



SCHOOL OF AEROSPACE MECHANICAL AND MECHATRONIC ENGINEERING

AERO3760: SPACE ENGINEERING 2

SnapSat Preliminary Design Report

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Contents

1	Introduction	2
2	Spacecraft Design Overview	2
2.1	Subsystem Design Schematic	2
3	Payload Design Overview	4
4	Spacecraft Modes of Operation	4
5	Structural Design	6
6	System Budgets	7
6.1	Mass Budget	7
6.2	Power Budget	9
6.3	Pointing Budget	9
6.3.1	Error Calculation	10
6.4	Link Budgets	10
6.4.1	Uplink Budget	10
6.4.2	Downlink Budget	11
6.5	Data Budget	11
7	Project Plans and Schedule	12
7.1	Gantt Chart	13
A	Appendix: Supplementary Calculations	15
A.1	Mapping Calculation Considerations	15
A.2	Magnetorquer Calculations	15

List of Figures

2.1	Design Schematic	3
4.1	Mode Transition Diagram during satellite lifetime	5

List of Tables

2.1	SnapSat Design Overview	2
6.1	SnapSat Mass Budget (target mass of 1000 g)	8
6.2	SnapSat Power Budget	9
6.3	Pointing budget error calculation breakdown	10
7.1	SnapSat Project Schedule	12

1 Introduction

SnapSat is a design solution as a part of the AERO3760: Space Engineering 2 course at the University of Sydney. The project involves specific design specifications as set out by the course administrator and the CubeSat requirements [?]. This report details the selected mission and preliminary design considerations. Satellite components will be purchased off the shelf, where financially viable. Otherwise, components will be made in-house. Over the course of the project development, components will be tested separately and a series of final testing will be conducted once assembly is completed. SnapSat will undergo vibration testing, vacuum testing, communications and power testing and the attitude determination and control system will be tested on an air-bearing table.

2 Spacecraft Design Overview

Summarised in table 2.1 below is the outline of all components in the SnapSat proposed design.

Table 2.1: SnapSat Design Overview

Subsystem	Description
Structural	<ul style="list-style-type: none">- industrial grade aluminium- laser cut, bent to shape and riveted together
ADCS	<ul style="list-style-type: none">- air core magneto-torquers made in-house- Osram SFH203P Photodiodes- IMU: Adafruit 9-DOF
EPS	<ul style="list-style-type: none">- Australian Robotics solar panels- battery: LiNiMnCo 26650 rechargeable cell
OBC / OBDH	<ul style="list-style-type: none">- Arduino DUE- 4 × PCBs
TT&C	<ul style="list-style-type: none">- VHF (Xbee)- UHF- tape measure antennae
Thermal	<ul style="list-style-type: none">- thermal tapings and passive coatings (Kapton tape)- selected components will have multi-layer insulation
Payload	<ul style="list-style-type: none">- Arducam

2.1 Subsystem Design Schematic

The layout of Snapsat, with the interconnects of power and data lines between the subsystems is shown in the figure below. (NOTE: this is only an example for now)

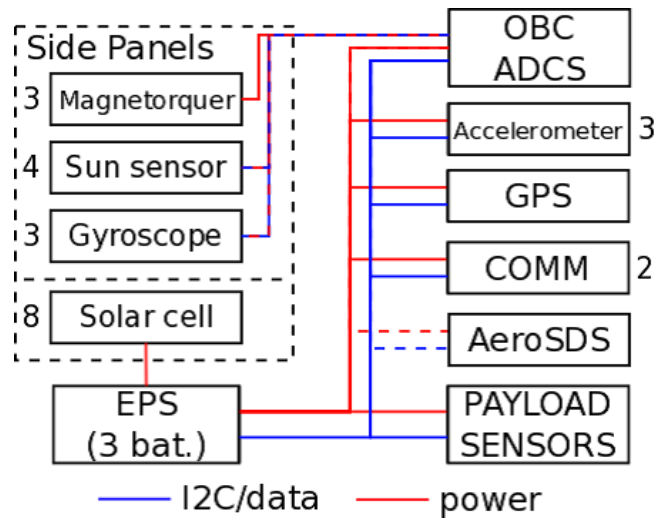


Figure 2.1: Design Schematic

3 Payload Design Overview

The CubeSat had been pivotal to the space research and development industry and had generally increased our accessibility to the cosmos. The cubesat platform uniquely offers an extremely low construction and launch cost in comparison to major satellite manufacturers. This has spurred on many educational bodies and small research groups to collect and analyse their own data, especially in developing nations [1]. Universities have pioneered the build of the smallest of satellites (nano- and pico-), this has been assisted with the miniaturisation in many technological fields such as electronics, materials and sensors. These small sizes enable the cubesat to 'piggy-back' on the launch of much larger satellites, because of this they are able to get to very high (and expensive) orbits of a fraction of the price. Many big aerospace companies have also made use of the tiny platform such as Orbital Sciences (2006 [2]) and Boeing (2009 [3]) along with the United Nations, who have formally recognised the developmental benefits of small satellites [4].

Despite the quick growth of this industry in the aerospace and related academia fields, we are only now seeing the cubesat break into early STEM education. Currently, only science and technology scholars and graduates have the full accessibility to the design of cubesats, our ease of access is not well known amongst the general public. SnapSat hopes to change this, by bringing space to social media via beautiful photographs and Twitter. SnapSat is a nano-satellite designed for outreach and space accessibility for educational bodies and the general public. In a sun-synchronous orbit at an altitude of 350km, SnapSat will be in the prime position of Earth observation. Users and sponsors can send a message to the cubesat, which will take a low resolution image of the Earth and tweet it to the world.

Currently, the final build will result in a balloon launch test. Following the success of this, SnapSat will be launched on a sounding rocket, where it will be placed in a low Earth orbit for a maximum lifetime of three months.

4 Spacecraft Modes of Operation

The spacecraft will experience the following modes during its lifetime. A different configuration of system operations and instructions will be executed by *SnapSat* in each case. These are summarised in below.

Launch Mode: This turns the satellite off for launch to comply with CubeSat Design Specification 2.3.1. During launch the deployment switch is tripped which will turn the satellite on and transfer it into Establish Contact Mode.

Safe mode: In this mode, only essential satellite systems are kept ON such as the OBC, power board and VHF receiver. The attitude is not controlled and the transmitter is turned on occasionally for status updates.

Recovery/De-tumble mode: This mode is used to de-tumble the spacecraft after deployment into orbit as well as to recover it from any spin states (such as after Safe Mode). All Safe Mode components are ON, as well as the ADCS system. Other devices can be turned ON by ground command.

Establish Contact Mode: In this mode the satellite waits 30 seconds before deploying the antenna and attempting to communicate with the ground station. The ACS system works to orient the satellite correctly.

Payload Operation Mode: This mode is used only when taking a picture. The camera module is booted up, the camera takes a picture, stores it in RAM/ROM and then the camera is powered down again to conserve power. This mode can be triggered by reaching a preset GPS location or manually via communications. This mode can be entered either by reaching a GPS coordinate or through ground control command. It exists this mode straight into Relay Picture Mode.

Relay Picture Mode: This mode is entered after Payload Operation Mode and causes the CubeSat to start sending pictures to the ground station.

Relay Picture Mode: In this mode the camera is almost constantly transmitting images taken through the camera. It exists into Telemetry Mode when the picture has been sent.

Telemetry Mode: In this mode the CubeSat is idle, just displaying basic telemetry. Attitude controlled.

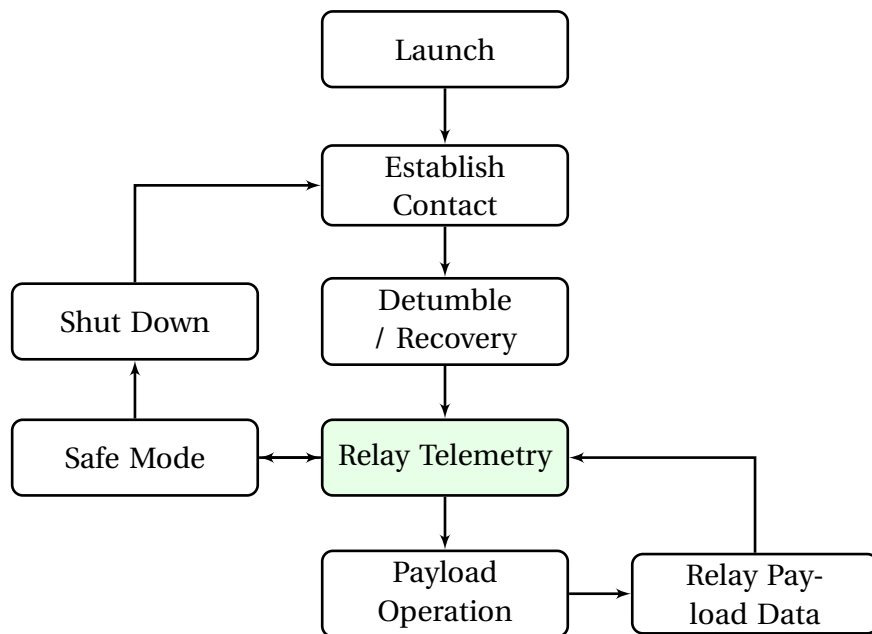


Figure 4.1: Mode Transition Diagram during satellite lifetime

5 Structural Design

The proposed one-unit satellite structure will be 3D printed using ABS plastic. This method was chosen in preference of an aluminium chassis primarily because of the ease of access of production.

6 System Budgets

This section detail the power and mass budgets of SnapSat. (overview/description)

6.1 Mass Budget

The mass budget is shown in table 6.1, it is ensured that *SnapSat* meets the requirement of a maximum weight of 1kg. The component masses were used to determine the center of gravity for the satellite, it is desirable to keep this located close to the geometric centre as the attitude control system (magneto-torquers) are placed on the outermost surfaces. Centroid averaging across all three axes was used to calculate this as follows

$$x_{cg} = \frac{\sum x_i \cdot m_i}{\sum m_i} \quad y_{cg} = \frac{\sum y_i \cdot m_i}{\sum m_i} \quad z_{cg} = \frac{\sum z_i \cdot m_i}{\sum m_i}$$

The moment of inertia about all three axes is given by

$$I = \int r^2 dm$$

The inertial of each individual component was ignored, assuming these were roughly symmetrical. Only the relative locations of the component contributed to the total inertia. Thus, the inertias were given

$$I_{xx} = \frac{1}{\sum m_i} \cdot \left(\sum \sqrt{(y_i - y_{cg})^2 + (z_i - z_{cg})^2} \cdot m_i \right) \quad (6.1)$$

$$I_{yy} = \frac{1}{\sum m_i} \cdot \left(\sum \sqrt{(x_i - x_{cg})^2 + (z_i - z_{cg})^2} \cdot m_i \right) \quad (6.2)$$

$$I_{zz} = \frac{1}{\sum m_i} \cdot \left(\sum \sqrt{(x_i - x_{cg})^2 + (y_i - y_{cg})^2} \cdot m_i \right) \quad (6.3)$$

and so on; where x_i , y_i and z_i are the positions of each component and m_i is the mass of each component. The inertial matrix was computed using *Solidworks*. It was found to be:

$$I = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix} = \begin{bmatrix} 886508.05 & 287196.55 & 245002.46 \\ 287196.55 & 77032823 & 292616.34 \\ 245002.46 & 292616.34 & 880334.84 \end{bmatrix} \text{ g} \cdot \text{mm}^2 \quad (6.4)$$

note: would be better after we put the components in

Table 6.1: SnapSat Mass Budget (target mass of 1000 g)

Subsystem	Mass	Contingency	Mass + Con- tingency	Fraction of Total Mass
<i>Structural</i> - chassis - solar panels	100g 9 × 25g	30g 9 × 5g	415g	47.6%
<i>ADCS</i> - air core coils - sun sensors - IMU	3 × 50g 6 × 1.8g 2.8g	3 × 5g 6 × 0.3g 0.4g	180.2g	22%
<i>EPS</i> - batteries - power bus	103g 10g	7g 2g	122g	14.9%
<i>OBS / OBDH</i> - Arduino board - memory storage	25g 1g	5g 0.2g	31.2g	3.8%
<i>TT&C</i> - antennae - transceiver	3g 75g	1g 5g	84g	10.3%
<i>Thermal</i> - tapings - MLI	1g 3g	0.3g 0.5g	4.8g	0.6%
<i>Payload</i> - camera	25g	5g	25g	3.1%
<i>Integration</i> - bolts/rivets - cabling/wires	5g 2g	2g 0.5g	9.5g	1.2%
Total			817.7g	
Mass Margin			182.3g	18.2%

6.2 Power Budget

Table 6.2: SnapSat Power Budget

			Average Duty Cycle by Mode (%)				
Load	Power Consumption (W)	Number of Units On	Safe Mode	Recovery Mode	Payload Mode	Other Mode	
OBC							
VHF Rx							
S-band Tx							
Magnetorquers	150mW	1	0 %	on			
Power Board							
Camera	1950mW	1	0	0	100 %		
IMU	30mW	1	off	on	on	on	
GPS	100mW	1	off				
Solar Panels	935mW	5	on	on	on		
Sum Loads (W)							
Efficiency							
Power Consumed (W)							
Power Generated (W)							
Power Margin							

6.3 Pointing Budget

Since this spacecraft is performing Earth observation, it requires a pointing budget. This refers to the ability to orient the spacecraft towards a target having a specific geographical orientation. Along with the pointing accuracy, the satellite needs to be able to map the location from its own location. Errors in both pointing and mapping accuracies will be discussed here.

The attitude control system for SnapSat will consist of three air core magnetorquers operating on 3 separate planes capable of producing 0.05Am^2 each. Only two of the magnetorquers can work at any one time, which will reduce total power usage for the system. The first component of the determination system is a 9-DOF IMU which will primarily be used in the de-tumble phase due to accumulated error issues with this equipment which are expected to occur later in the mission. The second component is a solar tracker system consisting of six photodiode pins, one on each face, which will be used to accurately determine the attitude of the satellite based on the location

of the Sun.

According to the specification data, the IMU will experience a 2% error based on the expected temperature range, although this will increase over the course of the mission due to the accumulated error. Although the exact error will need to be calculated during calibration and testing, based on current literature there are a number of similar solar tracking systems which are able to achieve an accuracy of 0.2% [5]. However given the low budget and subsequently slightly inferior equipment conservative estimate of 0.5% will be used for the solar tracker error. In regards to the magnetorquers expected error based on similar models 1%, although error will be finalised during the calibration and testing phase.

6.3.1 Error Calculation

Due to the fact that the two attitude determination systems will almost always be used separately we have calculated three different total errors. The total errors were calculated using the following formula:

$$\text{System Error} = \sqrt{(\text{IMU error})^2 + (\text{sun sensor error})^2 + (\text{magnetorquers error})^2} \quad (6.5)$$

$$= \sqrt{(2\%)^2 + (0.5\%)^2 + (1\%)^2} \quad (6.6)$$

$$= 2.3\% \quad (6.7)$$

$$= 8.3^\circ \quad (6.8)$$

This is summarised in the table below

Table 6.3: Pointing budget error calculation breakdown

	IMU Error (%)	Sun Tracker Error (%)	Magnetorquer Error (%)	Total (%)	Total (°)
Overall System	2.0	0.5	1.0	2.3	8.3
System 1	2.0	-	1.0	2.2	7.9
System 2	-	1.0	1.0	1.1	4.0

The majority of the mission is expected to be spent using system 2 (utilising the sun trackers), which produces an error of 4°. Whilst this is within the range for the widest application of the three mapping scenarios (see Appendix A.1) it is slightly outside of the range of the second more focused scenario. However, it should be noted that these are conservative calculations and the finalised error may be lower than these figures.

6.4 Link Budgets

Calculations for both link budgets (list assumptions here).

6.4.1 Uplink Budget

The uplink budget allows for XXX. The specifications are

- Antenna type at satellite: (omni, directional+gain)
- Frequency Band: (VHF (145.800MHz) , UHF (435.xxx MHz), SHF etc.)
- Objective C/N:
- Bit rate and modulation type:
- Expected occupied bandwidth:

6.4.2 Downlink Budget

The downlink budget allows for XXX. The specifications are

- Antenna type at satellite: (omni, directional+gain)
- Frequency Band: (VHF (145.800MHz) , UHF (435.xxx MHz), SHF etc.)
- Objective C/N:
- Bit rate and modulation type:
- Expected occupied bandwidth:

6.5 Data Budget

Data budget CALCULATIONS.

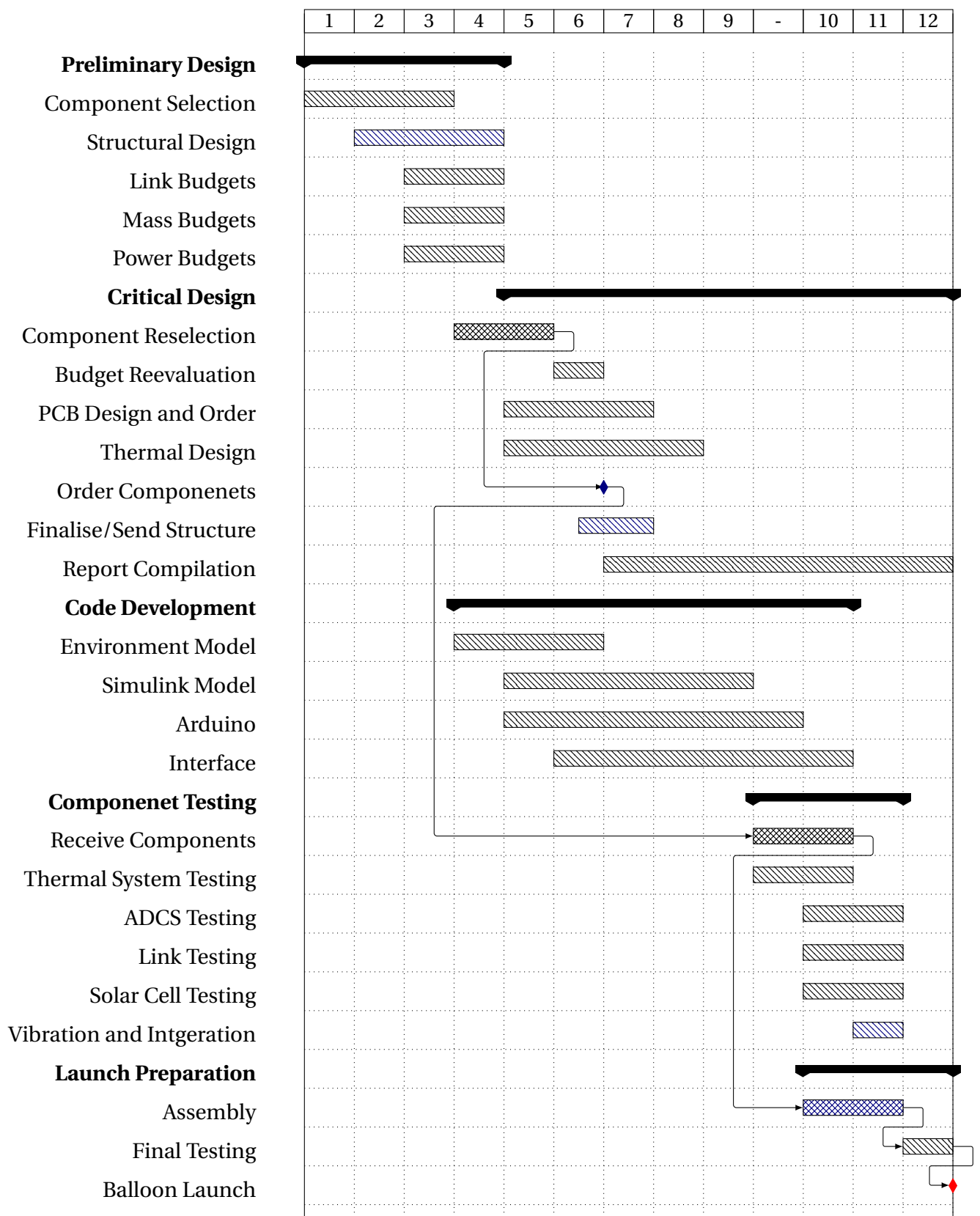
7 Project Plans and Schedule

A general schedule for the SnapSat project is outlined below. A Gantt chart is provided on the following page.

Table 7.1: SnapSat Project Schedule

Major Task	Responsibility	Start Date	End Date
Structural Development	Oscar McNulty	03/08/2015	21/08/2015
Preliminary Design Report	Nikita Sardesai	03/08/2015	23/08/2015
Component Selection	All members	03/10/2015	17/10/2015
Link Budgets	Thomas Forbutt	10/08/2015	23/08/2015
Mass Budgets	Nikita Sardesai	10/08/2015	23/08/2015
Power Budgets	Penelope Player	10/08/2015	23/08/2015
Pointing Budget	James Allworth	10/08/2015	23/08/2015
Component Reselection	All members	21/08/2015	28/08/2015
PCB Design	Penelope Player	23/08/2015	11/09/2015
Thermal Design	Nikita Sardesai	23/08/2015	18/09/2015
Code Development	All members	16/08/2015	09/09/2015
Environment Model	Nikita Sardesai	17/08/2015	04/09/2015
Simulink Model	James Allworth	24/08/2015	25/09/2015
Arduino Code	Thomas Forbutt	24/08/2015	02/10/2015
Interface	Penelope Player	07/09/2015	09/09/2015
Report Compilation	All members	07/09/2015	23/10/2015
Component Testing	All members	25/09/2015	16/10/2015
Thermal Systems Testing	Nikita Sardesai	28/09/2015	09/10/2015
ADCS Systems Testing	James Allworth	05/09/2015	16/10/2015
Link Systems Testing	Thomas Forbutt	05/09/2015	16/10/2015
Solar Cell Testing	Oscar McNulty	05/09/2015	16/10/2015
Final Assembly	Oscar McNulty	05/10/2015	16/10/2015
Vibration & Integration Testing	Penelope Player	12/10/2015	16/10/2015
Final Testing	All members	16/10/2015	23/10/2015
Balloon Launch	Available members	24/10/2015	25/10/2015

7.1 Gantt Chart



References

- [1] K. Woellert, P. Ehrenfreund, A. J. Ricco, and H. Hertzfeld, “Cubesats: Cost-effective science and technology platforms for emerging and developing nations,” *Advances in Space Research*, vol. 47, no. 4, pp. 663–684, 2011.
- [2] H. Heidt, J. Puig-Suari, A. Moore, S. Nakasuka, and R. Twiggs, “Cubesat: A new generation of picosatellite for education and industry low-cost space experimentation,” 2000.
- [3] J. Straub, “Cubesats: A low-cost, very high-return space technology,” 2012.
- [4] M. J. Rycroft and N. Crosby, *Smaller Satellites: Bigger Business?: Concepts, Applications and Markets for Micro/Nanosatellites in a New Information World*, vol. 6. Springer Science & Business Media, 2013.
- [5] N. Raghu, K. Manjunatha, and B. Kiran, “Tracking of satellites by using phased array antenna,” in *Electronics and Communication Systems (ICECS), 2014 International Conference on*, pp. 1–6, IEEE, 2014.
- [6] W. J. Larson and J. R. Wertz, “Space mission analysis and design,” tech. rep., Microcosm, Inc., Torrance, CA (US), 1992.

A Appendix: Supplementary Calculations

A.1 Mapping Calculation Considerations

Calculations are based on an orbit of 300km altitude. In general if we are targeting cities, metropolitan areas for a number of major cities are approximately 100 km². Thus assume a target size of 10km by 10km. For an orbit path that goes directly over the city:

$$\alpha = 2 \times \tan^{-1} \left(\frac{5}{300} \right) = 1.9^\circ$$

This is a very narrow window however if we instead photograph an area of 100km by 100km, or 10,000km² (roughly the area of Sydney), this equation changes to:

$$\alpha = 2 \times \tan^{-1} \left(\frac{50}{300} \right) = 18.9^\circ$$

Thus if the satellite is misaligned by as much as 8.5° in any direction it will still capture the original 10km by 10km area that was intended. However this is a much larger area and as such there will be less focus on the intended target. Thus the third option is a 50km by 50km picture:

$$\alpha = 2 \times \tan^{-1} \left(\frac{25}{300} \right) = 9.5^\circ$$

This image would provide greater focus but would require the attitude of the satellite to be within 3.8° accuracy of the measured attitude. It must be noted that this calculation is for an orbit where the satellite will pass directly over the target area. If this does not occur it will require the satellite to be more accurately aligned due to the fact that it is aiming at a comparatively smaller target. However at small angles this effect is not that significant and since the idea of the mission is to capture cities only when the satellite passes over them it should not be a major issue or consideration.

A.2 Magnetorquer Calculations

Although there is significant data to support the fact that a 0.05Am² magnetorquer will be powerful enough to control a satellite in space I did some simplistic calculations to check it on an order of magnitude basis. Calculation of the magnetic dipole of the magnetorquer:

$$M = NiA = 312 \times 0.025 \times 0.064 = 0.05 \text{ Am}^2$$

Calculation of the minimum earth's magnetic field at 300km:

$$B = \frac{\mu_0 m_e}{4\pi R^3} = 2.68 \times 10^{-6}$$

Calculation of torque:

$$T = M \times B = 1.34 \times 10^{-6}$$

Given the satellite will weigh 1kg and its centre of mass is at the structural centre of the satellite. Assuming that the magnetorquers are located 1cm away from the edge of the satellite. Thus we

use the equation:

$$T = mr^2\alpha$$

so then

$$\alpha = \frac{1.34 \times 10^{-6}}{1 \times 0.05^2} \quad (\text{A.1})$$

$$= 5.36 \times 10^{-4} \text{ rad/s}^2 \quad (\text{A.2})$$

$$= 0.0307 \text{ deg/s}^2 \quad (\text{A.3})$$

Design requirements for the system are that it can recover from a 10 deg/s spin within two days. Assuming average acceleration and that the correct axis is perpendicular to the earths magnetic field.

$$t = \frac{\omega}{\alpha} \quad (\text{A.4})$$

$$= \frac{10}{0.0307} \quad (\text{A.5})$$

$$= 326 \text{ seconds} \quad (\text{A.6})$$

$$= 5.5 \text{ minutes} \quad (\text{A.7})$$

This is obviously an oversimplification and there are a number of other factors involved which will cause this number to increase. However it is clear from these calculations that the system will have the power to recover form a 10 deg/s spin within the two-day limit.