

# DESCENTE DE CHARGES

Ville de Besançon La City - 4 rue Gabriel Plançon BESANCON CEDEX 25043





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## **SYNAPSE**\*

SYNAPSE / Structure, Fluides, VRD, CSSI 200 Bd de la résistance 71 000 MACON vbourillon@synapse-construction.com 03 85 38 66 22

Complexe sportif Diderot

Lot 4 Ossature et Veture bois



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			Affaire N°:	2404-234
			Réf.S:	GBM Diderot
			Doc N°:	2409-501



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Projet: Complexe sportif Diderot

Reference: GBM Diderot



# Chapitre 1 INFORMATIONS GENERALES

### 1.1 Situation de l'ouvrage

Affaire/projet : 2404-234GBM Diderot

Note d'hypothèse  $N^{\circ}$  : 2409-500

Adresse: Gymnase Diderot Rue de Cologne 25000 BESANCON

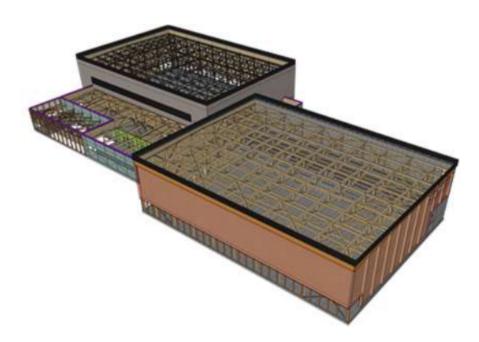


FIGURE 1.1 – Description de l'ouvrage

### 1.2 Plan de situation

### 1.3 Description de l'ouvrage

### 1.4 Règles de calcul et de conception

Les calculs de structures sont réalisés conformément aux normes Eurocode en vigueur :

(i) Eurocode 0 EN 1990 : Base de calcul des structures

(ii) Eurocode 1 EN 1991 : Actions sur les structures

(iii) Eurocode 2 EN 1992 : Calculs des structures en béton

(iv) Eurocode 3 EN 1993 : Calculs des structures en acier

(v) Eurocode 4 EN 1994 : Calculs des structures mixtes acier-béton

(vi) Eurocode 5 EN 1995 : Calculs des structures en bois

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- (vii) Eurocode 6 EN 1996 : Calculs des structures en maçonnerie
- (viii) Eurocode 8 EN 1998 : Calculs des structures pour leur résistance aux séismes
- (ix) Résix® Technique d assemblage sous avis technique CSTB 3.3-19-986 V1

### 1.5 Stabilité et Repérage des points d'appuis

### 1.5.1 Principe de stabilité de la structure

### 1.5.2 Repérage des points d'appuis

K_1 1	K_2	<b>K</b> _3	K_4	K_5	<b>K</b> _6	<b>K</b> _7	<b>K</b> _8	<b>K</b> _9	K_10	K_11
<u></u> 1										<b>↓</b> 11
H_1										H_11
G_1										G_11
F_1										F_11
<b>F</b> _1										<b>E</b> _11
P_1										P_11
<u>C</u> _1										C_11
B_1 A_1	<b>A</b> _2	<b>A</b> _3	<u>A_4</u>	<b>A</b> _5	<b>A</b> _6	<b>A</b> _7	<b>A</b> _8	<b>A</b> _9	A_10	B_11 A_11

Figure 1.2 – Repèrage des points d'appui 2D - Groupe 1



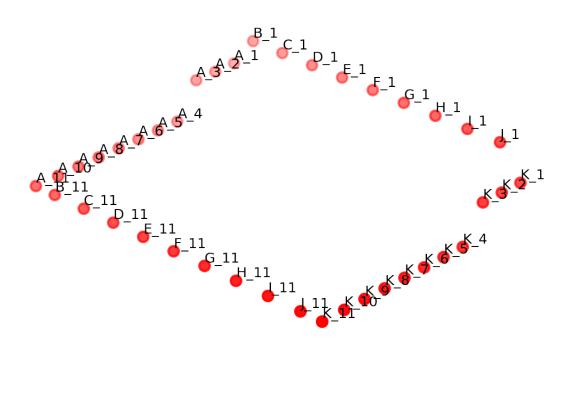


FIGURE 1.3 – Repèrage des points d'appui 3D - Groupe 1





Figure 1.4 – Repèrage des points d'appui 2D - Groupe 2

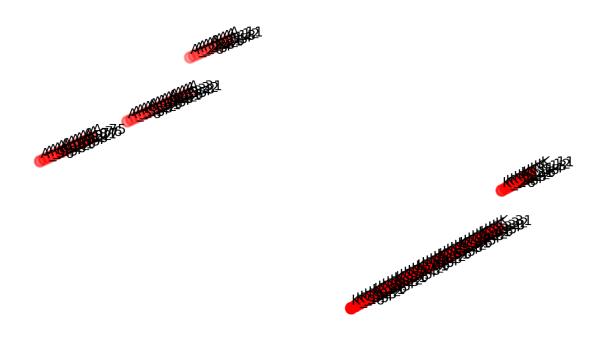


Figure 1.5 – Repèrage des points d'appui 3D - Groupe 2



# Chapitre 2 DESCENTE DE CHARGES

## 2.1 Charges permanentes (G)

Nom point	Х	Y	Z	RFx_kN	RFy_kN	RFz_kN
A_1	0	0	5790	0	0	-5
A_2	3250	0	5790	0	0	-7
A_3	6500	0	5790	1	0	-13
A_4	9750	0	0	-3	0	-14
A_5	13000	0	0	0	0	-25
A_6	16250	0	0	3	0	-48
A_7	19500	0	0	0	0	-55
A_8	22750	0	0	-5	0	-30
A_9	26000	0	0	0	0	-24
A_10	29250	0	0	1	0	-33
A_11	32740	0	0	-1	-24	-82
B_1	0	3160	11112	0	10	-94
B_11	32740	3160	0	1	-1	-138
C_1	0	7960	11112	0	-3	-97
C_11	32740	7960	0	1	17	-194
D_1	0	12760	11112	0	0	-99
D_11	32740	12760	0	1	0	-165
E_1	0	17560	11112	0	-2	-101
E_11	32740	17560	0	0	0	-195
F_1	0	22360	11112	0	0	-101
F_11	32740	22360	0	1	0	-167
G_1	0	27160	11112	0	2	-101
G_11	32740	27160	0	0	0	-195
H_1	0	31960	11112	0	0	-99
H_11	32740	31960	0	1	0	-165
I_1	0	36760	11112	0	3	-97
I_11	32740	36760	0	1	-17	-194
J_1	0	41560	11112	0	-10	-94
J_11	32740	41560	0	1	1	-138
K_1	0	44720	5790	0	0	-5
K_2	3250	44720	5790	0	0	-7
K_3	6500	44720	5790	1	0	-13
K_4	9750	44720	0	-3	0	-12
K_5	13000	44720	0	0	0	-16
K_6	16250	44720	0	4	0	-24
K_7	19500	44720	0	0	0	-13
K_8	22750	44720	0	-6	0	-26
K_9	26000	44720	0	0	0	-18
K_10	29250	44720	0	2	0	-30
K_11	32740	44720	0	-1	24	-82

Projet: Complexe sportif Diderot

Reference: GBM Diderot



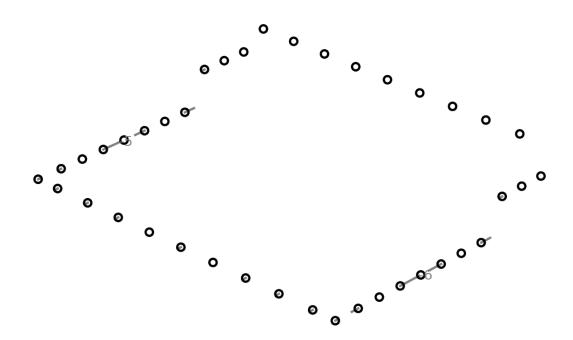


Figure 2.1 – Charges permanentes (G)\_RFx\_kN



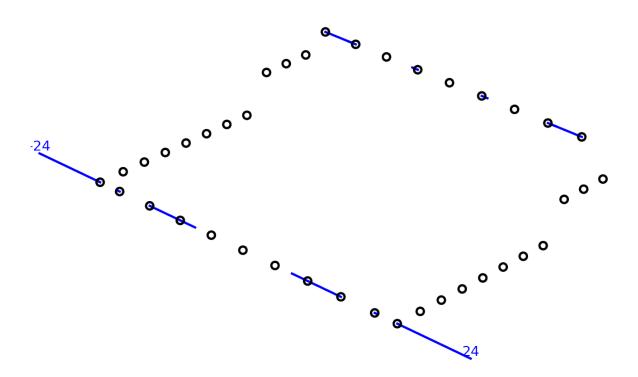


Figure 2.2 – Charges permanentes (G)\_RFy\_kN



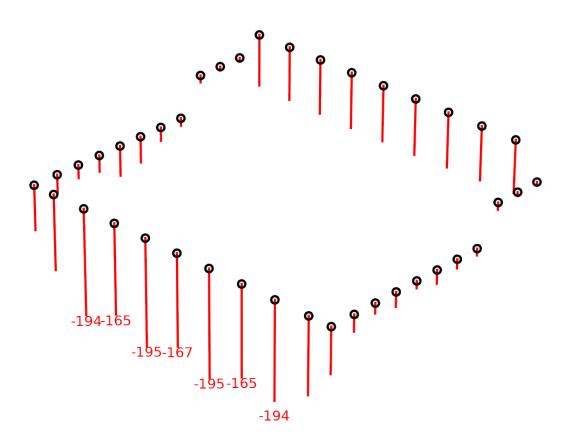


Figure 2.3 – Charges permanentes (G)\_RFz\_kN



# 2.2 Charges d'exploitation (Q)

Nom point	Х	Y	Z	RFx_kN	RFy_kN	RFz_kN
A_1	0	0	5790	0	0	0
A_2	3250	0	5790	0	0	0
A_3	6500	0	5790	0	0	0
A_4	9750	0	0	0	0	0
A_5	13000	0	0	0	0	0
A_6	16250	0	0	0	0	0
A_7	19500	0	0	0	0	0
A_8	22750	0	0	0	0	0
A_9	26000	0	0	0	0	0
A_10	29250	0	0	0	0	0
A_11	32740	0	0	0	0	0
B_1	0	3160	11112	0	0	0
B_11	32740	3160	0	0	0	0
C_1	0	7960	11112	0	0	0
C_11	32740	7960	0	0	0	-1
D_1	0	12760	11112	0	0	0
D_11	32740	12760	0	0	0	-1
E_1	0	17560	11112	0	0	0
E_11	32740	17560	0	0	0	0
F_1	0	22360	11112	0	0	0
F_11	32740	22360	0	0	0	0
G_1	0	27160	11112	0	0	0
G_11	32740	27160	0	0	0	0
H_1	0	31960	11112	0	0	0
H_11	32740	31960	0	0	0	-1
I_1	0	36760	11112	0	0	0
I_11	32740	36760	0	0	0	-1
J_1	0	41560	11112	0	0	0
J_11	32740	41560	0	0	0	0
K_1	0	44720	5790	0	0	0
K_2	3250	44720	5790	0	0	0
K_3	6500	44720	5790	0	0	0
K_4	9750	44720	0	0	0	0
K_5	13000	44720	0	0	0	0
K_6	16250	44720	0	0	0	0
K_7	19500	44720	0	0	0	0
K_8	22750	44720	0	0	0	0
K_9	26000	44720	0	0	0	0
K_10	29250	44720	0	0	0	0
K_11	32740	44720	0	0	0	0



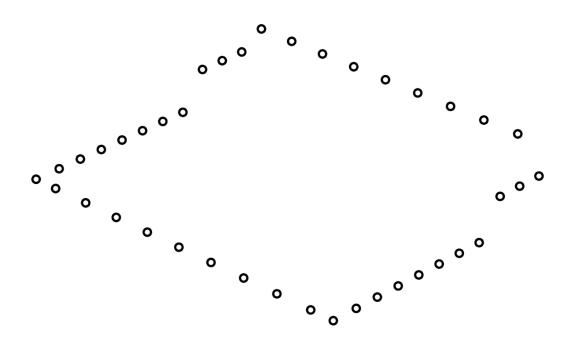


Figure 2.4 – Charges d'exploitation (Q)\_RFx\_kN



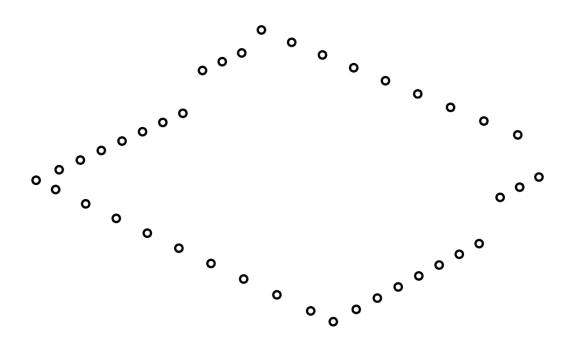


Figure 2.5 – Charges d'exploitation (Q)\_RFy\_kN



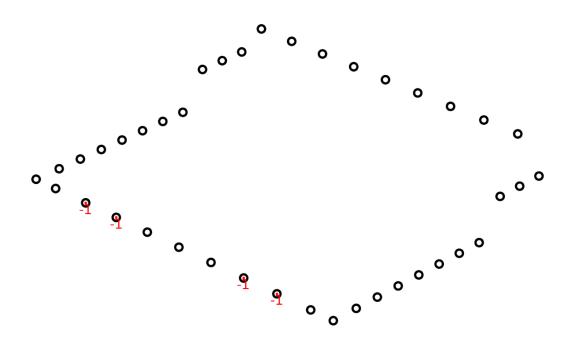


Figure 2.6 – Charges d'exploitation (Q)\_RFz\_kN



# 2.3 Neige (S)

Nom point	Х	Y	Z	RFx_kN	RFy_kN	RFz_kN
A_1	0	0	5790	0	0	-2
A_2	3250	0	5790	0	0	-3
A_3	6500	0	5790	-1	0	-4
A_4	9750	0	0	-1	0	-5
A_5	13000	0	0	0	0	-5
A_6	16250	0	0	0	0	-4
A_7	19500	0	0	0	0	-3
A_8	22750	0	0	-2	0	-11
A_9	26000	0	0	0	0	-5
A_10	29250	0	0	-1	0	3
A_11	32740	0	0	0	-7	-14
B_1	0	3160	11112	0	4	-47
B_11	32740	3160	0	1	0	-34
C_1	0	7960	11112	0	-4	-47
C_11	32740	7960	0	1	4	-51
D_1	0	12760	11112	0	0	-47
D_11	32740	12760	0	1	0	-46
E_1	0	17560	11112	0	-2	-47
E_11	32740	17560	0	1	0	-50
F_1	0	22360	11112	0	0	-47
F_11	32740	22360	0	1	0	-46
G_1	0	27160	11112	0	2	-47
G_11	32740	27160	0	1	0	-50
H_1	0	31960	11112	0	0	-47
H_11	32740	31960	0	1	0	-46
I_1	0	36760	11112	0	4	-47
I_11	32740	36760	0	1	-4	-51
J_1	0	41560	11112	0	-4	-47
J_11	32740	41560	0	1	0	-34
K_1	0	44720	5790	0	0	-2
K_2	3250	44720	5790	0	0	-3
K_3	6500	44720	5790	-1	0	-4
K_4	9750	44720	0	-2	0	-5
K_5	13000	44720	0	0	0	-4
K_6	16250	44720	0	0	0	-4
K_7	19500	44720	0	0	0	-2
K_8	22750	44720	0	-3	0	-11
K_9	26000	44720	0	0	0	-4
K_10	29250	44720	0	-1	0	2
K_11	32740	44720	0	0	7	-14



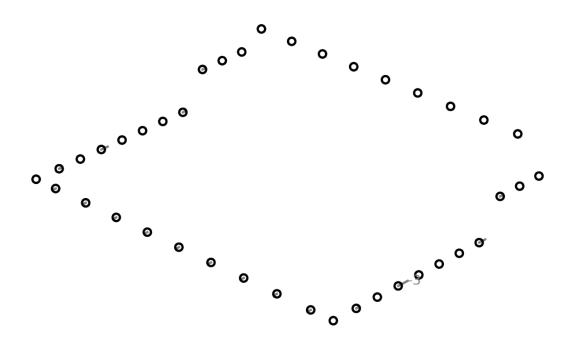


Figure  $2.7 - Neige(S)_RFx_kN$ 



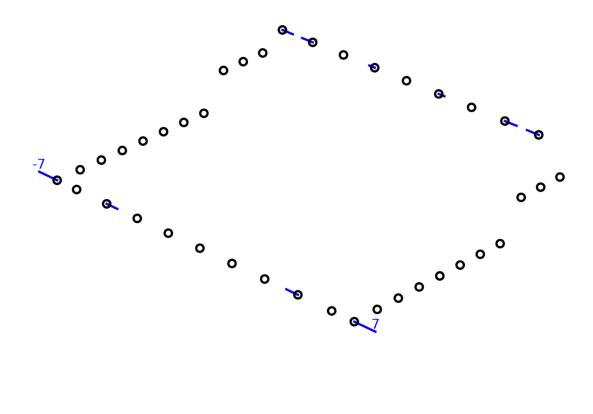


Figure 2.8 – Neige (S)\_RFy\_kN



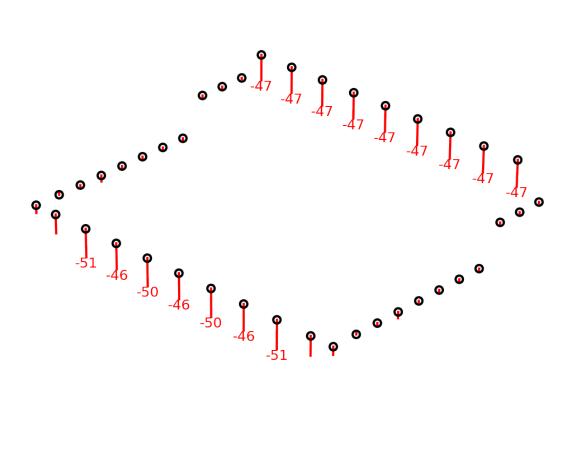


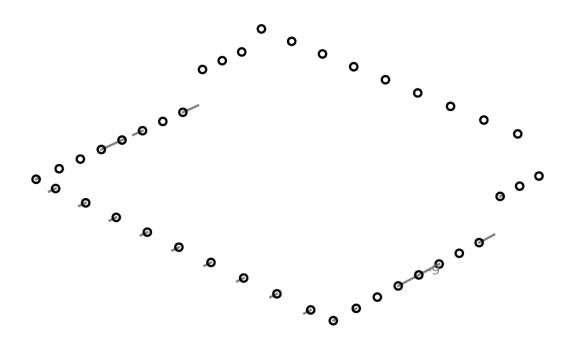
FIGURE 2.9 - Neige (S)\_RFz\_kN



## 2.4 G+S

Nom point	Х	Y	Z	RFx_kN	RFy_kN	RFz_kN
A_1	0	0	5790	0	0	-7
A_2	3250	0	5790	0	0	-10
A_3	6500	0	5790	0	0	-17
A_4	9750	0	0	-5	0	-19
A_5	13000	0	0	0	0	-30
A_6	16250	0	0	3	0	-53
A_7	19500	0	0	0	0	-58
A_8	22750	0	0	-7	0	-41
A_9	26000	0	0	0	0	-29
A_10	29250	0	0	0	0	-30
A_11	32740	0	0	-1	-31	-96
B_1	0	3160	11112	0	14	-141
B_11	32740	3160	0	2	-1	-172
C_1	0	7960	11112	0	-7	-144
C_11	32740	7960	0	2	21	-245
D_1	0	12760	11112	0	0	-146
D_11	32740	12760	0	2	0	-211
E_1	0	17560	11112	0	-3	-148
E_11	32740	17560	0	2	0	-244
F_1	0	22360	11112	0	0	-148
F_11	32740	22360	0	2	0	-213
G_1	0	27160	11112	0	3	-148
G_11	32740	27160	0	2	0	-244
H_1	0	31960	11112	0	0	-146
H_11	32740	31960	0	2	0	-211
I_1	0	36760	11112	0	7	-144
I_11	32740	36760	0	2	-21	-245
J_1	0	41560	11112	0	-14	-141
J_11	32740	41560	0	2	1	-172
K_1	0	44720	5790	0	0	-7
K_2	3250	44720	5790	0	0	-10
K_3	6500	44720	5790	-1	0	-17
K_4	9750	44720	0	-5	0	-17
K_5	13000	44720	0	0	0	-20
K_6	16250	44720	0	4	0	-28
K_7	19500	44720	0	0	0	-15
K_8	22750	44720	0	-9	0	-37
K_9	26000	44720	0	0	0	-22
K_10	29250	44720	0	1	0	-27
K_11	32740	44720	0	-1	31	-96





 $FIGURE~2.10-G+S\_RFx\_kN$ 



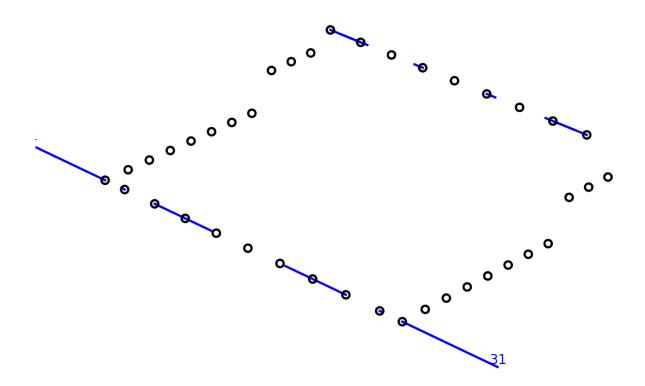
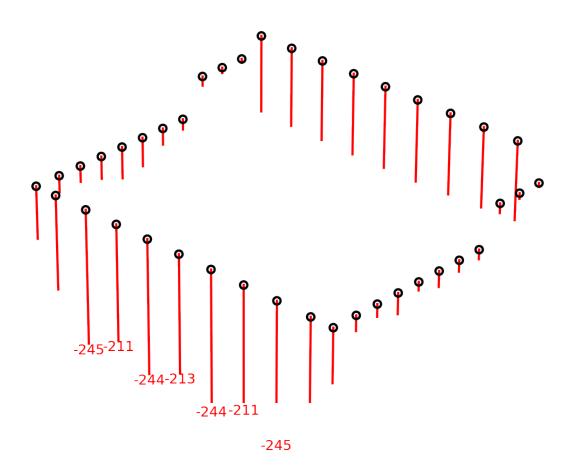


FIGURE  $2.11 - G + S_RFy_kN$ 





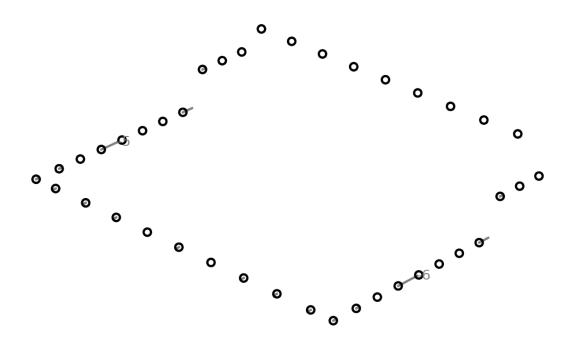
 $FIGURE~2.12-G+S\_RFz\_kN$ 



# 2.5 max(G,S)

Nom point	Х	Y	Z	RFx_kN	RFy_kN	RFz_kN
A_1	0	0	5790	0	0	-5
A_2	3250	0	5790	0	0	-7
A_3	6500	0	5790	-1	0	-13
A_4	9750	0	0	-3	0	-14
A_5	13000	0	0	0	0	-25
A_6	16250	0	0	0	0	-48
A_7	19500	0	0	0	0	-55
A_8	22750	0	0	-5	0	-30
A_9	26000	0	0	0	0	-24
A_10	29250	0	0	-1	0	-33
A_11	32740	0	0	-1	-24	-82
B_1	0	3160	11112	0	4	-94
B_11	32740	3160	0	1	-1	-138
C_1	0	7960	11112	0	-4	-97
C_11	32740	7960	0	1	4	-194
D_1	0	12760	11112	0	0	-99
D_11	32740	12760	0	1	0	-165
E_1	0	17560	11112	0	-2	-101
E_11	32740	17560	0	0	0	-195
F_1	0	22360	11112	0	0	-101
F_11	32740	22360	0	1	0	-167
G_1	0	27160	11112	0	2	-101
G_11	32740	27160	0	0	0	-195
H_1	0	31960	11112	0	0	-99
H_11	32740	31960	0	1	0	-165
I_1	0	36760	11112	0	3	-97
I_11	32740	36760	0	1	-17	-194
J_1	0	41560	11112	0	-10	-94
J_11	32740	41560	0	1	0	-138
K_1	0	44720	5790	0	0	-5
K_2	3250	44720	5790	0	0	-7
K_3	6500	44720	5790	-1	0	-13
K_4	9750	44720	0	-3	0	-12
K_5	13000	44720	0	0	0	-16
K_6	16250	44720	0	0	0	-24
K_7	19500	44720	0	0	0	-13
K_8	22750	44720	0	-6	0	-26
K_9	26000	44720	0	0	0	-18
K_10	29250	44720	0	-1	0	-30
K_11	32740	44720	0	-1	7	-82





 $FIGURE~2.13-max(G,\!S)\_RFx\_kN$ 



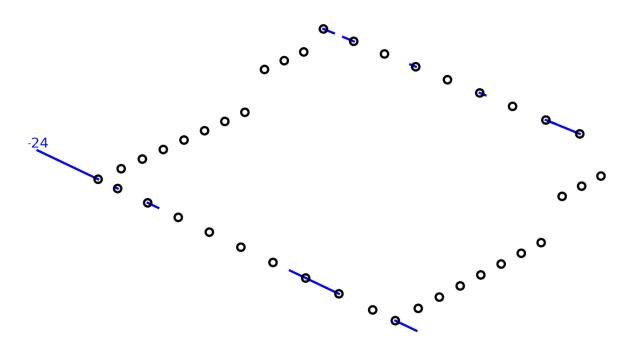


FIGURE  $2.14 - max(G,S)_RFy_kN$ 



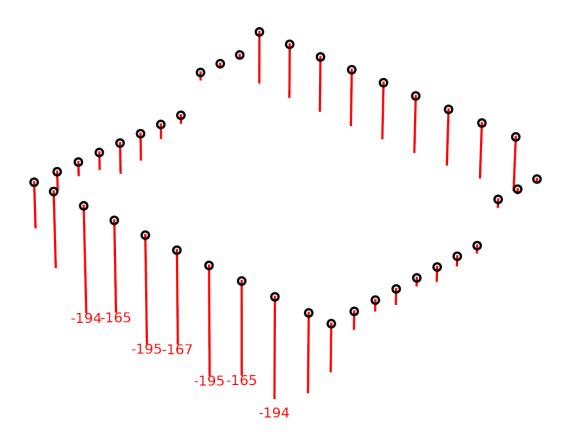


FIGURE  $2.15 - max(G,S)_RFz_kN$ 





Projet: Complexe sportif Diderot

Reference: GBM Diderot



# 2.6 Charges permanentes (G)

Projet: Ckor2plexe sport3875de44720

Reference 23BM Dider 3975

Nom point	Х	Y	Z	RFx_kN	RFy_kN	RFz_kN
A_11	125	0	5790	0	0	-3
_ A_12	725	0	5790	0	0	-5
A_13	1325	0	5790	0	0	-5
A_14	1925	0	5790	0	0	-5
A_15	2525	0	5790	0	0	-5
A_16	3125	0	5790	0	0	-4
A_21	3375	0	5790	0	0	-4
A_22	3975	0	5790	0	0	-5
A_23	4575	0	5790	0	0	-5
A_24	5175	0	5790	0	0	-5
A_25	5775	0	5790	0	0	-5
A_26	6375	0	5790	0	0	-4
A_31	6625	0	0	0	0	-6
A_32	7225	0	0	0	0	-9
A_33	7825	0	0	0	0	-10
A_34	8425	0	0	0	0	-10
A_35	9025	0	0	0	0	-9
A_36	9625	0	0	0	0	-5
A_41	9875	0	0	0	0	-5
A_42	10475	0	0	0	0	-9
A_43	11075	0	0	0	0	-10
A_44	11675	0	0	0	0	-10
A_45	12275	0	0	0	0	-9
A_46	12875	0	0	0	0	-6
A_51	13125	0	0	0	0	-6
A_52	13725	0	0	0	0	-9
A_53	14325	0	0	0	0	-10
A_54	14925	0	0	0	0	-10
A_55	15525	0	0	0	0	-9
A_56	16125	0	0	0	0	-6
A_75	21425	0	0	0	0	-19
A_76	22025	0	0	0	0	-9
A_77	22625	0	0	0	0	-5
A_81	22875	0	0	0	0	-6
A_82	23475	0	0	0	0	-9
A_83	24075	0	0	0	0	-10
A_84	24675	0	0	0	0	-10
A_85	25275	0	0	0	0	-9
A_86	25875	0	0	0	0	-6
A_91	26125	0	0	0	0	-6
A_92	26725	0	0	0	0	-10
A_93	27325	0	0	0	0	-8
A_94	27925	0	0	0	0	-9
A_95	28525	0	0	0	0	-9
A_96	29125	0	0	0	0	-6
K_11	125	44720	5790	0	0	-3
K_12	725	44720	5790	0	0	-5
K_13	1325	44720	5790	0	0	-5
K_14	1925	44720	5790	0	0	-5
K_15	2525	44720	5790	0	0	-5
K_16	3125	44720	5790	0	0	-4

5790

5790

44720

0

0

-4

-5

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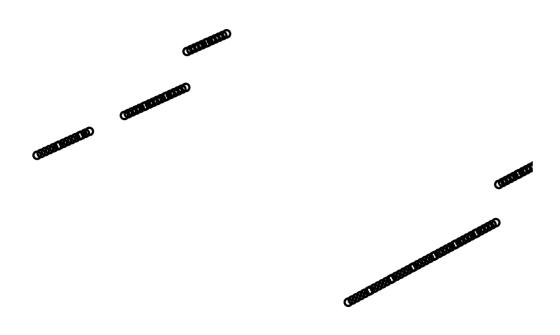


Figure 2.16 - Charges permanentes (G)\_RFx\_kN



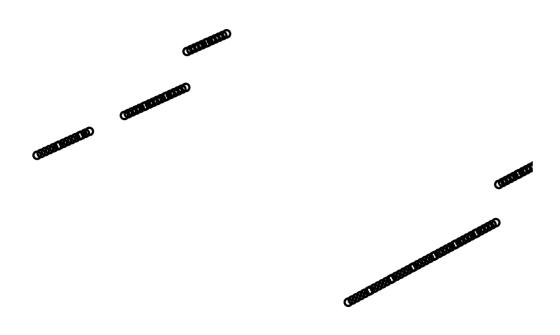


Figure 2.17 – Charges permanentes (G)\_RFy\_kN

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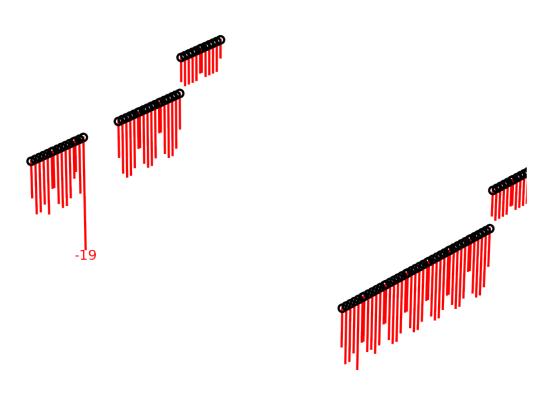


Figure 2.18 – Charges permanentes (G)\_RFz\_kN

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# 2.7 Combinaison ELU STR (Charges en kN)

Nom point	RFxmin_kN	RFxmax_kN	RFymin_kN	RFymax_kN	RFzmin_kN	RFzmax_kN
A_1	0	0	-1	0	-10	-2
A_2	0	0	-1	1	-15	-2
A_3	-49	40	-8	9	-24	-9
A_4	-38	23	-6	6	-165	103
A_5	0	0	-6	7	-43	-19
A_6	-29	30	-7	8	-176	95
A_7	0	0	-7	8	-80	-52
A_8	-52	30	-6	6	-183	75
A_9	0	0	-6	6	-40	-19
A_10	-44	36	-10	7	-147	119
A_11	-1	0	-73	10	-214	0
B_1	0	0	-6	34	-212	-44
B_11	-7	11	-1	-1	-251	-95
C_1	0	0	-69	72	-219	-50
C_11	-9	11	-21	53	-369	-64
D_1	0	0	0	0	-222	-52
D_11	-8	10	0	0	-309	-121
E_1	0	0	-39	50	-225	-54
E_11	-11	12	0	0	-356	-147
F_1	0	0	0	0	-224	-54
F_11	-8	11	0	0	-310	-122
G_1	0	0	-49	37	-225	-53
G_11	-11	12	0	0	-356	-146
H_1	0	0	0	0	-222	-52
H_11	-8	10	0	0	-309	-121
I_1	0	0	-71	68	-219	-50
I_11	-9	11	-53	20	-368	-66
J_1	0	0	-34	6	-212	-44
J_11	-7	11	1	1	-251	-95
K_1	0	0	0	1	-10	-2
K_2	0	0	-1	1	-15	-2
K_3	-54	43	-9	8	-24	-9
K_4	-37	22	-4	4	-149	93
K_5	0	0	-4	4	-31	-10
K_6	-25	27	-4	4	-129	102
K_7	0	0	-4	4	-21	-10
K_8	-53	29	-4	4	-173	76
K_9	0	0	-4	4	-31	-14
K_10	-43	36	-5	8	-138	116
K_11	-1	0	-10	73	-213	-2

Projet: Complexe sportif Diderot

Reference: GBM Diderot



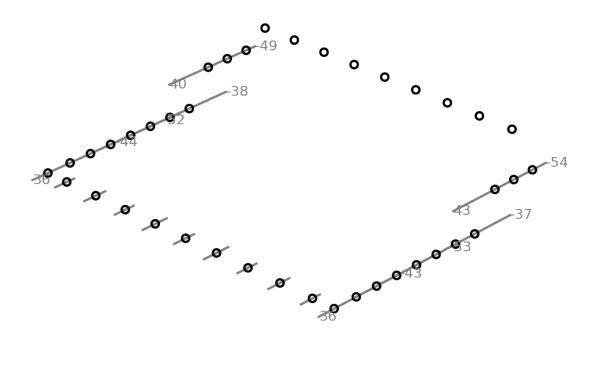


FIGURE 2.19 – Combinaison ELU STR (Charges en kN)\_RFx\_kN



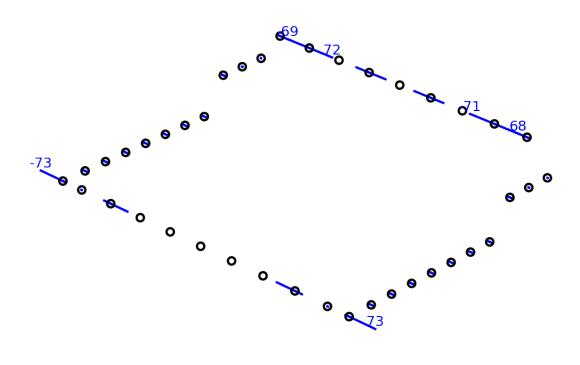


FIGURE 2.20 – Combinaison ELU STR (Charges en kN)\_RFy\_kN



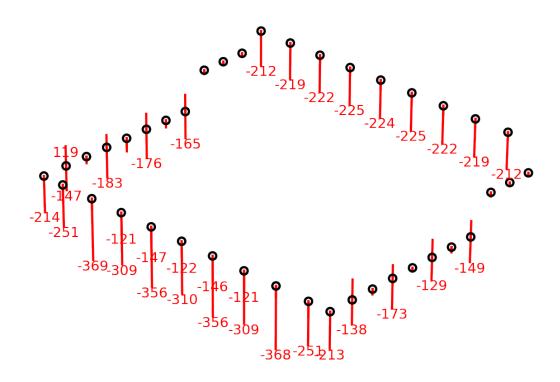


FIGURE 2.21 - Combinaison ELU STR (Charges en kN)\_RFz\_kN



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Projet: Complexe sportif Diderot

Reference: GBM Diderot