

Solutions

DATE

$$X_{\text{gas}} = \frac{n_{\text{gas}}}{n_{\text{gas}} + n_{\text{H}_2\text{O}}}$$

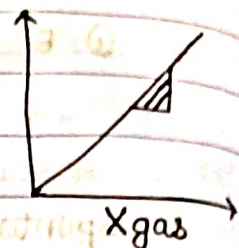
- solubility of gas in liquid : (Henry's law)

② $K_H \propto \frac{1}{\text{solubility}}$

$P \cdot P \propto \text{solubility}$

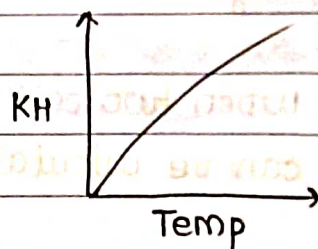
$P \cdot P \propto \text{mole fraction of gas}$

$$PP = K_H X_{\text{gas}}$$



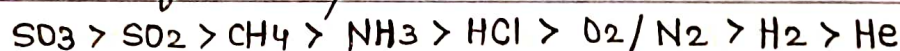
$K_H = \text{Henry's constant of gas}$ ③ slope = $K_H = \tan \theta$
Depends on nature of gas

① $K_H \propto \text{Temp}$



- Factors affecting solubility of Gas:

① Nature of gas : Order of solubility



② Nature of solvent \propto Dielectric constant \propto Polarity

③ Temp \propto 1

solubility

④ $P \cdot P = K_H \text{ solubility}$

$PP \propto \text{solubility}$

- Limitations of Henry's law :

① $P = \text{low}$ $T = \text{low}$

② Gas dissolved in liq

③ Ideal gas Behaviour

④ V.V small amount of gas soluble in liq

- solubility of liquid in liquid :

① Evaporation : liquid \rightarrow Vapour

② condensation : Vapour \rightarrow liquid

③ At equilibrium pressure exerted by vapours on the surface area of liquid when both liquid and Vapour Both are at equilibrium



Vapour pressure \rightarrow Depends only on the Temperature

• Imp points of vapour pressure :

- ① In closed vessel.
- ② $V.P \propto \text{Temp}$
- ③ Depends on Temp and nature of liquid.
- ④ Open vessel \rightarrow evaporation
closed vessel \rightarrow Both evaporation and condensation
- ⑤ $\text{Temp} \propto K.E$ ⑥ At Higher altitude
 $K.E = \frac{3}{2} nRT$ $P = \text{low}$
 $B.P (H_2O) < 100^\circ C$
- ⑦ In pressure cooker \rightarrow cooking time for food $\rightarrow B.P (H_2O) \uparrow$
Reduced
- ⑧ During eva/conden \rightarrow no. of molecules on the surface area always constant.

⑨ $B.P$ — Temp at which $V.P$ of liq = 1 atm

$$B.P \propto \frac{1}{V.P}$$

H_2O — $100^\circ C$

CH_3OCH_3 — $38^\circ C$

C_6H_6 — $65^\circ C$

C_2H_5OH — $85^\circ C$

$C_6H_5NH_2$ — $225^\circ C$

Low BP — High VP — Volatile liquid

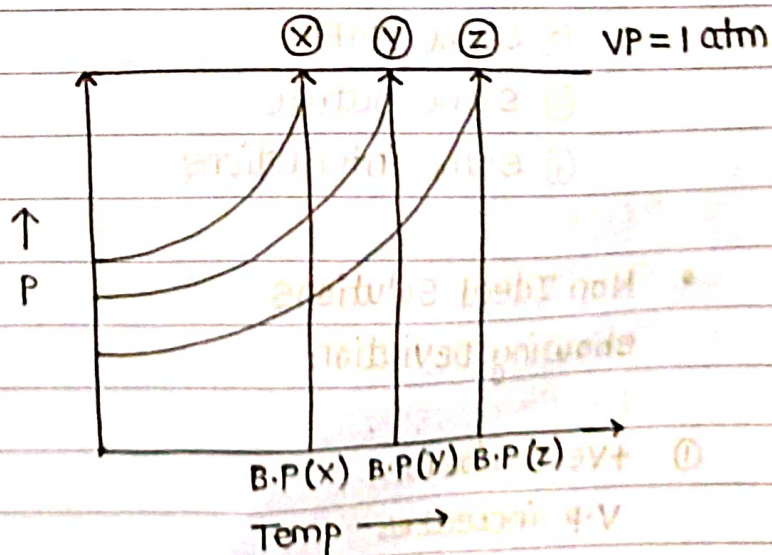
High BP — Low VP — Non-Volatile liquid

① BP order = $x < y < z$

$z > y > x$

② VP order

$z < y < x$

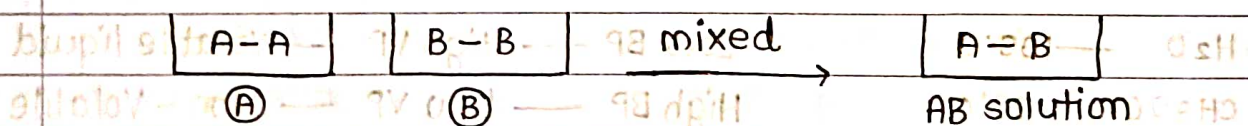


• Mixing of two volatile liquids (Raoult's Law 1)

- Vapour state
 - P_A — partial pressure of A
 - P_B — partial pressure of B
 - P_A° — V.P. of pure liquid A
 - P_B° — V.P. of pure liquid B
- Liquid state
 - $P_A = X_A P_A^\circ$ — MF of A in liquid state
 - $P_B = X_B P_B^\circ$ — MF of B in liquid state
- Dalton's law of PP
 - Y_A — MF of A in Vap. state
 - Y_B — MF of B in Vap. state
 - TP sum of the PP
 - $TP = P_A + P_B$ — Total M.F = 1
 - $TP = X_A P_A^\circ + X_B P_B^\circ$ — $X_A + X_B = 1$

• Ideal Solutions:

The solution which obeys Raoult's law exactly over entire range of concentrations is called Ideal solution



A and B liq should have

(Ideal solution)

① same FG

① $A-A = B-B = A-B$

② Same IMFA

② $P_A = X_A P_A^\circ$

③ same nature

$P_B = X_B P_B^\circ$

④ same interactions

③ $TP = P_A + P_B$

④ $\Delta V_{\text{mix}} = 0$

• Non Ideal solutions showing deviation

⑤ $\Delta H_{\text{mix}} = 0$

① +ve Deviation

② -ve Deviation

V.P. increases

V.P. decreases

① A-A and B-B strong
A-B - weak

① A-A and B-B weak
A-B - strong

② $P_A > X_A P_A^\circ$
 $P_B > X_B P_B^\circ$
 $T_P > P_A + P_B$

② $P_A < X_A P_A^\circ$
 $P_B < X_B P_B^\circ$
 $T_P < P_A + P_B$

③ $\Delta H_{mix} > 0$ — endothermic

③ $\Delta H_{mix} < 0$ — exothermic

④ $\Delta V_{mix} > 0$ — Volume increases

④ $\Delta V_{mix} < 0$ — Volume decreases

ex: $\text{CH}_3\text{COCH}_3 + \text{C}_2\text{H}_5\text{OH}$
 $\text{CH}_3\text{COCH}_3 + \text{ether}$

ex: $\text{H}_2\text{O} + \text{CH}_3\text{COOH}$
 $\text{H}_2\text{O} + \text{HCl}$

$\text{CCl}_4 + \text{CH}_3\text{OH}$

$\text{CH}_3\text{OH} + \text{CH}_3\text{COOH}$

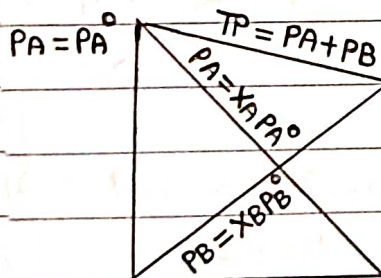
$\text{H}_2\text{O} + \text{CH}_3\text{OH}$

$\text{CHCl}_3 + \text{CH}_3\text{COCH}_3$

$\text{CH}_3\text{COCH}_3 + \text{CS}_2$

$\text{CHCl}_3 + \text{C}_6\text{H}_6$

$\text{C}_6\text{H}_5\text{NH}_2 + \text{CH}_3\text{COCH}_3$



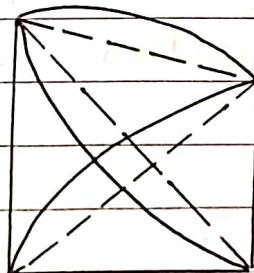
$X_A = 1$

$X_B = 1$

$X_B = 0$

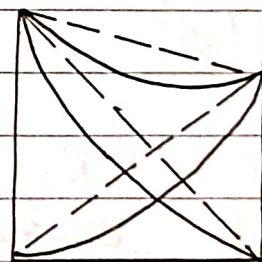
$X_A = 0$

$X_A + X_B = 1$



+ve Deviation

V.P Increases



-ve Deviation

V.P Decreases

- Azeotropic mixture: A mixture of 2 or more components can boil at same temp and can't be separated by distillation process called Azeotropic mixture

• Note:

- ① Non-Ideal solution give azeotropic mixture.
- ② After mixing V.P of both liquids inc or dec than pure liquids
- ③ After mixing BP of both liquids inc or dec than pure liquids
- ④ Means BP of Azeotropic mixture \rightarrow Greater or lesser than BP of pure liquids
- ⑤ B.P of both liquids same \rightarrow At this BP composition of both liquid phase and vapour phase are same.

• Colligative properties:

Properties depends on No. of solute particles But not nature of solute is called colligative properties.

① Relative lowering of V.P:

On addition of Non volatile solids solute, V.P of solvent decreases called lowering of vapour pressure.

a) $LVP = P^s - P^0$ (P^s = Vapour P of solution / P^0 = Vapour P of solvent)

b) $RLVP = \frac{LVP}{P^0} = \frac{P^0 - P^s}{P^0}$ (Value Increases)

c) $RLVP = X_{\text{solute}}$ — According to Raoult's law

d) $\frac{P^0 - P^s}{P^0} = \frac{n}{N}$ — Find $P^0 / P^s / LVP / RLVP$

e) $\frac{P^0 - P^s}{P^0} = \frac{wt}{m.wt} \times \frac{M.wt}{Wt}$ — Find M.wt of solute

f) $\frac{p^0 - p^s}{p^0} = m \times \frac{M \cdot wt}{1000}$ m - molality

- Elevation of BP (ΔT_b)
On addition of Non volatile solute, V.P of solvent decreases
So BP of solution increases called elevation of B.P.
 $T_{bs} > T_b^0$

① $\Delta T_b = T_b^s - T_b^0$ (T_b^s = B.P of solution / T_b^0 = B.P of pure solvent)

② $\Delta T_b = K_b m$ K_b = Ebullioscopic / molal elevation / B.P of
elevation constant
→ Elevation of Bp at conc of solⁿ 1 molal

③ $T_b^s - T_b^0 = K_b \times \frac{wt}{mwt} \times \frac{1000}{Mwt}$

- Depression of Freezing point (ΔT_f):

On addition of Non volatile solute V.P of solution decreases
So FP of solution decreases called Depression of FP.

$T_f^0 > T_f^s$

① $\Delta T_f = T_f^0 - T_f^s$ (T_f^0 = FP of solvent / T_f^s = FP of solution)

② $\Delta T_f = K_f m$ K_f — cryoscopic / F.P depression constant

③ $\Delta T_f = K_f \times \frac{wt}{mwt} \times \frac{1000}{Wg}$

- Osmotic pressure:

- Moving of solvent molecules High conc → Low conc through semi-permeable membrane called osmosis.
- The external pressure applied on the piston to stop the osmosis called osmotic pressure.

① $\pi = CST$ (C = conc. = molarity = $n \times \frac{1}{V_L} = \frac{wt}{mwt} \times \frac{1}{V_L} = \frac{wt \times 1000}{mwt \times V_{ml}}$)
 $S = R = 0.0821 = \frac{1}{12}$

② Two solutions mixed $\pi_{RS} = \pi_1 + \pi_2$
 $= C_1 S T_1 + C_2 S T_2$
 $= C_1 S T + (C_2 S T)$
 $= (C_1 + C_2) S T$

③ A and B two solutions

a. $OP(A) < OP(B)$ — A is hypotonic than B

b. $OP(A) = OP(B)$ — A is isotonic than B

c. $OP(A) > OP(B)$ — A is hypertonic than B

• A and B are isotonic solution

$$\pi_A = \pi_B$$

$$C_1 S T_1 = C_2 S T_2$$

$$T_1 = T_2$$

$$V_1 = V_2$$

$$C_1 = C_2$$

$$n_1 = n_2$$

• Formulae:

① $RLVP = i \times \text{solute}$

(i) No. of solute particles (i)

② $\Delta T_b = i \times K_b m$ (ii) Amount of solute

③ $\Delta T_f = i \times K_f m$ (iii) No. of moles of solute ($\times \text{solute}$)

④ $\pi = i \times C S T$ (iv) Conc. of solution (C)

(v) C: concentration

$$RLVP / LVP / BP / \Delta T_b / \Delta T_f / \pi = \alpha \times (i) (ii) (iii) (iv) (v) \pi$$

• According to Roults law:

① Dilute $\longrightarrow \frac{P^0 - P_s}{P^0} = \frac{wt}{mwt} \times \frac{M \cdot wt}{Wt} \longrightarrow \frac{P^0}{LVP}$

② conc $\longrightarrow \frac{P^0 - P_s}{P_s} = \frac{wt}{mwt} \times \frac{M \cdot wt}{Wt} \longrightarrow \frac{P^0}{RLVP} = \frac{P_s}{RLVP} + \frac{m \cdot wt \text{ of solute}}{Wt}$

• A and B are isotonic solution $\longrightarrow \frac{wt_1}{mwt_1} \times \frac{1000}{V_1} = \frac{wt_2}{mwt_2} \times \frac{1000}{V_2}$

• Roults law: $RLVP = X_{\text{solute}}$

$$\frac{LVP}{P^0} = X_{\text{solute}}$$

• Abnormal Mwt - VantHoff Factor (i)

$i = \text{No. of solute particles} \longrightarrow \text{For dissociation} \longrightarrow i > 1$
 $\text{For Association} \longrightarrow i < 1$

For glucose, sucrose, $\longleftarrow \text{For diss/Associ} \longrightarrow i = 1$

Fructose, Non volatile

solutes, Non electrolytic solutes

Association

① For degree of dissociation (α) = $\frac{l-1}{n-1}$ $2A \longrightarrow A_2 \quad i = 1/2$
of solute $3A \longrightarrow A_3 \quad i = 1/3$

② For degree of association (α) = $\frac{l-1}{\frac{1}{n}-1}$ $4A \longrightarrow A_4 \quad i = 1/4$
of solute

$n = \text{no. of particles asso/disso when } \alpha = 100\%$

$l = \text{no. of particles asso/disso when } \alpha = 100\% \text{ or } \alpha \neq 100\%$

- Relation b/w normal and abnormal wt:

① $i = \frac{\text{No. of particles asso/diss}}{\text{No. of particles taken}}$

② $i = \frac{\text{Normal wt}}{\text{Abnormal wt}}$ $\text{Abnormal wt} = \frac{\text{Normal weight}}{i}$

A and B are isotonic solution $\rightarrow i \cdot w \cdot M \times \text{wt} = \text{eq-eg}$

Abnormal wt - Vanthoff factor (i)

$i = \text{no. of solute particles}$
 $i > 1$ — For dissociation
 $i < 1$ — For Association
 $i = 1$ — For diss/Assoc

For glucose, sucrose, Fructose, Non volatile solutes, non electrolytic solutes

① For degree of dissociation (%) $\alpha = \frac{i-1}{n-1}$ $i = 1 + \alpha(n-1)$
 $\alpha = 100\%$ when $i = n$
 $\alpha \neq 100\%$ when $i \neq n$

$n = \text{no. of particles asso/diss}$ when $\alpha = 100\%$
 $i = \text{no. of particles asso/diss}$ when $\alpha \neq 100\%$ or $\alpha \neq 100\%$

Relation b/w normal and abnormal wt :