Independent Joint Control

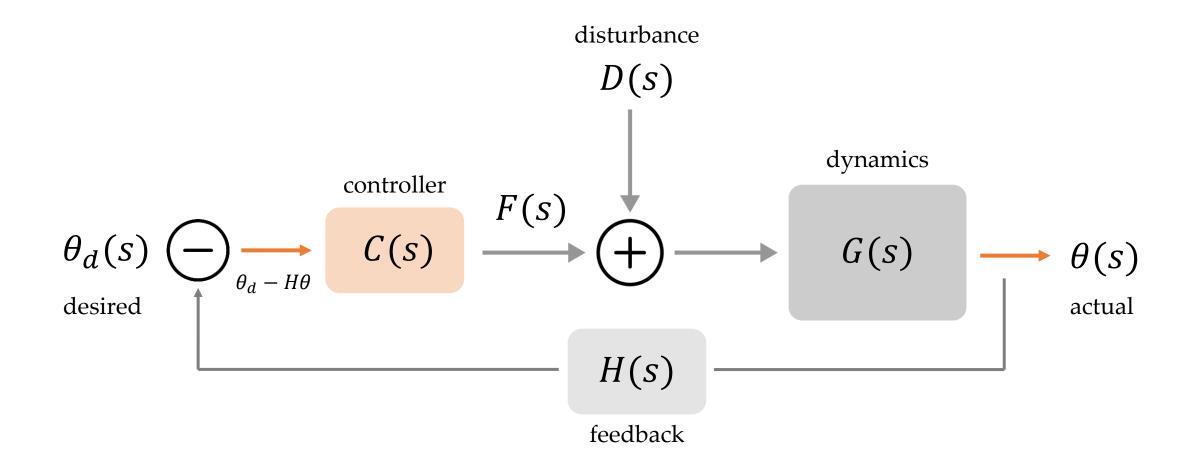
Reading: Robot Modeling and Control 6.2, 6.3, 6.4



This Lecture

- How do we choose a controller?
- How do we know if a controller is stable?
- How do we extend this to multi-DoF robot arms?

Closed-Loop Control



Closed-Loop Control

From the block diagram we obtain the input-output relationship:

$$\theta(s) = \frac{C(s)G(s)}{1 + C(s)H(s)G(s)}\theta_d(s) + \frac{G(s)}{1 + C(s)H(s)G(s)}D(s)$$

$$\frac{\theta(s)}{\theta_d(s)}$$

Closed-loop transfer function

Closed-Loop Control

When controlling an individual robot joint, common choices are:

- (P) Proportional control. $C(s) = k_p$
- (PD) Proportional-derivative control. $C(s) = k_d s + k_p$
- (PI) Proportional-integral control. $C(s) = \frac{k_i}{s} + k_p$
- (PID) Proportional-integral-derivative control. $C(s) = k_d s + k_p + \frac{k_i}{s}$



Stability

- A linear system is **stable** if all poles of characteristic equation have negative real values
- Characteristic equation: set denominator of closed-loop transfer function equal to zero

$$1 + C(s)H(s)G(s) = 0$$

Characteristic equation for the **example** block diagram.

Stability

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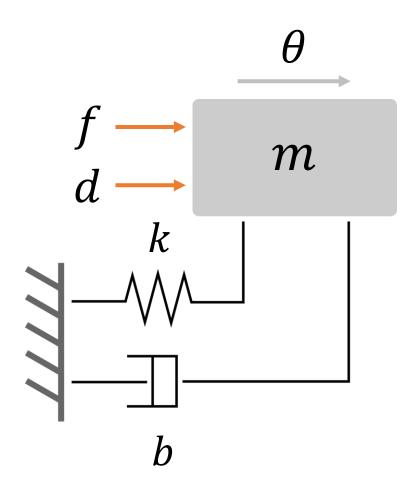
Imagine the characteristic equation is s(s - 5) = 0Then the poles are s = 0 and s = 5, and the system is not stable

Stability

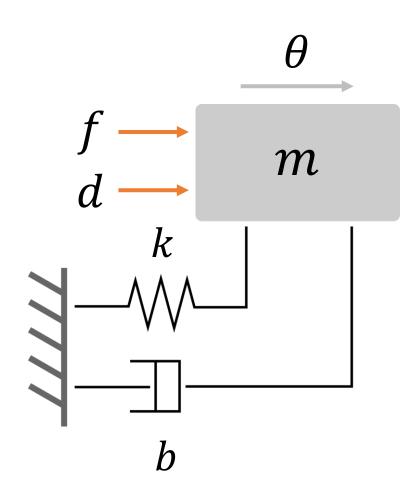
- A linear system is **stable** if all poles of characteristic equation have negative real values
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Use the **Routh–Hurwitz criterion** to find when polynomials have negative real poles:

- $s^2 + a_1 s + a_0 = 0$ is stable when $a_1 > 0$ and $a_0 > 0$
- $s^3 + a_2 s^2 + a_1 s + a_0 = 0$ is stable when $a_2 > 0$, $a_1 > 0$, $a_0 > 0$ and $a_2 a_1 > a_0$



Find the gains for a PD controller that result in stability. Assume you have a sensor that measures joint position θ .

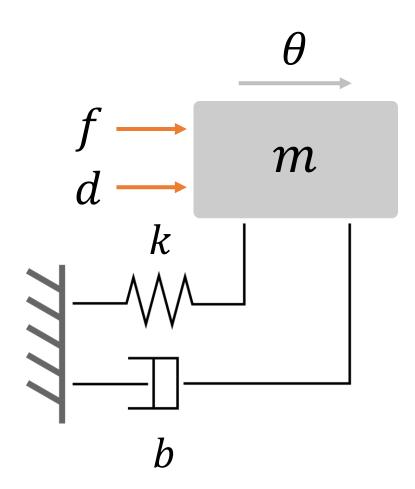


Step 1. Get dynamics G(s)

$$f + d = m\ddot{\theta} + b\dot{\theta} + k\theta$$

$$F(s) + D(s) = (ms^2 + bs + k)\theta(s)$$

$$G(s) = \frac{\theta(s)}{F(s) + G(s)} = \frac{1}{ms^2 + bs + k}$$

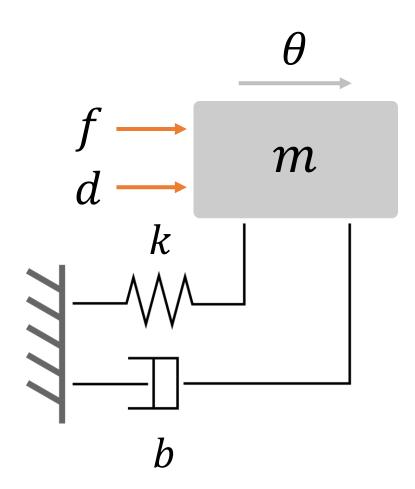


Step 2. Get closed-loop transfer function

$$\theta(s) = \frac{C(s)G(s)}{1 + C(s)H(s)G(s)}\theta_d(s)$$

We observe θ , so H(s) = 1

$$\theta(s) = \frac{C(s)G(s)}{1 + C(s)G(s)}\theta_d(s)$$

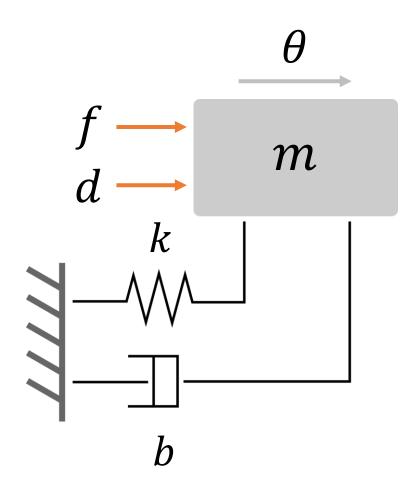


Step 3. Solve characteristic equation

$$1 + C(s)G(s) = 0$$

$$1 + \frac{k_d s + k_p}{ms^2 + bs + k} = 0$$

$$ms^2 + (b + k_d)s + (k + k_p) = 0$$

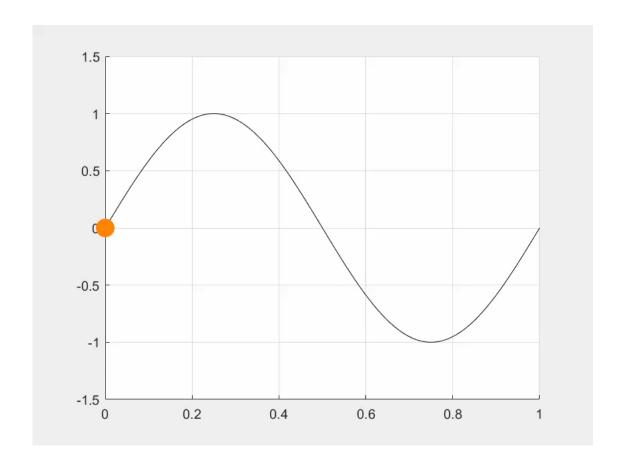


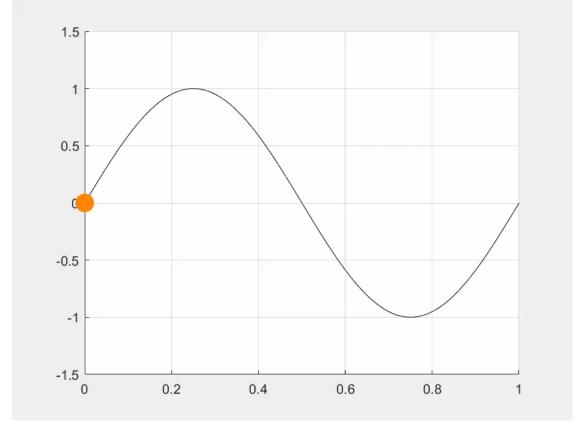
$$ms^2 + (b + k_d)s + (k + k_p) = 0$$

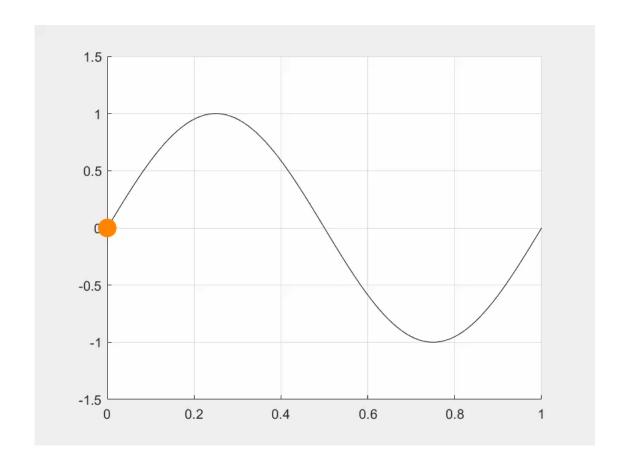
Assuming m > 0, the system is stable when:

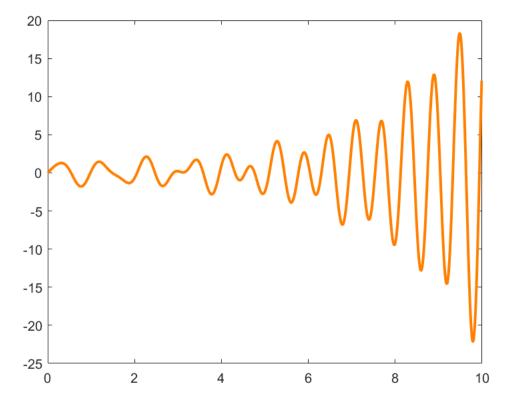
•
$$b + k_d > 0$$

•
$$k + k_p > 0$$

















Independent Joint Control

In **independent joint control** each joint is treated as a separate single-input single-output system. The interaction forces between joints are **disturbances**.

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In Practice. Design separate controllers for each 1-DoF joint so that the joint is stable and tracks the desired trajectory.

$$f_1 + d_1 = m_1 \ddot{\theta}_1 + b_1 \dot{\theta}_1$$

$$f_2 + d_2 = m_2 \ddot{\theta}_1 + k_2 (\theta_2 - \theta_1)$$

$$\vdots$$

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Next Lecture

• Multivariable control using the robot's dynamics