

Tensor Calculus  
J.L. Synge and A.Schild (Dover Publication)  
Solutions to exercises  
Part II  
Chapters V to VIII

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## Remarks and warnings

You're welcome to use these notes, but they may contain errors, so proceed with caution. If you do find an error, however, I'd be happy to receive bug reports, suggestions, and the like through Github. An overview of the material covered in the book can be found in the separate document "Synge overview.pdf".

## Some notation conventions

$$\partial_r \equiv \frac{\partial}{\partial x^r}$$

$$\Gamma_{mn}^r \equiv \left\{ \begin{matrix} r \\ mn \end{matrix} \right\} \quad \text{Christoffel symbol of the second kind}$$

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# Applications to Classical Mechanics

## 5.1 p153 - Exercise

If  $\mu^\alpha$  are the contravariant components of a unit vector in a surface  $S$ , show that  $\mu^\alpha f_\alpha$  is the physical component of acceleration in the direction tangent to  $S$  defined by  $\mu^\alpha$ .

As we are in an Euclidean space we can interpret  $a_{mn}\mu^\alpha f^\alpha$  as  $|\mu||f|\cos\theta$  with  $\theta$  the angle between the two vectors. As  $|\mu| = 1$  we have

$$a_{mn}\mu^\alpha f^\alpha = \mu^\alpha f_\alpha \tag{1}$$

$$= |f|\cos\theta \tag{2}$$

which is the projection of the vector  $f$  on the unit vector  $\mu$ .



## 5.2 p154 - Clarification to 5.226.

$$5.226. \quad \mathbf{v} \frac{d\mathbf{v}}{ds} = \mathbf{0}, \quad \bar{\kappa} \mathbf{v}^2 = \mathbf{0}$$

Assuming that the particle is not at rest  $v \neq 0$ , and therefore  $\bar{\kappa} = 0$ . ***Since this implies that the curve is a geodesic...***

The assertion in bold is a direct consequence

$$2.513. \quad \frac{\delta \frac{dx^r}{ds}}{\delta s} = 0$$

As in **5.233** we have  $\frac{\delta \lambda^\alpha}{\delta s} = \frac{\delta \frac{dx^\alpha}{ds}}{\delta s} = 0$ , the considered curve follows the geodesic curve.



### 5.3 p155 - Exercise

Show that in relativity the force 4-vector  $X^r$  lies along the first normal of the trajectory in space-time. Express the first curvature in terms of the proper mass  $m$  of the particle and the magnitude  $X$  of  $X^r$ .

Let us recall the first Frenet formula **2.705** without forgetting that the metric form is not positive-definite,

$$\frac{\delta \lambda^r}{\delta s} = \kappa \nu^r, \quad \epsilon_{(1)} \nu_n \nu^n = 1$$

As **5.299**

$$m \frac{\delta \lambda^r}{\delta s} = X^r$$

it is clear that  $X^r = m \kappa \nu^r$  and is collinear with the first normal.

$$X^r = m \kappa \nu^r \tag{1}$$

$$\times \quad a_{mr} X^m \quad \Rightarrow \quad \underbrace{a_{mr} X^m X^r}_{=(X^1)^2 + (X^2)^2 + (X^3)^2 - (X^4)^2} = m \kappa \underbrace{a_{mr} \nu^m \nu^r}_{=\epsilon_{(1)}} \tag{2}$$

$$\Rightarrow \quad \kappa = \epsilon_{(1)} \frac{(X^1)^2 + (X^2)^2 + (X^3)^2 - (X^4)^2}{m}$$





## 5.4 p156 - Clarification

Interpretation of

$$\mathbf{5.231.} \quad M_{rs} = \epsilon_{rsn} M_n = z_r F_s - z_s F_r$$

What do the  $M_{rs}$  represent?

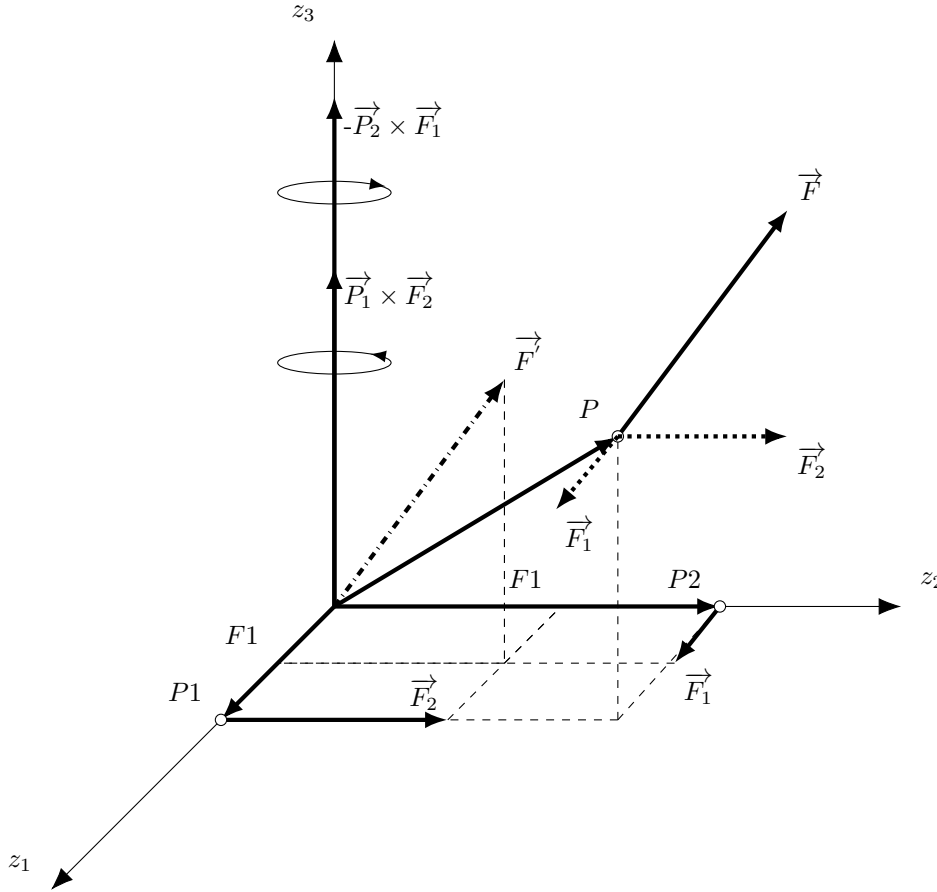


Figure 5.1: Interpretation of the tensor moment  $M_{12}$

Let's consider a mass point  $P$  on which a force  $\vec{F}$  is acting. The force has components  $(F_x, F_y, F_z)$  in the space  $V'_3$  (which is by the way not the space  $V_3$  of the considered mass point).

Let's investigate the element  $M_{12}$  of the *tensor moment*.

$P_1 F_2 \vec{e}_3$  is the vector product  $\vec{P}_1 \times \vec{F}_2$  and is as such the torque of the component  $F_2$  of  $\vec{F}$  acting on the mass point situated at  $P_1$ . The origin being fixed,  $\vec{F}_2$  tries to move  $P_1$ , clockwise along the  $z_3$  axis. The same is true for the component  $\vec{F}_1$  acting on the mass point situated at  $P_2$ , and is represented here by the vector  $-\vec{P}_2 \times \vec{F}_1$  ( $\vec{F}_1$  tries to move  $P_2$ , counter clockwise along the  $z_3$  axis). Hence,  $P_1 F_2 - P_2 F_1$  is the net force trying to move the point  $P$  along the  $z_3$  axis (i.e. in the plane  $\parallel$  with the  $z_3 = 0$  plane).



## 5.5 p156 - Clarification

$$\mathbf{5.234.} \quad \frac{dh_r}{dt} = M_r$$

$$h_r = m\epsilon_{rmn}z_mv_n \tag{1}$$

$$\Rightarrow \quad \frac{dh_r}{dt} = m\epsilon_{rmn} \frac{dz_m}{dt} v_n + m\epsilon_{rmn} z_m \frac{dv_n}{dt} \tag{2}$$

$$= m \underbrace{\epsilon_{rmn} v_m v_n}_{=0} + \underbrace{\epsilon_{rmn} z_m F_n}_{=M_r} \tag{3}$$

$$= M_r \tag{4}$$



## 5.6 p158-159 - Clarification

$$\mathbf{5.313.} \quad \omega_{rs} = -\omega_{sr}$$

From 5.310 and the vector character of  $v_r$  and  $z_r$  (for transformations which do not change the origin), **it follows that  $\omega_{rs}$  is a Cartesian tensor of second order.**

Be

$$v_r = -\omega_{rn} z_n \quad (1)$$

Considering orthogonal transformation in a flat space  $z'_m = A_{mr} z_r + B_m$  with  $B_m = 0$  as we consider only transformations which do not change the origin. Differentiation with the parameter  $t$  gives

$$v'_m = A_{mr} v_r \quad (2)$$

$$= -\omega_{rn} A_{mr} z_n \quad (3)$$

$$(4)$$

But  $z'_q = A_{qr} z_r \Rightarrow A_{qn} z'_q = A_{qn} A_{qr} z_r \Rightarrow A_{qn} z'_q = z_n$  Hence

$$v'_m = -\omega_{rn} A_{mr} z_n \quad (5)$$

$$= -\underbrace{\omega_{rn} A_{mr} A_{qn}}_{\stackrel{\text{def}}{=} \omega'_{mq}} z'_q \quad (6)$$

$$v'_m = -\omega'_{mq} z'_q \quad (7)$$



## 5.7 p159 - Exercise

Show that if a rigid body rotates about the point  $z_r = b_r$  as fixed point, the velocity of a general point of the body is given by

$$v_r = -\omega_{rm} (z_m - b_m)$$

By **5.302**..

$$\left(z_m^{(1)} - z_m^{(2)}\right) \left(dz_m^{(1)} - dz_m^{(2)}\right) = 0 \quad (1)$$

At the fixed point we have  $z_m^{(2)} = b_m$  and  $dz_m^{(2)} = 0$ , hence

$$\left(z_m^{(1)} - b_m\right) \left(dz_m^{(1)}\right) = 0 \quad (2)$$

$$\Rightarrow z_m^{(1)} dz_m^{(1)} = b_m dz_m^{(1)} \quad (3)$$

As this is true for any point of the rigid mass, expanding (1) and using (3) we get when dividing by  $dt$

$$\left(z_m^{(2)} - b_m\right) v_m^{(1)} + \left(z_m^{(1)} - b_m\right) v_m^{(2)} = 0 \quad (4)$$

Taking twice the partial derivative  $\frac{\partial^2}{\partial z_p^{(1)} \partial z_q^{(1)}}$  we get

$$\left(z_m^{(2)} - b_m\right) \frac{\partial^2 v_m}{\partial z_p^{(1)} \partial z_q^{(1)}} = 0 \quad (5)$$

As this is true for any arbitrary point in the rigid body we get

$$\frac{\partial^2 v_m}{\partial z_p^{(1)} \partial z_q^{(1)}} = 0 \quad (6)$$

$$\Rightarrow v_m = K_{mr} z_r + B_m \quad (7)$$

At the fixed point we have

$$K_{mr} b_r + B_m = 0 \quad (8)$$

Plugging this in (7)

$$v_m = K_{mr} (z_r - b_m) \quad (9)$$

Putting  $K_{mr} = -\omega_{mr}$  gives us indeed the asked expression.



## 5.8 p161 - Clarification

$$\mathbf{5.325.} \quad \Omega_{np} \sum (m f_n z_p) = \Omega_{np} \sum F_n z_p$$

and hence, since  $\Omega_{np}$  is arbitrary,

$$\mathbf{5.326.} \quad \sum m (f_n z_p - f_p z_n) = \sum (F_n z_p - F_p z_n)$$

To be complete the following step should be inserted

$$\Omega_{np} \sum (m f_n z_p) = \Omega_{np} \sum F_n z_p \quad (1)$$

As  $\Omega_{np}$  is skew-symmetric:

$$- \Omega_{np} \sum (m f_p z_n) = - \Omega_{np} \sum F_p z_n \quad (2)$$

$$(1)+(2) \quad \Omega_{np} \sum m (f_n z_p - f_p z_n) = \Omega_{np} \sum (F_n z_p - F_p z_n) \quad (3)$$

and hence, since  $\Omega_{np}$  is arbitrary,

$$\mathbf{5.326.} \quad \sum m (f_n z_p - f_p z_n) = \sum (F_n z_p - F_p z_n)$$



## 5.9 p161 - Clarification

$$\begin{aligned} \mathbf{5.329.} \quad h_{np} &= \sum m (\omega_{nq} z_q z_p - \omega_{pq} z_q z_n) \\ &= J_{npqr} \omega_{rq} \end{aligned}$$

where

$$\mathbf{5.330.} \quad J_{npqr} = \sum m (\delta_{nr} z_q z_p - \delta_{pr} z_n z_q)$$

$$h_{np} = \sum m (\omega_{nq} z_q z_p - \omega_{pq} z_q z_n) \tag{1}$$

$$= \sum m (\omega_{rq} \delta_{rn} z_q z_p - \omega_{rq} \delta_{rp} z_q z_n) \tag{2}$$

$$= \omega_{rq} \sum m (\delta_{rn} z_q z_p - \delta_{rp} z_q z_n) \tag{3}$$

$$= J_{npqr} \omega_{rq} \tag{4}$$



### 5.10 p181 and p182 - Clarification Figures 13., 14. and 15.

There are several ways to show the homeomorphism of the configuration space of a rigid body with fixed point.

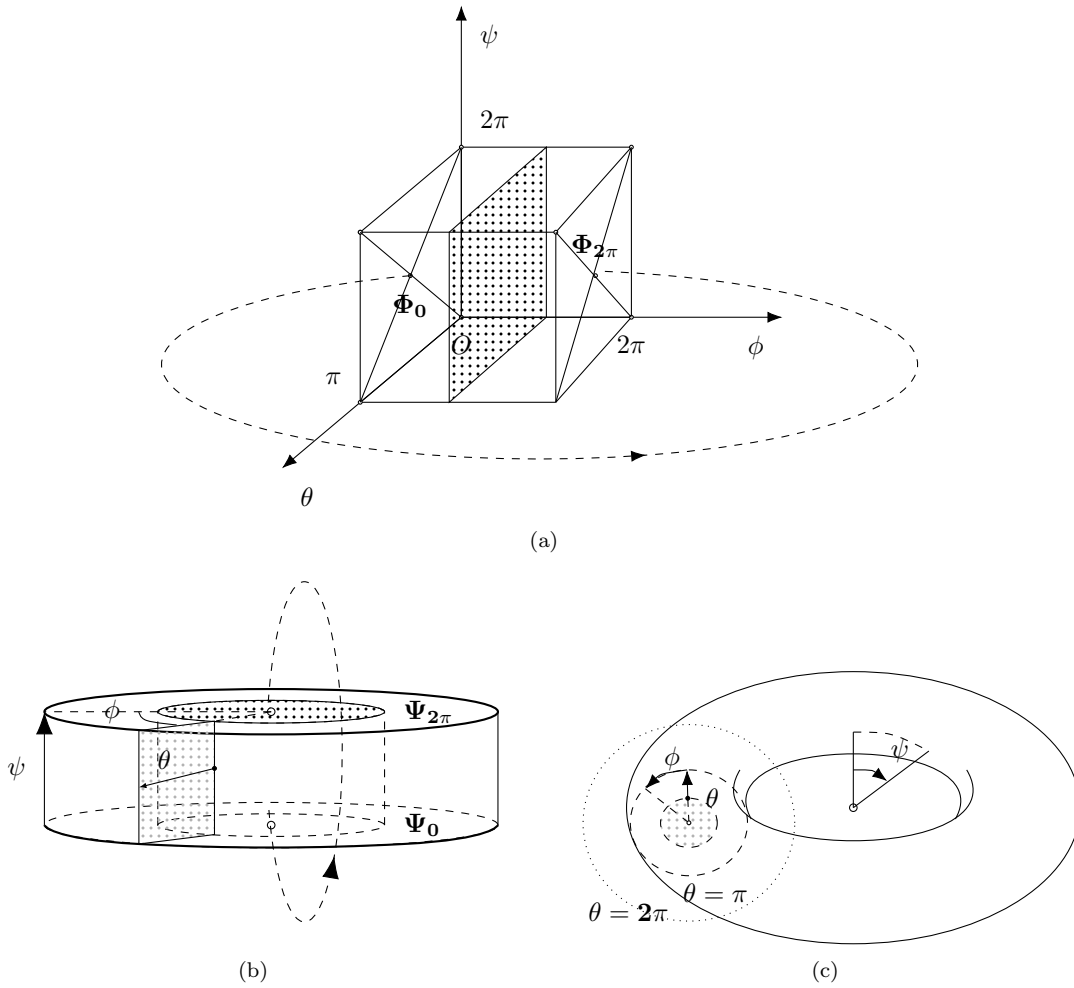


Figure 5.2: Homeomorphism of the configuration space of a rigid body with fixed point.

