## DIGITAL CONTROL SYSTEMS MAE 444/544 Project 2

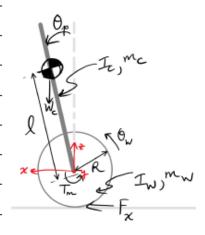
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Part One: Designing a regulator for a self-balancing robot. For this part of the project, you will design a controller that keeps this robot upright, by commanding the wheels to spin at the right speed.

## Vehicle Parameters:

Stepper Motor Mass, $m_{SM}$	300 g (each)
Motor Rotor Inertia, $I_R$	54 g·cm² (each)
Tire Mass, $m_T$	52 g (each)
Tire Inertia, $I_T$	520 g⋅cm² (each)
Tire Radius, $R$	4 cm
Frame Mass, $m_F$	160 g
Arduino and Breadboard, $m_A$	100 g
Battery Mass, $m_B$	120 g
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## Combined Parameters:

Chassis Combined Mass, $m_C$	980 g
Chassis Combined Inertia about Axle, $I_C$	92,336 g·cm <sup>2</sup>
Distance from Axle to CG of Chassis, ℓ	6 cm
Wheel and Rotor Combined Mass, $m_W$	150 g
Wheel and Rotor Combined Inertia, $I_W$	1150 g⋅cm <sup>2</sup>

The linearized equation of motion for the self-balancing robot is given by

$$\alpha \ddot{\theta}_p - \eta \theta_p = -\gamma \ddot{\theta}_w \tag{1}$$

where

1. 
$$\alpha = I_C + m_C R \ell$$

2. 
$$\eta = m_C g \ell$$
 (where  $g = 981$  cm/s<sup>2</sup>)

3. 
$$\gamma = I_W + (m_W + m_C)R^2$$

We measure **two outputs**: the pitch rate of the robot,  $\dot{\theta}_p$ , and the angular velocity of the wheels,  $\dot{\theta}_w$ . The system has **one control input**: the angular acceleration of the wheels,  $\ddot{\theta}_w$ . Therefore,

Therefore, 
$$\mathbf{y} = \begin{bmatrix} \dot{\theta}_p \\ \dot{\theta}_w \end{bmatrix}$$
 and  $u = \ddot{\theta}_w$ 

## Project Deliverables: Part One

 Derive the A<sub>c</sub> and B<sub>c</sub> matrices from the continuous-time state-space model for the system, assuming that the system states are given by

$$\mathbf{x} = \begin{bmatrix} \theta_p \\ \dot{\theta}_p \end{bmatrix} \tag{2}$$

You may write these matrices in terms of the parameters  $\alpha$ ,  $\eta$ , and  $\gamma$  (you don't have to plug in all the numbers right now, in other words).

- Using your results from the previous part, derive the A and B matrices for the discretetime state-space model, assuming that the sampling frequency is f<sub>s</sub> = 100 Hz. You should do this in MATLAB, using the provided numerical values for each parameter.
- Add the wheel velocity, θ̂<sub>w</sub>(k) as an additional state to your discrete-time state-space model, where

$$\dot{\theta}_w(k) = \dot{\theta}_w(k-1) + \ddot{\theta}_w(k-1) \cdot T$$
 (3)

so that the state vector becomes

$$\mathbf{x}(k) = \begin{bmatrix} \theta_p(k) \\ \dot{\theta}_p(k) \\ \dot{\theta}_w(k) \end{bmatrix}$$
(4)

Derive new A and B matrices to accommodate this additional state.

4. Now, define the control input as

$$\ddot{\theta}_w(k) = u(k) = -Kx(k)$$
 (5)

and calculate the feedback gain matrix, K, such that the closed-loop system settling time is approximately 1.5 s, with 30% overshoot.

5. Next, we need to design an estimator to give θ̂<sub>p</sub>(k), Θ̂<sub>p</sub>(k), and Θ̂<sub>w</sub>(k) at each time step. We measure Θ̂<sub>p</sub>(k) with a gyroscope, and let us assume that we also measure Θ̂<sub>w</sub>(k) (we know the wheel velocity fairly accurately because we regulate the stepper motor timing). Therefore, assume that our output equation is

$$\mathbf{y}(k) = \begin{bmatrix} \dot{\theta}_p(k) \\ \dot{\theta}_w(k) \end{bmatrix} = C\mathbf{x}(k)$$
 (6)

Appropriately define C, then use the place command in MATLAB to calculate the L matrix so that the state estimation error has a settling time of  $0.5 \, \mathrm{s}$ , and an overshoot of 20%. (The reason we use the place command instead of acker is that acker only works for systems with one output. Here, we have two outputs.) You can use the following syntax: L = place(A', C', betastar)' where betastar is a vector of your estimator poles.

Given your controller and your estimator, simulate the closed-loop system response in MATLAB. Assume that the true initial state vector is

$$\mathbf{x}(0) = \begin{bmatrix} \theta_p(0) \\ \dot{\theta}_p(0) \\ \dot{\theta}_w(0) \end{bmatrix} = \begin{bmatrix} 0 \\ 0.2 \\ 0 \end{bmatrix}$$
(7)

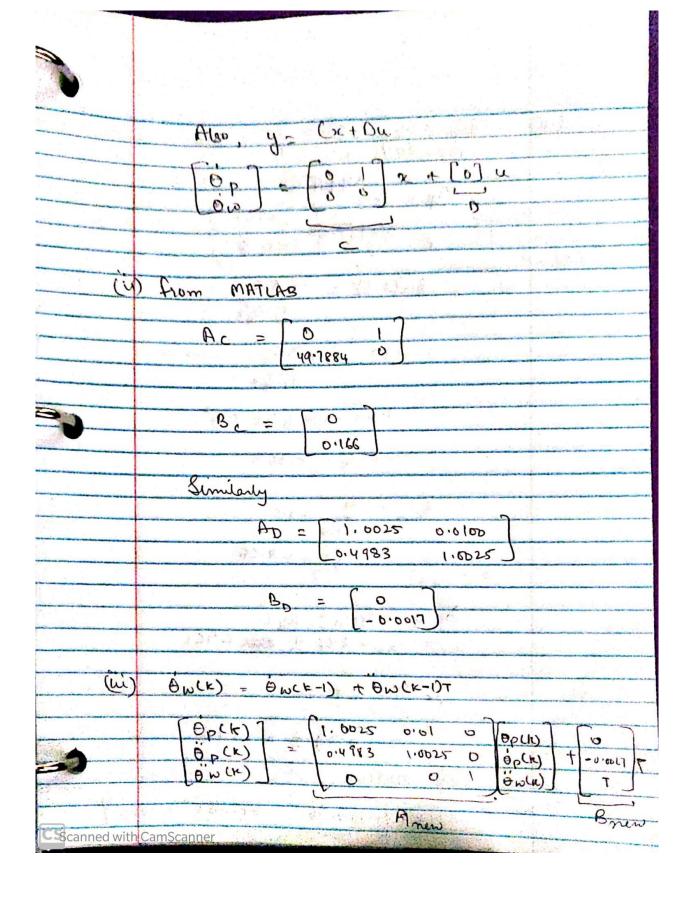
and that the estimated initial state vector is

$$\hat{\mathbf{x}}(0) = \begin{bmatrix} \hat{\theta}_p(0) \\ \hat{\theta}_p(0) \\ \hat{\theta}_w(0) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$
(8)

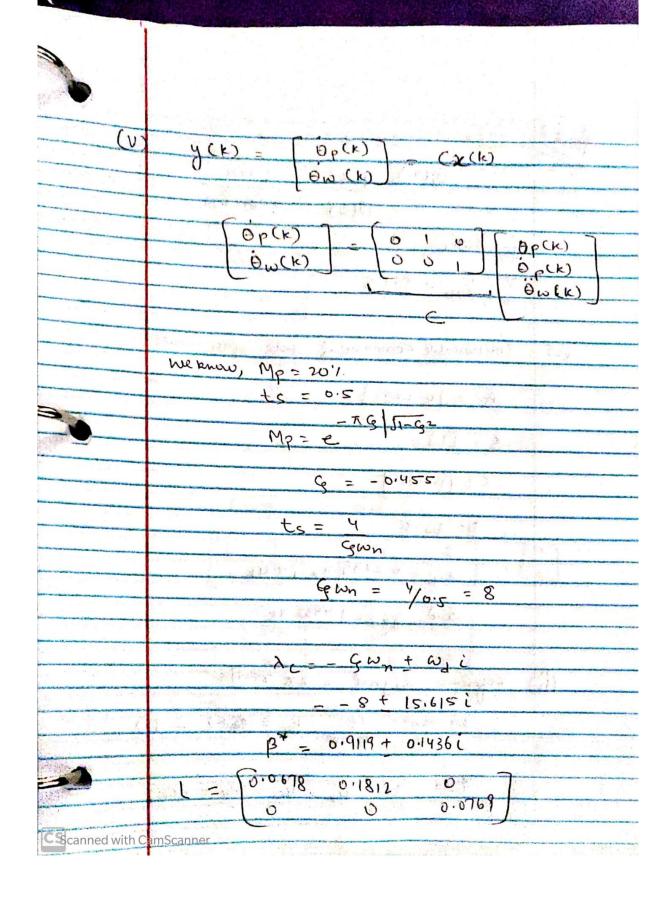
For this simulation, include the following plots:

- (a) The two system outputs, y(k), as a function of time
- (b) The system control input, u(k), as a function of time
- (c) The state estimation error,  $\hat{\mathbf{x}}(k) = \hat{\mathbf{x}}(k) \mathbf{x}(k)$ , as a function of time.

R=4am me = 980g Ic = 92,336 g-cm² l = 6cm, mw = 150g Iw = 1150 g-cm² α Bp - η Bp = - γθω -(1) d= Ic+mcRl X = 115856 2. n = magl n = 5768280 3. Y = Iw + (mw +mc) R2 V = 19230 (i) Rom (1) 20 p = 70p - 800 x= A2 + Bu CS canned with CamScanner

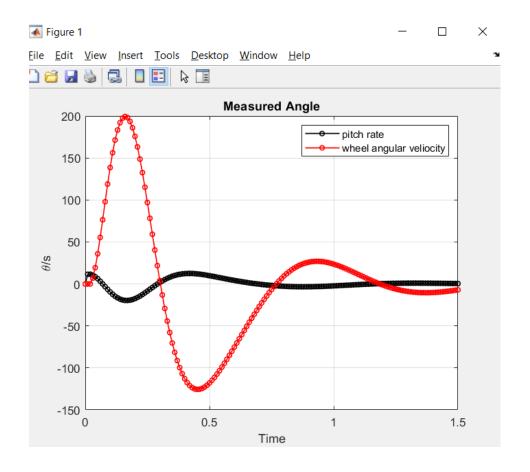


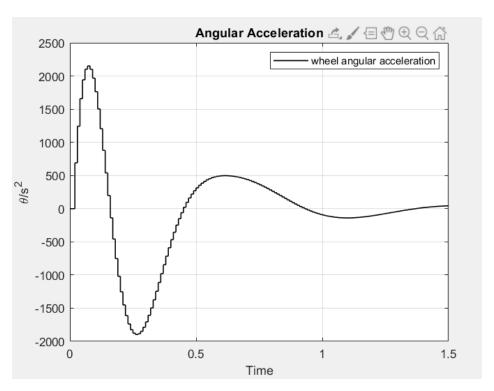
ts=1.88 (10) Mp = 30'1. =0.3 lu(0.3) = - T (g) J1-52 +1.2 = + TG 1.44 - 1.44 52 = 736° G= 0.363 gwn = 2.66 20 = - Gwnt Wi - 2.66 + to 6.96i From MATLAB K= [-707.76 -67,0084 -2.855]

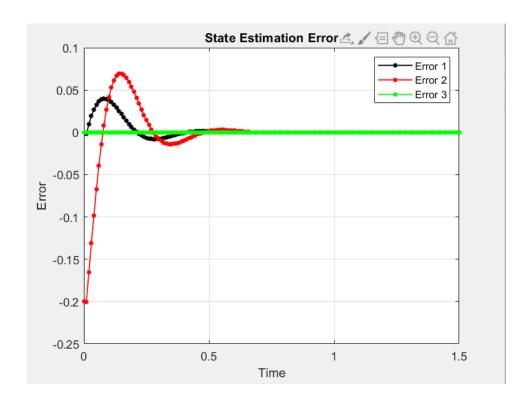


```
clear all; close all; clc;
%% Declaring intial values
Tfinal = 1.5;
frequency = 100;
T = 1/frequency;
t = (0:T:Tfinal)';
N = length(t);
n = 5768280;
alpha = 115856;
gamma = 19230;
Ts = 1.5;
Mp = 0.3;
zeta = sqrt((log(Mp))^2/(pi^2+(log(Mp))^2));
zeta omegaN = 4/Ts;
omega N = zeta omegaN/zeta;
omega D = omega N*sqrt(1-zeta^2);
Roots_cont = [-zeta_omegaN+omega_D*li -zeta_omegaN-omega_D*li];
Roots disc = exp(Roots cont*T);
z star = [Roots disc(1) Roots disc(2)];
Ac = [0 1; n/alpha 0]; %continous state space model
Bc = [0 -gamma/alpha]';
A = expm(Ac*T);
                %continous to discrete state space
B = (A - eye(length(A)))*Ac^-l*Bc;
A(1:2.3) = 0;
A(3,1:2) = 0;
A(3,3) = 1;
B(3,1) = T;
K matrix = acker(A,B,[Roots disc(1), Roots disc(2), abs(Roots disc(1))]); % 
calculating k matrix
C = [0 \ 1 \ 0; 0 \ 0 \ 1];
Ts estimate = 0.5;
Mp estimate = 0.2;
zeta_estimate = sqrt((log(Mp_estimate))^2/(pi^2+(log(Mp_estimate))^2));
zeta_omegaN_estimate = 4/Ts_estimate;
omega_N_estimate = zeta_omegaN_estimate/zeta_estimate;
omega_D_estimate = omega_N_estimate*sqrt(1-zeta_estimate^2);
Roots_cont_estimate = [-zeta_omegaN_estimate+omega_D_estimate*li ...
    -zeta_omegaN_estimate-omega_D_estimate*li];
Roots disc estimated = exp(Roots cont estimate*T);
beta_star = [Roots_disc_estimated(1) Roots_disc_estimated(2)];
char_Equation = poly([beta_star]);
L_matrix = place(A', C', [Roots_disc_estimated(1) Roots_disc_estimated(2) ...
   abs(Roots disc estimated(1))])';
%% Simulation
x = zeros(3,N);
x hat = zeros(3,N);
y = zeros(2,N);
y hat = zeros(2,N);
u = zeros(1,N);
```

```
x(:,1) = [0;0.2;0];
x hat(:,1) = [0;0;0];
y hat(1) = C(1,:)*x_hat(:,1);
u(1) = -K_{matrix*x(:,1)};
u(1) = 0;
error(:,1) = x_hat(:,1)-x(:,1);
for k = 2:N
    x(:,k) = A*x(:,k-1)+B*u(k-1);
    x_{hat}(:,k) = A*x_{hat}(:,k-1) + B*u(k-1) - L_{matrix} * (y_{hat}(:,k-1)-y(:,k-1));
    y_hat(:,k) = C(:,:)*x_hat(:,k);
    y(:,k) = C(:,:)*x(:,k);
    u(k) = -K_matrix*x_hat(:,k);
    error(:,k) = x_hat(:,k) - x(:,k);
end
%% Plots
figure(1)
plot(t,y(1,:)*180/pi, 'k-o', t,y(2,:)*180/pi,'r-o', 'linewi',1,'MarkerSize',4)
title('Measured Angle')
xlabel('Time')
ylabel('\theta/s')
legend('pitch rate','wheel angular veliocity')
figure(2)
stairs(t,u*180/pi,'k-','linewi',1, 'MArkersize',4)
grid on
title('Angular Acceleration')
xlabel('Time')
ylabel('\theta/s^2')
legend('wheel angular acceleration')
figure(3)
plot(t,error(1,:), 'k-*', t,error(2,:), 'r-*', t,error(3,:), 'g-*', 'linewi', &
1, 'MarkerSize', 4)
grid on
title('State Estimation Error')
xlabel('Time')
ylabel('Error')
legend('Error 1', 'Error 2', 'Error 3')
```







Part Two: The goal of this part of the project is to design a tracking controller for the 6V DC motor we have used as a demo in class, using state-feedback control, with an integrator.

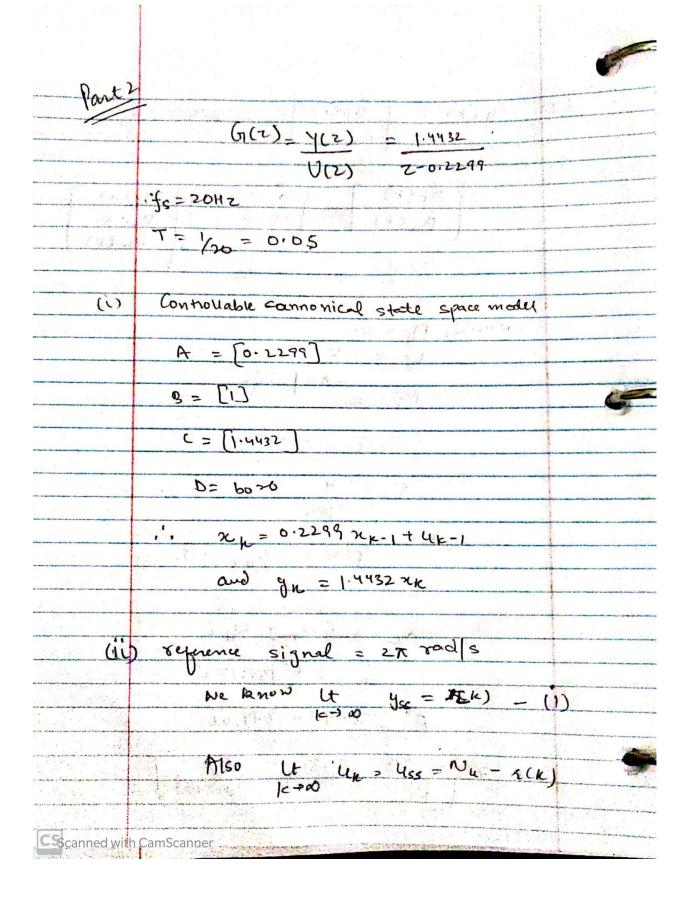


The transfer function for the motor is given by

$$G(z) = \frac{Y(z)}{U(z)} = \frac{1.4432}{z - 0.2299}$$
(9)

where y(kT) is the motor angular velocity in rad/s and u(kT) is the input voltage in volts. The sampling frequency for this transfer function is  $f_s = 20$  Hz.

- Put this system in controllable-canonical state-space form. (It will be a first-order system)
- Calculate the reference state for a reference signal of 2π rad/s
- Augment the system state vector to include the integral of the output error. Derive new A and B matrices to accommodate this additional state. Call these new matrices A<sub>AUG</sub> and B<sub>AUG</sub>.
- Calculate the feedback gain matrix so that the following performance criteria are satisfied (remember to choose 2 poles, because the integrator has added a second state)
  - (a)  $t_s = 0.6 \text{ s}$
  - (b)  $M_p = 0.2$
- 5. Derive an estimator that estimates just the first state (not the integral state) for your system. Calculate L such that the settling time of your estimator is 0.2 s. Note: your estimator is first order, so you have to pick one, real, target pole. L will be a scalar.
- 6. Simulate the system in MATLAB when a reference signal of r = 2π rad/s is provided, and generate the following plots (remember to define your control signal in such a way that your output will track the reference! This is not a regulator problem):
  - (a) The system output, y(k), as a function of time
  - (b) The system control input, u(k), as a function of time
  - (c) The state estimation error,  $\tilde{x}(k) = \hat{x}(k) x(k)$ , as a function of time.



6	
	KTW = NSS = Nz 1(k)
	From (I)
	Lt Cxx = CNxx=x
	C N = 1
	At Steady state we know,
-	$\kappa(k+1) = A \kappa(k) + B \kappa(k) - (1)$
	and Mss = Axss+Buss -(2)
	From (1) and (2)
	$\begin{bmatrix} N_{2} \\ N_{1} \end{bmatrix} = \begin{bmatrix} A - I & B \\ C & G \end{bmatrix} \begin{bmatrix} G \\ A \end{bmatrix}$
	$\begin{bmatrix} N_X \\ N_U \end{bmatrix} = \begin{bmatrix} 0.6929 \\ 0.5226 \end{bmatrix}$
	Therefore reference state
•	n-h = Nx·h 4.3536
CS <sub>Scanned</sub>	with CamScanner

(iii) x(1) = x(1) +x(1) - (x(1)-1)  $\begin{bmatrix} x_1 a \\ x_2 a \end{bmatrix} = \begin{bmatrix} A & O \\ -C & 1 \end{bmatrix} \begin{bmatrix} x_1 b \\ x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} O \\ u(k-1) \end{bmatrix}$ 0.2299 0 (1-1) + 4(1-1) AAUG = 0.2299 - 1.4432 BANG = (10) ts= 6.6 Mp = 02 0:2 = e 79 Figz 9 = 0.4559 CScanned with CamScanner

$$E_{S} = 4$$

$$gw_{N}$$

$$Qw_{N} = 4 = 6.67$$

$$o.6$$

$$A = -9w_{N} + w_{N}i$$

$$-6.67 + 13.01i$$

$$Z^{*} = e$$

$$= 0.5 | a_{1} + 0.434i$$

$$K = [0.0896 - 0.2586]$$

$$K = [0.0896 - 0.2586]$$

$$W_{P} = 0.2$$

$$+ c = 0.2$$

$$- RG | J_{F}G_{Z}|$$

$$W_{P} = e$$

$$G = 0.455 G$$

$$4 = 94$$

$$Gw_{N}$$

$$Gw_{N} = G^{*}Z$$

$$Gw_{N} = 30$$

$$Gw_{N} = 30$$

$$Gw_{N} = 30$$

$$Gw_{N} = 30$$

			7
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(6)		1	-
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```
close all; clear all; clc;
%% declaring intial values
frequency = 20;
T = 1/frequency;
Tfinal = 1;
t = (0:T:Tfinal)';
N = length(t);
r = 2*pi;
A = 0.2299;
B = 1;
C = 1.4432;
Nvec = [(A-eye(size(A))) B;C 0] \setminus [zeros(size(A));1];
N \times = Nvec(1);
%% reference state from reference signal
reference_state = N_x*r;
%% new augmentation matrices
A AUG = [A zeros(size(A));-C 1];
B AUG = [B;0];
%% K matrix
Ts = 0.6;
Mp = 0.2;
zeta = sqrt((log(Mp))^2/(pi^2+(log(Mp))^2));
zeta omegaN = 4/Ts;
omega N = zeta omegaN/zeta;
omega D = omega N*sqrt(1-zeta^2);
Roots_cont = [-zeta_omegaN+omega_D*li -zeta_omegaN-omega_D*li];
Roots disc = exp(Roots cont*T);
z_star = [Roots_disc(1) Roots_disc(2)];
K_matrix = acker(A_AUG, B_AUG, [z_star]);
%% L matrix
Ts_estimate = 0.2;
zeta_omegaN_estimate = 4/Ts_estimate;
Roots cont estimate = [-zeta omegaN estimate];
Roots_disc_estimate = exp(Roots_cont_estimate*T);
beta_star = [Roots_disc_estimate];
L_matrix = acker(A', C',beta_star)';
%% Simulation
x = zeros(1, N);
x_hat = zeros(1,N);
y = zeros(1,N);
u = zeros(1,N);
e = zeros(1,N);
xI = zeros(1,N);
error = zeros(1,N);
x_{hat}(:,1) = zeros(1,1);
x(:,1) = zeros(1,1);
y(1) = C*x(:,1);
e(1) = r-y(1);
```

```
xI(1) = 0;
u(1) = 0;
for k=2:N
    x(k) = A*x(k-1)+B*u(k-1);
    y(k) = C*x(k);
    x_hat(k) = (A-L_matrix*C)*x_hat(k-1)+B*u(k-1)+L_matrix*y(k-1);
    e(k) = r-y(k);
    xI(k) = xI(k-1) + e(k-1);
    u(k) = K_matrix*([reference_state; 0]-[x_hat(k); xI(k)]);
    error(k) = x_hat(k) - x(k);
end
%% Plots
figure(1)
plot(t,y(1,:), 'k-o', t,r,'r-o', 'linewi',2, 'MArkersize', 6)
grid on
hold on
title('System Output, y')
xlabel('t')
ylabel('Angular Velocity')
legend('Motor Angular Velocity', 'reference line')
figure(2)
stairs(t,u, 'k-', 'linewi',2)
grid on
hold on
title('Control Input')
xlabel('t')
ylabel('Voltage')
legend('Input Voltage, [V]')
figure(3)
plot(t,error, 'k-', 'linewi', 2)
ylim([-1 1])
grid on
title('State estimation error')
xlabel('t')
ylabel('Amplitude')
legend('Error')
grid on
```

