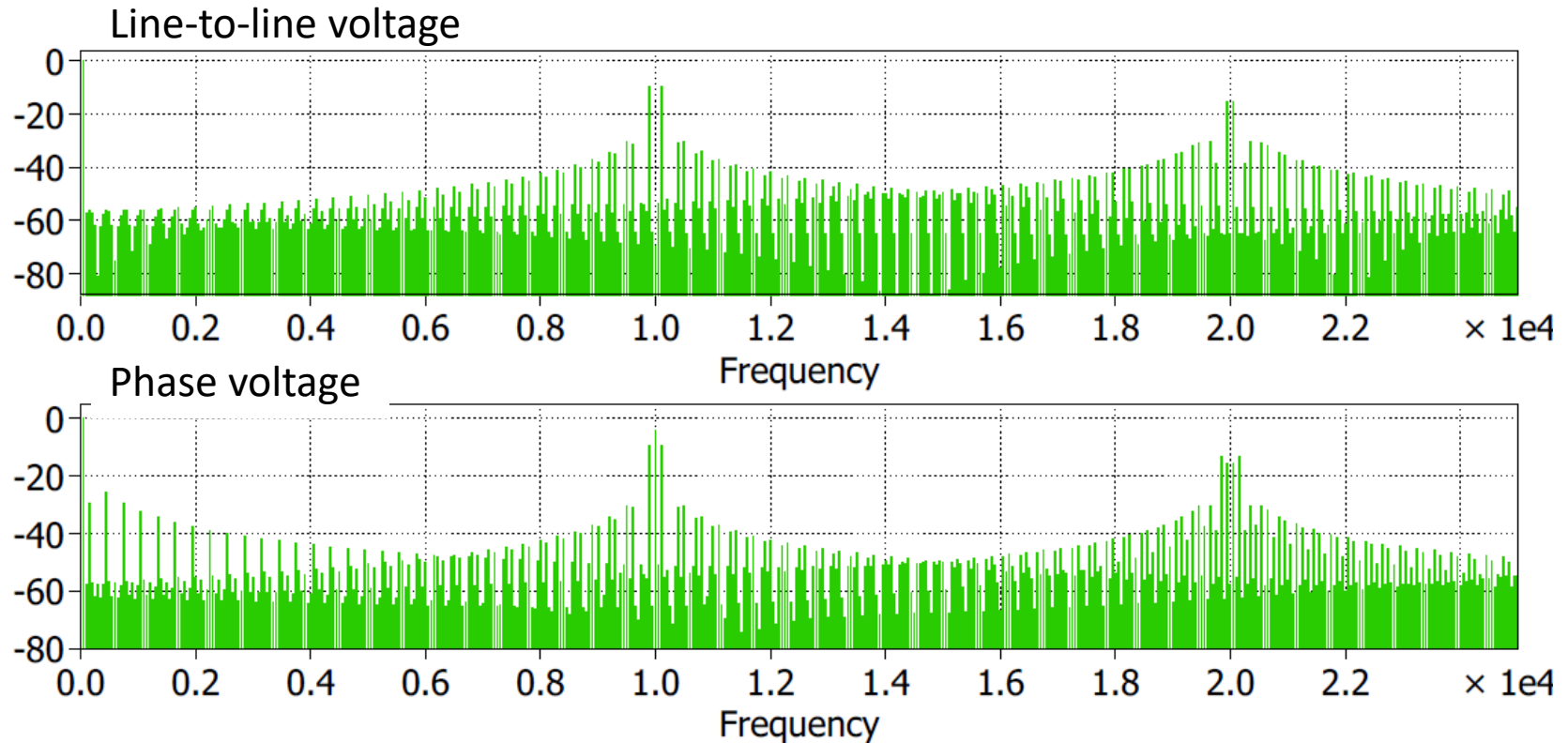
# Discontinuous PWM strategies



The two 120° PWM are alternatively applied for 60°, with a phase shift of: (a) 0 degree, (b) 30 degree, (c) 60 degree, (d) 90 degree

**Advantage:** better stress distribution for the switching devices

# Spectrum of DPWM



- Many harmonics are introduced

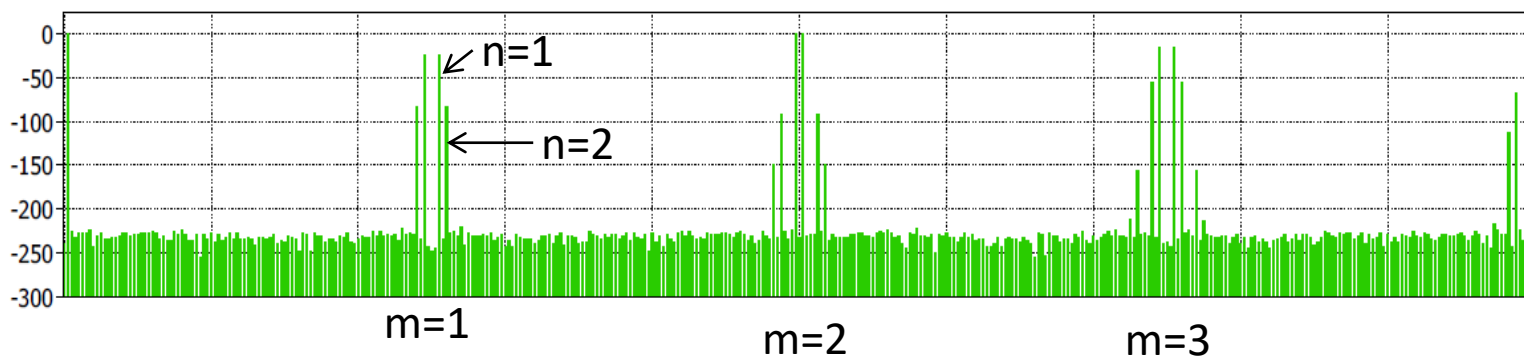


# Spectrum of the PWM signals

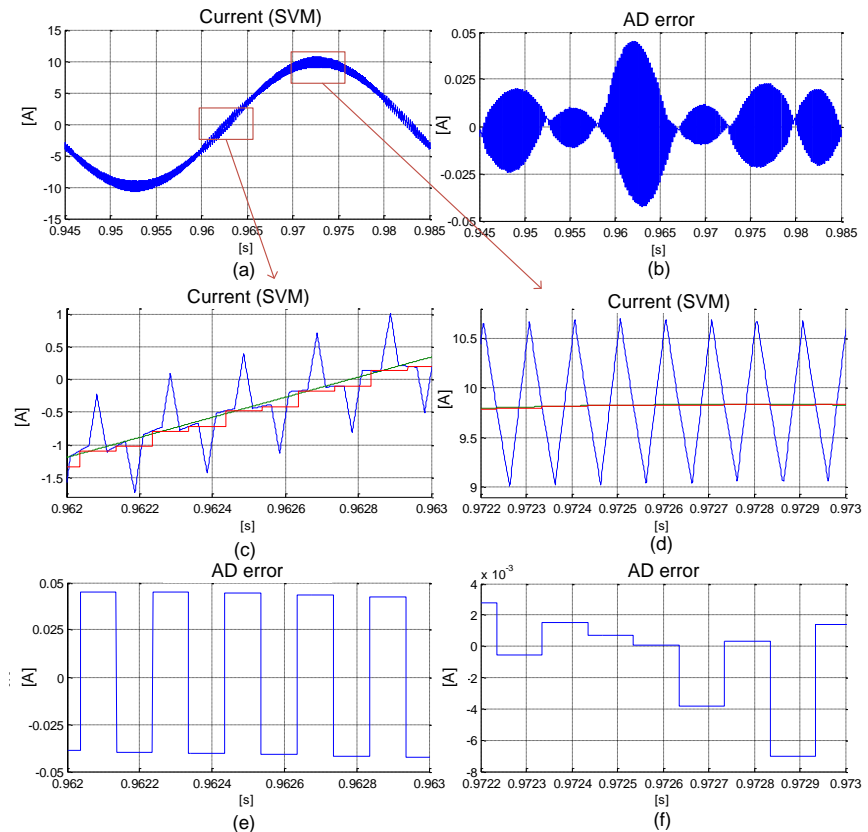
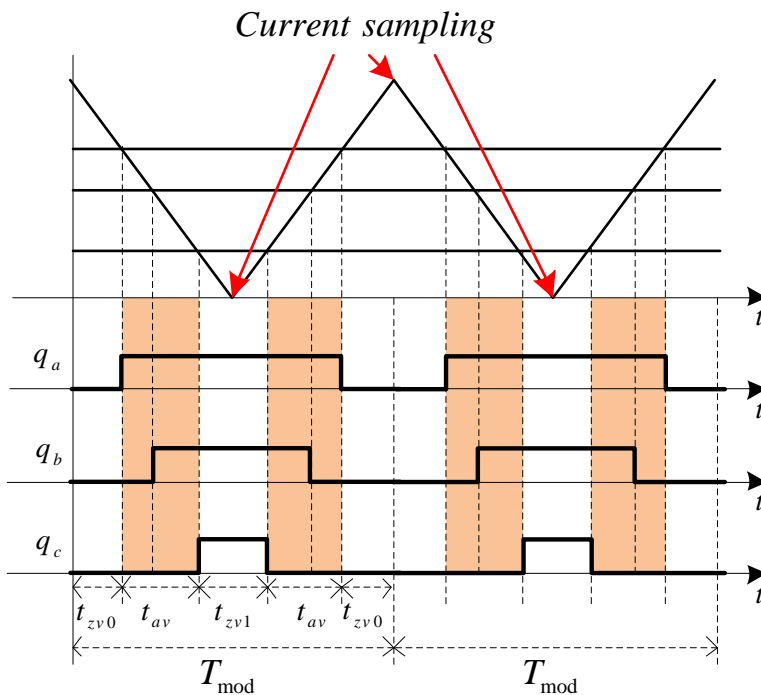
- The spectrum of the ST-PWM can be calculated by using:

$$u_{ag} = \frac{U_{dc}}{2} \left( 1 + M \cos(\omega_0 t + \theta_0) + \frac{4}{\pi} \sum_{m=1}^{\infty} \sum_{n=-\infty}^{\infty} \left( \frac{1}{m} J_n \left( m \frac{\pi}{2} M \right) \sin \left( (m+n) \frac{\pi}{2} \right) \times \cos \left( (m\omega_c + n\omega_c) t + (m\theta_c + n\theta_0) \right) \right) \right)$$

where,  $J_n(\beta)$  denotes the n-th order Bessel function of the first kind with the argument of  $\beta$ , M-is the modulation index,  $\omega_0$ -frequency of the fundamental component,  $\omega_c$ -carrier frequency, m- carrier harmonics and n-side band harmonics

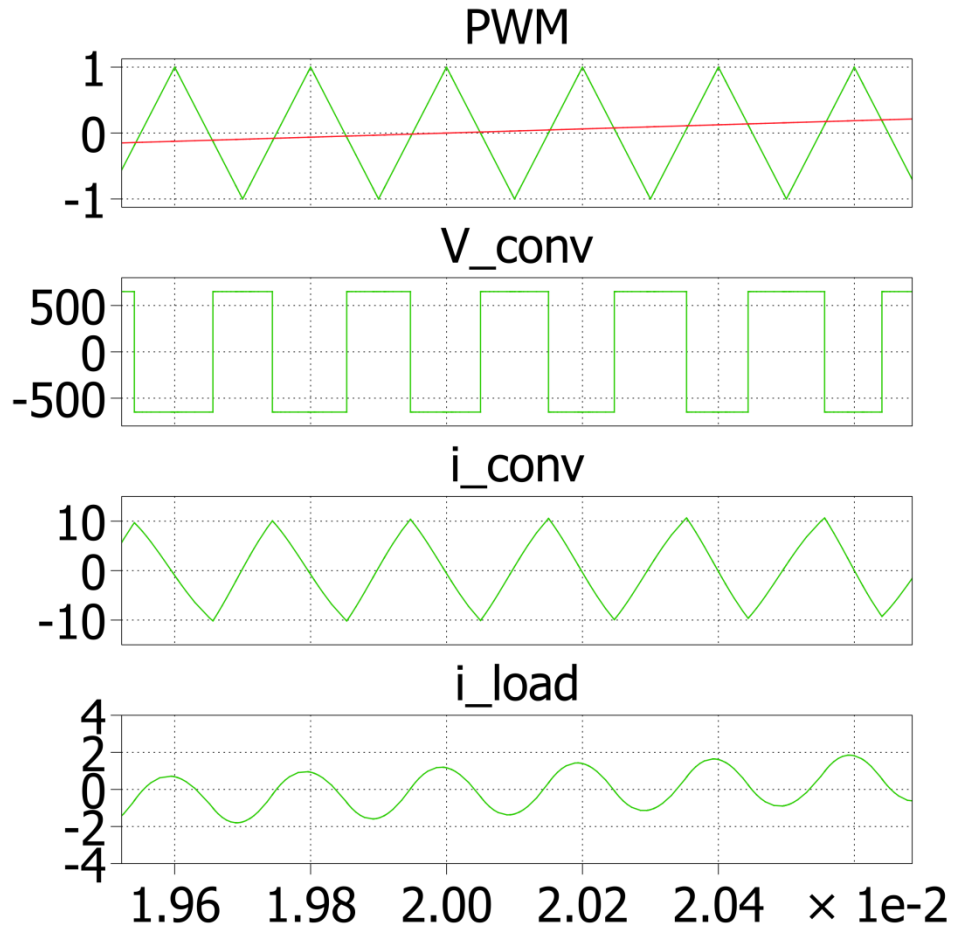
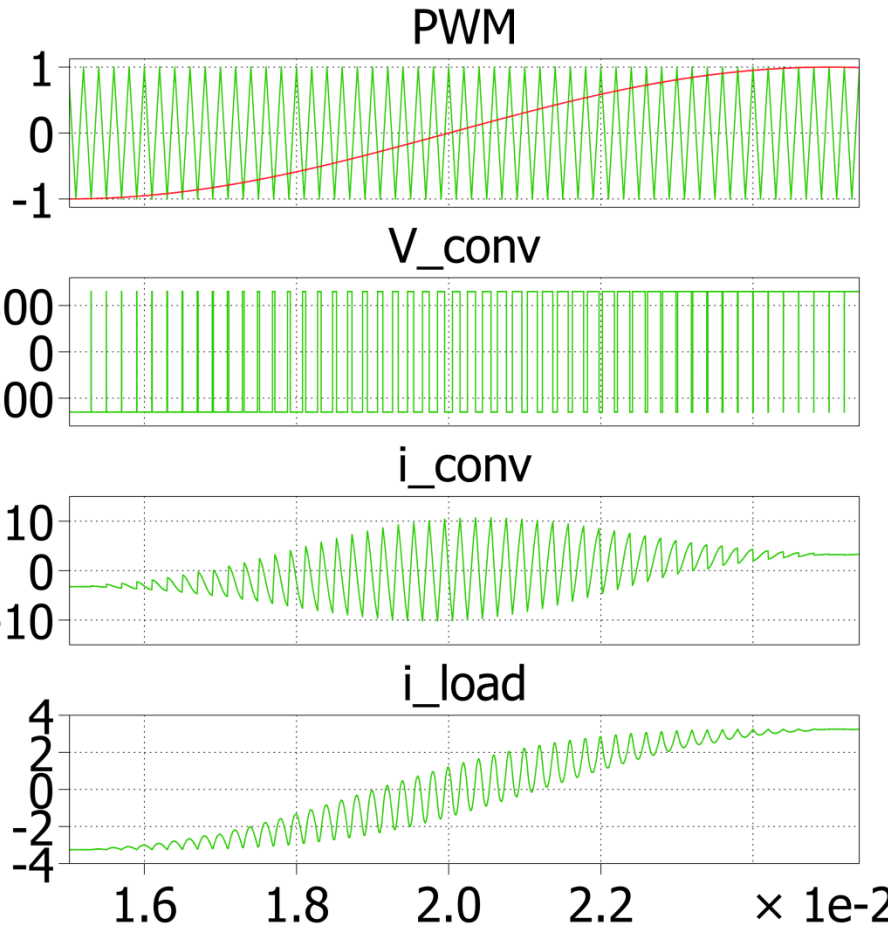


# Current measurement



- Current sampling has to be done in the middle of the time spent for generation of zero vectors (top and/or bottom of carrier)
- Note: in case of the DPWM methods the sampling can be done only once in a modulation period
- Sampling at TOP and BOTTOM results in minimum error
- At zero crossing the current sampling error will be maximum due to the slope of the current

# Current measurement



# Summary

**With a three phase system a rotating voltage vector can be created .**

## **ST-PWM with added 3rd harmonic**

- increase the linear range

## **Space vector modulation**

- smallest current ripple can be achieved

## **Discontinuous modulation**

- reduce the switching losses

## **Analytical spectrum calculation**

- the spectrum can be determined by using math. eq.

## **Current measurement**

# Exercise

- Implement the modulation types: SPWM, DPWM1, THIPWM and SVPWM in Simulink and use 'zero sequence signal calculator' the method is shown on Fig. 4.

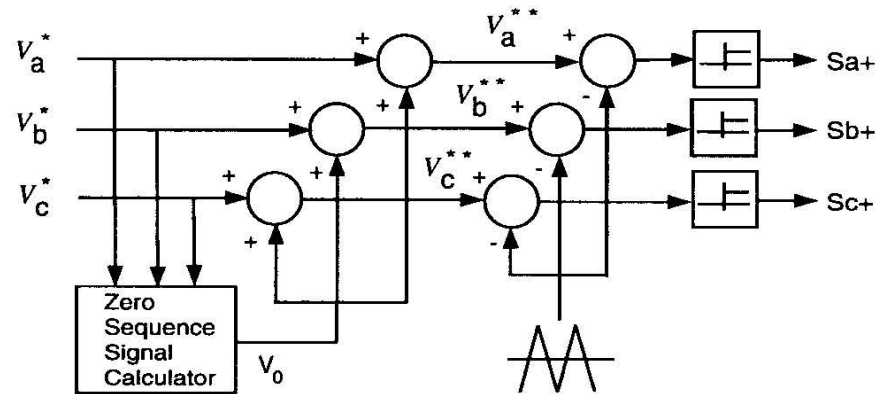


Fig. 4. The generalized signal block diagram of the triangle intersection technique-based PWM employing the zero-sequence injection principle.

- 1: Plot the  $v_a^{**}$  voltage of each modulation type.
- 2: Plot the inverter branch voltage:  
 $V_{dc}=100V$ ,  $f_1 = 50 \text{ Hz}$ ,  $f_s=1050\text{Hz}$ ,  $m_a=0.8$
- 3: Plot the inverter line to line voltage.
- 4: upload screen-shots to Moodle