

Legends

① $S_{12} = \sin(\theta_1 + \theta_2)$

④ $C_{12} = \cos(\theta_1 + \theta_2)$

⑥ $S_{123} = \sin(\theta_1 + \theta_2 + \theta_3)$

⑦ $S_1 \rightarrow \sin \theta_1 ; C_1 \rightarrow \cos \theta_1$

⑧ $S_{12-3} \rightarrow \sin(\theta_1 + \theta_2 - \theta_3)$

$S_{1-23} \rightarrow \sin(\theta_1 - \theta_2 + \theta_3)$

Similar for cosines.

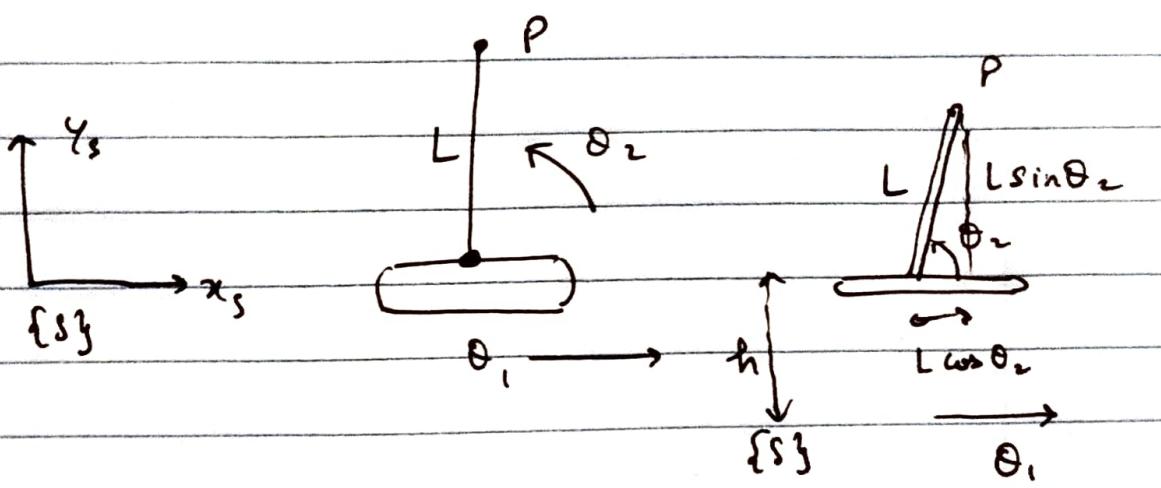
$C_{1-2} \rightarrow \cos(\theta_1 - \theta_2)$

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Robotics & Automation

HW - 4

[1.1].



We know,

$$\dot{p} = J(\theta) \dot{\theta} \quad \text{(velocity of the end-effector)}$$

Here,

$$p(t) = \begin{bmatrix} \theta_1(t) + L \cos \theta_2(t) \\ h + L \sin \theta_2(t) \end{bmatrix}$$

$$\therefore \dot{p} = \frac{d p(t)}{dt} = \begin{bmatrix} \dot{\theta}_1 - L \dot{\theta}_2 \sin \theta_2 \\ \dot{\theta}_2 \cos \theta_2 \end{bmatrix}$$

Now, we separate $\dot{\theta}_1$ and $\dot{\theta}_2$ from the above equation:

$$\dot{p} = \begin{bmatrix} 1 & -L \sin \theta_2 \\ 0 & \cos \theta_2 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} \Rightarrow J(\theta) = \begin{bmatrix} 1 & -L \sin \theta_2 \\ 0 & \cos \theta_2 \end{bmatrix}$$

1.21

We know:

$$[V_s] = \dot{T} T^{-1}$$

and $T = M e^{[S_1]\theta_1} e^{[S_2]\theta_2} e^{[S_3]\theta_3}$.

* we know the robot has 3 joints -

$$T = e^{[S_1]\theta_1} \cdot e^{[S_2]\theta_2} \cdot e^{[S_3]\theta_3} M$$

\therefore We solve for $\dot{T} \times T^{-1}$; ($\theta(t)$ is a fn. of time)

$$\begin{aligned} \dot{T} &= [S_1]\dot{\theta}_1 e^{[S_1]\theta_1} e^{[S_2]\theta_2} e^{[S_3]\theta_3} M + \\ &\quad e^{[S_1]\theta_1} [S_2]\dot{\theta}_2 e^{[S_2]\theta_2} e^{[S_3]\theta_3} M + \end{aligned}$$

$$e^{[S_1]\theta_1} e^{[S_2]\theta_2} [S_3]\dot{\theta}_3 e^{[S_3]\theta_3} M \quad \boxed{①}$$

$$T^{-1} = M^{-1} e^{-[S_3]\theta_3} e^{-[S_2]\theta_2} e^{-[S_1]\theta_1} \quad \boxed{⑪}$$

\therefore Using eq's $① \times ⑪$ -

$$[v_s] = \dot{T} T^{-1}$$

$$\Rightarrow [v_s] = [s_1] \theta_1 e^{[s_1]\theta_1} e^{[s_2]\theta_2} e^{[s_3]\theta_3} M \\ \cdot (M^{-1} e^{-[s_1]\theta_1} e^{-[s_2]\theta_2} e^{-[s_3]\theta_3})$$

$$+ e^{[s_1]\theta_1} [s_2] \dot{\theta}_2 e^{[s_2]\theta_2} e^{[s_3]\theta_3} M \cdot (M^{-1} e^{-[s_1]\theta_1} e^{-[s_3]\theta_3} e^{-[s_2]\theta_2})$$

$$+ e^{[s_1]\theta_1} e^{[s_2]\theta_2} [s_3] \dot{\theta}_3 e^{[s_3]\theta_3} M \\ \cdot (M^{-1} e^{-[s_1]\theta_1} e^{-[s_2]\theta_2} e^{-[s_3]\theta_3})$$

$$= [s_1] \dot{\theta}_1 + e^{[s_1]\theta_1} [s_2] \dot{\theta}_2 e^{-[s_1]\theta_1} + e^{[s_1]\theta_1} e^{[s_2]\theta_2} [s_3] \dot{\theta}_3 e^{-[s_1]\theta_1 - [s_2]\theta_2} e^{-[s_1]\theta_1}$$

We know:

for a transformation matrix T ;

$$T[S]T^{-1} = [\text{Ad}_T S]$$

Here;

$$\rightarrow e^{[s_n]\theta_n} = T_n; e^{-[s_n]\theta_n} = (e^{[s_n]\theta_n})^{-1} = T_n^{-1}$$

As they are some sort of transformation matrix.

Which follows the formula / simplification?

$$T[s]T^{-1} = [Ad_s s]$$

∴ Continuing simplification :-

$$\Rightarrow [V_s] = [s_1 \dot{\theta}_1 + \dot{\theta}_2 e^{[s_1 \theta_1]} [s_2] e^{-[s_1 \theta_1]} \\ + \dot{\theta}_3 \left[e^{[s_1 \theta_1 + s_2 \theta_2]} [s_3] (e^{[s_1 \theta_1 + s_2 \theta_2]})^{-1} \right]]$$

Applying the properties of adjoint operators :-

$$\therefore [V_s] = [s_1 \dot{\theta}_1 + \dot{\theta}_2 [Ad_{e^{[s_1 \theta_1]}} s_2]]$$

$$\Rightarrow [V_s] = [s_1 \dot{\theta}_1 + \dot{\theta}_2 [Ad_{e^{[s_1 \theta_1]}} e^{[s_1 \theta_1]} s_2]]$$

$$\Rightarrow V_s = s_1 \dot{\theta}_1 + Ad_{e^{[s_1 \theta_1]}} s_2 \dot{\theta}_2 + Ad_{e^{[s_1 \theta_1]}} e^{[s_1 \theta_1]} s_3 \dot{\theta}_3$$

$$\Rightarrow V_s = [s_1 + Ad_{e^{[s_1 \theta_1]}} s_2 + Ad_{e^{[s_1 \theta_1]}} e^{[s_1 \theta_1]} s_3] \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix}$$

$$\Rightarrow V_s = J_s(\theta) \dot{\theta} \quad \text{, where } J_s(\theta) \quad (\text{spatial Jacobian})$$

1.31

$$V = J(\theta)\dot{\theta}$$

Since, V is a six-dimensional vector, and robot has n joints.

The $J_s(\theta)$, matrix will have n columns, each column will be $A_{\theta} [s_i] \dot{\theta}$,

$$[1 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0] \begin{bmatrix} s_1 \\ s_2 \\ s_3 \\ s_4 \\ s_5 \\ s_6 \end{bmatrix} = [s_1]$$

The Jacobian J will be invertible if it has full rank, which means

$$\text{rank}(J) = \min(6, n).$$

Thus, it depends upon the fact if the columns of J are linearly independent or not and how many of them are.

For a square matrix ; $\det(J) = 0$

$$\text{else, } \det(JJ^T) = 0.$$

If the determinant is not equal to 0, then it's full rank and it is INVERTIBLE.

If determinant is equal to 0, then lost rank and is not INVERTIBLE.

$$M = \begin{bmatrix} 1 & 0 & 0 & 3L \\ 0 & 1 & 0 & L \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Since, all axes of $\{s\}$ align with $\{b\}$'s axes including z-axis coming out of screen.

- Joint 1 :-

Revolute joint ;

$$\therefore S_1 = \begin{bmatrix} \omega_s \\ -\omega_s \times q \end{bmatrix} \quad \omega_s \text{ is a unit vector in } +ve \text{ axis rotation direction}$$

$$\omega_s = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad q_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$S_1 = [0 \ 0 \ 1 \ 0 \ 0 \ 0]^T$$

- Joint 2 :-

$$\omega_{s_2} = [0 \ 0 \ 1]^T \quad q_2 = [L \ 0 \ 0]^T$$

$$S_2 = [0 \ 0 \ 1 \ 0 \ L \ 0]^T$$

• Joint 3 :

$$\begin{pmatrix} 0 \\ 0 \\ -1 \end{pmatrix} \times \begin{pmatrix} 2L \\ L \\ 0 \end{pmatrix} =$$

$$w_{s_3} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad q_3 = \begin{bmatrix} 2L \\ L \\ 0 \end{bmatrix}$$

$$\therefore S_3 = \begin{bmatrix} 0 \\ 0 \\ 1 \\ -2L \\ 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & L & -2L & 0 \end{bmatrix}^T$$

$$\therefore T_{sb}(\theta) = e^{[s_1]\theta_1} e^{[s_2]\theta_2} e^{[s_3]\theta_3} M$$

Using MATLAB, we find: $T_{sb}(\theta)$:

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Q2ForwardKinematics.m Q2AdjointJacobian.m +

```
1 clc; close all;
2 syms L theta1 theta2 theta3 real
3
4 %Forward Kinematics for Question 2
5 M = [1 0 0 3*L; 0 1 0 L; 0 0 1 0; 0 0 0 1];
6 S1 = [0; 0; 1; 0; 0; 0];
7 S2 = [0; 0; 1; 0; L; 0];
8 S3 = [0; 0; 1; L; -2*L; 0];
9
10 T_final = expm(bracket(S1) * theta1) * expm(bracket(S2) * theta2) * expm(bracket(S3) * theta3) * M;
11 T1 = expm(bracket(S1) * theta1);
12 T2 = expm(bracket(S2) * theta2);
13 T3 = expm(bracket(S3) * theta3);
14 T_12 = T1*T2;
15
16 function S_matrix = bracket(S)
17     S_matrix = [ 0 -S(3) S(2) S(4);
18                 S(3) 0 -S(1) S(5);
19                 -S(2) S(1) 0 S(6);
20                 0 0 0 0];
21 end
22
```

Command Window

New to MATLAB? See resources for [Getting Started](#).

```
>> disp(simplify(expand(T_final)))
[cos(theta1 + theta2 + theta3), -sin(theta1 + theta2 + theta3), 0, L*(cos(theta1 + theta2 + theta3) + 3*cos(theta1 + theta2) - sin(theta1 + theta2) - cos(theta1))]
[sin(theta1 + theta2 + theta3), cos(theta1 + theta2 + theta3), 0, L*(sin(theta1 + theta2 + theta3) + cos(theta1 + theta2) + 3*sin(theta1 + theta2) - sin(theta1))]
[ 0, 0, 1, 0]
[ 0, 0, 0, 1]
```

fxt >> |

2.2 Planar robot has 3 joints

$$\therefore J_s(\theta) = [S, Ad_e^{[s_1]\theta_1} S_2 \quad Ad_e^{[s_2]\theta_2} S_3]$$

$$V_s = J_s(\theta) \dot{\theta}$$

Using MATLAB :-

$$e^{[s_1]\theta_1} = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$e^{[s_2]\theta_2} = \begin{bmatrix} c_2 & -s_2 & 0 & L(c_2 - 1) \\ s_2 & c_2 & 0 & LS_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Now, for adjoint calculations :

$$Ad_e^{[s_1]\theta_1} = \begin{bmatrix} c_1 & -s_1 & 0 & 0 & 0 & 0 \\ s_1 & c_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & c_1 & -s_1 & 0 \\ 0 & 0 & 0 & s_1 & c_1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

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```
8
9 %VERIFICATION VALUES:
10
11 %T_expm1 = T1 = expm(bracket(S1) * theta1)
12 T_expm1 = [[cos(theta1), -sin(theta1), 0, 0]
13 [sin(theta1), cos(theta1), 0, 0]
14 [0, 0, 1, 0]
15 [0, 0, 0, 1]];
16
17 % T_expm12 = expm(bracket(S1) * theta1) * expm(bracket(S2) * theta2)
18 T_expm12 = [[cos(theta1)*cos(theta2) - sin(theta1)*sin(theta2), -cos(theta1)*sin(theta2) - cos(theta2)*sin(theta1), 0, -cos(theta1)*(L - L*cos(theta2)) - L*sin(theta1)*sin(theta2)]
19 [cos(theta1)*sin(theta2) + cos(theta2)*sin(theta1), cos(theta1)*cos(theta2) - sin(theta1)*sin(theta2), 0, L*cos(theta1)*sin(theta2) - sin(theta1)*(L - L*cos(theta2))]
20 [0, 0, 1, 0]
21 [0, 0, 0, 1]];
22
23 %Simplified version of the final Tsb(theta) forward kinematics
24 T_sb = [[cos(theta1 + theta2 + theta3), -sin(theta1 + theta2 + theta3), 0, L*(cos(theta1 + theta2 + theta3) + 3*cos(theta1 + theta2) - sin(theta1 + theta2) - cos(theta1))]
25 [sin(theta1 + theta2 + theta3), cos(theta1 + theta2 + theta3), 0, L*(sin(theta1 + theta2 + theta3) + cos(theta1 + theta2) + 3*sin(theta1 + theta2) - sin(theta1))]
26 [0, 0, 1, 0]
27 [0, 0, 0, 1]];
28 %Inverse of Tsb(theta) for calculation of Body Jacobian
29
```

Command Window

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l u, u, u, 1]

```
>> disp(simplify(expand(T_expm12)))
[cos(theta1 + theta2), -sin(theta1 + theta2), 0, L*(cos(theta1 + theta2) - cos(theta1))]
[sin(theta1 + theta2), cos(theta1 + theta2), 0, L*(sin(theta1 + theta2) - sin(theta1))]
[0, 0, 1, 0]
[0, 0, 0, 1]
```

fx >>

∴ Since, the calculations get complex for longer adjoints, using MATLAB :

⇒ $\text{Ad}_{e^{[S_1\theta]}} S_2$

$$= \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ -Ls_1 & Lc_1 & 0 & 0 \\ Lc_1 & -Ls_1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Now for $\text{Ad}_{e^{[S_1\theta]}} e^{[S_2\theta]} S_3 =$

$$\begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 3L(c_2s_1 + c_1s_2) + L(c_1c_2 - s_1s_2) - LS_1 & 0 & 0 & 0 \\ 3L(s_1s_2 - c_1c_2) + L(c_1s_2 + s_1c_2) + LC_1 & 0 & 0 & 0 \end{bmatrix}$$

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```
50
57 %Adjoint calculations for all the respective Transformation matrices
58 R1 = T_expm1(1:3, 1:3);
59 p1 = T_expm1(1:3, 4);
60 Adjoint_1 = [R1, zeros(3, 3);
61 bracket(p1)*R1, R1];
62
63
64 R12 = T_expm12(1:3, 1:3);
65 p12 = T_expm12(1:3, 4);
66 Adjoint_2 = [R12, zeros(3, 3);
67 bracket(p12)*R12, R12];
68
69 R_sb = T_sb(1:3, 1:3);
70 p_sb = T_sb(1:3, 4);
71 Adjoint_final = [R_sb, zeros(3, 3);
72 bracket(p_sb)*R_sb, R_sb];
73
74 R_inverseQ2 = inverse_Q2(1:3, 1:3);
75 p_inverseQ2 = inverse_Q2(1:3, 4);
76 Adjoint_inverseQ2 = [R_inverseQ2, zeros(3, 3);
77 bracket(p_inverseQ2)*R_inverseQ2, R_inverseQ2];
```

Command Window

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```
>> disp(simplify(expand(Adjoint_2*S3)))
0
0
1
L*(cos(theta1 + theta2) + 3*sin(theta1 + theta2) - sin(theta1))
L*(sin(theta1 + theta2) - 3*cos(theta1 + theta2) + cos(theta1))
0
```

fx

Space Jacobian $J_s(\theta)$: relates all joint
variables given stiffness

$J_s(\theta)$

=

$$\begin{matrix} & & & 0 \\ & 0 & 0 & \\ & 0 & 0 & \\ 1 & 1 & 1 & \\ 0 & -LS_1 & 3L(c_2s_1 + c_1s_2) + L(c_1c_2 - s_1s_2) - LS_1 & \\ 0 & LC_1 & 3L(s_1s_2 - c_1c_2) + L(c_1s_2 + c_2s_1) + LC_1 & \\ 0 & 0 & 0 & \end{matrix}$$

Space Jacobian $J_s(\theta)$:

$$J_s(\theta) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \\ 0 & -Ls_1 & L(3s_{12} + c_{12} - s_1) \\ 0 & +Lc_1 & L(-3c_{12} + s_{12} + c_1) \\ 0 & 0 & 0 \end{bmatrix}$$

2.31

Body Jacobian:

$$V_b = J_b(\theta) \dot{\theta}$$

$$\Rightarrow J_b(\theta) = \text{Ad}_{T_{S6}}^{-1} J_s(\theta)$$

Using MATLAB:-

$$J_b(\theta) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \\ -L(s_{23} + c_3 - 3s_3) & -L(c_3 - 3s_3) & 0 \\ L(3c_3 - c_{23} + s_3 + 1) & L(3c_3 + s_3 + 1) & L \\ 0 & 0 & 0 \end{bmatrix}$$

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```
29 inverse_Q2 = [[ cos(theta1 + theta2 + theta3), sin(theta1 + theta2 + theta3), 0, -L*(3*cos(theta3) - cos(theta2 + theta3) + sin(theta3) + 1)]
30 [-sin(theta1 + theta2 + theta3), cos(theta1 + theta2 + theta3), 0, -L*(sin(theta2 + theta3) + cos(theta3) - 3*sin(theta3))]
31 [ 0, 0, 1, 0]
32 [ 0, 0, 0, 0];
33
34 %Final Space jacobian evaluation
35 SpaceJac = [[0, 0, 0]
36 [0, 0, 0]
37 [1, 1, 1]
38 [0, -L*sin(theta1), L*(cos(theta1 + theta2) + 3*sin(theta1 + theta2) - sin(theta1))]
39 [0, L*cos(theta1), L*(sin(theta1 + theta2) - 3*cos(theta1 + theta2) + cos(theta1))]
40 [0, 0, 0]];
41
42 %Final Body jacobian evaluation
43 BodyJac = [[ 0, 0, 0]
44 [ 0, 0, 0]
45 [ 1, 1, 1]
46 [-L*(sin(theta2 + theta3) + cos(theta3) - 3*sin(theta3)), -L*(cos(theta3) - 3*sin(theta3)), 0]
47 [L*(3*cos(theta3) - cos(theta2 + theta3) + sin(theta3) + 1), L*(3*cos(theta3) + sin(theta3) + 1), L]
48 [ 0, 0, 0]];
49
50
```

Command Window

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```
>> disp(simplify(expand(Adjoint_inverseQ2*SpaceJac)))
[ 0, 0, 0]
[ 0, 0, 0]
[ 1, 1, 1]
[-L*(sin(theta2 + theta3) + cos(theta3) - 3*sin(theta3)), -L*(cos(theta3) - 3*sin(theta3)), 0]
[L*(3*cos(theta3) - cos(theta2 + theta3) + sin(theta3) + 1), L*(3*cos(theta3) + sin(theta3) + 1), L]
fx [ 0, 0, 0]
```

(2.4)

Geometric Jacobian ($J(\theta)$) :-

$$\begin{bmatrix} \omega_s \\ \dot{\rho} \end{bmatrix} = J(\theta) \dot{\theta}$$

$$\Rightarrow J(\theta) = \begin{bmatrix} R_{s6} & 0 \\ 0 & R_{s5} \end{bmatrix} J_b(\theta)$$

Here R_{s6} can be taken from $T_{sb}(\theta)$
calculated through MATLAB :-

$$R_{s6} = \begin{bmatrix} c_{123} & -s_{123} & 0 \\ s_{123} & c_{123} & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Using MATLAB, we get :-

$$J(\theta) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \\ -L(s_{123} + c_{12} + 3s_{12} - s_1) & -L(s_{123} + c_{12} + 3s_{12}) & -Ls_{123} \\ L(c_{123} + 3c_{12} - s_{12} - c_1) & L(c_{123} + 3c_{12} - s_{12}) & Lc_{123} \\ 0 & 0 & 0 \end{bmatrix}$$

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```
75 p_inverseQ2 = inverse_Q2(1:3, 4);
76 Adjoint_inverseQ2 = [R_inverseQ2, zeros(3, 3);
77     bracket(p_inverseQ2)*R_inverseQ2, R_inverseQ2];
78
79 %Rsb used for Geometric Jacobian calculation
80 R_geometric = [[cos(theta1 + theta2 + theta3), -sin(theta1 + theta2 + theta3), 0]
81     [sin(theta1 + theta2 + theta3), cos(theta1 + theta2 + theta3), 0]
82     [0, 0, 1]];
83
84 Geometric_Matrix = [R_geometric, zeros(3, 3);
85     zeros(3, 3), R_geometric];
86
87 Geometric_Jacobian = Geometric_Matrix*BodyJac;
88
89 %Px and Py from the geometric jacobian for singularity and manipulability
90 %calculations
91 J = [-L*(sin(theta1 + theta2 + theta3) + cos(theta1 + theta2) + 3*sin(theta1 + theta2) - sin(theta1)), -L*(sin(theta1 + theta2 + theta3) + cos(theta1 + theta2) + 3*sin(theta1 + theta2)), -
92     [L*(cos(theta1 + theta2 + theta3) + 3*cos(theta1 + theta2) - sin(theta1 + theta2) - cos(theta1)), L*(cos(theta1 + theta2 + theta3) + 3*cos(theta1 + theta2) - sin(theta1 + theta2)), L*
93
94 %Skew symmetric convertor
95 function w_matrix = bracket(w)
```

Command Window

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```
>> disp(simplify(expand(Geometric_Matrix*BodyJac)))
[
[                               0,
[                               0,
[                               1,
[-L*(sin(theta1 + theta2 + theta3) + cos(theta1 + theta2) + 3*sin(theta1 + theta2) - sin(theta1)), -L*(sin(theta1 + theta2 + theta3) + cos(theta1 + theta2) + 3*sin(theta1 + theta2)), -L*
[ L*(cos(theta1 + theta2 + theta3) + 3*cos(theta1 + theta2) - sin(theta1 + theta2) - cos(theta1)), L*(cos(theta1 + theta2 + theta3) + 3*cos(theta1 + theta2) - sin(theta1 + theta2)), L*
[
[                               0,
```

fx

3.11

home position: M_{home} defined

$$M = \begin{bmatrix} 1 & 0 & 0 & L_2(\theta) \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & L_1 + L_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & L_2(\theta) \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & L_1 + L_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} = (0)I$$

$$R = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

as all axes align with

horizontal about left base of phragto

each other in the same direction for both frames {s} and {b}

Now for screws S_1 :

$$w_s = [0 \ 0 \ 1]^T \quad q = [0 \ 0 \ L_1]^T$$

or $[0 \ 0 \ 0]^T$

$$\therefore S_1 = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix}$$

- for screw S_2 :

Prismatic joint so, $S_2 = \begin{bmatrix} v_s \\ 0 \end{bmatrix}$

$$v_s = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}^T$$

$$S_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

- for screw S_3 :

$$S_3 = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

- for screw S_4 :

$$\omega_s = [1 \ 0 \ 0]^T \quad q = [0 \ 0 \ L_1 + L_2]^T$$

$$S_4 = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ L_1 + L_2 \\ 0 \end{bmatrix}$$

$$\therefore T_{Sb}(\theta) = e^{[S_1]\theta_1} e^{[S_2]\theta_2} e^{[S_3]\theta_3} e^{[S_4]\theta_4} M$$

Using MATLAB and simplification, we get :-

$$T_{Sb}(\theta) = \begin{vmatrix} C_{12} & -\frac{S_{1+2-3-4}}{2} - \frac{S_{1234}}{2} & \frac{C_{1+2-3-4} - C_{1234}}{2} & T_{Sb}(1,4) \\ S_{12} & \frac{C_{1+2-3-4} + C_{1234}}{2} & \frac{S_{1+2-3-4} - S_{1234}}{2} & T_{Sb}(2,4) \\ 0 & S_{34} & C_{34} & T_{Sb}(3,4) \\ 0 & 0 & 0 & T_{Sb}(4,4) \end{vmatrix}$$

Since, values are long; ill write the last column separately :-

$$T_{Sb}(1,4) = \frac{L_1 C_{12-3}}{2} + \frac{L_2 C_{1+2-3}}{2} + L_2 C_{12} - \frac{L_1 C_{123}}{2} - \frac{L_2 C_{123}}{2}$$

$$T_{Sb}(2,4) = \frac{L_1 S_{12-3}}{2} + \frac{L_2 S_{1+2-3}}{2} + L_2 S_{12} - \frac{L_1 S_{123}}{2} - \frac{L_2 S_{123}}{2}$$

$$T_{Sb}(3,4) = C_3 (L_1 + L_2)$$

$$T_{Sb}(4,4) = 1$$

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```
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Q3AdjointJacobian.m x Q3ForwardKinematics.m x + |
```

```
23 [           0,           0, 0, 1]];
24
25 % T_expm123 = expm(bracket(S1) * theta1) * expm(bracket(S2) * theta2) * expm(bracket(S3) * theta3)
26 T_expm123 = [[cos(theta1 + theta2), -sin(theta1 + theta2)*cos(theta3), sin(theta1 + theta2)*sin(theta3), 0]
27 [sin(theta1 + theta2), cos(theta1 + theta2)*cos(theta3), -cos(theta1 + theta2)*sin(theta3), 0]
28 [           0,           sin(theta3),           cos(theta3), 0]
29 [           0,           0,           0, 1]];
30
31 %Simplified version of the final Tsb(theta) forward kinematics
32 T_sb = [[cos(theta1 + theta2), - sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)/2, cos(theta1 + theta2 - theta3 - theta4)/2 - cos(theta1 + theta2 + theta3 + theta4)/2
33 [sin(theta1 + theta2),   cos(theta1 + theta2 - theta3 - theta4)/2 + cos(theta1 + theta2 + theta3 + theta4)/2, sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)
34 [           0,           sin(theta3 + theta4),           cos(theta3 + theta4)
35 [           0,           0,
36
37 %Inverse of Tsb(theta) for calculation of Body Jacobian
38 T_sb_inverse = [
39 [           0,           cos(theta1 + theta2),           sin(theta1 + theta2),
40 [- sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)/2, cos(theta1 + theta2 - theta3 - theta4)/2 + cos(theta1 + theta2 + theta3 + theta4)/2, sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)
41 [           0,           0,
42
43 %Final Space jacobian evaluation
```

Command Window

New to MATLAB? See resources for [Getting Started](#).

```
>> Q3ForwardKinematics
>> disp(simplify(expand(T_finalQ3)))
[cos(theta1 + theta2), - sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)/2, cos(theta1 + theta2 - theta3 - theta4)/2 - cos(theta1 + theta2 + theta3 + theta4)/2
[sin(theta1 + theta2),   cos(theta1 + theta2 - theta3 - theta4)/2 + cos(theta1 + theta2 + theta3 + theta4)/2, sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)
[           0,           sin(theta3 + theta4),           cos(theta3 + theta4)
[           0,
```

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3.2

$$e^{[S_1]\theta_1} = \begin{bmatrix} C_1 & -S_1 & 0 & 0 \\ S_1 & C_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$e^{[S_1]\theta_1} e^{[S_2]\theta_2}$$

$$= \begin{bmatrix} C_{12} & -S_{12} & 0 & 0 \\ S_{12} & C_{12} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$e^{[S_1]\theta_1} e^{[S_2]\theta_2} e^{[S_3]\theta_3}$$

$$= \begin{bmatrix} C_{12} & -C_3 S_{12} & S_3 S_{12} & 0 \\ S_{12} & C_3 C_{12} & -S_3 C_{12} & 0 \\ 0 & 0 & S_3 & C_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

```
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Q3ForwardKinematics.m Q3AdjointJacobian.m + ✓

10
11 %VERIFICATION VALUES:
12
13 %T_expm1 = T1 = expm(bracket(S1) * theta1)
14 T_expm1 = [[cos(theta1), -sin(theta1), 0, 0]
15 [sin(theta1), cos(theta1), 0, 0]
16 [0, 0, 1, 0]
17 [0, 0, 0, 1]];
18
19 % T_expm12 = expm(bracket(S1) * theta1) * expm(bracket(S2) * theta2)
20 T_expm12 = [[cos(theta1 + theta2), -sin(theta1 + theta2), 0, 0]
21 [sin(theta1 + theta2), cos(theta1 + theta2), 0, 0]
22 [0, 0, 1, 0]
23 [0, 0, 0, 1]];
24
25 % T_expm123 = expm(bracket(S1) * theta1) * expm(bracket(S2) * theta2) * expm(bracket(S3) * theta3)
26 T_expm123 = [[cos(theta1 + theta2), -sin(theta1 + theta2)*cos(theta3), sin(theta1 + theta2)*sin(theta3), 0]
27 [sin(theta1 + theta2), cos(theta1 + theta2)*cos(theta3), -cos(theta1 + theta2)*sin(theta3), 0]
28 [0, sin(theta3), cos(theta3), 0]
29 [0, 0, 0, 1]];
30
31 %Simplified version of the final Tsb(theta) forward kinematics
32 T_sb = [[cos(theta1 + theta2), -sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)/2, cos(theta1 + theta2 - theta3 - theta4)/2 - cos(theta1 + theta2 + theta3
33 [sin(theta1 + theta2), cos(theta1 + theta2 - theta3 - theta4)/2 + cos(theta1 + theta2 + theta3 + theta4)/2, sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)
34 [0, sin(theta3 + theta4),
35 [0, 0, 0, 1]];


```

(Space Jacobian)

For 4-joints:

$$J_s(\theta) = \begin{bmatrix} S_1 & Ad_{e^{S_1\theta}} S_2 & Ad_{e^{S_1\theta}, e^{S_2\theta}} S_3 \\ 0 & 0 & C_{12} \\ 0 & 0 & S_{12} \\ 1 & 1 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$Ad_{e^{S_1\theta}, e^{S_2\theta}, e^{S_3\theta}} S_4$

$$= \begin{bmatrix} 0 & 0 & C_{12} & C_{12} \\ 0 & 0 & S_{12} & S_{12} \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & -C_3(L_1+L_2) S_{12} \\ 0 & 0 & 0 & C_3(L_1+L_2) C_{12} \\ 0 & 0 & 0 & S_3(L_1+L_2) S_{12} \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

3.3

Body Jacobian $J(\theta)$:

$$J_b(\theta) = \text{Ad}_{T_{sb}^{-1}} J_s(\theta)$$

$$\text{Ad}_{T_{sb}^{-1}} = \text{Ad}_{T_{sb}^Y}$$

Using MATLAB, we compute and simplify :-

$$J_b(\theta) = \begin{bmatrix} 0 & 0 & 1 & 1 \\ S_{34} & S_{34} & 0 & 0 \\ C_{34} & C_{34} & 0 & 0 \\ S_3(L_1 + L_2) & -S_3(L_1 + L_2) & 0 & 0 \\ L_2 C_{34} & L_2 C_{34} & -C_4(L_1 + L_2) & 0 \\ -L_2 S_{34} & -L_2 S_{34} & S_4(L_1 + L_2) & 0 \end{bmatrix}$$

3.4.1

Geometric Jacobian :- (a) If without joint 1 & 3

$$\begin{bmatrix} \omega_s \\ \dot{\rho} \end{bmatrix} = J(\theta) \dot{\theta}$$

$$J(\theta) = \begin{bmatrix} R_{Sb} & 0 \\ 0 & R_{Sb} \end{bmatrix} \quad J_S(\theta)$$

Here, R_{Sb} from $T_{Sb}(\theta)$:

$$R_{Sb} = \begin{bmatrix} c_{12} - s_{12-3-4} - s_{1234} & c_{12-3-4} + c_{1234} \\ s_{12} & c_{12-3-4} + c_{1234} \\ 0 & s_{34} \end{bmatrix}$$

Computing Using
MATLAB:-

0

0

1

0

0

0

C_{12}

S_{12}

C_{12}

S_{12}

0

$$\frac{(L_1 + L_2)}{2} (S_{123} - S_{12-3}) - L_2 S_{12}$$

repeat

$$+ S_{12} C_3 (L_1 + L_2)$$

$$\frac{(L_1 + L_2)}{2} (C_{12-3} - C_{123}) + L_2 C_{12}$$

repeat

$$- C_{12} C_3 (L_1 + L_2) 0$$

0

0

$$- S_3 (L_1 + L_2) 0$$

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```

40     L * cos(theta1 + theta2 - theta3 - theta4)/2 - cos(theta1 + theta2 + theta3 + theta4)/2, sin(theta1 + theta2 - theta3 - theta4) * 0,
41     [
42
43     %Final Space jacobian evaluation
44     SpaceJacQ3 = [[0, 0, cos(theta1)*cos(theta2) - sin(theta1)*sin(theta2), cos(theta1)*cos(theta2) - sin(theta1)*sin(theta2)]
45     [0, 0, cos(theta1)*sin(theta2) + cos(theta2)*sin(theta1), cos(theta1)*sin(theta2) + cos(theta2)*sin(theta1)]
46     [1, 1, 0, 0]
47     [0, 0, 0, -cos(theta3)*(cos(theta1)*sin(theta2) + cos(theta2)*sin(theta1))*(L1 + L2)]
48     [0, 0, 0, cos(theta3)*(cos(theta1)*cos(theta2) - sin(theta1)*sin(theta2))*(L1 + L2)]
49     [0, 0, 0, sin(theta3)*(L1 + L2)]];
50
51
52     %Final Body jacobian evaluation
53     BodyJacQ3 = [[0, 0, 0, 1, 1]
54     [sin(theta3 + theta4), sin(theta3 + theta4), 0, 0]
55     [cos(theta3 + theta4), cos(theta3 + theta4), 0, 0]
56     [sin(theta3)*(L1 + L2), sin(theta3)*(L1 + L2), 0, 0]
57     [L2*cos(theta3 + theta4), L2*cos(theta3 + theta4), -cos(theta4)*(L1 + L2), 0]
58     [-L2*sin(theta3 + theta4), -L2*sin(theta3 + theta4), sin(theta4)*(L1 + L2), 0]];
59
60     %Final Geometric Jacobian evaluation
61     GeometricJacQ3 = [[0, 0, cos(theta1 + theta2), cos(theta1 + theta2)]
62     [0, 0, sin(theta1 + theta2), sin(theta1 + theta2)]
63     [1, 1, 0, 0]
64     [(L1*sin(theta1 + theta2 + theta3))/2 - (L2*sin(theta1 + theta2 - theta3))/2 - L2*sin(theta1 + theta2) - (L1*sin(theta1 + theta2 - theta3))/2 + (L2*cos(theta1 + theta2 - theta3))/2 + L2*cos(theta1 + theta2) - (L1*cos(theta1 + theta2 - theta3))/2, 0]
65     [0, 0, -sin(theta3)*(L1 + L2), 0]];
66
67     %Adjoint calculations for all the respective Transformation matrices
68     R1 = T_expm1(1:3, 1:3);
69     p1 = T_expm1(1:3, 4);
70     Adjoint_1 = [R1, zeros(3, 3);
71                 bracket(p1)*R1, R1];
72
73

```

Command Window

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```

>> disp(simplify(expand(Adjoint_sb_inverse*SpaceJacQ3)))
[ 0, 0, sin(theta3 + theta4), sin(theta3 + theta4),
  cos(theta3 + theta4), cos(theta3 + theta4),
  sin(theta3)*(L1 + L2), sin(theta3)*(L1 + L2),
  L2*cos(theta3 + theta4), L2*cos(theta3 + theta4), -cos(theta4)*(L1 + L2),
  -L2*sin(theta3 + theta4), -L2*sin(theta3 + theta4), sin(theta4)*(L1 + L2))

>> disp(simplify(expand(Geometric_JacobianQ3)))
[ (L1*sin(theta1 + theta2 + theta3))/2 - (L2*sin(theta1 + theta2 - theta3))/2 + (L1*cos(theta1 + theta2 - theta3))/2 + (L2*cos(theta1 + theta2 - theta3))/2, 0]

fix >>

```

```

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Q3ForwardKinematics.m  Q3AdjointJacobian.m * + ✓

74      n1z = T_expm12(1:3, 1:3);
75      p12 = T_expm12(1:3, 4);
76      Adjoint_12 = [R12, zeros(3, 3);
77                    bracket(p12)*R12, R12;];
78
79      R123 = T_expm123(1:3, 1:3);
80      p123 = T_expm123(1:3, 4);
81      Adjoint_123 = [R123, zeros(3, 3);
82                      bracket(p123)*R123, R123;];
83
84      R_sb_inverse = T_sb_inverse(1:3, 1:3);
85      p_sb_inverse = T_sb_inverse(1:3, 4);
86      Adjoint_sb_inverse = [R_sb_inverse, zeros(3, 3);
87                            bracket(p_sb_inverse)*R_sb_inverse, R_sb_inverse;];
88
89 %Geometric Jacobian calculation
90 R_geometricQ3 = [[cos(theta1 + theta2), - sin(theta1 + theta2 - theta3 - theta4)/2 - sin(theta1 + theta2 + theta3 + theta4)
91                   [sin(theta1 + theta2),   cos(theta1 + theta2 - theta3 - theta4)/2 + cos(theta1 + theta2 + theta3 + theta4)/2, sin(theta
92                   [0, sin(theta3 + theta4), cos(theta3 + theta4)]];]
93
94 Geometric_MatrixQ3 = [R_geometricQ3, zeros(3, 3);
95                      zeros(3, 3), R_geometricQ3];
96
97 Geometric_JacobianQ3 = Geometric_MatrixQ3*BodyJacQ3;
98
99 %Skew symmetric convertor
100 function w_matrix = bracket(w)
101     w_matrix = [ 0 -w(3) w(2);
102                  w(3) 0 -w(1);
103                  -w(2) w(1) 0];
104 end
105
106
107

```

Command Window

New to MATLAB? See resources for [Getting Started](#).

```

>> disp(simplify(expand(Adjoint_sb_inverse*SpaceJacQ3)))
[ 0, 0,
[ sin(theta3 + theta4), sin(theta3 + theta4),
[ cos(theta3 + theta4), cos(theta3 + theta4),
[ sin(theta3)*(L1 + L2), sin(theta3)*(L1 + L2),
[ L2*cos(theta3 + theta4), L2*cos(theta3 + theta4), -cos
[-L2*sin(theta3 + theta4), -L2*sin(theta3 + theta4), sin

>> disp(simplify(expand(Geometric_JacobianQ3)))
[
[
[
[ (L1*sin(theta1 + theta2 + theta3))/2 - (L2*sin(theta1 +
[ (L1*cos(theta1 + theta2 - theta3))/2 + (L2*cos(theta1 +
[

fx >>

```

(4)

finding the screws for each joint :

$$S_1 = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad S_2 = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ -L_1 \\ 0 \end{bmatrix} \quad S_3 = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ L_1 - L_2 \\ 0 \end{bmatrix}$$

∴ Space Jacobian :

$$J_s(\theta) = [S_1 \quad \text{Ad}_e^{[S_1]\theta} \cdot S_2 \quad \text{Ad}_e^{[S_1\theta] \cdot e^{[S_2]\theta}} \cdot S_3]$$

⇒ Using MATLAB, we get :

$$J_s(\theta) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1 & 1 \\ 0 & L_1 S_1 & L_1 S_1 + L_2 S_{12} \\ 0 & -L C_1 & -L_1 C_1 - L_2 C_{12} \\ 0 & 0 & 0 \end{bmatrix}$$

Then we proceed to find the Geometric

Jacobian $(\dot{\theta}_1, \dot{\theta}_2, \dot{\theta}_3)$

$$J(\theta) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

$\left[\begin{array}{c} -L_1 S_1 - L_2 S_{12} - L_3 S_{123} \\ L_1 C_1 + L_2 C_2 + L_3 C_{123} \\ 0 \end{array} \right] = \left[\begin{array}{c} -L_1 S_1 - L_2 S_{12} - L_3 S_{123} \\ L_2 C_2 + L_3 C_{123} \\ 0 \end{array} \right]$

$$= \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \\ \dot{p}_x \\ \dot{p}_y \\ \dot{p}_z \end{bmatrix}$$

bottom three rows capture minimum linear velocity.

$$\left(\because \begin{bmatrix} \omega_s \\ \dot{p} \end{bmatrix} = J(\theta) \dot{\theta} \right)$$

$$\begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3 \end{bmatrix}$$

minimum at center of triangle

$$\Rightarrow \begin{bmatrix} \dot{P}_x \\ \dot{P}_y \\ \dot{P}_z \end{bmatrix} = \begin{bmatrix} (-L_1 S_1 - L_2 S_{12} - L_3 S_{123}) \dot{\theta}_1 + (-L_2 S_{12} - L_3 S_{123}) \dot{\theta}_2 + (-L_3 S_{123}) \dot{\theta}_3 \\ (L_1 C_1 + L_2 C_{12} + L_3 C_{123}) \dot{\theta}_1 + (L_2 C_{12} + L_3 C_{123}) \dot{\theta}_2 + (L_3 C_{123}) \dot{\theta}_3 \end{bmatrix}$$

Case I

Joint positions $\theta_1 = \frac{-\pi}{8}$, $\theta_2 = \frac{\pi}{4}$, $\theta_3 = \frac{\pi}{8}$

$$\Rightarrow \begin{bmatrix} \dot{P}_x \\ \dot{P}_y \\ \dot{P}_z \end{bmatrix} = \begin{bmatrix} -L_1(0.707) \dot{\theta}_1 - 1.08L_1 \dot{\theta}_2 - 0.707L_1 \dot{\theta}_3 \\ 2.55L_1 \dot{\theta}_1 + 1.63L_1 \dot{\theta}_2 + 0.707L_1 \dot{\theta}_3 \end{bmatrix}$$

Here, we want to maximize $|\dot{P}_x|$

$$\therefore \dot{P}_x = (-0.707L_1 \dot{\theta}_1 - 1.08L_1 \dot{\theta}_2 - 0.707L_1 \dot{\theta}_3)$$

Since, we want to find out which joint to ~~maximize~~ actuate to maximize $|\dot{P}_x|$.

Thus, upon actuating joint $\dot{\theta}_2 = 1 \text{ rad/s}$.

$$\Rightarrow \dot{P}_x = -1.08L_1 ; \text{ taking the absolute}$$

$$\underline{|\dot{P}_x| = 1.08L_1 \text{ for actuating joint } 2 (\dot{\theta}_2)}.$$

• Case II

$$\theta_1 = 3\pi/4 ; \theta_2 = -\pi/4 ; \theta_3 = 0$$

* We want to maximize $|\dot{p}_x|$:

$$\therefore \dot{p}_x = (-2.707 L_1 \dot{\theta}_1 - 2L_1 \dot{\theta}_2 - L_1 \dot{\theta}_3)$$

\therefore By actuating Joint 1; $\dot{\theta}_1 = 1 \text{ rad/s}$.

We get :

$$\dot{p}_x = -2.707 L_1$$

$$\Rightarrow |\dot{p}_x| = 2.707 L_1 \quad \text{by actuating Joint 1} (\dot{\theta}_1 = 1 \text{ r/s})$$

• Case III : $\dot{\theta}_1 = \dot{\theta}_2$ and $\dot{\theta}_3 = 0$

$$\theta_1 = \pi/2 ; \theta_2 = -\pi/8 ; \theta_3 = -\pi/2 .$$

And we want to maximize $|\dot{p}_y|$ this time.

Substituting the initial joint positions given above:-

$$\dot{p}_y = (1.3066 L, \dot{\theta}_1 + 1.3066 L, \dot{\theta}_2 + 0.924 L, \dot{\theta}_3)$$

∴ Thus, we can either actuate Joint 1 or 2;
i.e. either $\dot{\theta}_1 = 1 \text{ rad/s}$ or $\dot{\theta}_2 = 1 \text{ rad/s}$, both
will result in equal solutions.

$$|\dot{p}_y| = 1.3066 L, \quad (\text{for either } \dot{\theta}_1 \text{ or } \dot{\theta}_2 \text{ actuation}).$$

5.1 | We have the Geometric Jacobian for the provided robot configuration

$$J(\theta) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \\ -L(S_{123} + C_{12} + 3S_{12} - S_1) & -L(S_{123} + C_{12} + 3S_{12}) & -LS_{123} \\ L(C_{123} + 3C_{12} - S_{12} - C_1) & L(C_{123} + 3C_{12} - S_{12}) & LC_{123} \\ 0 & 0 & 0 \end{bmatrix}$$

∴ We take out the linear velocities:

$$\begin{bmatrix} \dot{P}_x \\ \dot{P}_y \end{bmatrix} = \underbrace{\begin{bmatrix} -L(S_{123} + C_{12} + 3S_{12} - S_1) & -L(S_{123} + C_{12} + 3S_{12}) & -LS_{123} \\ L(C_{123} + 3C_{12} - S_{12} - C_1) & L(C_{123} + 3C_{12} - S_{12}) & LC_{123} \end{bmatrix}}_{\text{Jacobion } J} \underbrace{\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix}}_{\text{task space}}$$

$$\Rightarrow J = \begin{bmatrix} -L(s_{123} + c_{12} + 3s_{12} - s_1) & -L(s_{123} + c_{12} + 3s_{12}) & -Ls_{123} \\ L(c_{123} + 3c_{12} - s_{12} - c_1) & L(c_{123} + 3c_{12} - s_{12}) & LC_{123} \end{bmatrix}$$

$$\det(JJ^T) = L^4(3\cos(\theta_2 + 2\theta_3) - 3\cos(2\theta_2 + \theta_3) + \sin(\theta_2 + 2\theta_3) + \sin(2\theta_2 + \theta_3) - 4\cos(2\theta_2) - 8\cos(2\theta_3) + 3\sin(2\theta_2) - 6\sin(2\theta_3) - \cos(2\theta_2 + 2\theta_3) - 3\cos(\theta_2) + 3\cos(\theta_3) + \sin(\theta_2) + \sin(\theta_3) + 16).$$

$$\Rightarrow \det JJ^T = 0$$

Solving this gives:

$$\theta_1 = 0, \quad \theta_2 = -0.3218 \text{ rad. } (-18.4349^\circ)$$

$$\theta_3 = 0.3218 \text{ rad. } (18.4349^\circ) \quad (\text{Jacobian drops Rank})$$

The joint positions for Singularity:

$$\theta_1 = 0$$

$$\theta_2 = -0.3218 \text{ radians}$$

$$\theta_3 = 0.3218 \text{ rads.}$$

for $\theta_1 = -0.245$ or 2.8966 radians

-14 degrees or 165.96 degrees

$$\theta_2 = \theta_3 = 0$$

$$\Rightarrow \begin{bmatrix} \dot{P}_x \\ \dot{P}_y \end{bmatrix} = \begin{bmatrix} 0 \\ -3.153L\dot{\theta}_1 - 4.123L\dot{\theta}_2 - 0.97L\dot{\theta}_3 \end{bmatrix}$$

In this configuration, for these specific joint values, we can only see that the robot can ~~not~~ instantaneously move in y-direction only, as \dot{p}_x is 0.

Similarly;

for $\theta_1 = -1.816$ or 1.3258 radians

-104.03 or 75.96 degrees

We get :

$$\begin{bmatrix} \dot{p}_x \\ \dot{p}_y \end{bmatrix} = \begin{bmatrix} 3.153 \\ -\cancel{0.215} \theta_1 + 4.123 \theta_2 + 0.9701 \theta_3 \\ 0 \end{bmatrix}$$

for these joint values, the robot can only instantaneously move in x-axis.

→ Rank ($J(\theta)$) < 2 for both cases.

$$\downarrow = 1$$

\therefore for $\theta = [1.3258, 0, 0]$ joint positions,

the robot can only ~~sing~~ instantaneously move in x_{up} -direction (i.e. the x -axis).

& for $\theta = [2.8966, 0, 0]$ joint positions,

the robot can only instantaneously move in y -directions (y -axis).

∴ we know,

$n = 2$, robot's task space's dimensions.

for both of those joint positions configurations,

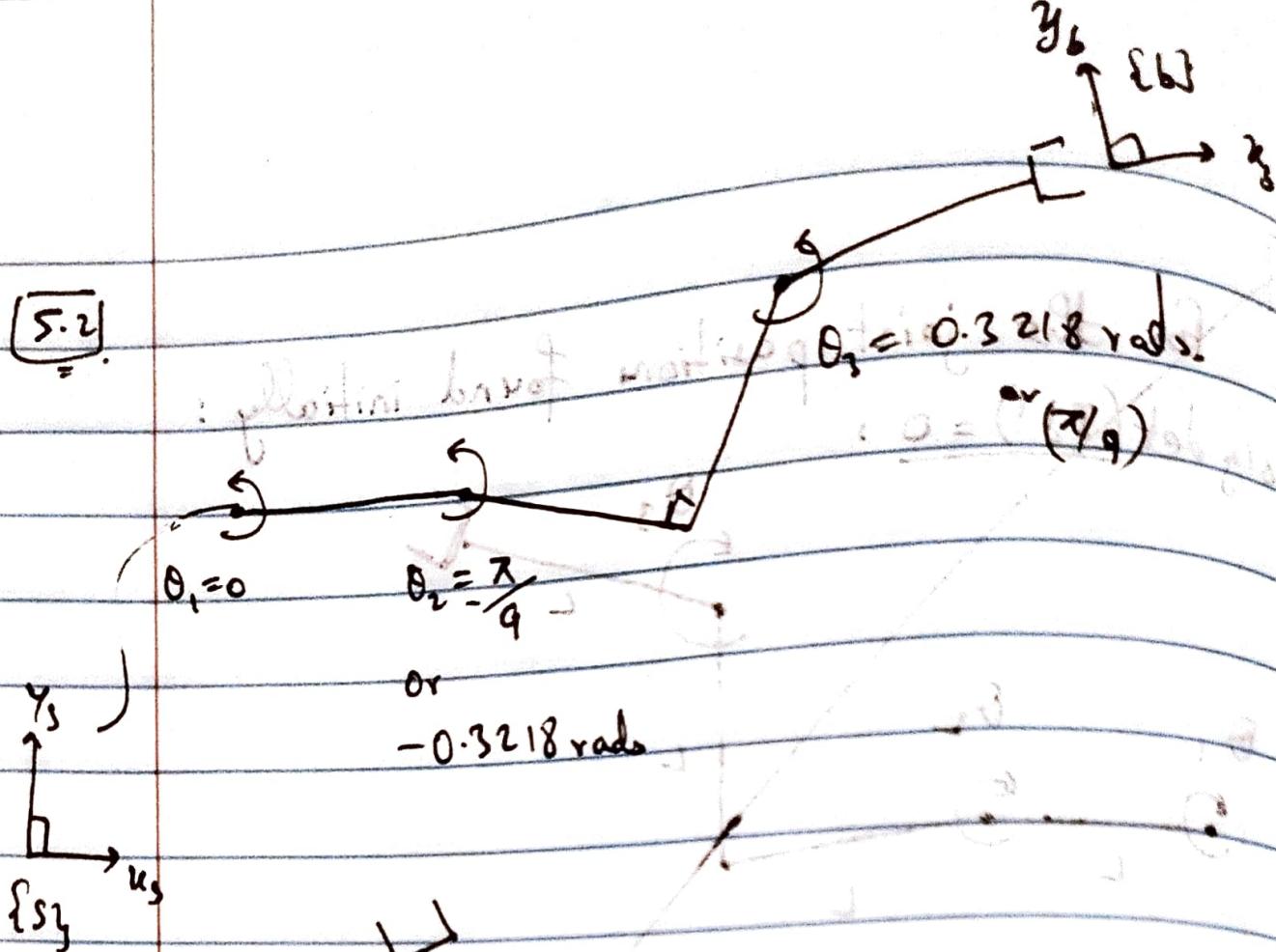
rank of $J(\theta)$ drops below n , i.e. 2, losing movement/rotation in one of the axes respectively.

- We found 2 cases of singularities above.

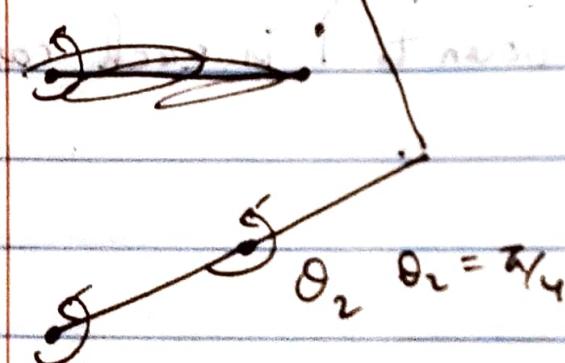
$$[\text{rank}(J(\theta)) < 2]$$

Here, $\det(JJ^T) = 0$ to further verify.

5.2.



bentham I



$$\theta_1 = \pi/4$$

$$\theta_3 = 3\pi/2$$



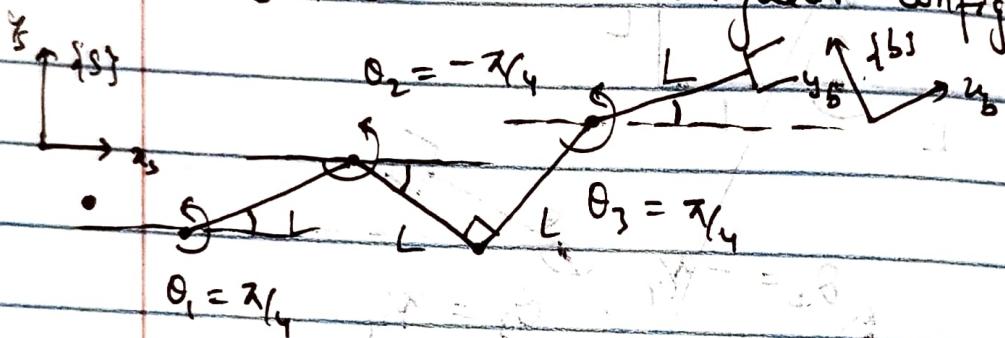
[5.3] for $\theta = [\pi/4, -\pi/4, \pi/4]$

putting in $\det J J^T = 0$.

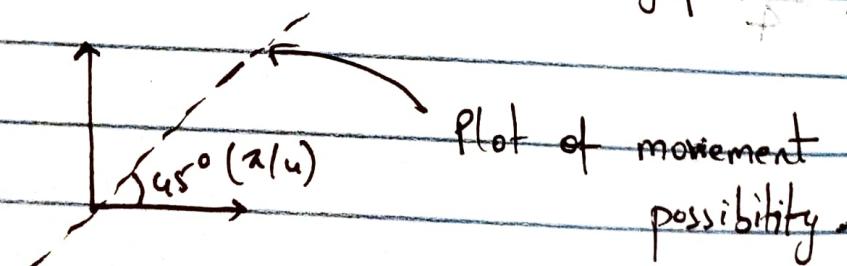
We get the result as 6

$\times 6 \neq 0$.

- Thus this is not a singular configuration.



- The robot can move in the $x-y$ plane.



- Robot cannot move out of its task space, that is along the z -axis or rotations about x/y axes.

(5.4)

We want to find a joint position
that maximizes $\sqrt{\det(JJ^T)}$.

$$\therefore J(\theta) = \begin{bmatrix} -L(S_{123} + C_{12} + 3S_{12} - S_1) & -L(S_{123} + C_{12} + 3S_{12}) & -LS_{123} \\ L(C_{123} + 3C_{12} - S_{12} - C_1) & L(C_{123} + 3C_{12} - S_{12}) & LC_{123} \end{bmatrix}$$

$\sqrt{\det(JJ^T)}$ = Long solution (thus, referring to
MATLAB :-

We maximize the robot's manipulability when

$$\rightarrow \theta = 0 \pm \frac{n\pi}{9}$$

(6)

6.11

Noting down Geometric Jac. of the configuration.

$$\begin{matrix} 0 & \dots & 0 & C_{12} & C_{12} \\ 0 & \dots & 0 & S_{12} & S_{12} \\ 1 & \dots & 0 & 0 & 0 \end{matrix}$$

$\frac{(L_1+L_2)}{2}(S_{123} - S_{12-3}) - L_2 S_{12}$ repeat $+ S_{12} C_3 (L_1+L_2) 0$

$\frac{(L_1+L_2)}{2}(C_{12-3} - C_{123}) + L_2 C_{12}$ repeat $- C_{12} C_3 (L_1+L_2) 0$

$$\begin{matrix} 0 & \dots & 0 & -S_3 (L_1+L_2) & 0 \end{matrix}$$

Here, w_x, w_y, w_z have + values thus movement occurs,
as well as $p_x \rightarrow p_y \rightarrow p_z$ if have dependent variables.

Here, $\det(JJ^T) \neq 0$.

due to the invertibility

$$\underline{\det(JJ^T) \neq 0}$$

Due to having angular velocity as well as linear velocity, the rank is unable to go below task space n.

Rank (J) doesn't go below the

task space n.

∴ Alternatively, there is not any singular ~~for~~ configuration that exists.

Rank doesn't go below n.

$$[6.2] \sqrt{\det(JJ^T)}$$

∴ Upon calculation, we get

$$\theta = 0 \pm n\pi$$

Variable manipulability due to the

Different dependent values in ω_x, ω_y

* p_1, p_2, p_3