

DESCENTE DE CHARGES

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SYNAPSE*

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Complexe sportif Diderot

Lot 4 Ossature et Veture bois



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Chapitre 1 INFORMATIONS GENERALES

1.1 Situation de l'ouvrage

Affaire/projet : 2404-234GBM Diderot

Note d'hypothèse N° : 2409-500

Adresse: Gymnase Diderot Rue de Cologne 25000 BESANCON

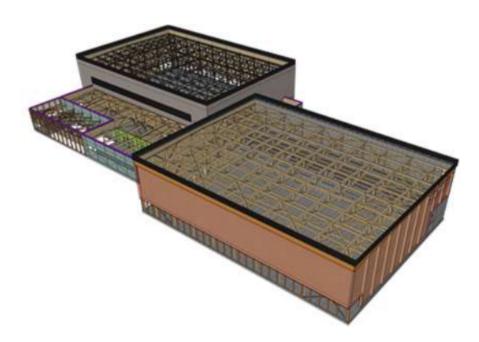


FIGURE 1.1 – Description de l'ouvrage

1.2 Plan de situation

1.3 Description de l'ouvrage

1.4 Règles de calcul et de conception

Les calculs de structures sont réalisés conformément aux normes Eurocode en vigueur :

(i) Eurocode 0 EN 1990 : Base de calcul des structures

(ii) Eurocode 1 EN 1991 : Actions sur les structures

(iii) Eurocode 2 EN 1992 : Calculs des structures en béton

(iv) Eurocode 3 EN 1993 : Calculs des structures en acier

(v) Eurocode 4 EN 1994 : Calculs des structures mixtes acier-béton

(vi) Eurocode 5 EN 1995 : Calculs des structures en bois

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- (vii) Eurocode 6 EN 1996 : Calculs des structures en maçonnerie
- (viii) Eurocode 8 EN 1998 : Calculs des structures pour leur résistance aux séismes
- (ix) Résix® Technique d assemblage sous avis technique CSTB 3.3-19-986 V1

1.5 Stabilité et Repérage des points d'appuis

1.5.1 Principe de stabilité de la structure

1.5.2 Repérage des points d'appuis



Figure 1.2 – Repèrage des points d'appui 2D

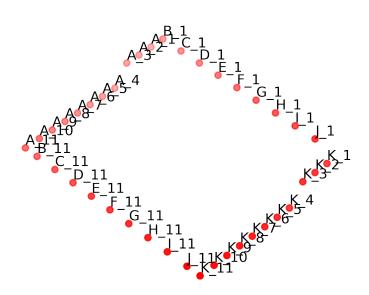


FIGURE 1.3 – Repèrage des points d'appui 3D

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Chapitre 2 DESCENTE DE CHARGES

2.1 Charges permanentes (G)

Nom point	X	Y	Z	RFx_kN	RFy_kN	RFz_kN
A 1	0	0	5790			-5
A 2	3250	0	5790			-7
A 3	6500	0	5790	1		-13
A 4	9750	0	0	-3		-14
$\overline{\mathrm{A}}^{-}5$	13000	0	0			-25
$\overline{A} 6$	16250	0	0	3		-48
A_7	19500	0	0			-55
A_8	22750	0	0	-5		-30
A_9	26000	0	0			-24
A_10	29250	0	0	1		-33
A_11	32740	0	0		-24	-82
B_1	0	3160	11112		10	-94
B_11	32740	3160	0			-138
C_1	0	7960	11112		-3	-97
C_11	32740	7960	0		17	-194
D_1	0	12760	11112			-99
D_11	32740	12760	0	1		-165
E_1	0	17560	11112		-2	-101
E_11	32740	17560	0			-195
F_1	0	22360	11112			-101
F_11	32740	22360	0	1		-167
G_1	0	27160	11112		2	-101
G_11	32740	27160	0			-195
H_1	0	31960	11112			-99
H_11	32740	31960	0	1		-165
I_1	0	36760	11112		3	-97
I_11	32740	36760	0		-17	-194
J_1	0	41560	11112		-10	-94
J_11	32740	41560	0			-138
K_1	0	44720	5790			-5
K_2	3250	44720	5790			-7
K_3	6500	44720	5790	9		-13
K_4	9750	44720	0	-3		-12
K_5	13000	44720	0	4		-16
K_6	16250	44720	0	4		-24
K_7	19500	44720	0	C		-13
K_8	22750	44720	0	-6		-26
K_9 K_10	26000	44720	0	2		-18
K_10	29250	44720	0	<i>L</i>	24	-30
K_11	32740	44720	0		24	-82

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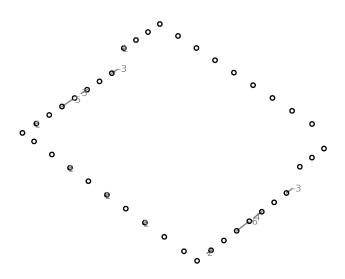


Figure 2.1 – Charges permanentes (G)_RFx_kN



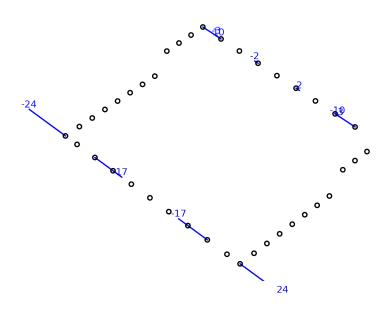


Figure 2.2 – Charges permanentes (G)_RFy_kN



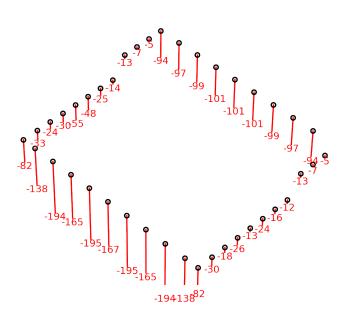


Figure 2.3 – Charges permanentes (G)_RFz_kN



2.2 Charges d'exploitation (Q)

Nom point	X	Y	Z	RFx_kN	RFy_kN	RFz_kN
A 1	0	0	5790			
$\overline{\mathrm{A}}_{2}^{-}$	3250	0	5790			
A_3	6500	0	5790			
A_4	9750	0	0			
A_5	13000	0	0			
A_6	16250	0	0			
A_7	19500	0	0			
A_8	22750	0	0			
A_9	26000	0	0			
A_10	29250	0	0			
A_11	32740	0	0			
B_1	0	3160	11112			
B_11	32740	3160	0			
C_1	0	7960	11112			
C_11	32740	7960	0			
D_1	0	12760	11112			
D_11	32740	12760	0			
E_1	0	17560	11112			
E_11	32740	17560	0			
F_1	0	22360	11112			
F_11	32740	22360	0			
G_1	0	27160	11112			
G_11	32740	27160	0			
H_1	0	31960	11112			
H_11	32740	31960	0			
I_1	0	36760	11112			
I_11	32740	36760	0			
J_1	0	41560	11112			
J_11	32740	41560	0			
K_1	0	44720	5790			
K_2	3250	44720	5790			
K_3	6500	44720	5790			
K_4	9750	44720	0			
K_5	13000	44720	0			
K_6	16250	44720	0			
K_{-7}	19500	44720	0			
K_8	22750	44720	0			
K_9	26000	44720	0			
K_10	29250	44720	0			
K_11	32740	44720	0			



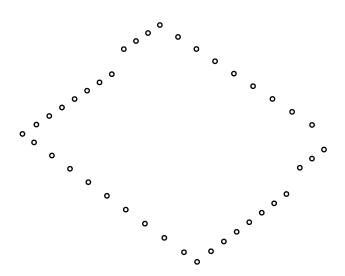


Figure 2.4 – Charges d'exploitation (Q)_RFx_kN



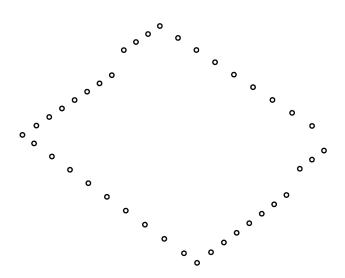


FIGURE 2.5 – Charges d'exploitation (Q)_RFy_kN

Reference: GBM Diderot

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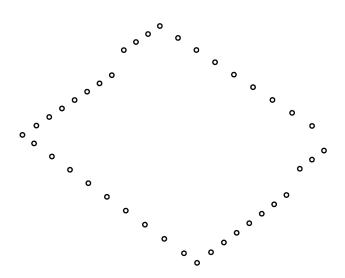


Figure 2.6 – Charges d'exploitation (Q)_RFz_kN



2.3 Neige (S)

Nom point	X	Y	Z	RFx_kN	RFy_kN	RFz_kN
A 1	0	0	5790			-2
$\overline{\mathrm{A}}_{2}^{-}$	3250	0	5790			-3
A_3	6500	0	5790			-4
A_4	9750	0	0	-1		-5
A_5	13000	0	0			-5
A_6	16250	0	0			-4
A_7	19500	0	0			-3
A_8	22750	0	0	-2		-11
A_9	26000	0	0			-5
A_10	29250	0	0	-1		3
A_11	32740	0	0		-7	-14
B_1	0	3160	11112		4	-47
B_11	32740	3160	0	1		-34
C_1	0	7960	11112		-4	-47
C_11	32740	7960	0	1	4	-51
D_1	0	12760	11112			-47
D_11	32740	12760	0	1		-46
E_1	0	17560	11112		-2	-47
E_11	32740	17560	0	1		-50
F_1	0	22360	11112			-47
F_11	32740	22360	0	1		-46
G_1	0	27160	11112		2	-47
G_11	32740	27160	0	1		-50
H_1	0	31960	11112			-47
H_11	32740	31960	0	1		-46
I_1	0	36760	11112		4	-47
I_11	32740	36760	0	1	-4	-51
J_1	0	41560	11112		-4	-47
J_11	32740	41560	0	1		-34
K_1	0	44720	5790			-2
K_2	3250	44720	5790			-3
K_3	6500	44720	5790	-1		-4
K_4	9750	44720	0	-2		-5
$K_{\underline{-}}5$	13000	44720	0			-4
K_6	16250	44720	0			- 4
K_{2}	19500	44720	0			-2
K_8	22750	44720	0	-3		-11
K_9	26000	44720	0			- 4
K_10	29250	44720	0			2
K_11	32740	44720	0		7	-14



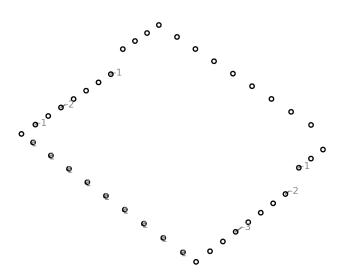


FIGURE 2.7 – Neige (S)_RFx_kN



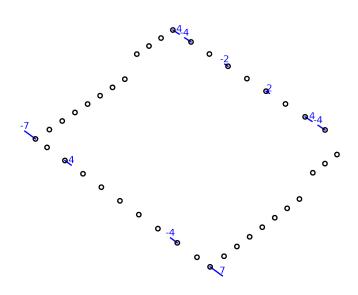


FIGURE 2.8 – Neige (S)_RFy_kN



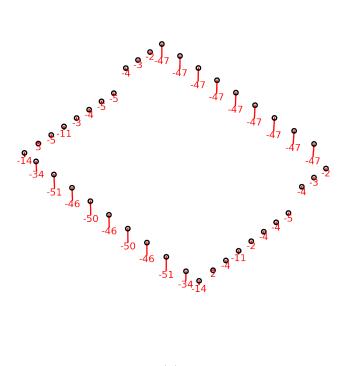


FIGURE 2.9 - Neige (S)_RFz_kN



2.4 G+S

Nom point	X	Y	Z	RFx_kN	RFy_kN	RFz_kN
A1	0	0	5790			-7
$\overline{\mathrm{A}}_{-2}^{-}$	3250	0	5790			-10
A_3	6500	0	5790			-17
A_4	9750	0	0	-5		-19
A_5	13000	0	0			-30
A_6	16250	0	0	3		-53
A_7	19500	0	0			-58
A_8	22750	0	0	-7		-41
A_9	26000	0	0			-29
A_10	29250	0	0			-30
A_11	32740	0	0		-31	-96
B_1	0	3160	11112		14	-141
B_11	32740	3160	0	2		-172
C_1	0	7960	11112		-7	-144
C_11	32740	7960	0	2	21	-245
D_1	0	12760	11112			-146
D_11	32740	12760	0	2		-211
E_1	0	17560	11112		-3	-148
E_11	32740	17560	0	2		-244
F_1	0	22360	11112			-148
F_11	32740	22360	0	2		-213
G_1	0	27160	11112		3	-148
G_11	32740	27160	0	2		-244
H_1	0	31960	11112			-146
H_11	32740	31960	0	2		-211
I_1	0	36760	11112		7	-144
I_11	32740	36760	0	2	-21	-245
J_1	0	41560	11112		-14	-141
J_11	32740	41560	0	2		-172
K_1	0	44720	5790			-7
K_2	3250	44720	5790			-10
K_3	6500	44720	5790			-17
K_4	9750	44720	0	-5		-17
K_5	13000	44720	0			-20
K_6	16250	44720	0	4		-28
K_7	19500	44720	0	_		-15
K_8	22750	44720	0	-9		-37
K_9	26000	44720	0			-22
K_10	29250	44720	0	1		-27
K_11	32740	44720	0		31	-96



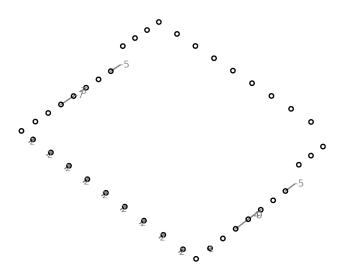


FIGURE $2.10 - G + S_RFx_kN$



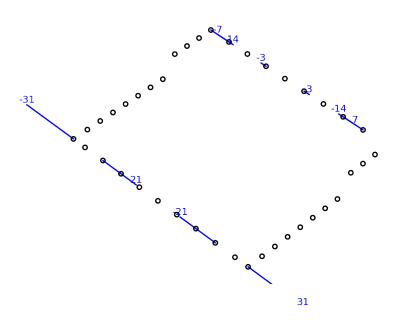


FIGURE $2.11 - G + S_RFy_kN$



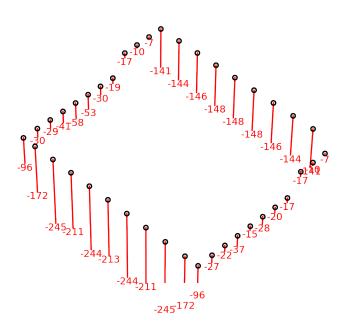


FIGURE $2.12 - G + S_RFz_kN$



2.5 max(G,S)

Nom point	X	Y	Z	RFx_kN	RFy_kN	RFz_kN
A 1	0	0	5790			-5
A_2	3250	0	5790			-7
A_3	6500	0	5790			-13
A_4	9750	0	0	-3		-14
A_5	13000	0	0			-25
A_6	16250	0	0			-48
A_7	19500	0	0			-55
A_8	22750	0	0	-5		-30
A_9	26000	0	0			-24
A_10	29250	0	0	-1		-33
A_11	32740	0	0		-24	-82
B_1	0	3160	11112		4	-94
B_11	32740	3160	0			-138
C_1	0	7960	11112		-4	-97
C_11	32740	7960	0		4	-194
D_1	0	12760	11112			-99
D_11	32740	12760	0	1		-165
E_1	0	17560	11112		-2	-101
E_11	32740	17560	0			-195
F_1	0	22360	11112			-101
F_11	32740	22360	0	1		-167
G_1	0	27160	11112		2	-101
G_11	32740	27160	0			-195
H_1	0	31960	11112			-99
H_11	32740	31960	0	1		-165
I_1	0	36760	11112		3	-97
I_11	32740	36760	0		-17	-194
J_1	0	41560	11112		-10	-94
J_11	32740	41560	0			-138
K_1	0	44720	5790			-5
K_2	3250	44720	5790			-7
K_3	6500	44720	5790	-1		-13
K_4	9750	44720	0	-3		-12
K_5	13000	44720	0			-16
K_6	16250	44720	0			-24
K_{2}	19500	44720	0			-13
K_8	22750	44720	0	-6		-26
K_9	26000	44720	0			-18
K_10	29250	44720	0			-30
K_11	32740	44720	0		7	-82



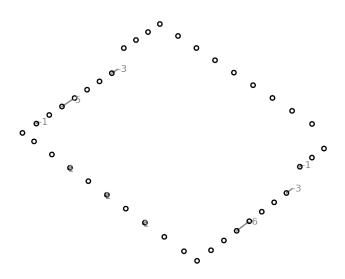


FIGURE $2.13 - max(G,S)_RFx_kN$



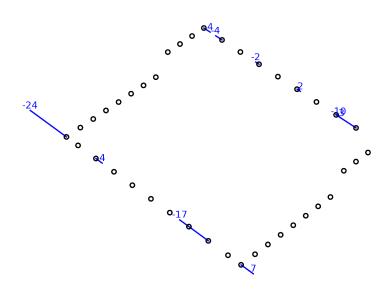


FIGURE $2.14 - max(G,S)_RFy_kN$



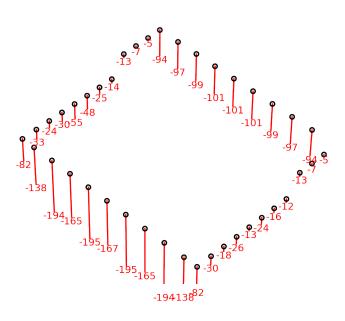


FIGURE $2.15 - max(G,S)_RFz_kN$



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2.5	Charges d'exploitation (Q)_RFy_kN
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2.7	Neige (S)_RFx_kN
2.8	Neige (S)_RFy_kN
2.9	Neige (S)_RFz_kN
	G+S_RFx_kN
	G+S_RFy_kN
	G+S_RFz_kN
	$\max(\overline{G}, S) \underline{R} Fx \underline{k} N \dots $
	$\max(G,S) = RFy = kN $
	$\max(G,S) \text{RFz kN} \dots 24$

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