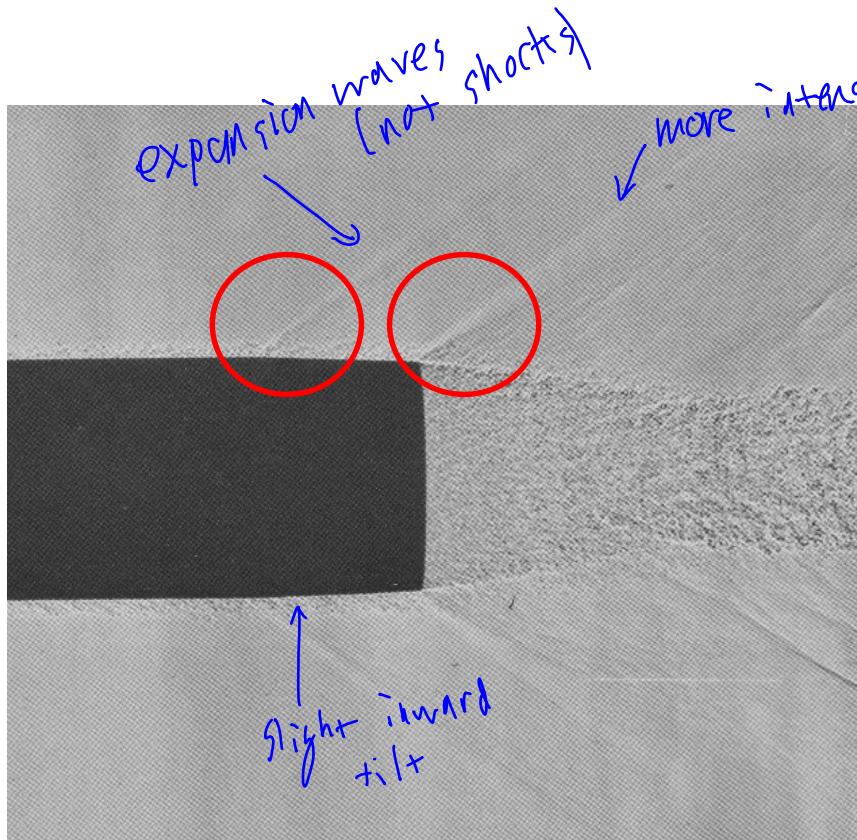


# SESA3029

## Aerothermodynamics

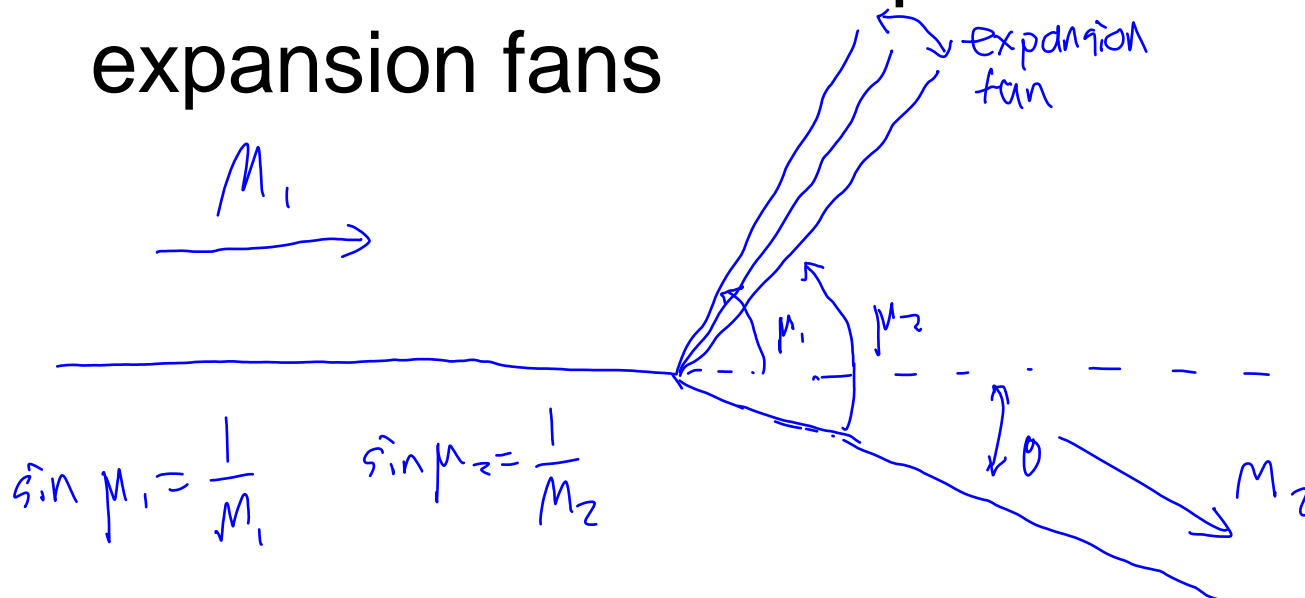


### Lecture 2.4

### Expansion waves

# Expansion waves

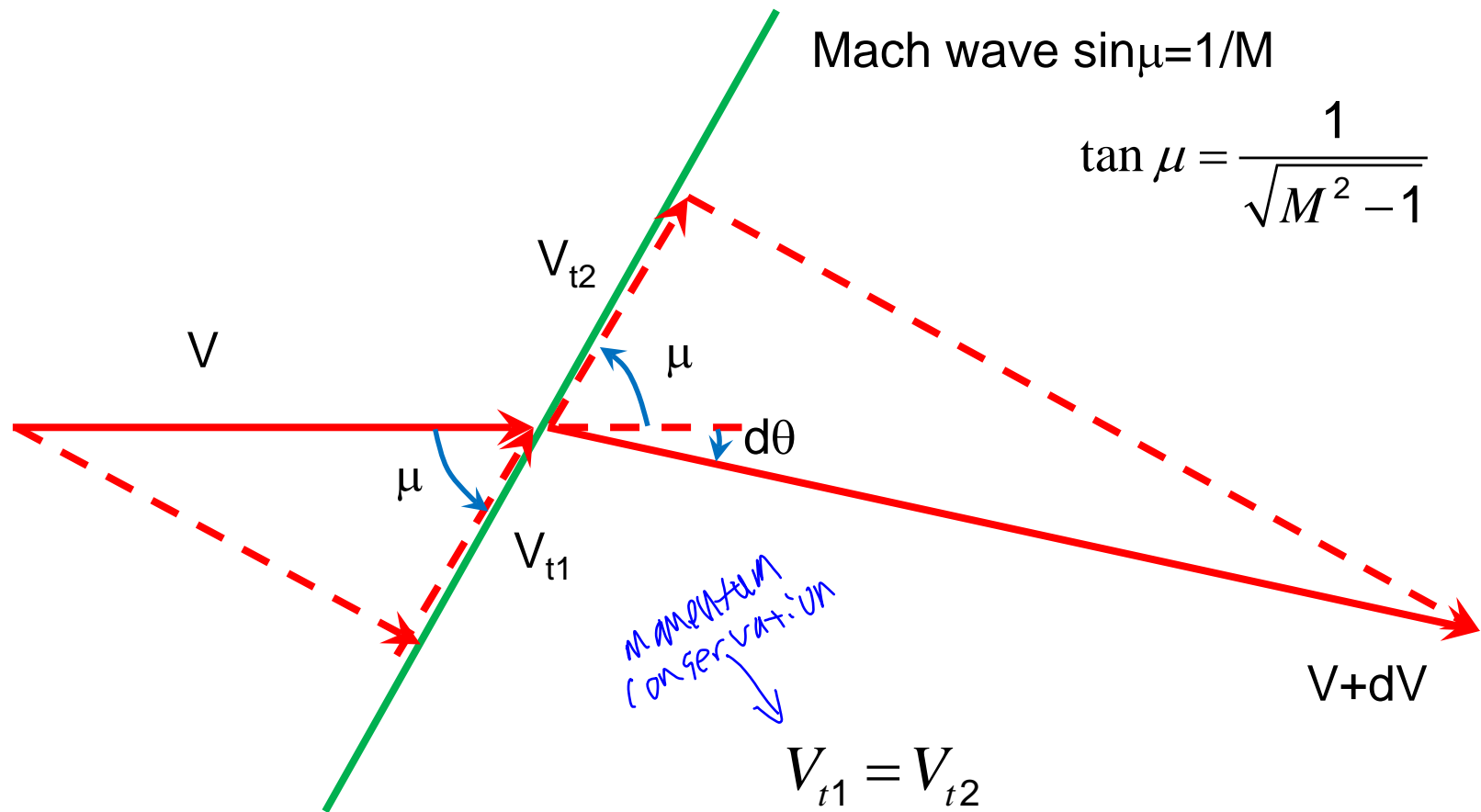
- Must be isentropic (i.e. Mach waves)
- Finite pressure changes are produced by a series (a 'fan') of small changes
- Convex corners in supersonic flow give expansion fans



distributed

The expansion fan turns the flow gradually

# Turning a flow by a small angle $d\theta$



$$V \cos \mu = (V + dV) \cos(\mu + d\theta)$$

$$V \cos \mu = (V + dV) \cos(\mu + d\theta)$$

Expand out

1  $\xleftarrow{\text{small angle approx}} d\theta$

$$V \cos \mu = (V + dV) [\cos \mu \cancel{\cos d\theta} - \sin \mu \cancel{\sin d\theta}]$$

Let  $d\theta \rightarrow 0$  and remove products of small quantities

$$0 = dV \cos \mu - V d\theta \sin \mu$$

$$\frac{dV}{V} = d\theta \tan \mu = \frac{d\theta}{\sqrt{M^2 - 1}}$$

$$V = Ma, \text{ so } dV = Mda + a dM$$

$$\frac{dV}{V} = \frac{da}{a} + \frac{dM}{M} \quad \text{and hence} \quad \frac{d\theta}{\sqrt{M^2 - 1}} = \frac{da}{a} + \frac{dM}{M} \quad (1)$$

$$\frac{d\theta}{\sqrt{M^2 - 1}} = \frac{da}{a} + \frac{dM}{M} \quad (1)$$


---

We know  
(adiabatic flow)

$$\frac{a_0^2}{a^2} = 1 + \frac{\gamma - 1}{2} M^2$$

or

$$a = a_0 \left[ 1 + \frac{\gamma - 1}{2} M^2 \right]^{\frac{1}{2}}$$

$\frac{d}{dM}$

$$\begin{aligned} \frac{da}{dM} &= -\frac{1}{2}(\gamma - 1) M a_0 \left[ 1 + \frac{\gamma - 1}{2} M^2 \right]^{-\frac{3}{2}} \\ &= -\frac{1}{2}(\gamma - 1) M a \left[ 1 + \frac{\gamma - 1}{2} M^2 \right]^{-1} \end{aligned}$$

Rewrite as

$$\frac{da}{a} = -\frac{\gamma - 1}{2} M \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{-1} dM \quad (2)$$

$$\frac{d\theta}{\sqrt{M^2 - 1}} = \frac{da}{a} + \frac{dM}{M} \quad (1) \quad \frac{da}{a} = -\frac{\gamma - 1}{2} M \left(1 + \frac{\gamma - 1}{2} M^2\right)^{-1} dM \quad (2)$$


---

Substitute (2) into (1) and rearrange

$$\frac{d\theta}{\sqrt{M^2 - 1}} = \left[ 1 - \frac{\gamma - 1}{2} M^2 \left(1 + \frac{\gamma - 1}{2} M^2\right)^{-1} \right] \frac{dM}{M}$$

$$= \left[ 1 + \frac{\gamma - 1}{2} M^2 \right]^{-1} \frac{dM}{M}$$

(Take over common denominator and cancel terms)

$$\boxed{d\theta = \frac{\sqrt{M^2 - 1}}{1 + \frac{\gamma - 1}{2} M^2} \frac{dM}{M}} \quad (3)$$

# Define a standard integral

nu symbol  
is angle ish  
v is theta

$$\nu(M') = \int_1^{M'} \frac{\sqrt{M^2 - 1}}{1 + \frac{\gamma-1}{2} M^2} \frac{dM}{M}$$

Exact solution (tabulated on IFT) – the Prandtl-Meyer function

$$\nu(M) = \sqrt{\frac{\gamma+1}{\gamma-1}} \tan^{-1} \sqrt{\frac{\gamma-1}{\gamma+1} (M^2 - 1)} - \tan^{-1} \sqrt{M^2 - 1}$$

**Isentropic-flow table ( $\gamma = 1.4$ ):**

| $M$    | $p/p_0$ | $\rho/\rho_0$ | $T/T_0$ | $\nu$ (deg.) | $A/A^*$ |
|--------|---------|---------------|---------|--------------|---------|
| 1.0000 | 0.5283  | 0.6339        | 0.8333  | 0.0000       | 1.0000  |
| 1.0200 | 0.5160  | 0.6234        | 0.8278  | 0.1257       | 1.0003  |
| 1.0400 | 0.5039  | 0.6129        | 0.8222  | 0.3510       | 1.0013  |
| 1.0600 | 0.4919  | 0.6024        | 0.8165  | 0.6367       | 1.0029  |
| 1.0800 | 0.4800  | 0.5920        | 0.8108  | 0.9680       | 1.0051  |

Return to

$$d\theta = \frac{\sqrt{M^2 - 1}}{1 + \frac{\gamma-1}{2} M^2} \frac{dM}{M} \quad (3)$$

Integrate from  $\theta=0$   $M = M'_1$  to  $\theta=\theta'$   $M = M'_2$

Giving

$$\theta' = \nu(M'_2) - \nu(M'_1)$$

Drop primes for  
convenience

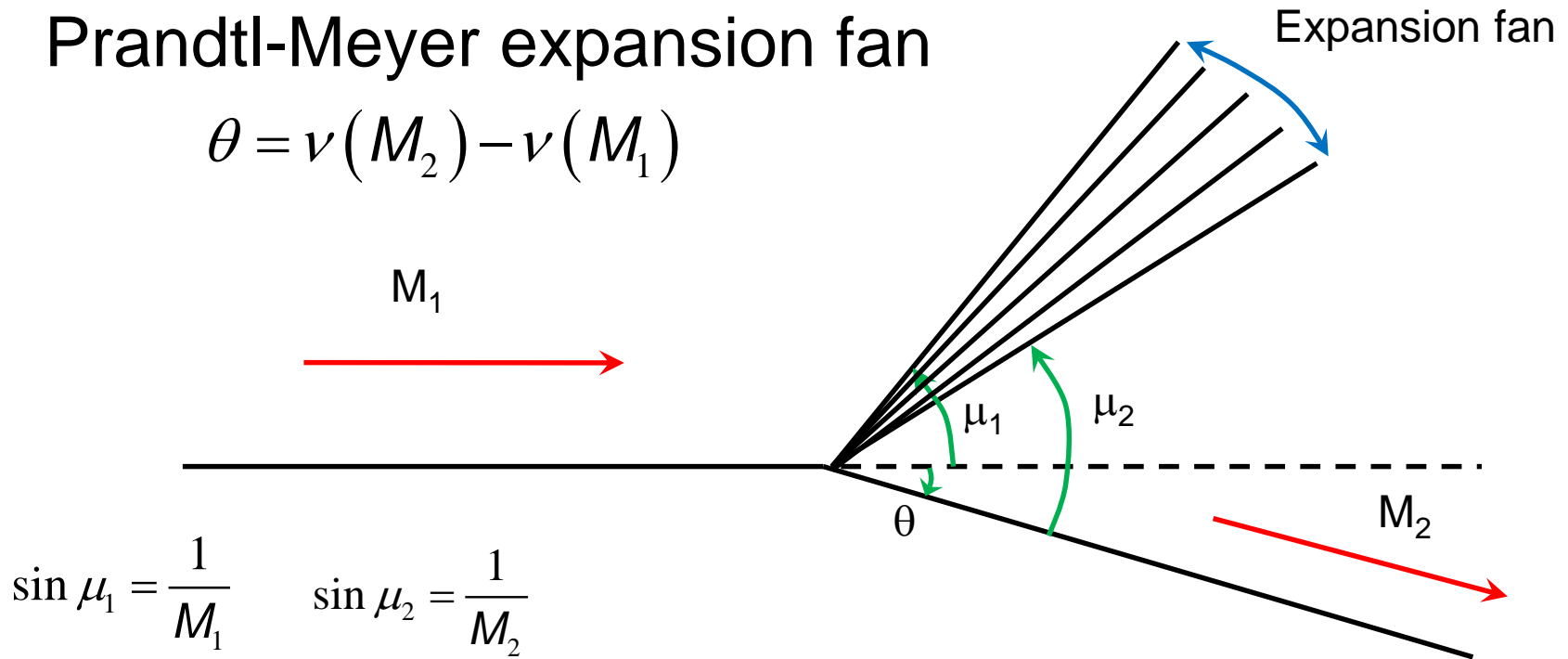
$$\theta = \nu(M_2) - \nu(M_1)$$

Fundamental equation for expansion fans  
( $\theta$ =turning angle and  $\nu$ =Prandtl-Meyer function)



# Prandtl-Meyer expansion fan

$$\theta = \nu(M_2) - \nu(M_1)$$



Example: A Mach 3 flow is turned by  $13^\circ$  over a convex corner. Find:

- (a) the Mach number after the corner,
- (b) the percentage pressure drop, and
- (c) the included angle of the P-M expansion fan.

$$\theta = \nu(M_2) - \nu(M_1)$$

**Isentropic-flow table ( $\gamma = 1.4$ ):**

| $M$    | $p/p_0$ | $\rho/\rho_0$ | $T/T_0$ | $\nu$ (deg.) | $A/A^*$ |
|--------|---------|---------------|---------|--------------|---------|
| 3.0000 | 0.0272  | 0.0762        | 0.3571  | 49.7573      | 4.2346  |
| 3.0200 | 0.0264  | 0.0746        | 0.3541  | 50.1417      | 4.3160  |
| 3.0400 | 0.0256  | 0.0730        | 0.3511  | 50.5231      | 4.3989  |
| 3.0600 | 0.0249  | 0.0715        | 0.3481  | 50.9016      | 4.4835  |
| 3.0800 | 0.0242  | 0.0700        | 0.3452  | 51.2771      | 4.5696  |
| 3.7000 | 0.0099  | 0.0370        | 0.2675  | 61.5953      | 8.1691  |
| 3.7200 | 0.0096  | 0.0363        | 0.2654  | 61.8893      | 8.3202  |
| 3.7400 | 0.0094  | 0.0356        | 0.2633  | 62.1812      | 8.4739  |
| 3.7600 | 0.0091  | 0.0349        | 0.2613  | 62.4709      | 8.6302  |
| 3.7800 | 0.0089  | 0.0342        | 0.2592  | 62.7584      | 8.7891  |
| 3.8000 | 0.0086  | 0.0335        | 0.2572  | 63.0438      | 8.9506  |
| 3.8200 | 0.0084  | 0.0329        | 0.2552  | 63.3271      | 9.1148  |
| 3.8400 | 0.0082  | 0.0323        | 0.2532  | 63.6083      | 9.2817  |
| 3.8600 | 0.0080  | 0.0316        | 0.2513  | 63.8874      | 9.4513  |
| 3.8800 | 0.0077  | 0.0310        | 0.2493  | 64.1645      | 9.6237  |

+13 deg

Example: A Mach 3 flow is turned by  $13^\circ$  over a convex corner. Find:

- (a) the Mach number after the corner,
- (b) the percentage pressure drop, and
- (c) the included angle of the P-M expansion fan.

(a) From IFT  $\nu(M_1)=49.76^\circ$  hence  $\nu(M_2)=\nu(M_1)+\theta=49.76^\circ+13^\circ=62.76^\circ$

Hence from IFT  $M_2=3.78$

(b) Also from IFT  $p_1/p_0=0.0272$  and  $p_2/p_0=0.0089$

Percentage pressure drop 
$$\frac{p_1 - p_2}{p_1} \cdot 100 = \left( 1 - \frac{p_2/p_0}{p_1/p_0} \right) \cdot 100 = 67.3\%$$

(c)  $\mu_1=\sin^{-1}(1/M_1)=19.5^\circ$

$\mu_2=\sin^{-1}(1/M_2)=15.3^\circ$

Included angle of PM fan  $= \mu_1 + \theta - \mu_2 = 17.2^\circ$