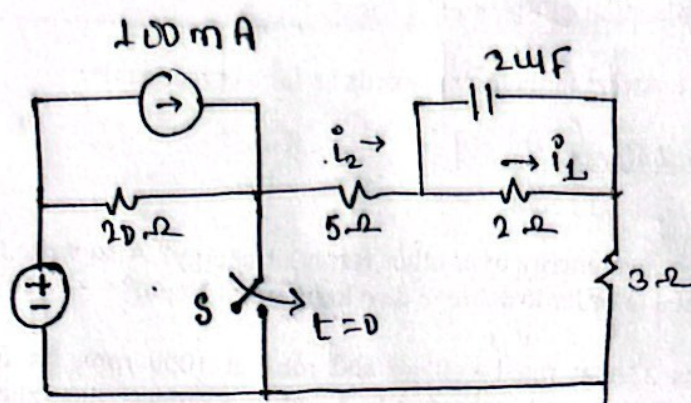


Q1) Soln

Find (a) $i_1(0^-)$, $i_2(0^-)$
 ~~$i_1(0^-)$~~

(b) $i_1(0^+)$, $i_2(0^+)$

(c) $i_1(t)$ for $t > 0$



Note → The term used in the qⁿ is 'switch' is closed at $t=0$ after being opened for long time; the significance of the statement is that capacitor has sufficient time to discharge or in other words it has enough time to reach D.C. steady state value, before we turn on the switch.

(a) Soln Find $i_1(0^-)$ & ~~$i_1(0^-)$~~ $i_2(0^-)$

Step 1: For 100 mA we are going for PCS to PVS conversion

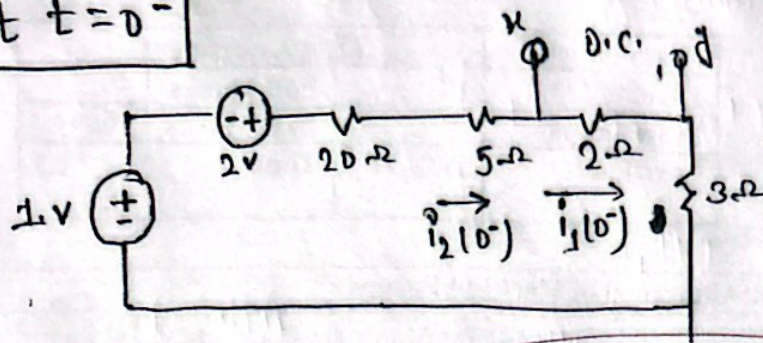
PCS → practical current source

PVS → practical voltage source.

Step 2: The capacitor is modelled as D.C. in D.C. steady state.

→ the eqv ckt after step 1 & step 2 is

At $t=0^-$



At $t=0^-$; $i_2(0^-) = i_1(0^-) = \frac{V}{R_{eq}} = \frac{1+2}{20+5+2+3}$

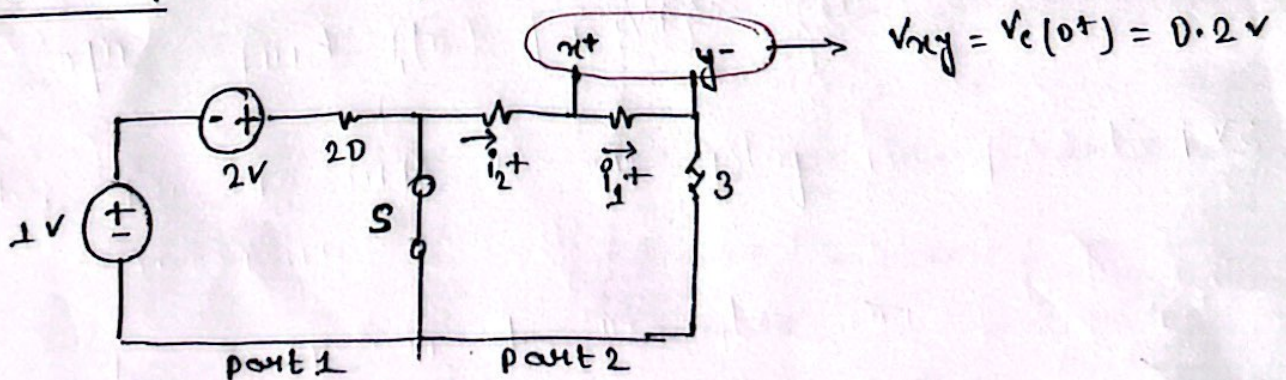
$i_1(0^-) = i_2(0^-) = \frac{3}{30} = 0.1 \text{ A}$

Note : We know voltage across capacitor will not change instantly, $\therefore V_{xy} = V_c(0^-) = 2 \times 0.1$
 $= 0.2 \text{ V} =$

$\therefore V_c(0^+) = V_c(0^-) = 0.2 \text{ V}$

(b) find $i_1(0^+)$ & $i_2(0^+)$

At $t=0^+$ the eqv. circuit is

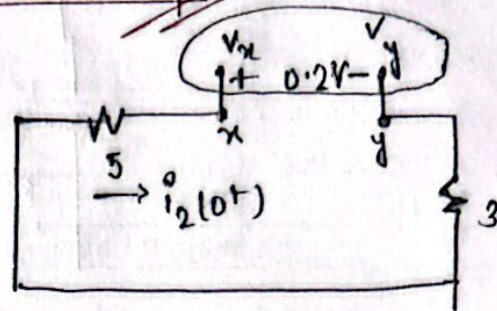


Note : The switch divides the circuit in 2 part
Hence, KVL in part ① has no effect on KVL in part 2

Since, $V_{xy} = V_c(0^+) = 0.2 \text{ V}$

$$\therefore \boxed{i_1(0^+) = \frac{0.2}{2} = 0.1 \text{ A}}$$

KVL in part 2



$$5i_2(0^+) + 0.2 + 3i_2(0^+) = 0$$

$$8i_2(0^+) = -0.2$$

$$\therefore \boxed{i_2(0^+) = -\frac{0.2}{8} = -0.025 \text{ A}}$$

(Note) \rightarrow KCL at x, y gives $i_{3\Omega} = i_2(0^+) = -0.025 \text{ A}$

(Note) $\underline{i_1(0^-) = i_1(0^+)}$, But $\underline{i_2(0^-) \neq i_2(0^+)}$

\downarrow
Because 'C' is
in parallel with 2Ω , through
which i_1 flows.

\downarrow
 i_2 is current -
- through resistor (5Ω),
For L, C only Inductor
Current & capacitor voltage
is a continuous fn of
time (ie. do not change
instantly, but for Resistor
(5Ω) we can certainly
have instantaneous
change in voltage &
current, & there is nothing
preventing that from happening
 i_2 current branch.

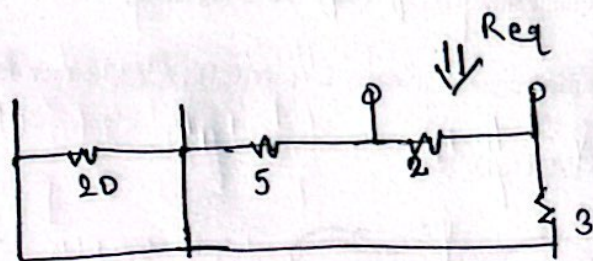
(c) let $x_f \rightarrow$ Final value
 $x_0 \rightarrow$ Initial value

The general soln of the electrical circuit is

$$x(t) = x_f + (x_0 - x_f) e^{-t/\tau}$$

\rightarrow 1st: ~~sketch~~ sketch the system for $(t \geq 0)$

\rightarrow 2nd: use thevenins theorem & find eq^v Resistance as seen by energy storing element (ie. Req from capacitor point of view)



$$R_{eq} = 8 \parallel 2$$

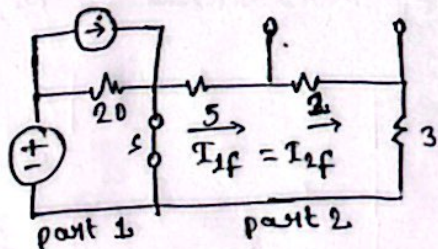
$$= 1.6 \Omega$$

\therefore Time constant $\tau = R_{eq} \times C$ (For RC ckt)

$$= 1.6 \times 2.4 \mu F$$

$$= 3.2 \mu s$$

\rightarrow 3rd: $i_{1f} = ? \rightarrow$ Final value ($t \rightarrow \infty$) sketch the circuit under DC steady state situation (the appropriate model of capacitor will be O.C.)

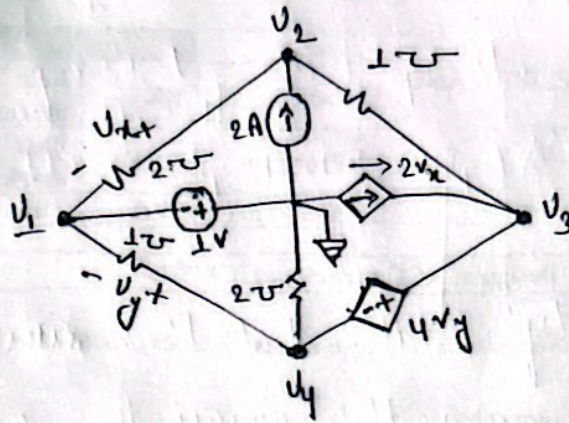


\rightarrow Switch is closed, No interaction b/w Part 1 & Part 2 loop $\therefore I_{1f} = I_{2f}$
 Since no any source is present in loop 2

$$\therefore i_{1f}(t) = 0 + (0.1 - 0) e^{-t/3.2 \mu s}$$

$$\therefore i_{1f}(t) = 0.1 e^{-3.2 t / 10^6} \text{ A}$$

Q2) Obtain the node voltage v_1, v_2, v_3, v_4



Soln Voltage b/w Node-1 & Ref Node is

$$v_1 = -1V \longrightarrow (1)$$

KCL at Node 2: $2 = (v_2 - v_1) \times 2 + (v_2 - v_3) \times 1$

$$2 = (v_2 - (-1)) \times 2 + (v_2 - v_3)$$

$$3v_2 - v_3 = 0 \longrightarrow (2)$$

KCL at Super Node (3) & (4)

$$2v_x = (v_3 - v_2) \times 1 + v_4 \times 2 + (v_4 - v_1) \times 1$$

But $v_x = v_2 - v_1$

Then, $2(v_2 - v_1) = (v_3 - v_2) \times 1 + v_4 \times 2 + (v_4 - v_1) \times 1$

$$\text{or, } v_1 - 3v_2 + v_3 + 3v_4 = 0$$

$$-1 - 3v_2 + v_3 + 3v_4 = 0$$

$$-3v_2 + v_3 + 3v_4 = 1 \longrightarrow (3)$$

Voltage b/w Node (3) & (4) is; $v_3 - v_4 = 4v_y$

But, $v_y = v_4 - v_1$

Then, $v_3 - v_4 = 4(v_4 - v_1)$

$$\text{or, } v_3 - 5v_4 = 4 \longrightarrow (4)$$

Solving (2), (3), (4) we get $v_2 = 1.89V, v_3 = 5.67V$
 $\phi v_4 = 0.33V$