

SESA3029

Aerothermodynamics

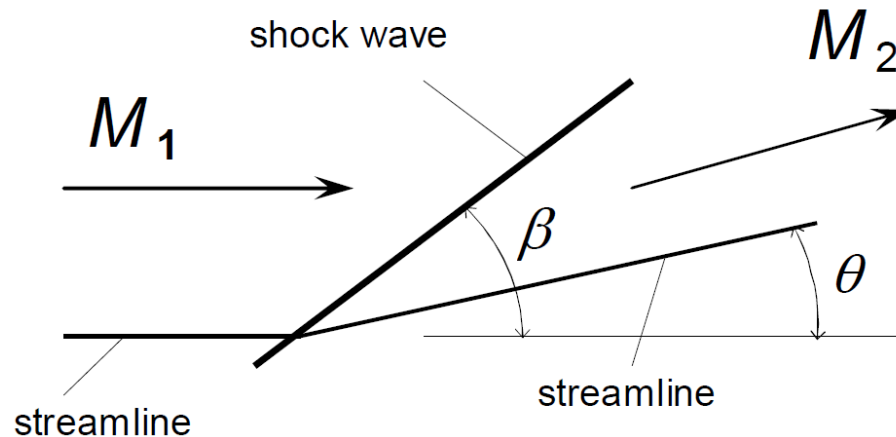
Lecture 2.2

Oblique shock
examples, engine
intake and
detached shocks



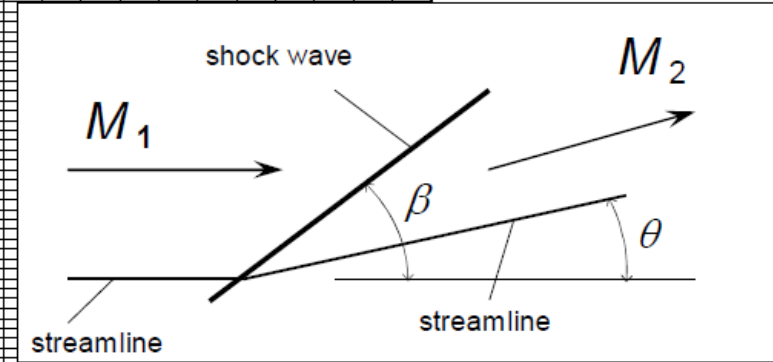
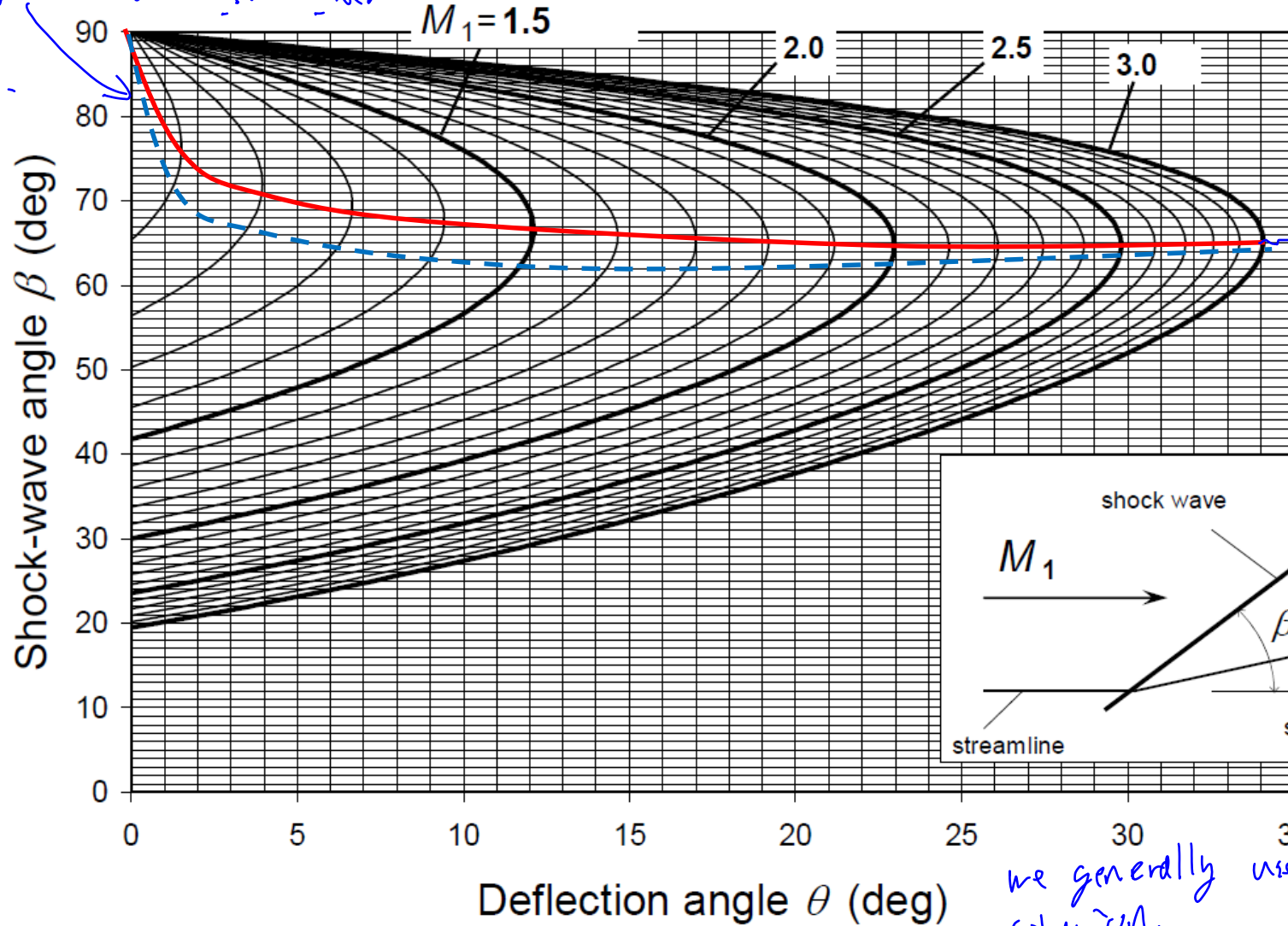
APG photo

Oblique shock relation



$$\tan \theta = 2 \cot \beta \left[\frac{M_1^2 \sin^2 \beta - 1}{M_1^2 (\gamma + \cos 2\beta) + 2} \right]$$

Oblique-shock chart: $\gamma = 1.4$



we generally use the weak solution.

It is (just) possible to have a weak shock with $M_2 < 1$

(barely/rarely)

in internal flows (compressor/turbine) there can be strong shocks (is subsonic)
 red strong shock $M_2 < 1$
 blue weak shock $M_2 > 1$ (usually supersonic)

for line is where mach number after shock is 1
 below is supersonic
 above is subsonic

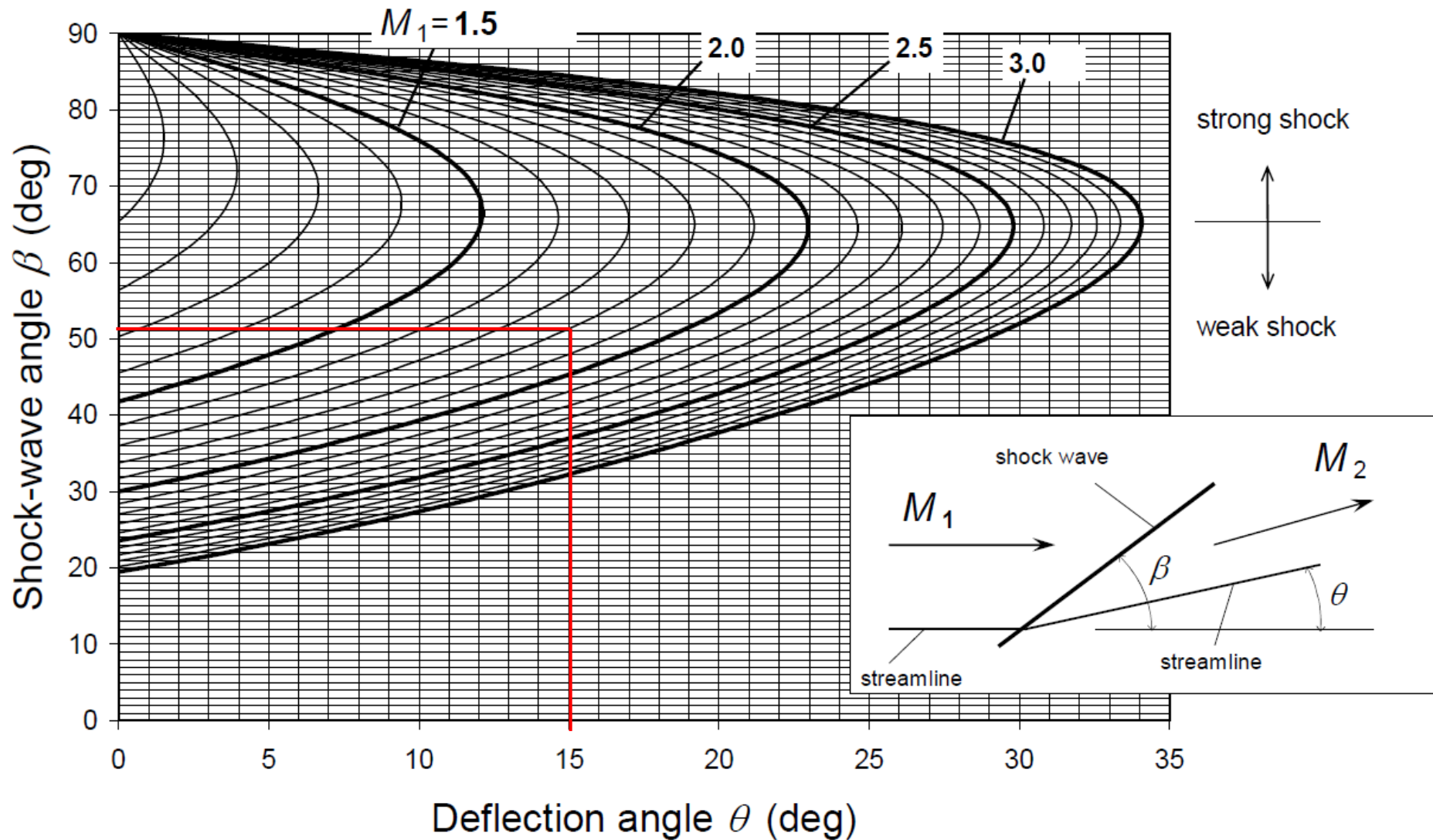
Example

An $M_1=1.8$ stream is deflected by 15 degrees.

Find

- (a) the shock angle (weak solution), and
- (b) M_2 (the flow Mach number after the shock)

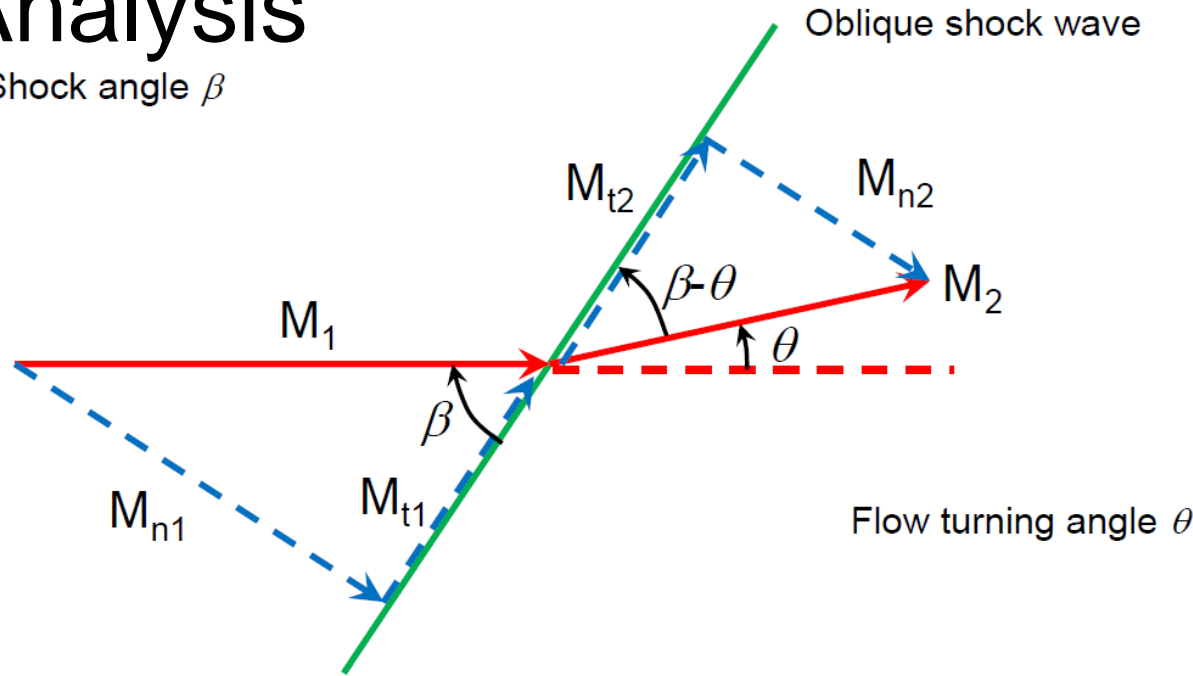
Oblique-shock chart: $\gamma = 1.4$



Shock angle $\beta=51$ degrees

Analysis

Shock angle β



$$M_{n1} = M_1 \sin \beta$$

$$M_{n2} = M_2 \sin(\beta - \theta)$$

$$M_{n1} = M_1 \sin \beta = 1.8 \sin(51^\circ) = 1.399$$

NST

M_{n1}	M_{n2}	p_2/p_1	ρ_2/ρ_1	T_2/T_1	p_{02}/p_{01}	" p_{02}/p_1 "
1.3800	0.7483	2.0551	1.6549	1.2418	0.9630	2.9798
1.4000	0.7397	2.1200	1.6897	1.2547	0.9582	3.0492
1.4200	0.7314	2.1858	1.7243	1.2676	0.9531	3.1198

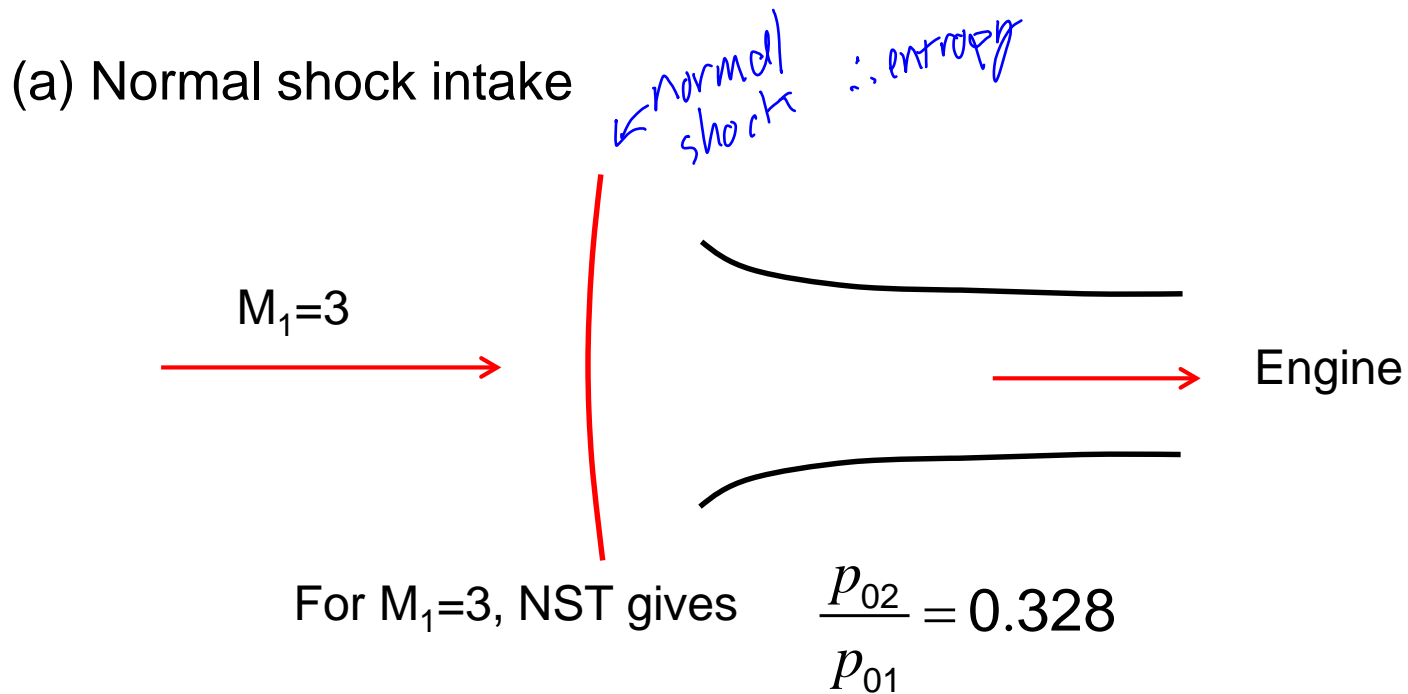
$$M_2 = \frac{M_{n2}}{\sin(\beta - \theta)} = \frac{0.74}{\sin(51^\circ - 15^\circ)} = 1.259$$

link website on blackboard

On-line shock calculator gives 51.3° and $M_2 = 1.245$

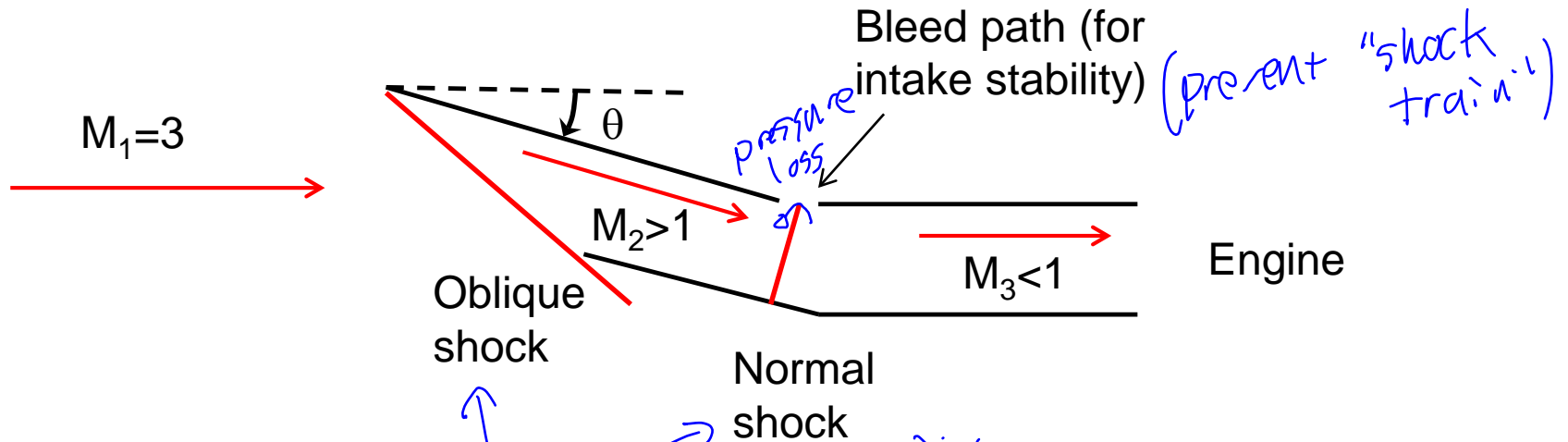
Engine intake design in supersonic flow

We are interested particularly in the reduction ('loss') of stagnation pressure, since this affects the engine performance



i.e. a 67% loss of stagnation pressure

(b) Oblique + normal shock



e.g. take $\theta = 22^\circ$

both produce entropy

OSC gives $\beta = 40^\circ$

$$M_{n1} = 3 \sin 40^\circ = 1.93$$

Note that is too chaotic and wouldn't work.

NST gives $M_{n2} = 0.59$, $M_2 = 0.59 / \sin(40^\circ - 22^\circ) = 1.91$ and $p_{02}/p_{01} = 0.754$

For normal shock NST gives $M_3 = 0.593$ and $p_{03}/p_{02} = 0.762$

Total stagnation pressure change

$$\frac{p_{03}}{p_{01}} = 0.754 \times 0.762 = 0.574$$

i.e. a 43% loss, compared to 67% for the normal shock intake

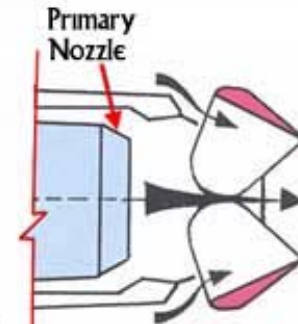
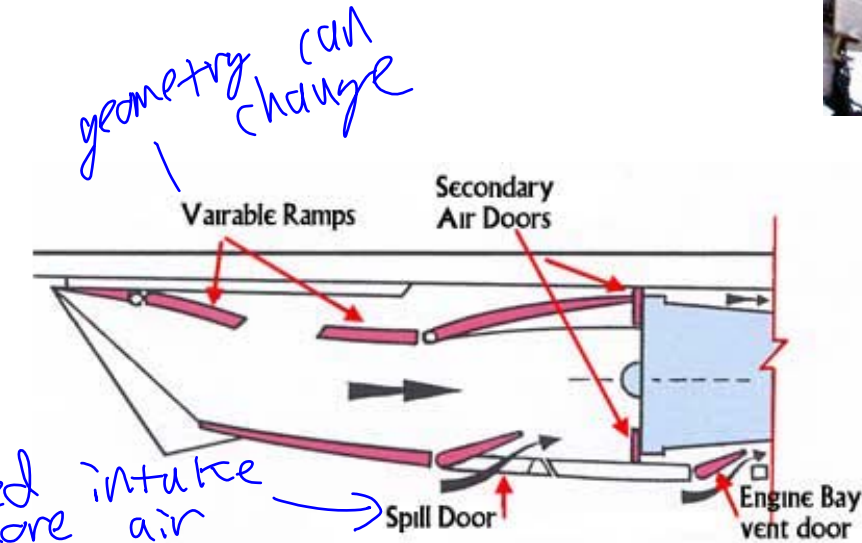
We can do better with more oblique shocks: The minimum loss occurs when the stagnation pressure drop across each shock is the same. *but more oblique shocks creates new issues*

A limiting case is isentropic compression using a curved surface.

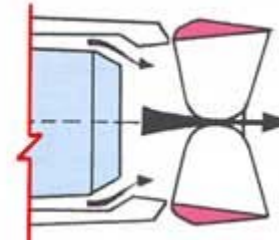
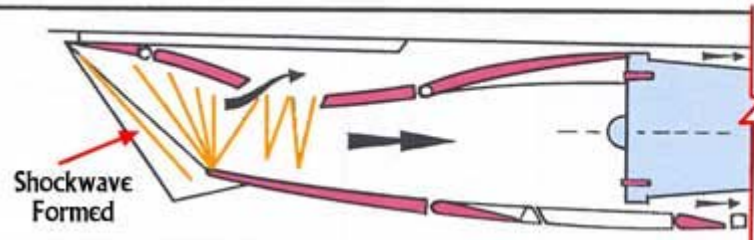
Concorde intake



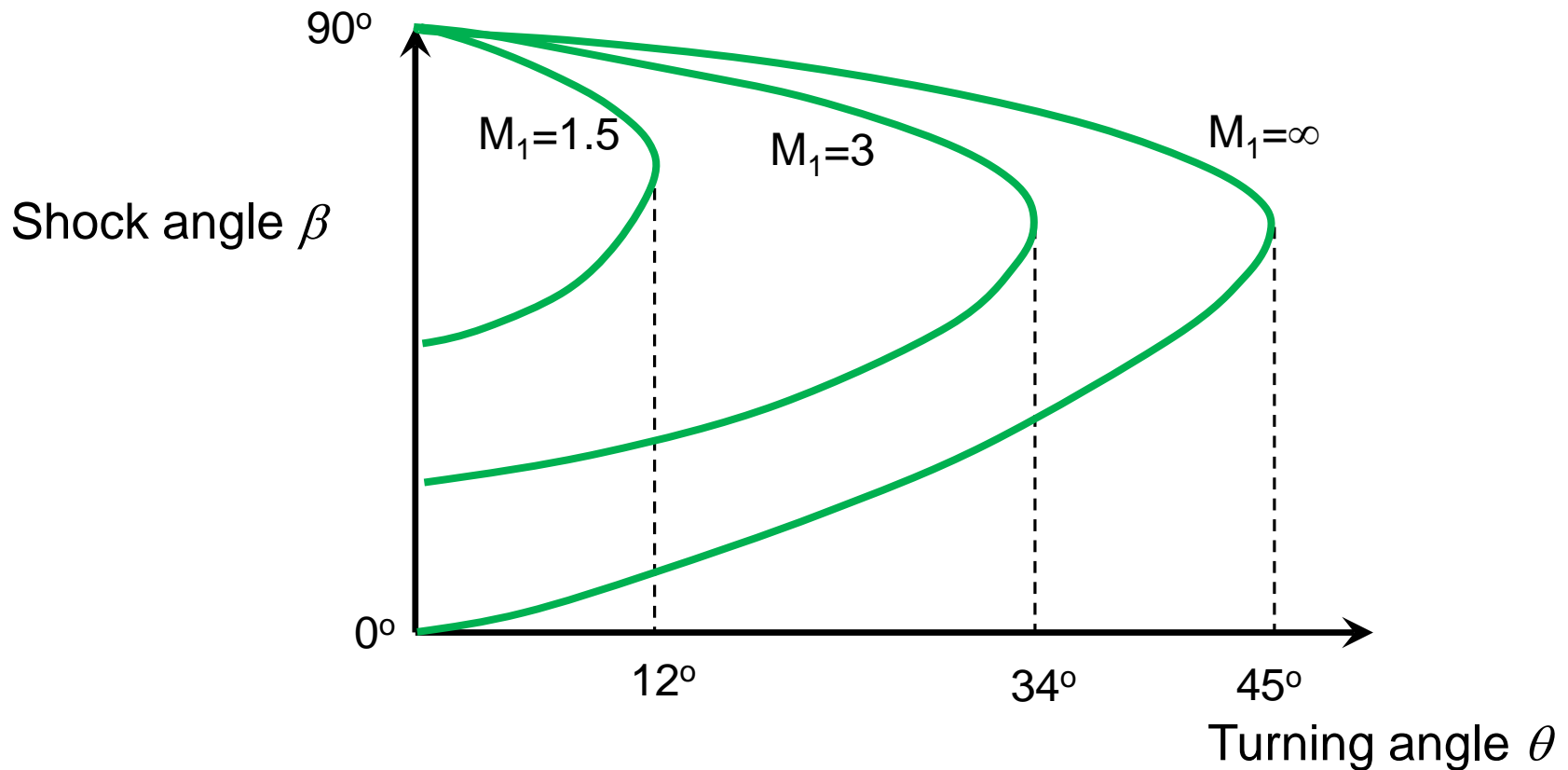
Subsonic operation



Supersonic operation



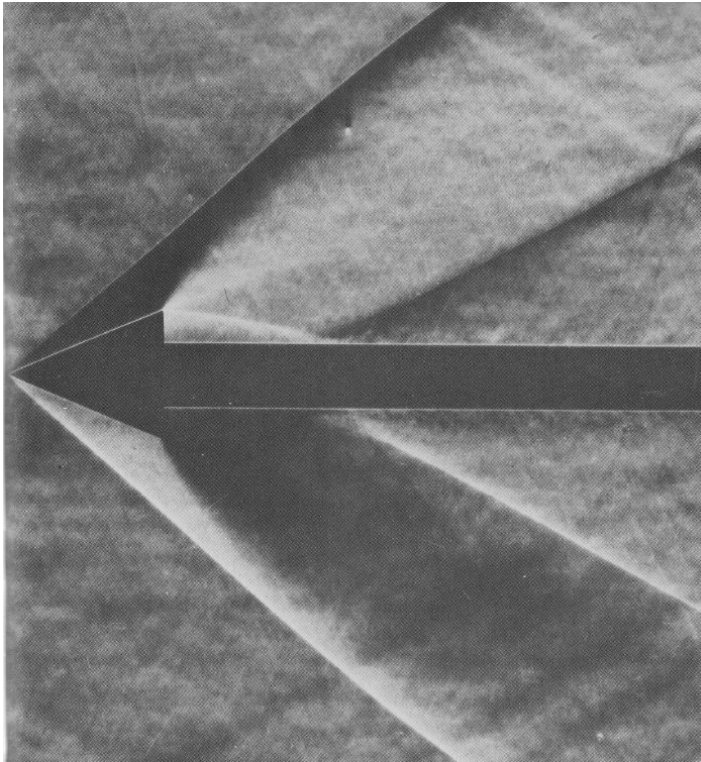
Reminder: Oblique shock chart ($\gamma=1.4$, simplified)



- For every M_1 there is a maximum turning angle θ_{max}

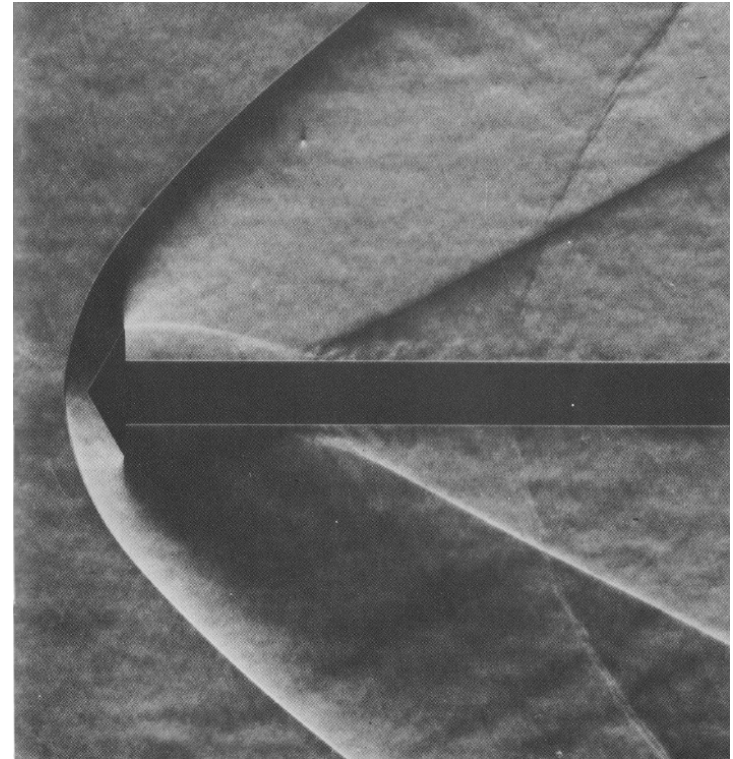
If your turning angle is greater than θ_{max} your shock will detach

M=1.96 flow over a cone



$$\theta = 22.5^\circ$$

Attached oblique shock

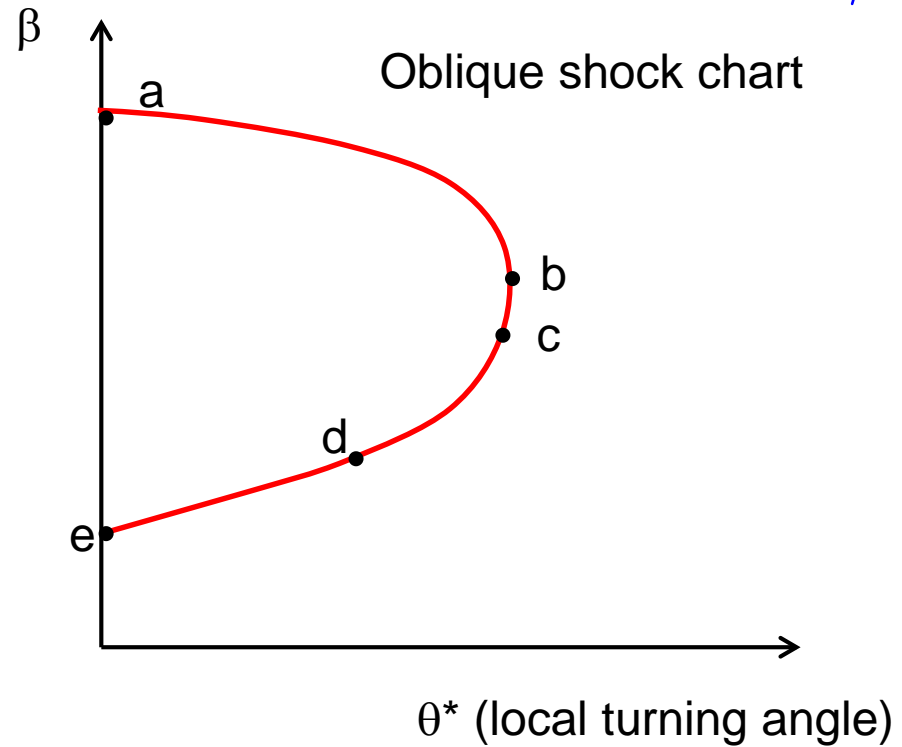
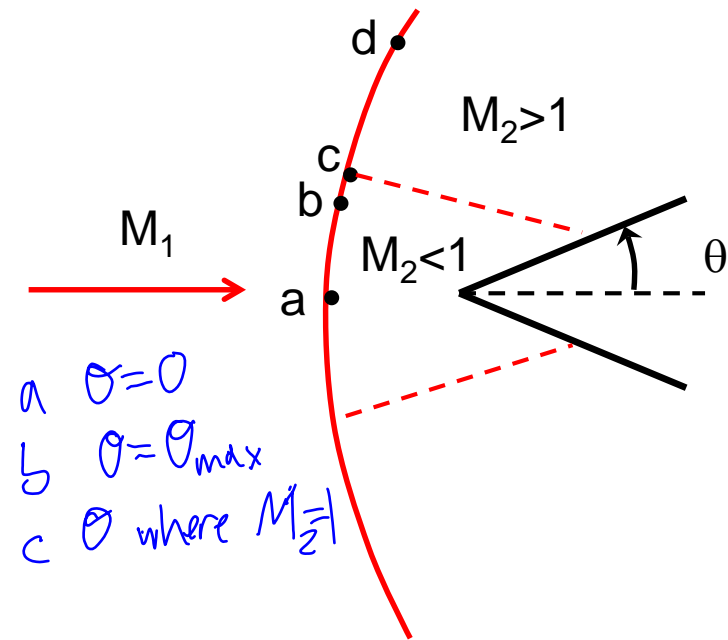


$$\theta = 60^\circ$$

Detached curved shock

$$\theta_{\max} \approx 23^\circ$$

Flow past a cone or 2D wedge for $\theta > \theta_{\max}$ (detached shock)



- a: flow through a normal shock wave
- b: maximum turning angle
- c: limiting case $M_2 = 1$
- d: weak solution
- e: Mach wave (far from object)

detached shocks work with many θ solutions hence the curve.