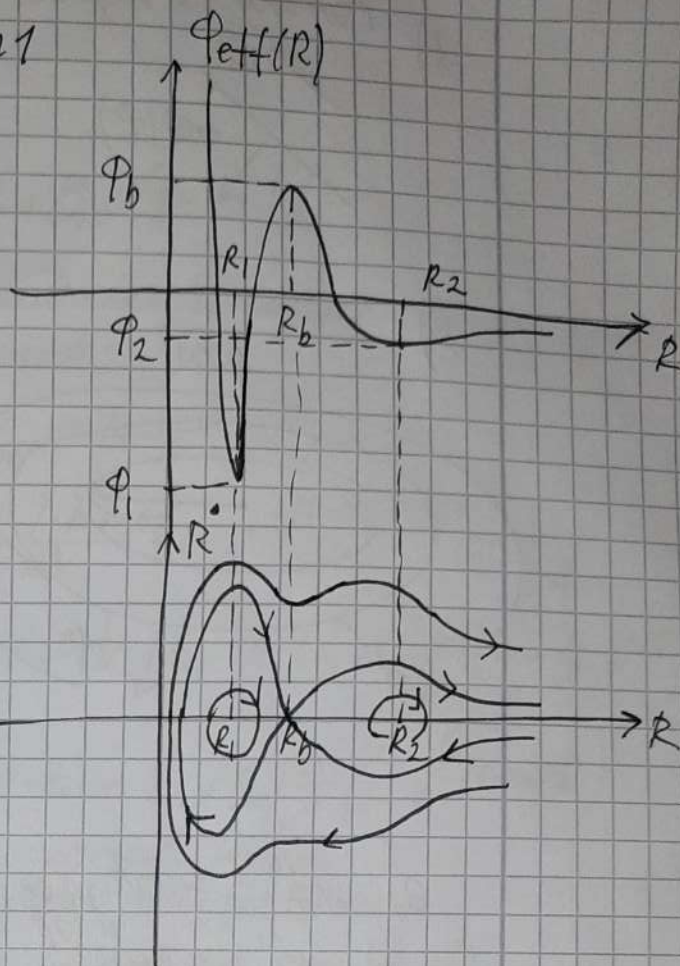
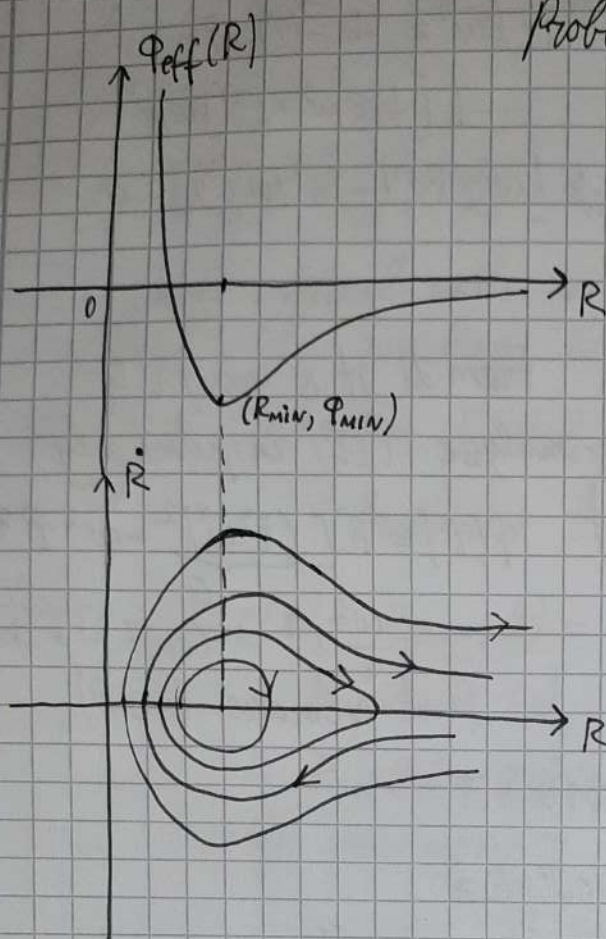


# Problem 1



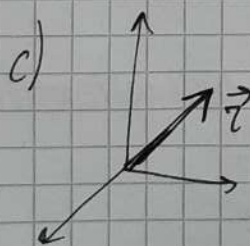
# Problem 2

a)  $\vec{F}(\vec{r}) = \vec{\omega} \times (\vec{\omega} \times \vec{r}) = \vec{\omega}(\vec{\omega} \cdot \vec{r}) - \vec{r}(\vec{\omega} \cdot \vec{\omega}) = f(\vec{r})\vec{\omega} + c\vec{r}$ ,  $\begin{cases} f(\vec{r}) = \vec{\omega} \cdot \vec{r} \\ c = -\omega^2 \end{cases}$

b)  $\forall i \neq j \quad \frac{\partial F_i}{\partial r_j} = \frac{\partial F_j}{\partial r_i} : \frac{\partial}{\partial r_j} \left[ \left( \sum_k \omega_k r_k \right) \omega_i - \omega^2 r_i \right] = \omega_i \omega_j$

$\frac{\partial}{\partial r_i} \left[ \left( \sum_k \omega_k r_k \right) \omega_j - \omega^2 r_j \right] = \omega_i \omega_j$

(in other words  $\exists \Phi(\vec{r}) \quad \frac{\partial \Phi}{\partial r_i \partial r_j} = \frac{\partial^2 \Phi}{\partial r_j \partial r_i}$ , or  $\nabla \times \vec{F} = \vec{0}$ )



c)  $\vec{q} = s\vec{r}, s \in [0, 1], \frac{d\vec{q}}{ds} = \vec{r}$

$W = \int_{\vec{q}_i}^{\vec{q}_f} \vec{F}(\vec{q}) d\vec{q} = \int_{s=0}^1 (\vec{\omega}(\vec{\omega} \cdot s\vec{r}) - s\vec{r}(\vec{\omega} \cdot \vec{\omega})) \vec{r} ds = \int_0^1 s [(\vec{\omega} \cdot \vec{r})^2 - \omega^2 \vec{r}^2] \vec{r} ds$

guess  $\Phi(\vec{r}) = -\frac{1}{2} [(\vec{\omega} \cdot \vec{r})^2 - \omega^2 \vec{r}^2]$ ,  $\frac{d}{ds} \Big|_{s=0}^1 = \frac{A}{2} \Big|_0^1 = \frac{A}{2} = \Phi(\vec{0}) - \Phi(\vec{r})$ ,  $\downarrow$  set 0

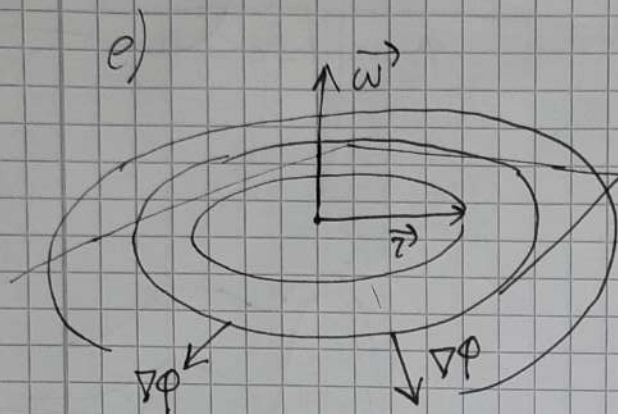
This trick assumed straight line path  $\vec{q}$  for given  $\vec{r}$ , but this indeed is potential;

$-\nabla \Phi(\vec{r}) = \frac{1}{2} \left[ 2(\vec{\omega} \cdot \vec{r}) \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} - \omega^2 2\vec{r} \right] = (\vec{\omega} \cdot \vec{r})\vec{\omega} - \omega^2 \vec{r} = \vec{F}(\vec{r})$



d) Probably a simpler way is to check  $\nabla\Phi$ :

$$\begin{aligned}\nabla\Phi(\vec{r}) \cdot k\vec{\omega} &= -k \vec{F}(\vec{r}) \cdot \vec{\omega} = \\ &= -k [f(\vec{r})\vec{\omega} + c\vec{r}] \cdot \vec{\omega} = \\ &= -k [\omega^2(\vec{r} \cdot \vec{\omega}) - \omega^2(\vec{r} \cdot \vec{\omega})] = 0.\end{aligned}$$



From d) it is enough to analyze  $\Phi(\vec{r})$  in plane only

$$\begin{aligned}\Phi(\vec{r}) &= k \left[ \underbrace{(\vec{r} \cdot \vec{\omega})^2}_0 - \omega^2 \vec{r}^2 \right] = \\ &= \frac{\omega^2}{2} \vec{r}^2 = \text{Const} \rightarrow \text{circles.} \\ &\text{(and cylinders in 3-D)}\end{aligned}$$

### Problem 3

a)  $m\ddot{z} = \frac{4}{3}\pi R^3 g (\rho_f - \rho) - 6\pi\eta R \dot{z}$

(\*)  $m\ddot{z} + 6\pi\eta R (\dot{z} - \dot{z}_\infty) = 0$  when  $\ddot{z} = 0, \dot{z} = \dot{z}_\infty = \frac{2R^2 g (\rho_f - \rho)}{9\eta}$  — terminal velocity

$$\ddot{z}(t) + \underbrace{\frac{6\pi\eta R}{m}}_{c^{-1}} \dot{z} = \underbrace{\frac{6\pi\eta R}{m}}_I \dot{z}_\infty$$

$c^{-1}$   $(c_0=0)$   $I$

b) From (\*) Consider <sup>relative</sup> reference velocity inside moving frame

$$\dot{z}_{\text{rel}}(t) = \dot{z}(t) - \dot{z}_\infty, \quad \ddot{z}_{\text{rel}}(t) = \ddot{z}(t)$$

$$\ddot{z}_{\text{rel}}(t) + \underbrace{\frac{6\pi\eta R}{m}}_{c^{-1}} \dot{z}_{\text{rel}}(t) = 0$$

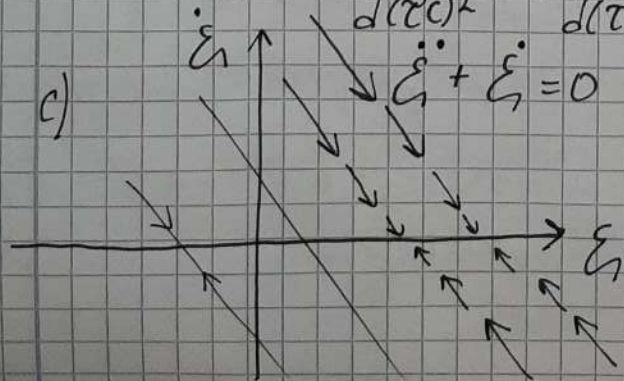
Non-dimensionalization:

$$\tau = \frac{t - t_0}{c}$$

$$\xi = \frac{z_{\text{rel}}}{R} \quad \left| \cdot \frac{c^2}{R} \right.$$

Now  $\frac{d^2(\xi R)}{d(\tau c)^2} + c^{-1} \frac{d(\xi R)}{d(\tau c)} = 0$

c)



w.r.t. moving frame

$$\ddot{\xi} = -\dot{\xi}$$

Traj. are straight lines reaching fixed position in the moving frame.



$$*d) \quad \dot{\epsilon} = -\epsilon \quad (\tau_0 = 0)$$

$$\dot{\epsilon} = -\epsilon$$

$$\epsilon = \epsilon_0 e^{-\tau}, \quad \epsilon_1(\tau) = \epsilon_1(\tau_0) + \epsilon_0 (1 - e^{-\tau})$$

\*e) To restore original units and coordinates I rewrite the res. equation & multiply - working backwards:

$$Z_{rel}(t) = \epsilon_1(\tau) \cdot R = \epsilon_1(0) \cdot R + \epsilon_0 \cdot R (1 - e^{-\frac{t-t_0}{C}}) = \\ = Z_{rel}(t_0) + \frac{\dot{Z}_{rel}(t_0) \cdot R m}{6\pi\eta R^2} (1 - e^{-(t-t_0) \frac{6\pi\eta R}{m}})$$

$$Z(t) = Z_{rel}(t) + \underbrace{\frac{Z_{frame}(t)}{\dot{Z}_{\infty}(t-t_0)}}_{\dot{Z}_{\infty}(t-t_0)} = Z_{rel}(t_0) + \dot{Z}_{\infty}(t-t_0) + \frac{\dot{Z}_{rel}(t_0)}{6\pi\eta R/m} (1 - e^{-(t-t_0) \frac{6\pi\eta R}{m}}) \\ = Z_{rel}(t_0) + \dot{Z}_{rel}(t_0) \cdot (t-t_0) + \dot{Z}_{rel}(t_0) \frac{m}{\mu} (1 - e^{-(t-t_0) \frac{\mu}{m}})$$

Exactly same equation,  $m$  represents inertia,  $\mu$  represents speed decay.

Problem 4 - population (COVID!!!), "physics"

susceptible	$\frac{d}{dt} S(t) = -\gamma S(t) I(t) + \beta R(t)$	$\gamma$ - infection rate
infected	$\frac{d}{dt} I(t) = \gamma S(t) I(t) - \rho I(t)$	$\rho$ - recovery rate
recovered	$\frac{d}{dt} R(t) = \rho I(t) - \beta R(t)$	$\beta$ - losing immunity

$$a) \quad \frac{d}{dt} (S + I + R) = -\gamma SI - \gamma SI + \beta R + \gamma SI + \gamma SI - \rho I + \rho I - \beta R = 0$$

$$b) \quad R(t) = 1 - [S(t) + I(t)], \quad \tau = \gamma t$$

$$\dot{S} = -\gamma SI + \beta(1 - S - I)$$

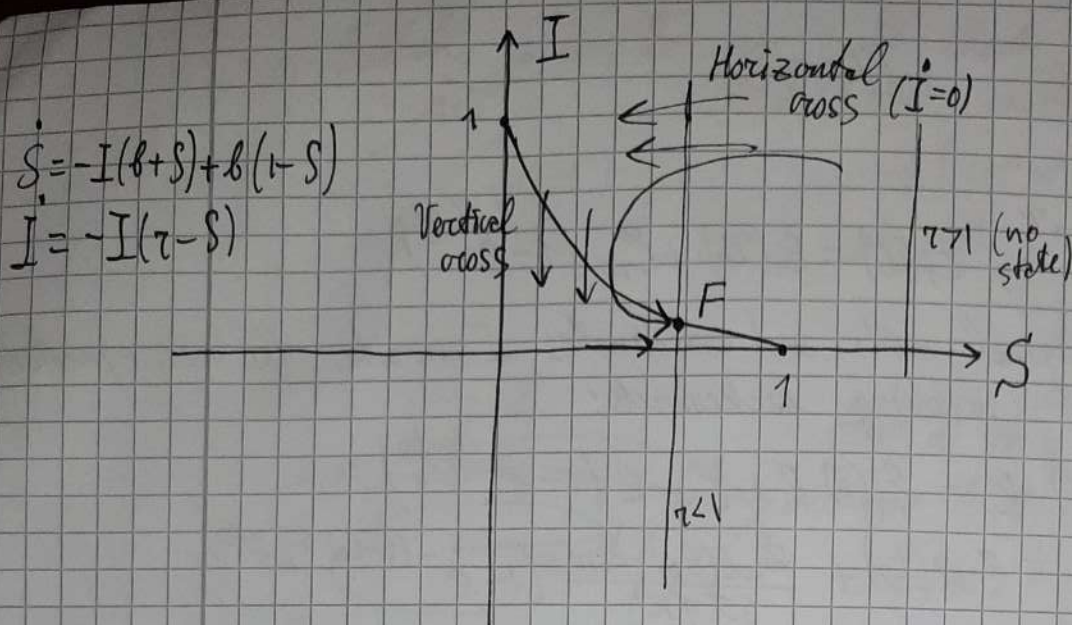
$$\frac{dS}{d\tau} = -SI + \frac{\beta}{\gamma}(1 - S - I) = -I(\tau) \cdot (\frac{\beta}{\gamma} + S(\tau)) + \frac{\beta}{\gamma}(1 - S(\tau))$$

$$\frac{dI}{d\tau} = S(\tau)I(\tau) - \frac{\rho}{\gamma}I(\tau) = -I(\tau) \left[ \frac{\rho}{\gamma} - S(\tau) \right]$$

$$\text{So } b = \frac{\beta}{\gamma} = \frac{\text{"losing immun." rate}}{\text{"infection" rate}}, \\ \tau = \frac{\rho}{\gamma} = \frac{\text{"recovery" rate}}{\text{"infection" rate}}$$

c) Show everything in  $(S, I)$  space -  
 $0 \leq S + I \leq 1$  are valid states





Nullclines

$\dot{I}=0 \rightarrow I=0$   
or  $S=\tau$

$\dot{S}=0 \rightarrow I = b \frac{1-S}{b+S} = b \left( -1 + \frac{b+1}{b+S} \right)$   
hyperbola crossing at  
 $(S=1, I=0)$   
 $(S=0, I=1)$

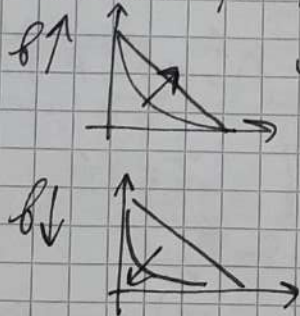
- d) Fixed point  $(1,0)$  - nothing interesting, no one infected
- Fixed point  $F = (\tau, b(-1 + \frac{b+1}{b+\tau}))$  - possible only for  $\tau < 1$  when recovery rate does not "win"

2 parameters control the system

(main)  $\tau$  - shows whether final state F is towards "no infected" (vert. line  $\rightarrow$ ) or "all infected" (vert. line  $\leftarrow$ )

$b$  - accounts for  $R(\tau)$  not shown here

Meaning less part left for R ("immun. loss")



- \* e) The idea is to represent as linear function of  $S, I$  using 1st part of Taylor:

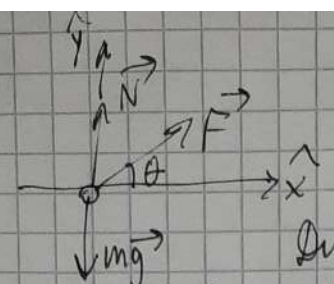
$$\frac{dS}{d\tau} = f(F) + \nabla f(F) \cdot \begin{pmatrix} S - S_F \\ I - I_F \end{pmatrix}$$

and similarly for  $\frac{dI}{d\tau}$ , only  $\nabla g(F)$  changes.

TBD.



# Problem 5

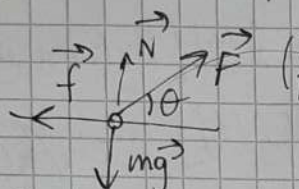
a)   $\tan \theta = \frac{3}{4}$

Duck moves along  $\hat{x}$  so that

$$\begin{cases} m\ddot{x} = \vec{F} \cdot \hat{x} = F \cos \theta \\ \vec{0} = \vec{N} + \vec{F} \cdot \hat{y} + mg(-\hat{y}) \end{cases} \Rightarrow \begin{cases} m\ddot{x} = F \cos \theta \\ N + F \sin \theta = mg \end{cases}$$

$\dot{x} = \frac{F}{m} \cos \theta \cdot t, x = \frac{F}{m} \cos \theta \frac{t^2}{2} \quad (t_0 = 0)$

b) Additional force  $\rightarrow$  smaller  $\dot{x}$  up to uniform motion

  $(f)_{\max} = \mu N$

$$\begin{cases} F \cos \theta - \mu N = m\ddot{x} \\ F \sin \theta + N = mg \end{cases} \Rightarrow x(t) = \left( -\mu g + \frac{F}{m} (\mu \sin \theta + \cos \theta) \right) \frac{t^2}{2}$$

c) direction will change, F and N and f change,  $\dot{x}$  not const

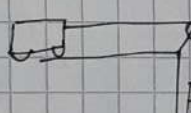
Idea here: get EOM by Newton

# Problem 6

a, b)  $a = \frac{F}{m}$

$$v(t) = \frac{F}{m} t, x(t) = x_0 + \int_0^t v(t') dt' = \frac{F}{m} \frac{t^2}{2}$$

c) Same as F

d)   $E = E_k + E_{\text{pot}} = \frac{m+M}{2} v^2 + Mgh, \dot{E} = 0$

$h < 0, |h(t)| = x(t)$  for car

Idea here: get EOM by  $\frac{dE}{dt} = 0$

$$\dot{E} = \frac{M+m}{2} \cdot 2v\dot{v} + Mg\dot{h} = 0$$

$$(M+m)\dot{v} - Mg = 0$$

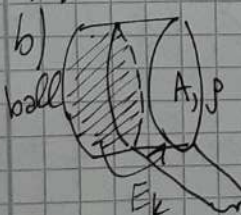
$\dot{v} = \frac{Mg}{M+m}$  — it is less than before (same causing force, as car's mg is compensated by N, but masses of both of them)

# Problem 7

Idea here: derive turb. friction simply

$$\vec{F}_d = -\frac{\rho u^2}{2} C_d A \vec{u}$$

a)  $|\vec{F}_d| = \frac{\rho}{m^3} \cdot \frac{m^2}{s^2} \cdot m^2 = \frac{\rho \cdot m}{s^2} = N \checkmark$

b)  ball loses  $E_k \rightarrow$  giving to air,  $F_d$  does negative work.

$$-(u dt) F_d = \underbrace{(u dt) A}_{V} \rho \frac{u^2}{2} (-1) K \leftarrow \text{the higher, the more losses}$$

c)  $Mg = \rho \frac{u_{\infty}^2}{2} C_d \pi \frac{d^2}{4} \Rightarrow F_d = K \frac{\rho A}{2} u^2$

$$u_{\infty} = \sqrt{\frac{8 \cdot Mg}{\pi C_d \rho}} = [\text{calculate}]$$

d)  $L \approx \frac{u_{\infty}^2}{g}, t \approx \frac{u_{\infty}}{g}$  roughly Idea here dim. analysis gives order of magnitude guesses



# Problem 9

$$\dot{x}(t) = v(t)$$

$$\dot{v}(t) = -\frac{k}{m}x(t) - \gamma v(t)$$

a)  $[k] = \frac{N}{m} = \text{kg} \cdot \text{s}^{-2}$ ,  $[\gamma] = \frac{N \cdot s}{\text{kg} \cdot m} = \frac{\text{kg} \cdot m \cdot \text{s}^{-1}}{\text{kg} \cdot m} = \text{s}^{-1}$

b)  $\dot{v}(t) = 0$ ,  $v(t) = 0 \rightarrow x(t) = 0$  is rest position (no grav.)

c)  $E = \frac{m\dot{x}(t)^2}{2} + \frac{kx(t)^2}{2}$

$$\frac{dE}{dt} = \frac{m}{2} \cdot 2 \cdot \dot{x}(t) \ddot{x}(t) + \frac{k}{2} \cdot 2 \cdot x(t) \dot{x}(t) = \dot{x}(t) [kx(t) + m\ddot{x}(t)] = \dot{x}(t) [kx(t) + (-kx(t) - \gamma \dot{x}(t))] = -m\gamma \dot{x}(t)^2$$

(non-conservat. system)

But  $E$  gives the current contour line in phase space  $\rightarrow$  evolution of dynamics is fall to lower contour lines until  $E=0$ .

d)  $A = \sqrt{E_0/k}$ ,  $[\sqrt{E_0/k}] = [\sqrt{\frac{m}{2} \dot{x}^2 + x^2}] = [x] = m$   
 $\mathcal{E} = \frac{E}{E_0}$ ,  $T = \sqrt{m/k}$ ,  $[\sqrt{m/k}] = [(\frac{m}{k})^{\frac{1}{2}}] = s$  } Non-dim.  
 $\xi = \frac{x}{A}$ ,  $\tau = \frac{t-t_0}{T}$ ,  $\mathcal{E} = \frac{E}{E_0}$   
 $\rightarrow \zeta = \frac{\gamma T}{A}$

$$E_0 \mathcal{E} = \frac{m}{2} (\dot{x}(t))^2 + \frac{k}{2} (x(t))^2 = \frac{m}{2} \left( \frac{d(A\xi)}{d(\tau T)} \right)^2 + \frac{k}{2} (A\xi)^2 \quad [A^2 \equiv E_0/k]$$

$$A^2 k \mathcal{E} = \frac{mA^2}{2T^2} \xi^2 + \frac{kA^2}{2} \xi^2$$

$\zeta = \sqrt{\frac{m}{k}} \gamma$   
 simplest suggest.  
 from dim. anal.

$$\mathcal{E} = \frac{\dot{\xi}^2}{2} + \frac{\xi^2}{2}$$

Show dissipation:

$$\dot{\mathcal{E}} = \dot{\xi} \ddot{\xi} + \xi \dot{\xi} = \dot{\xi} [\ddot{\xi} + \xi]$$

[From  $\mathcal{E}$  all using same scales:

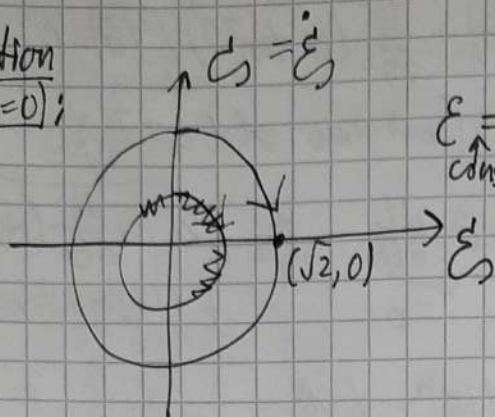
$$\ddot{x} = -\frac{k}{m}x - \gamma \dot{x} \rightarrow \frac{1}{T^2} \ddot{\xi} = -\frac{1}{T^2} \xi - \frac{\gamma}{T} \dot{\xi} \rightarrow \ddot{\xi} = -\xi - (\tau \gamma) \dot{\xi}$$

$$\dot{\mathcal{E}} = \dot{\xi} [\xi - \xi - (\tau \gamma) \dot{\xi}] = -(\tau \gamma) \dot{\xi}^2$$



e)  $\dot{\mathcal{E}} = -c \dot{\mathcal{C}}^2$   
 $\downarrow$   
 $\gamma \gamma$

No function  
 $(c=0)$ ;

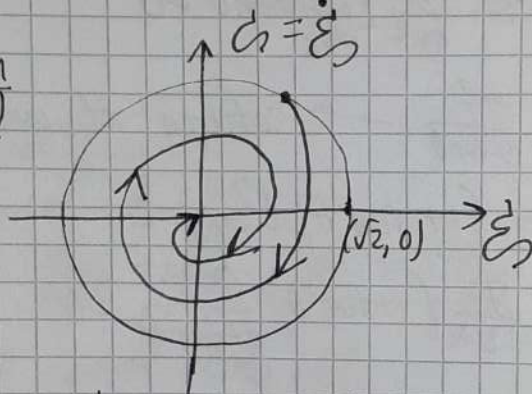


$\mathcal{E}_{const} = \frac{\mathcal{E}_1^2}{2} + \frac{\mathcal{C}^2}{2}$  — circles,  
 $dist. = \sqrt{2\mathcal{E}}$

Since  $\mathcal{E}_0 = 1$  (We choose  
the scale in such  
way!  $\mathcal{E} = \mathcal{E} \mathcal{E}_0$ )

There is always 1 circle,  
distance  $\sqrt{2}$ .

Function  
 $(c > 0)$



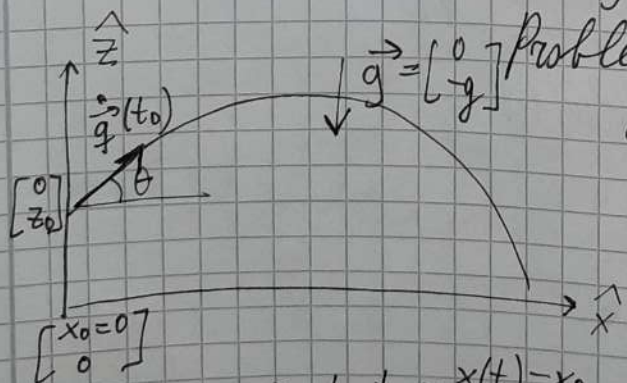
Infinitely long  
"motion" to  $(0,0)$ .

\*f)  $\ddot{x}(t) = -\frac{k}{m}x(t) - \gamma \dot{x}(t)$

Assume  $x(t) = x_0 \sin(\omega t - \varphi) e^{-t/t_c}$

1)  $\omega = \sqrt{\frac{k}{m}}$ ,  $t_c = \frac{1}{\gamma}$  — by dim. analysis or direct checking

2)  $\varphi$  is not determined by  $k, m, \gamma$ , but by  $x(0)$ ,  $\dot{x}(0)$



Problem 10 — projectile motion (with non-trivial stuff)

a) EOM:  $\ddot{\vec{q}} = \vec{g}$

$\ddot{\vec{q}}(t) = \begin{bmatrix} \ddot{x}(t) \\ \ddot{z}(t) \end{bmatrix} = \begin{bmatrix} 0 \\ -g \end{bmatrix} \Rightarrow \dot{\vec{q}}(t) = \begin{bmatrix} \dot{x}_0 \\ \dot{z}_0 - g(t-t_0) \end{bmatrix}$

$\vec{q}(t) = \begin{bmatrix} x(t) \\ z(t) \end{bmatrix} = \begin{bmatrix} x_0 + \dot{x}_0(t-t_0) \\ z_0 + \dot{z}_0(t-t_0) - \frac{g(t-t_0)^2}{2} \end{bmatrix}$

b) \*c)

$z(x) = z_0 + \frac{\dot{z}_0}{\dot{x}_0}x - \frac{g}{2\dot{x}_0^2}x^2$  — parabola,  $\dot{x}_0 = v \cos \theta$ ,  
 $\dot{z}_0 = v \sin \theta$ .



$$z(x) = H + \tan\theta \cdot x - \frac{g}{2v^2} \frac{x^2}{\cos^2\theta} = H + \tan\theta \cdot x - \frac{g}{2v^2} (1 + \tan^2\theta) x^2$$

$$z(L) = 0,$$

$$(x) \quad H + \tan\theta \cdot L(\theta) - \frac{g}{2v^2} (1 + \tan^2\theta) L^2(\theta) = 0 \quad \left| \frac{d}{d\theta} \right.$$

$L_{\max/\min}$  when  $\frac{dL}{d\theta} = 0$  (minimum at  $\theta = \pm \frac{\pi}{2}$ )

$$\frac{1}{\cos^2\theta} \cdot L(\theta) + \tan\theta \frac{dL}{d\theta} - \frac{g}{2v^2} \left[ 2L(\theta) \frac{dL}{d\theta} (1 + \tan^2\theta) + L(\theta)^2 \cdot 2 \tan\theta \cdot \frac{1}{\cos^2\theta} \right] = 0$$

$$\frac{L(\theta)}{\cos^2\theta} - \frac{g}{v^2} L_{\max}^2 \frac{\tan\theta}{\cos^2\theta} = 0$$

$$1 - \frac{g}{v^2} L_{\max}^2 \tan\theta = 0$$

$$L_{\max} = \frac{v^2}{g \tan\theta} \rightarrow \text{return at arc } (x)$$

$$H + \tan\theta \cdot L_{\max} - \frac{g}{2v^2} (1 + \tan^2\theta) L_{\max}^2 = 0$$

$$H + \tan\theta \frac{v^2}{g \tan\theta} - \frac{g}{2v^2} (1 + \tan^2\theta) \frac{v^4}{g^2 \tan^2\theta} = 0$$

$$gH + v^2 - \frac{v^2}{2g} (1 + \frac{1}{\tan^2\theta}) = 0$$

$$\tan\theta = \sqrt{\frac{1}{-1 + \frac{2}{v^2} (gH + v^2)}} = \frac{1}{\sqrt{1 + \frac{2gH}{v^2}}} \quad \text{-- best angle if "no friction" / Earth curvature}$$

(if  $H=0 \rightarrow$  from ground,

$$\theta = \arctan 1 = \frac{\pi}{4})$$

d) friction - TBD

Problem 11

TBD.



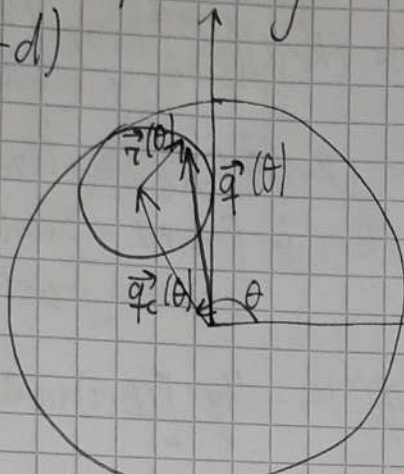
# Problem 8 - hypotrochoids etc.

- 2) Curve is always closed since after  $LCM(m, n)$  cogs the point will be at same spot after period

$$N_{\text{revolution}} = \frac{LCM(m, n)}{n} \text{ (w.r.t. outer circle)}$$

$$\text{Symmetry} = \frac{LCM(m, n)}{n} \text{ - fold}$$

b-d)



$m, n$  cogs measure circumf.

$$\frac{m}{n} = \frac{2\pi R}{2\pi r} = \frac{R}{r}$$

$$d = |\vec{q}_c(\theta) - \vec{q}(\theta)|$$

$$p = \frac{d}{r}$$

reference rotation

$$\vec{q}(\theta) = \vec{q}_c(\theta) + \vec{r}(\theta) = (R-r) \begin{pmatrix} \cos \theta \\ \sin \theta \end{pmatrix} + d \begin{pmatrix} \cos \gamma \\ \sin \gamma \end{pmatrix}$$

inner rotation

Connect  $\gamma$  and  $\theta$ :

disk moved  $l = \theta R$ ,

$$N_{\text{rot}} = \frac{l}{2\pi r} = \frac{\theta R}{2\pi r}$$

on curved line,  $+\theta$ ).

$$\gamma = \frac{\theta R}{2\pi r} (-2\pi) = -\theta \frac{R}{r} + \theta \text{ (due to rotation)}$$

other direction

to rotation

Length of one closed curve:  $\theta \in [0, 2\pi \frac{LCM(m, n)}{m}]$

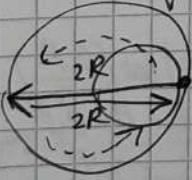
$$\vec{q}'(\theta) = (R-r) \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} + p r \begin{pmatrix} -\sin(\theta(1-\frac{R}{r})) \\ \cos(\theta(1-\frac{R}{r})) \end{pmatrix} \text{ take 1}$$

$$= (R-r) \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} - p(R-r) \begin{pmatrix} -\sin(\theta(1-\frac{R}{r})) \\ \cos(\theta(1-\frac{R}{r})) \end{pmatrix} = (R-r) \begin{pmatrix} -\sin \theta + p \sin(\theta(1-\frac{R}{r})) \\ \cos \theta - p \cos(\theta(1-\frac{R}{r})) \end{pmatrix}$$

$$|\vec{q}'(\theta)| = (R-r) \sqrt{\sin^2 \theta + \cos^2 \theta + p^2 \sin^2(\theta(1-\frac{R}{r})) + p^2 \cos^2(\theta(1-\frac{R}{r})) - 2p \sin \theta \sin(\theta(1-\frac{R}{r})) - 2p \cos \theta \cos(\theta(1-\frac{R}{r}))}$$

$$= \sqrt{1 + p^2 - 2p \cos(\theta \frac{R}{r})} (R-r)$$

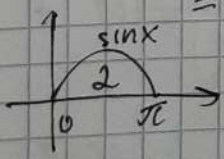
Take  $\frac{R}{r} = 2, p = 1$ ,



length must be  $4R$ .

Indeed  $L = \int_0^{2\pi} |\vec{q}'(\theta)| d\theta =$

$$= \frac{R}{\sqrt{2}} \int_0^{2\pi} |\sin \theta| d\theta = \frac{R}{\sqrt{2}} \cdot 4 = 4R$$





\* Now assume gravity acts, given initial conditions  $\theta_0, \dot{\theta}_0$  — constrained rotation. Is it possible to find  $\theta(t)$  by Lagrange?

1 DOF  $\theta(t)$

Lagrange function:

$$\mathcal{L}(\theta, \dot{\theta}, t) = T(\dot{\theta}) - V(\theta) = \left[ \frac{1}{2} m \dot{\vec{q}}(\theta)^2 - \mathcal{U}(\vec{q}(\theta)) \right]$$

$$\vec{q}(\theta) = (R-r) \begin{pmatrix} \cos \theta \\ \sin \theta \end{pmatrix} + \rho r \begin{pmatrix} \cos(\theta(1-\frac{R}{r})) \\ \sin(\theta(1-\frac{R}{r})) \end{pmatrix}$$

$$\dot{\vec{q}}(\theta) = (R-r) \dot{\theta} \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} + \rho \dot{\theta} (r-R) \begin{pmatrix} -\sin(\dots) \\ \cos(\dots) \end{pmatrix}$$

$$= (R-r) \dot{\theta} \begin{bmatrix} -\sin \theta + \rho \sin(\dots) \\ \cos \theta - \rho \cos(\dots) \end{bmatrix}$$

$$= \frac{m}{2} |\dot{\vec{q}}(\theta)|^2 + \mathcal{U}(\vec{q}(\theta)) = \left[ \mathcal{U} \begin{pmatrix} 0 \\ -g \end{pmatrix} \cdot \vec{q}(\theta) = -Mg \cdot [(R-r) \sin \theta + \rho r \sin(\dots)] \right]$$

$$= \frac{m}{2} (R-r)^2 \dot{\theta}^2 (1 + \rho^2 - 2\rho \cos(\theta \frac{R}{r})) - Mg [(R-r) \sin \theta + \rho r \sin(\dots)]$$

Euler-Lagrange equation:

$$\frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{\theta}} \right) = \frac{\partial \mathcal{L}}{\partial \theta} \Rightarrow \frac{d}{dt} \left[ m(R-r)^2 (1 + \rho^2 - 2\rho \cos(\theta \frac{R}{r})) \dot{\theta} \right] =$$

$$= m(R-r)^2 \left[ (1 + \rho^2 - 2\rho \cos(\theta \frac{R}{r})) \ddot{\theta} + (\dot{\theta})^2 2\rho \sin(\theta \frac{R}{r}) \frac{R}{r} \right] \stackrel{!}{=} 0$$

$$\stackrel{!}{=} \frac{m}{2} (R-r)^2 \dot{\theta}^2 \cdot 2\rho \sin(\theta \frac{R}{r}) \frac{R}{r} - mg [(R-r) \cos \theta + \rho r \cos(\theta(1-\frac{R}{r}))]$$

$$\Rightarrow (R-r)^2 [1 + \rho^2 - 2\rho \cos(\theta \frac{R}{r})] \ddot{\theta} = -(R-r)^2 \rho \sin(\theta \frac{R}{r}) \frac{R}{r} (\dot{\theta})^2 - g [(R-r) \cos \theta + \rho r \cos(\theta(1-\frac{R}{r}))]$$

$$(R-r) [1 + \rho^2 - 2\rho \cos(\theta \frac{R}{r})] \ddot{\theta} = - (R-r) \rho \sin(\theta \frac{R}{r}) \frac{R}{r} (\dot{\theta})^2 - g [\cos \theta + \rho \cos(\theta(1-\frac{R}{r}))]$$

Take  $\rho=1$  to get rid of this

$$(R-r) 2 \sin^2(\frac{\theta R}{2r}) \ddot{\theta} = - (R-r) \cdot 2 \sin(\frac{\theta R}{2r}) \cos(\frac{\theta R}{2r}) \frac{R}{r} (\dot{\theta})^2 + g 2 \cdot \sin \frac{\theta + \theta - \frac{\theta R}{r}}{2r} \sin \frac{\theta R}{2r}$$

$$(R-r) 2 \sin(\frac{\theta R}{2r}) \dot{\theta} = - (R-r) \cos(\frac{\theta R}{2r}) \frac{R}{r} (\dot{\theta})^2 + g \sin(\theta - \frac{\theta R}{2r})$$

$$\ddot{\theta} = \frac{1}{2} \frac{g \sin(\theta - \frac{\theta R}{2r})}{(R-r) \sin(\frac{\theta R}{2r})} - \cot(\frac{\theta R}{2r}) \cdot \frac{R}{2r} (\dot{\theta})^2$$

Set  $R = Kr$

$$\ddot{\theta} = \frac{g}{2} \frac{\sin(\theta - \frac{\theta K}{2})}{(K-1)r \sin(\frac{\theta K}{2})} - \cot(\frac{\theta K}{2}) \cdot \frac{K}{2} (\dot{\theta})^2$$



Special case  $K=2$ :

$$\ddot{\theta}' = -\cot\theta \cdot (\dot{\theta})^2$$

