TOS Module

Simply supported beam.

A beam is supported or resting freely on the wall or columns at its both ends.

3 Overhanging beam (single overhanging, double over. hanging) A beam in which certain span length is extended beyond the supposts on one of its side as both sides.

Single overhanging 1 Double overhanging.

4 Fixed beam The ends of the beam are signdly fixed or built in walls.

5 continuous beam. A beam supposted over more than two supposts is known as continuous beam.

The cantileves beam is supposted at free end-

Types of loadings.

(1, Point toad or concentrated load: These loads are considered to be acting at a point.

(UDL) (2) Uniformly distributed load: The load on a beam is equally distributed over a length of the beam. ie load pær unit length is goronog. Constant

Types of supports.

- · Simple suppost or knife edge suppost
- · Roller suppost
- . Hinged suppost
- . Fixed suppost
- . Smooth surface suppost

A beam rests simply on a support is known as simply supported beam.

A beam is supported on roller such support is called roller support.

If a beam is supposted on hinge or pin then such suppost is called hinged or pinned suppost.

The end of beam is fixed as built in such supposts are called fixed or built.

If a body is supposted on or in contact with a smooth surface then such supposts are called smooth surface supposts.

Types of beam.

1 Cantilever beam

One end is fixed and the other end is free

The load which is spread over a beam in such a manner that the rate of loading varies from point to point along the beam.

(Trapezoidal load).

(4) Craadually varying load on triangular load. In The load is uniformly varying along the length from zero intensity art at one end to the designated intensity at the other end.

Shearforce Is defined as the algebraic sum of all the vertical forces either to left on to right side of the section

Bending moment.

Sum of moments about that section of all external forces acting to one side of that section.

-ve.

Relation blw load, shearforce and bending moment.

1. The sate of change shear force is equal to the sate of loading.

 $\frac{dF}{d\alpha} = -\omega$

Rate of change of bending moment is equal to the shearface at the section

 $\frac{dM}{dx} = F$

Shear farce and bending moment diagram. 5H=0 EV=0 EM=0 ngcho EV=RA+RB-7-5=0 RA+RB=12-(1) MA = 5B-24.5 - 7.5 5B = 32 B = 6.4 KM.

A = 5.6 KM SFA = 6.4KH. SFC = -7 +6.4 = -0.6 KN SFD = -5 +-0.6 = -5.6 KM SFA = -5.6 +5.6 MA = MB =0 MC = 9.6KH Mb = 22.4-14 AOKN = 8-4KN GOKH · 5V=0 5H=0 5T/=0. HOKH AB SV=RA+RB-40-60 -0 . RA+ RB = 100 - (1). SM =0. = 10B-320 - 180 . 10B=500 B=50KNA = 50KN BM max B SFB = 50KN. MA = MB = 0 , SFC = 50-40=10 IXC = 100KNM 3FD=10. MD=200-80=120KNh 5FA=10-60 2-50 maximum bending moment at points EV=50-10x=0. oc = 50/10 = 5 m BME = 50 x 2.5 = 125 KNM

Point of contraflexure is a point where there is zero stending moment, at that point the direction of bending changes its sign from positive to negative or from negative to positive.

BM-Constit

Ture bending or simple bending

If a length of beam is subjected to a constant BM and no shear force Then the stresses will be setup in that length 5 of beam due to BM only and that length of the beam is said to be in pure bending or simple bending.

A beam or a part of it is said to be in a state of pure bending Simple bending when it bends under the action of uniform or constant bending moment without any shear force.

Assumptions used for the analysis of the beam under pure bending

-> The material of the beam is homogeneous

and isotropic.

-> Each layer of beam is free to expand

as contract

-> Young's modulus is considered as same far the compression and tension.

- The addius of curvature of the beam is comparatively higher than the width or the depth of the beam.

> The beam is loaded within the elastic 300

- The plane section remains plane after to

défarmation also.

Rending M = E Rending T = R Plescural Equation.

y=d/2 (distance.

I = moment of inestia

6 = stress

M = Bending moment.

E = Modulus of elasticity 1

&= Radius of curvature. from neutral layer.

Nature of bending stress

Due to bending of the beam its upper layer are compressed and the lower layer are stretched There fare longitudinal compressive stress are induced in the upper layer and longitudinal tensile stress are induced in the lower layer. These stresses are bending stress.

Neutral Surface)
Neutral layer - In a beam as cantileves there i one layer which retain its oxiginal length even after bending. So in this layer nether tensile stress nor compressive stress is setup, this layer is calle netral layer.

Neutral axis - 7 Is the line of intersection of the neutral layer with any normal section of the beam no bending stress is setup in neutral axis

Bending stress

The resistance against bonding offered by enternal stress induced when a bending moment tries to bend a beam is bending stress.

. Dending stress increases as the distance from the centroid increases.

> zero at the neutral axis

> maximum at the extreme fibres

Lension

maximum compresseive stress In 6 max = My y cmax

streen = F

F=stress xA

maximum lénsile stress = My max.

Moment of Resistance

Due to pure bending compressieve stress are deve-loped on the fibres above neutral ascis and tensile stress are developed on fibres below neta nentral assis

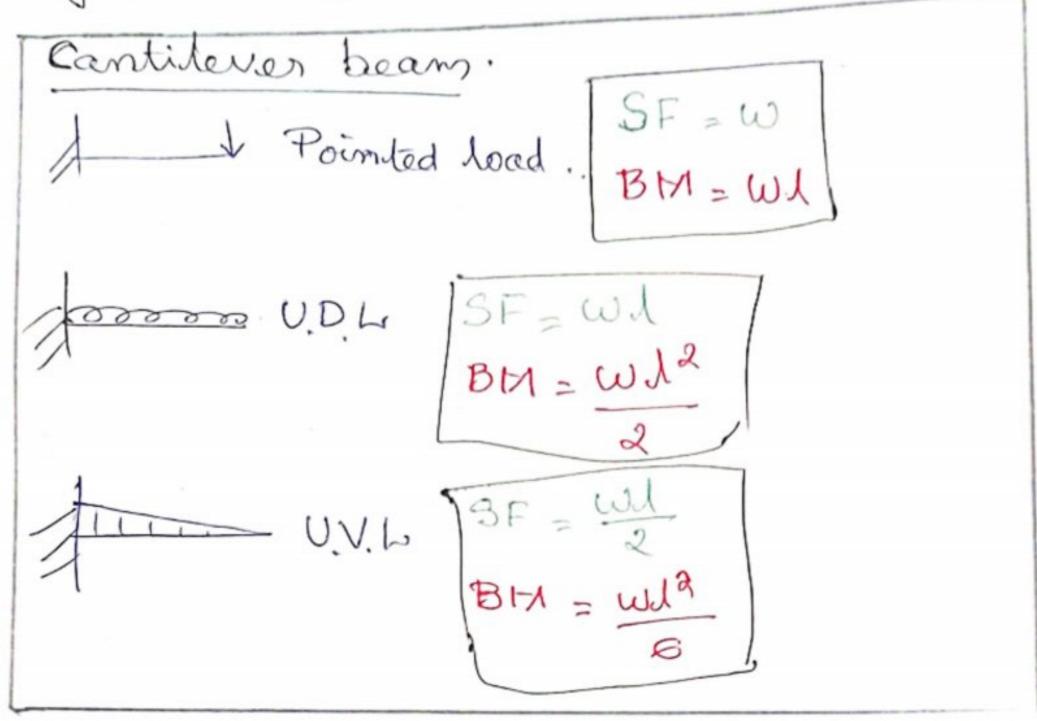
The stress causes forces on fibres.

· Total moment of these faces about the neutral epi assis is known as moment of resistance

(H 2)

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Moment of resistance is the resistance effered by the against the applied moment.



Simply supported beam

Pointed load $SF = \frac{\omega}{2}$ BM = $\frac{\omega l^2}{8}$ U.D.L. $SF = \frac{\omega l}{2}$ U.V.L. $SF = \frac{\omega l}{6}$ BM = 0.064 ωl^2 .

Shear stress T=F

= F = applied force

A = Cross sectional area

7 - Shear stress in pascal or 1 m2

Shear stress is the amount amount of force per curit area perpendicular to the axial of the member. Bending stress, also called flexural stress is parallel to the axial of the member.

Thear stress is perpendicular to the axial of the member

where F = shear force

Ay = moment of area

I = moment of inertia

b = width of the section.

The satio of maximum and average shear stress on a sectangular section is 3/2 or 1.5

ciscular section is 4/3 0x 1.33

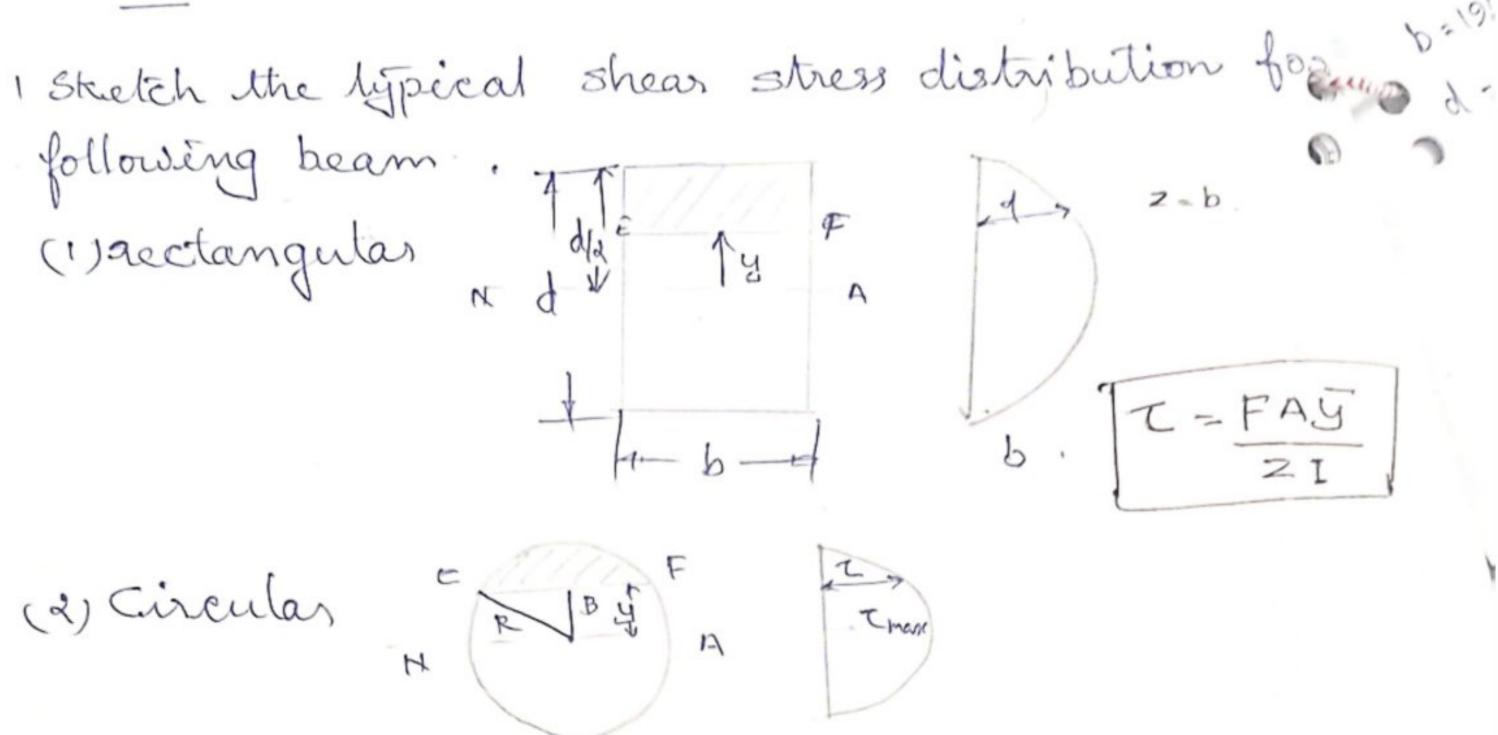
Algebraic sum of all vertical forces to left or right of the section is called.

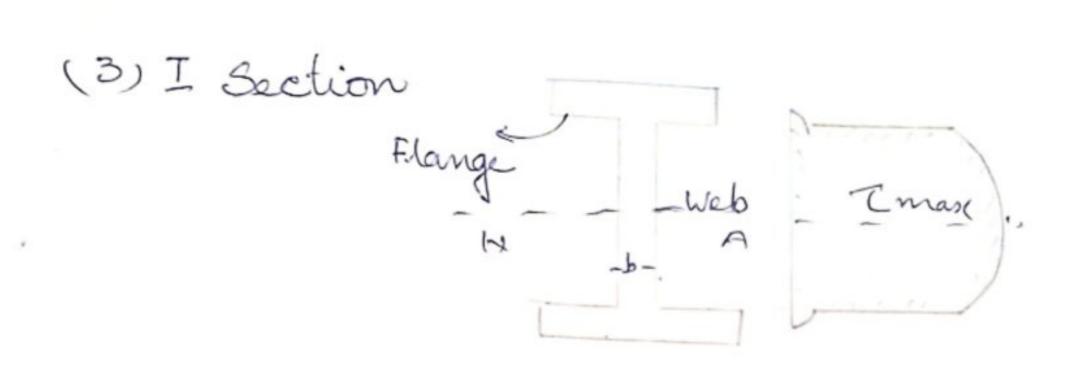
Shear force.

- 2 At point of contra flexure value of bending moment is zero.
- 3 In a rectangular homogeneous section the ratio of maximum shear stress to average shear stress.

3/2 09 1.5

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2 Write down the assumptions in theory of simple bending → The material of the beam is homogeneous and

isotropic

The value of young's modulus of elasticity is

same in lension and compression

- The transverse sections which were plane before bending, remain plane after bending also. -> beam is initially straight and all longi-

tudinal filaments bend 1/2 each into circular

are with a common centre of curvature.

ared to the demensions of cross sections.

Cinter of the Control of the Control

b=1903mm.

d - 26 - 3806mm

Derive the bending equation

consider a beam part subjected to simple bending



. MN = RO

, MF

AI M'

$$= \frac{(R+Y)Q - RQ}{RQ}$$

$$= \frac{RQ + YQ - RQ}{RQ}$$

Resistive moment developed by strip

= R.F. X dislavier.

= EydA xy => EydA.

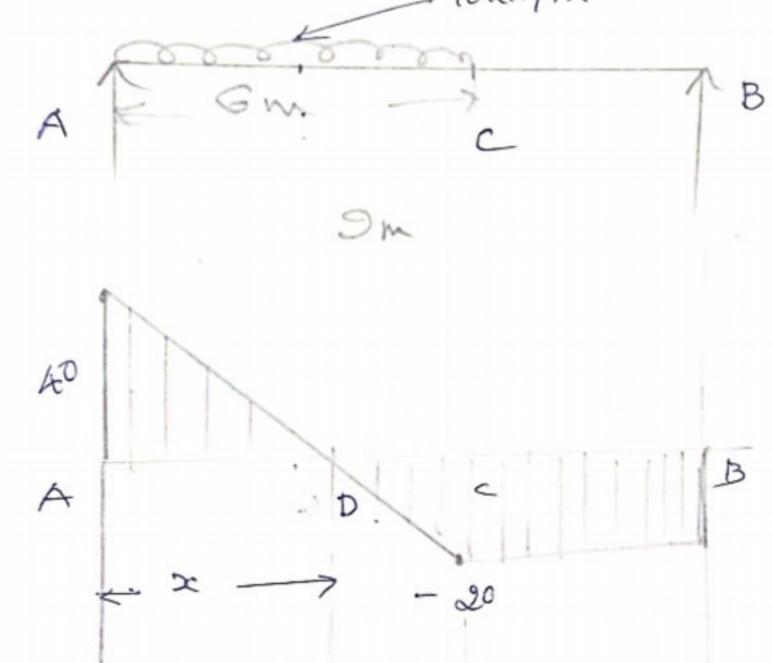
$$= \frac{XQ}{RQ}$$

$$M = \frac{E}{R} T \rightarrow \frac{M}{T} = \frac{E}{R}$$

expand on contract independently of the layer above on below it.

of length 9m and carrying a uniformly distribuled load of 10km/m for a distance of 6m from the left end. Also calculate the maximum Bix

on the section.



maramum BH = 80 KNm

$$\leq M = 0$$
.
 $M_{A} = 9B - (60 \times 3) = 0$.
 $9B = 180 - B = 20 - C$
 $A = 40KN B = 20KN$.

$$SF_{A} = +40 \text{KN} \cdot SF_{b} =$$

$$SF_{C} = -60 + 40 = -20$$

$$SF_{B} = -20 + 20 = 0$$

conseides AC. max BM at D.
Where SF = 0. 40+(IOXX) = 0

$$BM_D = (20x5) - (20x1)$$
. $DC = 4m$
= 100 - 20

RA timber beam of rectangular section supports of of AOKN uniformly distributed over a span of 3. On. the depth of the beam section is Twice the width o, maximum bending stress is not exceed 7 H/mm2 find the dimension of the beam section.

load w = 40KN -> 40×103 N.

length 1 = 3.6m -> 3.6 × 103 mm

depth d = 2b.

of bending stress. Fmare = 7 N/mm?

BM for UDL (Simply supported beam).

$$\frac{\omega 1^{2}}{8} = \frac{40 \times 10^{3} \text{N} \times (3.6 \times 10^{3})^{2}}{7}$$

$$=6.48 \times 10^{10} \text{Nmm}$$

$$= \frac{8b^{4}}{12} - \frac{6.48 \times 10^{10}}{8b^{4}} - \frac{7}{2b}$$

$$\frac{6.48\times10^{10}}{7} = \frac{8b^{4}}{146} \times \frac{1}{2b} = \frac{\frac{4}{8}b^{4}}{5\times 2b} = \frac{\frac{4}{8}b^{4}}{5\times 2b} = \frac{\frac{4}{8}b^{4}}{3}$$

9257142857 .

 $92\times10^{8} = \frac{4b^{3}}{3} - 34b^{3} = 2.76 \times 10^{10}$. $b^{3} = 69 \times 10^{8} - 3b = 1903 \text{ mm}$.

rear stress in beam.

Incase of bending of beams is the beam. Subjected to constant bending moment only and no Shear force and hence no shear stress.

But in actual practice when the beam is loads it is subjected to a bending moment, which varies from section to section and hence is subjected to shearfare which also varies from section to section.

· Due to these shear-forces, the beam is subjected to transverse shear stress, which produce complimentary horizondal shear stress. These shear stresses act on longitudinal dayers of the beam. Effect of shear stresses is negligible as compared to the bending stresses.

Shear stress equation $T = \frac{8M}{8x} = S$. The stress equation where $\frac{8M}{8x} = S$.

T= shear stress on a layer Y distance from N-A.

N/mm?

S= Shear force at the section (N).

A= Area. So, section above Y' distance from N-A (mm?)

7 = Distance of C.a. Obarea A from N-A. (mm)

A7 = Moment of area 'A' about N-A. (mm3)

b - width of section & distance from N-A (mm)

- moment of inertia the whole section

small excitent of survey and delained assign win contour interval should be small (for important work · 1 1 mines entous interval

moment of mertia is the property to oppose

I = mst (m = mars of the object

st = the distance from the asig
ef rotation