

- 24 Funciones Bilineales: Transferencia de dos polinomios de primer orden. Puede darse caso que haya ganancia  $K$  o que algún polinomio sea de grado "0" (sólo 1 de los dos)

$$T(s) = K \cdot \frac{s+g}{s+p}$$

$$T_I(s) = \frac{K}{s}$$

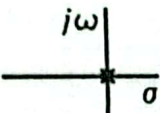
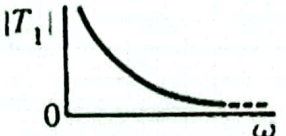
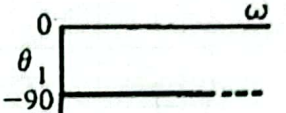

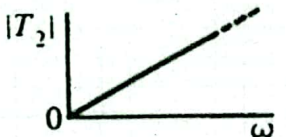
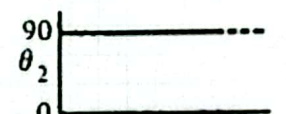
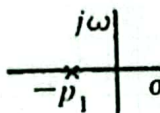
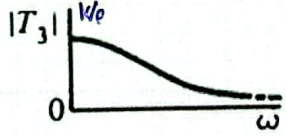
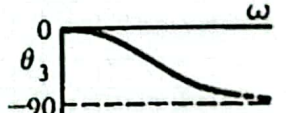
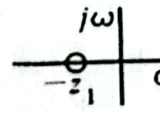
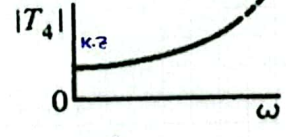
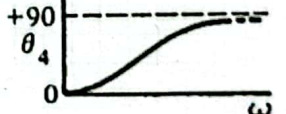
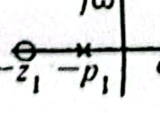
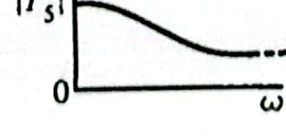

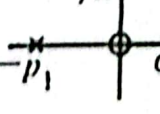
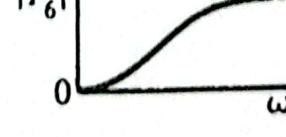
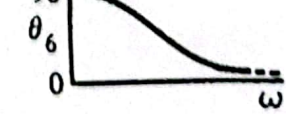
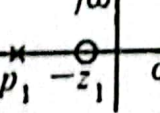
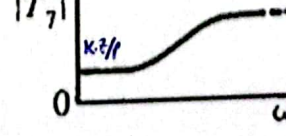
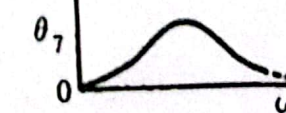
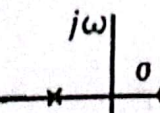
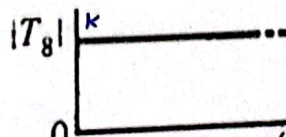
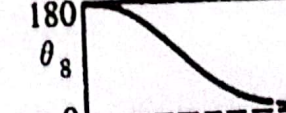
$$T_0 = s \cdot K \rightarrow \text{Integrador}$$

$$T_I(s) = \frac{K}{s+p_1}$$

$$T_0 = (s+p_1) \cdot K \rightarrow \text{Derivador}$$

Generalmente  $T(s) = K \cdot \frac{s+g}{s+p}$

- 25 Análisis de Módulo y Fase

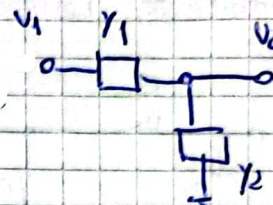
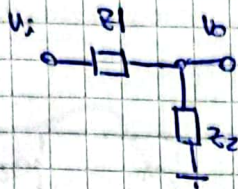
$T_n(s)^a$	Pole and Zero	Magnitude Response	Phase Response
$K > 0$			
$\frac{K_1}{s}$			
$K_2 s$			
$\frac{K_3}{s+p_1}$			
$K_4(s+z_1)$			
$K_5 \frac{s+z_1}{s+p_1}$			
$K_6 \frac{s}{s+p_1}$			
$K_7 \frac{s+z_1}{s+p_1}$			
$K_8 \frac{s-s_1}{s+s_1}$			



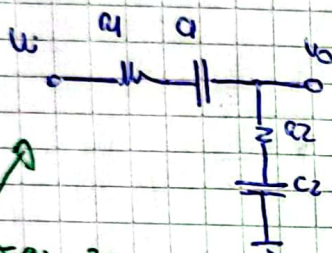
# Implementación por Resistores

$$T(s) = K \cdot \frac{s+p}{s+q}$$

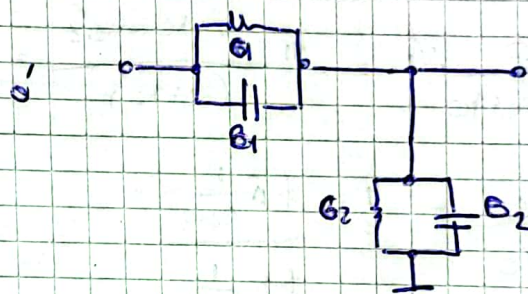
$K < 1$



- 0 Capacitor o bobina
- Para integrador → bobina y un capacitor.



$$T(s) = \frac{R2}{R1 + R2}$$



$$T(s) = \frac{R1}{R1 + R2}$$

$$T(s) = \frac{R2 + 1/sC2}{R1 + R2 + 1/sC1 + 1/sC2} = \frac{s(R2 + 1/C2)}{s(R1 + R2) + \frac{1}{C1} + \frac{1}{C2}} = \frac{R2 \cdot (s + \frac{1}{C2R2})}{s + \frac{1/R2 + 1/C2}{(R1 + R2)C2}}$$

$$T(s) = \frac{R2}{R1 + R2} \cdot \frac{s + \frac{1}{C2R2}}{s + \frac{C1 + C2}{C1C2(R1 + R2)}}$$

$$T(s) = \frac{G1 + sC1}{G1 + sC1 + G2 + sC2} = \frac{C1}{C1 + C2} \cdot \frac{s + \frac{G1}{C1}}{s + \frac{G1 + G2}{C1 + C2}}$$

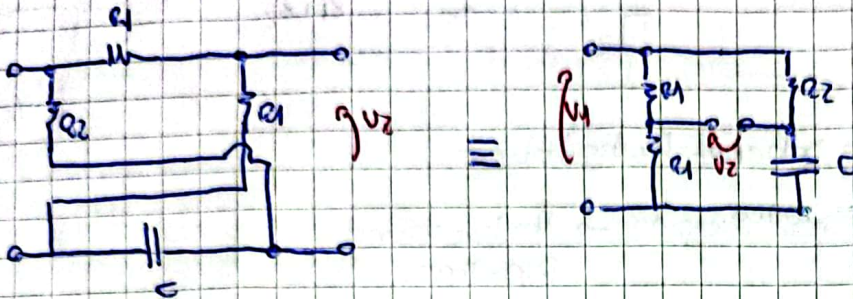
$$T(s) = \frac{C1}{C1 + C2} \cdot \frac{s + G1/C1}{s + \frac{G1 + G2}{C1 + C2}}$$



Com estas duas formas no conseguimos o paralelo.

① → Pro paralelo passivo:

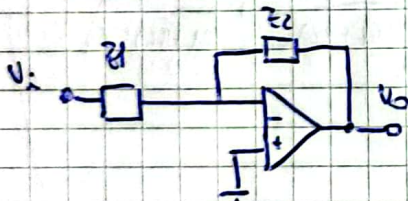
Circuito de Lattice



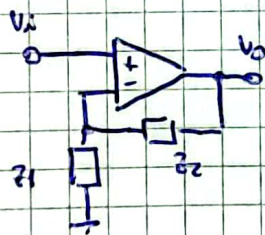
$$U_2(\phi) = \frac{U_1}{2} \cdot \frac{G_2}{G_1 + \phi C} = U_1 \cdot \frac{G_2 + \phi C - G_2}{2(G_2 + \phi C)} = U_1 \cdot \frac{1}{2} \cdot \frac{\phi - \frac{G_2}{C}}{\phi + \frac{G_2}{C}}$$

$$T(\phi) = \frac{1}{2} \cdot \frac{\phi - \frac{G_2}{C}}{\phi + \frac{G_2}{C}} = \frac{1}{2} \cdot \frac{\phi - \frac{1}{R_2 C}}{\phi + \frac{1}{R_2 C}}$$

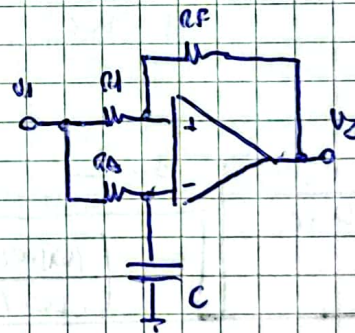
Implementação do U2



$$T(\phi) = -\frac{Z_2}{Z_1}$$



$$T(\phi) = 1 + \frac{Z_2}{Z_1} = \frac{Z_1 + Z_2}{Z_1}$$



$$T(\phi) = -K \cdot \frac{\phi - \frac{1}{K \cdot C \cdot R_A}}{\phi + \frac{1}{K \cdot C \cdot R_A}}$$

$$K = \frac{R_F}{R_A}$$

- Se considerarmos RA por C  
→ C por RA

Operação no inversor



$$T(b) = \frac{s^2 + s \cdot \frac{\omega_0}{Q} + \omega_0^2}{s^2 + s \cdot \frac{\omega_0}{Q} + \omega_0^2}$$

TABLE 5.1 Standard Forms of Second-Order Responses

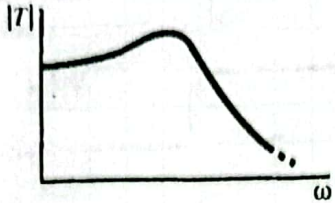
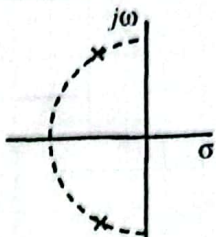
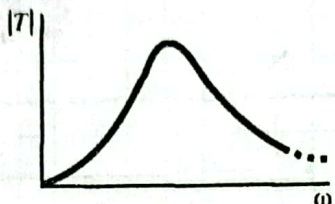
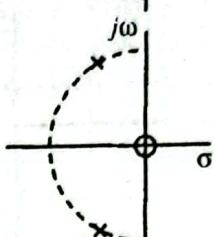
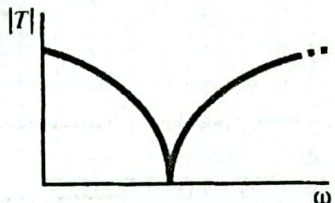
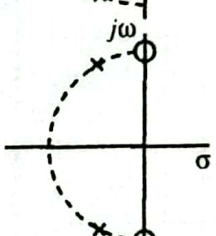
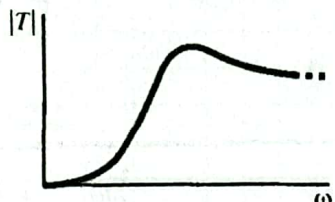
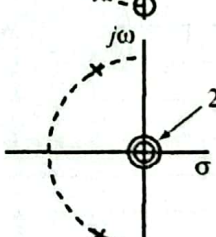
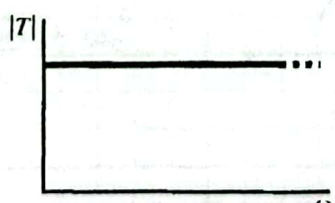
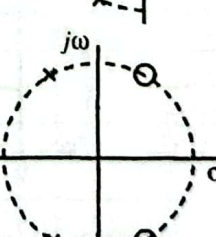
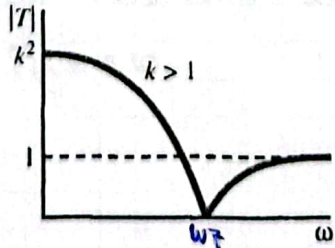
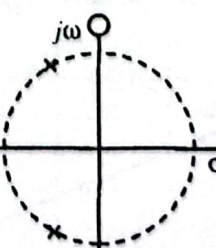
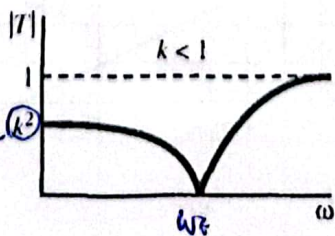
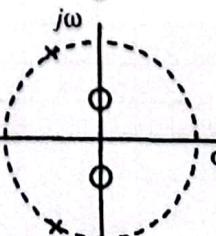
	Frequency Response	Poles/Zeros	Name
$T_{LP} = \frac{\omega_0^2}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}$			Lowpass
$T_{BP} = \frac{\frac{\omega_0}{Q}s}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}$			Bandpass
$T_{BS} = \frac{s^2 + \omega_0^2}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}$			Bandstop "notch"
$T_{HP} = \frac{s^2}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}$			Highpass
$T_{AP} = \frac{s^2 - \frac{\omega_0}{Q}s + \omega_0^2}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}$			Allpass
$T_{LPN} = \frac{s^2 + k^2 \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$ $k > 1$			Lowpass notch
$T_{HPN} = \frac{s^2 + h^2 \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$ $k < 1$			Highpass notch



TABLE 5.2 Common Forms of  $N(s)$  and Phases of  $N(j\omega) \rightarrow$  *Memoria de Frecuencia de Corte*

Name	$N(s)$	$N(j\omega)$	Plot of $\theta_1(\omega)$
Lowpass	$\omega_0^2$	$\omega_0^2$	
Bandpass	$\frac{\omega_0}{Q}s$	$j\frac{\omega_0\omega}{Q}$	
Bandstop	$s^2 + \omega_0^2$	$-\omega^2 + \omega_0^2$	
Highpass	$s^2$	$-\omega^2$	

si analizas la Frecuencia de Corte Tienen algunas formas para mostrar el BE. De las que son iguales solo le cambian los límites (o sea desplazados)

$\phi$ , degrees for case:

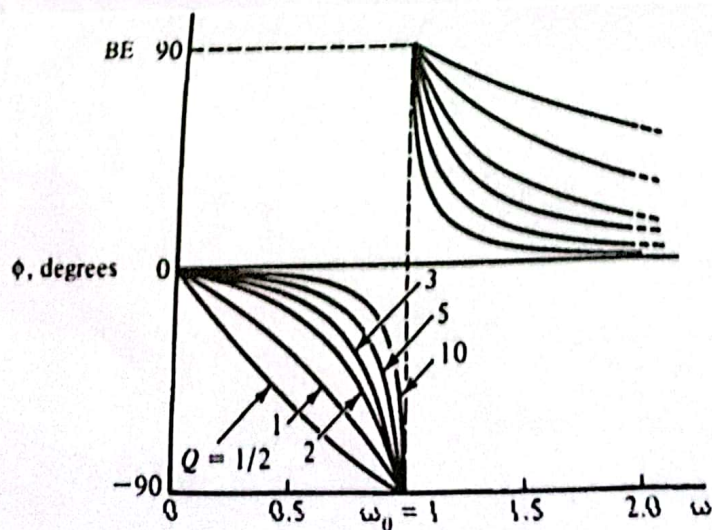
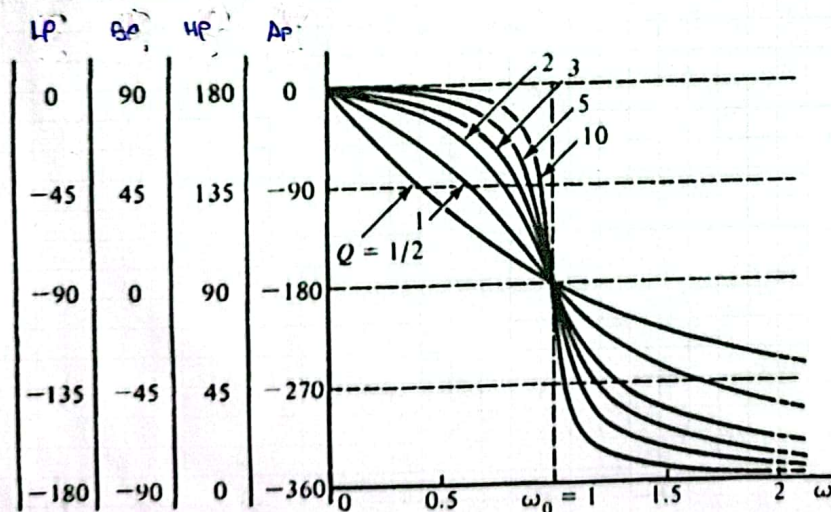
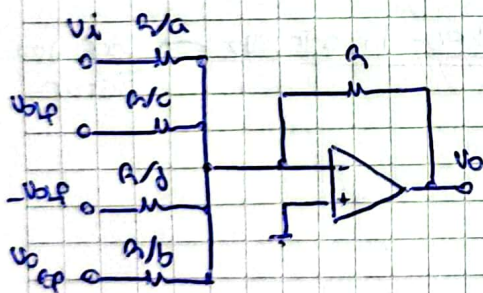
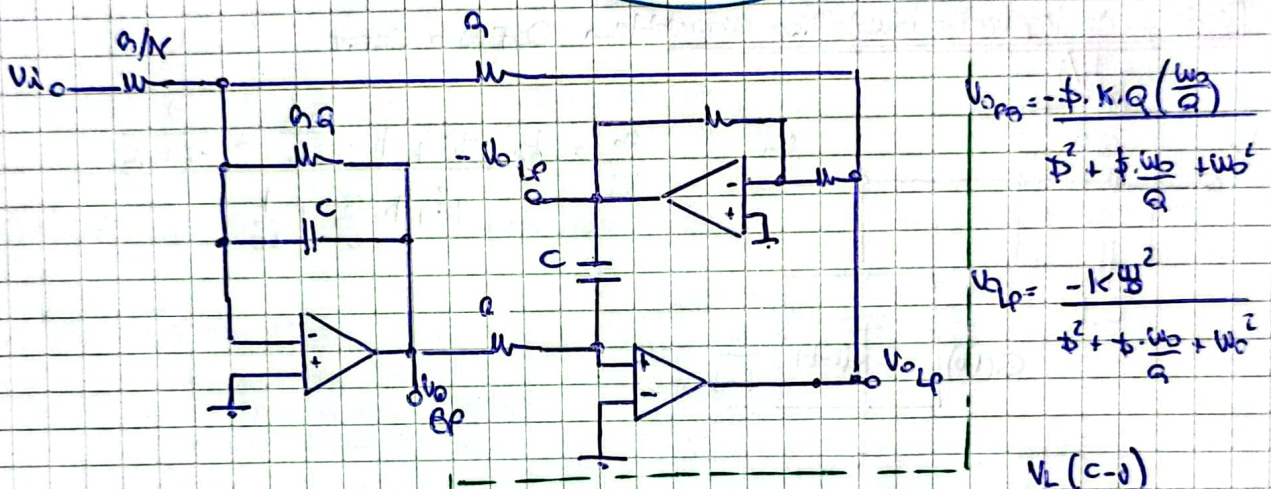
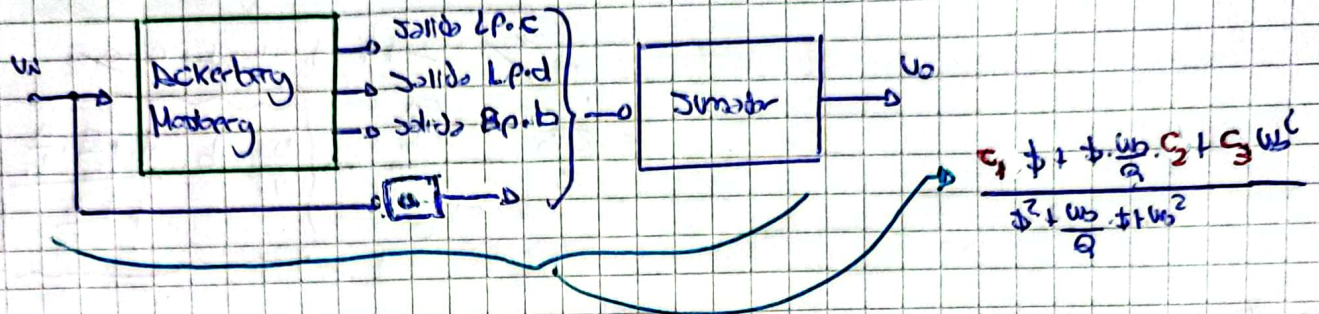


Figure 5.10 The phases of the most common second-order filters.



# Implementación de Función Bivariante por Suma de Transferencia

Para poder implementar una transferencia ajustada podemos hacer lo siguiente:



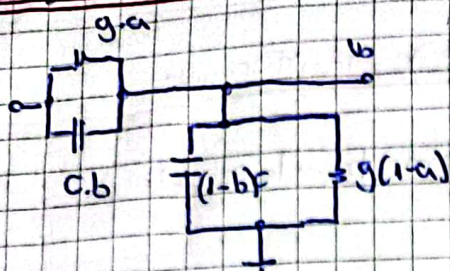
$$u_o = u_i \cdot \left( a + b \cdot \frac{-k \omega_0 \frac{\omega_0}{Q}}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2} + c \cdot \frac{-k \omega_0^2}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2} (c-d) \right)$$

$$\frac{u_o}{u_i} = \frac{a \left( s^2 + \frac{\omega_0}{Q} s + \omega_0^2 \right) - b \left( k \omega_0 \frac{\omega_0}{Q} \right) + (d-c) k \omega_0^2}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$

$$\frac{u_o}{u_i} = \frac{a \cdot s^2 + \frac{\omega_0}{Q} (a - b k \omega_0) s + \omega_0^2 [a + k(d-c)]}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$



② Estrategia de implementación bilingüe configurable → Configuración Cerrar

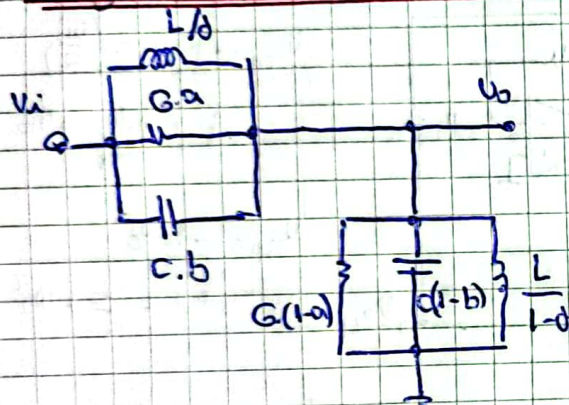


$$\frac{U_o}{U_i} = \frac{(G_a + c_b \phi)}{(G_a + c_b \cdot (1-b)\phi + (1-a)c)} \\ = c_b \left( \frac{G_a}{c_b} + \phi \right)$$

$$G_a + c_b \phi + c_b \phi - b\phi + c - a c$$

$$= \frac{c \cdot b}{c} \frac{\phi + \frac{G_a}{c_b}}{\phi + \frac{c}{c}} \rightarrow \boxed{\frac{U_o}{U_i} = b \cdot \frac{\phi + \frac{G_a}{c} \cdot \frac{a}{b}}{\phi + \frac{c}{c}}}$$

③ Estrategia de implementación bilingüe configurable → Configuración Cerrar



$$\frac{U_o}{U_i} = b \cdot \frac{\phi^2 + \phi \cdot \frac{G_a}{c_b} + \frac{a}{c \cdot b \cdot i}}{\phi^2 + \phi \cdot \frac{G}{c} + \frac{1}{Lc}}$$

④ Aplicando otro concepto al Áckerberg-Mossberg, puede modificarse la estructura → Configuración Cerrar

SECOND-ORDER FILTERS WITH ARBITRARY TRANSMISSION ZEROS

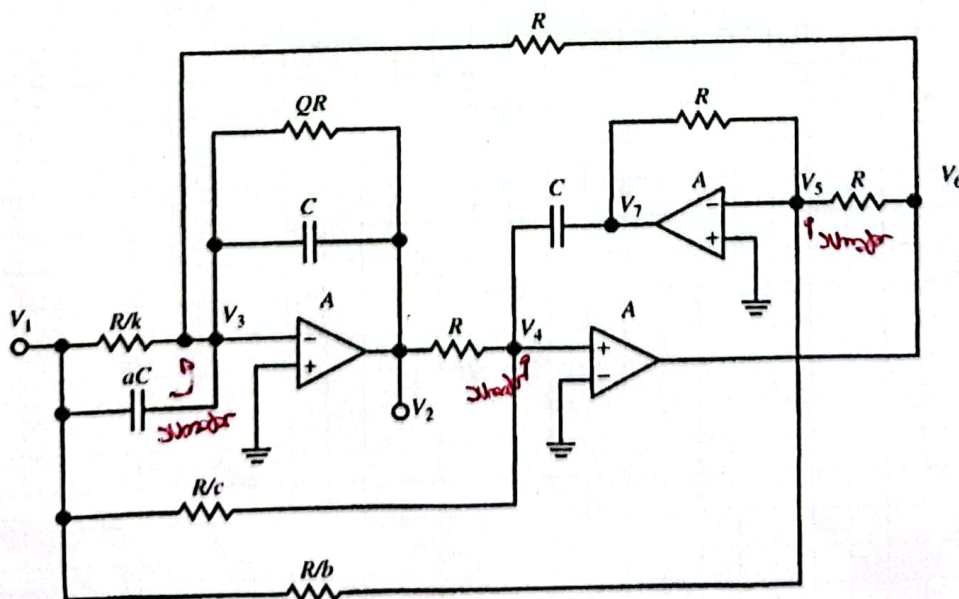


Figure 5.13 The general Áckerberg-Mossberg biquad.

$$\gamma(\phi) = - \frac{a\phi^2 + \phi \cdot \omega_0(\kappa - b) + c \cdot \omega_0^2}{\phi^2 + \phi \cdot \frac{\omega_0}{R} + \omega_0^2}$$

$$\omega_0 = \frac{1}{RC}$$