1 ZMP LQR Riccati Equation

Using z(t) as the 2D position of the ZMP, we formulate:

This can be rewritten as a cost on state, in coordinates relative to the final conditions, X = X $Z_d^T(t_f)$ 0 0 T , $Z_d(t) = Z_d(t)$ $Z_d(t_f)$:

Note that this implies that x(7) = 0 in order for the cost to be nite. The resulting cost-to-go is given by

$$J = x^T S_1(t) x + x^T S_2(t) + S_3(t)$$

with the corresponding Riccati di erential equation given by

$$S_{1} = Q_{1} (N + S_{1}B)R_{1}^{-1}(B^{T}S_{1} + N^{T}) + S_{1}A + A^{T}S_{1}$$

$$S_{2} = q_{2}(t) 2(N + S_{1}B)R^{-1}r_{s}(t) + A^{T}S_{2} ; r_{s}(t) = \frac{1}{2}(r_{2}(t) + B^{T}S_{2}(t))$$

$$S_{3} = q_{3}(t) r_{s}(t)^{T}R^{-1}r_{s}(t)$$

Note that S_1 has no time-dependent terms, and therefore $S_1(t)$ is a constant, given by the steady-state solution of the algebraic Riccati equation (e.g. from time-invariant LQR). Similarly, the feedback controller is given by

$$U(t) = K_1(t)x + k_2(t)$$

and again the feedback $K_1(t)$ is a constant (derived from the in nite horizon LQR with Q, R, and N set as above).

1.1 Solving for $s_2(t)$

Given this, the an e terms in the Riccati differential equation are given by the linear differential equations:

$$S_2(t) = A_2 S_2(t) + B_2 Z_d(t); \quad S_2(t_f) = 0$$

with

$$A_2 = (N + S_1 B) R^{-1} B^T$$
 A^T ; $B_2 = \begin{pmatrix} 2I_2 & 2 \\ 0_2 & 2 \end{pmatrix} + 2\frac{h}{g}(N + S_1 B) R^{-1}$

Assuming $z_d(t)$ is described by a *continuous* piecewise polynomial of degree k with n + 1 breaks at t_i (with $t_0 = 0$ and $t_n = t_f$):

$$z_d(t) = \begin{cases} x \\ t \\ t \\ t \end{cases} c_{j,i}(t - t_j)^i; \text{ for } j = 0; ...; n - 1; \text{ and } 8t \ 2[t_j; t_{j+1}); \end{cases}$$

this system has a closed-form solution given by:

$$s_2(t) = e^{A_2(t-t_j)} \int_{t=0}^{\infty} \int_{t=0}^{\infty} f(t-t_j)^i; \quad 8t \ 2[t_j;t_{j+1});$$

with j and j:j vector parameters to be solved for. Taking

$$S_{2}(t) = A_{2}e^{A_{2}(t-t_{j})} + A_{2-j;i}(t-t_{j})^{i} + B_{2}c_{j;i}(t-t_{j})^{i}$$

$$= A_{2}e^{A_{2}(t-t_{j})} + A_{2-j;i}(t-t_{j})^{i-1}$$

$$= A_{2}e^{A_{2}(t-t_{j})} + A_{2-j;i}(t-t_{j})^{i-1}$$

forces that

$$A_{2\ j;i} + B_{2}c_{j;i} = (i+1)_{j;i+1};$$
 for $i = 0; ...; k-1$
 $A_{2\ j;k} + B_{2}c_{j;k} = 0;$

Note: need to prove that A_2 is full rank (it appears to be in practice). Solve backwards (i = k; k = 1; ...; 0) for f_i . Finally, the continuity and the terminal boundary condition f_i solves

$$e^{A(t_{j+1} t_j)} j + \sum_{i=0}^{k} j_{i}(t_{j+1} t_j)^{i+1} = s(t_{j+1})$$
:

1.2 Reading out $k_2(t)$

The remaining term for the controller is a simple read-out given the solution to $s_2(t)$:

$$k_2(t) = -\frac{h}{g}R^{-1}Z_d(t) - \frac{1}{2}R^{-1}B^TS_2(t)$$

which can be written as

$$k_2(t) = Le^{A_2(t-t_j)} \int_{j:R} + \int_{i=0}^{k} j_{ij}(t-t_j)^i$$

with

$$L = \frac{1}{2}R^{-1}B^{T}$$

$$R = j_{R} = j$$

$$j_{R} = \frac{h}{q}R^{-1}Cj_{R} = \frac{1}{2}R^{-1}B^{T}$$

1.3 Solving for $x_{com}(t)$

The resulting system is

$$\underline{x} = Ax + B(K_1x + k_2(t)) = (A + BK_1)x + Bk_2(t)$$
;

where $x = [x_{com}; y_{com}; x_{com}; y_{com}]^T$: Since the solution $k_2(t)$ is the result of another linear system (cascaded in front of this one), it is easiest for me to solve jointly, using $y = \begin{pmatrix} x \\ s_2 \end{pmatrix}$:

$$A_{y} = A_{y}y + B_{y}z_{d}$$

$$A_{y} = A_{y}BK_{1} \frac{1}{2}BK_{1}B^{T} + B_{y} = B_{y} = B_{y}$$

$$y(t) = e^{A_{y}(t-t_{j})}a_{j} + b_{j,i}(t-t_{j})^{i}$$

i can solve for b using the same technique as above (and re-using the sol)