

SESA3029

Aerothermodynamics

Lecture 5.6

1D finite difference methods for
transient problems

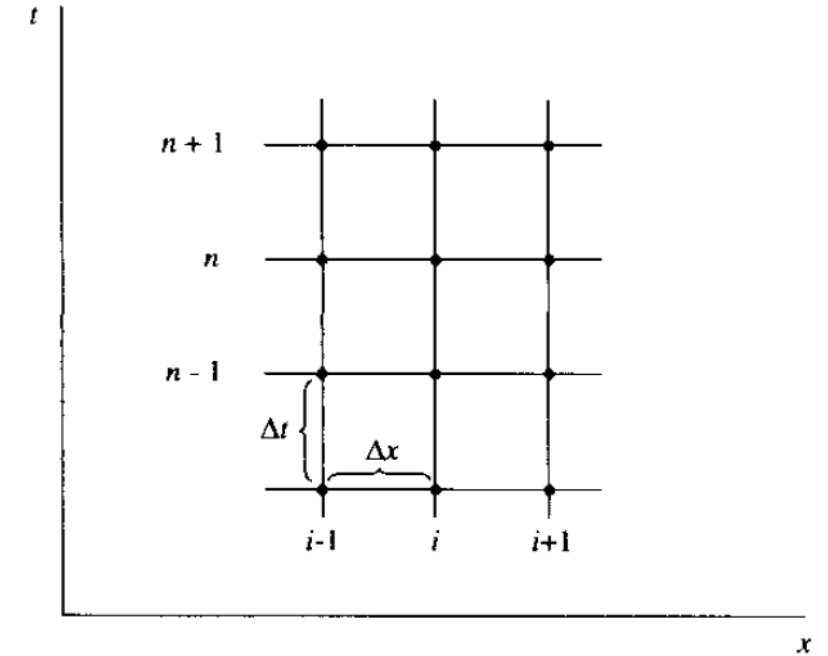
Explicit method

1D, no heat source $\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$

Now use a discrete finite difference grid with point-wise values T_i^n

Use a forward difference in time and approximate $\frac{\partial^2 T}{\partial x^2}$ at old time level n .

$$\frac{T_{i+1}^n - 2T_i^n + T_{i-1}^n}{\Delta x^2} = \frac{1}{\alpha} \frac{T_i^{n+1} - T_i^n}{\Delta t}$$



Introducing the Fourier number $F = \frac{\Delta t}{\Delta x^2} \alpha$ gives the iteration rule

$$T_i^{n+1} = T_i^n + F(T_{i+1}^n - 2T_i^n + T_{i-1}^n) \quad (4)$$

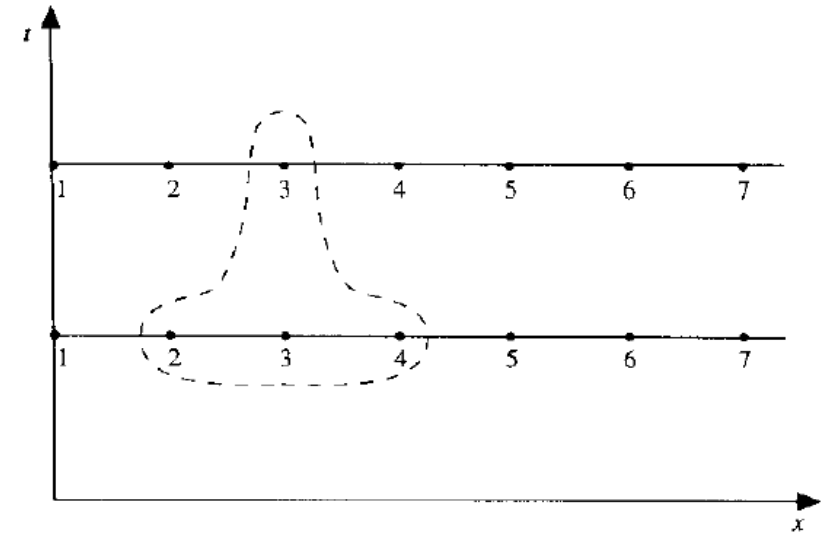
The developed method is explicit in time.

Choice of time steps

The dependency of each value on previous ones is visualised on the left.

This is a simple iteration scheme and just marching forward with a suitable time step Δt gives a time-accurate transient solution.

For steady problems a solution can be approximated by marching forward in (pseudo-)time until convergence.



Stability – von Neumann analysis (see FEEG6005):

Inserting a single Fourier mode $B(t) e^{ikx}$ into the iteration (4) formula, shows that the method is stable for

$$F \leq \frac{1}{2} \quad \text{or} \quad \Delta t \leq \frac{\Delta x^2}{2\alpha}$$

Discrete boundary conditions

Constant temperature: $T_0^{n+1} = T_{sl}$, $T_I^{n+1} = T_{sr}$

Surface convection on the left: $-k \frac{\partial T}{\partial x} \Big|_0 = h[T_\infty - T_0]$

$$\frac{\frac{\partial T}{\partial x} \Big|_{1/2} - \frac{\partial T}{\partial x} \Big|_0}{1/2 \Delta x} = \frac{1}{\alpha} \frac{\partial T}{\partial t} \rightarrow \frac{\frac{T_1^n - T_0^n}{\Delta x} - \left(-\frac{h}{k} [T_\infty - T_0^n] \right)}{1/2 \Delta x} = \frac{1}{\alpha} \frac{T_0^{n+1} - T_0^n}{\Delta t}$$

yields

$$T_0^{n+1} = T_0^n + 2F \left(T_1^n - \left(1 + \frac{h\Delta x}{k} \right) T_0^n + \frac{h\Delta x}{k} T_\infty \right)$$

On the right:

$$T_I^{n+1} = T_I^n + 2F \left(T_{I-1}^n - \left(1 + \frac{h\Delta x}{k} \right) T_I^n + \frac{h\Delta x}{k} T_\infty \right)$$

Adiabatic: $h = 0$ Constant surface heat flux: $h = 0$, $T_\infty = \frac{\dot{q}_x}{h}$

Explicit scheme for heat diffusion equation

Use forward difference for $\left(\frac{\partial T}{\partial t}\right)_i^n = \frac{T_i^{n+1} - T_i^n}{\Delta t} + O(\Delta t)$

and the previous central difference to approximate the entire equation as

$$0 = \frac{1}{\alpha} \frac{\partial T}{\partial t} - \frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{T_i^{n+1} - T_i^n}{\Delta t} + O(\Delta t) - \frac{T_{i+1}^n - 2T_i^n + T_{i-1}^n}{\Delta x^2} + O(\Delta x^2)$$

Taylor-series expansion yields

$$0 = \frac{1}{\alpha} \frac{T_i^{n+1} - T_i^n}{\Delta t} - \frac{T_{i+1}^n - 2T_i^n + T_{i-1}^n}{\Delta x^2} - \left[-\left(\frac{\partial^2 T}{\partial t^2}\right)_i^n \frac{\Delta t}{2\alpha} + \left(\frac{\partial^4 T}{\partial x^4}\right)_i^n \frac{\Delta x^2}{12} + \dots \right]$$

The truncation error of this method is $O(\Delta t, \Delta x^2)$.

The method is overall first-order accurate. (**Order of accuracy**)

The method is **consistent** with the original equation as for $\Delta t \rightarrow 0$ and $\Delta x \rightarrow 0$ the original equation is recovered.

Example

A thick slab of copper ($\alpha = 117 \cdot 10^{-6} \text{ m}^2/\text{s}$, $k = 401 \text{ W}/(\text{mK})$), initially at 20°C , is subjected to a constant net heat flux of $\dot{q}_x = 3 \cdot 10^5 \text{ W}/\text{m}^2$ at one surface.

Determine the temperatures at the surface and 150 mm from the surface after an elapsed time of 2 min.

Solution approach:

- For $\Delta x = 75 \text{ mm}$ and $F = \frac{1}{2} \rightarrow \Delta t \approx 24 \text{ s}$
- Chose number of time steps as $N = 5, 10, 20, 40 \dots$ for $F = \frac{1}{2}, \frac{1}{4}, \frac{1}{8}, \frac{1}{16}, \dots$
- Use at least $l \geq N$ to allow application of const. $T_0 = 20^\circ\text{C}$ as boundary condition on right
- Evaluate Δx from F and use overall length $L = l \Delta x$

From Bergman et al., p. 340ff / Incropera et al., p. 312ff.

Explicit Finite-Difference Solution for $Fo = \frac{1}{2}$

| p | $t(s)$ | T_0 | T_1 | T_2 | T_3 | T_4 |
|-----|--------|-------|-------|-------|-------|-------|
| 0 | 0 | 20 | 20 | 20 | 20 | 20 |
| 1 | 24 | 76.1 | 20 | 20 | 20 | 20 |
| 2 | 48 | 76.1 | 48.1 | 20 | 20 | 20 |
| 3 | 72 | 104.2 | 48.1 | 34.0 | 20 | 20 |
| 4 | 96 | 104.2 | 69.1 | 34.0 | 27.0 | 20 |
| 5 | 120 | 125.2 | 69.1 | 48.1 | 27.0 | 23.5 |

| Method | $T_0 = T(0, 120 \text{ s})$ | $T_2 = T(0.15 \text{ m}, 120 \text{ s})$ |
|---------------------------------|-----------------------------|--|
| Explicit ($Fo = \frac{1}{2}$) | 125.2 | 48.1 |
| Explicit ($Fo = \frac{1}{4}$) | 118.8 | 44.4 |
| Implicit ($Fo = \frac{1}{2}$) | 114.7 | 44.2 |
| Exact | 120.0 | 45.4 |

Explicit Finite-Difference Solution for $Fo = \frac{1}{4}$

| p | $t(s)$ | T_0 | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 |
|-----|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |
| 1 | 12 | 48.1 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |
| 2 | 24 | 62.1 | 27.0 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |
| 3 | 36 | 72.6 | 34.0 | 21.8 | 20 | 20 | 20 | 20 | 20 | 20 |
| 4 | 48 | 81.4 | 40.6 | 24.4 | 20.4 | 20 | 20 | 20 | 20 | 20 |
| 5 | 60 | 89.0 | 46.7 | 27.5 | 21.3 | 20.1 | 20 | 20 | 20 | 20 |
| 6 | 72 | 95.9 | 52.5 | 30.7 | 22.5 | 20.4 | 20.0 | 20 | 20 | 20 |
| 7 | 84 | 102.3 | 57.9 | 34.1 | 24.1 | 20.8 | 20.1 | 20.0 | 20 | 20 |
| 8 | 96 | 108.1 | 63.1 | 37.6 | 25.8 | 21.5 | 20.3 | 20.0 | 20.0 | 20 |
| 9 | 108 | 113.6 | 67.9 | 41.0 | 27.6 | 22.2 | 20.5 | 20.1 | 20.0 | 20.0 |
| 10 | 120 | 118.8 | 72.6 | 44.4 | 29.6 | 23.2 | 20.8 | 20.2 | 20.0 | 20.0 |

Implicit method

Now use only values at new time level $n+1$ in the spatial finite difference $\frac{\partial^2 T}{\partial x^2}$

$$\frac{T_{i+1}^{n+1} - 2T_i^{n+1} + T_{i-1}^{n+1}}{\Delta x^2} = \frac{1}{\alpha} \frac{T_i^{n+1} - T_i^n}{\Delta t}$$

yields eventually

$$T_{i+1}^{n+1} - \left(2 + \frac{1}{F}\right) T_i^{n+1} + T_{i-1}^{n+1} = -\frac{1}{F} T_i^n$$

The method is implicit in time.

Constant temperature BCs: $T_0^{n+1} = T_{sl}$, $T_l^{n+1} = T_{sr}$

Surface convection BCs:

$$T_1^{n+1} - \left(1 + \frac{h\Delta x}{k} + \frac{1}{2F}\right) T_0^{n+1} = -\frac{1}{2F} T_0^n - \frac{h\Delta x}{k} T_\infty$$
$$T_{l-1}^{n+1} - \left(1 + \frac{h\Delta x}{k} + \frac{1}{2F}\right) T_l^{n+1} = -\frac{1}{2F} T_l^n - \frac{h\Delta x}{k} T_\infty$$

Solution process

Starting from the initial conditions T_i^0 , solve the linear problem (here for surface convection boundary conditions) successively, using the data from the previous time step n in the right-hand side

$$\begin{pmatrix} -\left(1 + \frac{h_l \Delta x}{k} + \frac{1}{2F}\right) & 1 & 0 & \dots & 0 \\ 1 & -\left(2 + \frac{1}{F}\right) & 1 & 0 & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & 0 & 1 & -\left(2 + \frac{1}{F}\right) & 1 \\ 0 & \dots & 0 & 1 & -\left(1 + \frac{h_r \Delta x}{k} + \frac{1}{2F}\right) \end{pmatrix} \begin{pmatrix} T_0^{n+1} \\ \vdots \\ T_l^{n+1} \end{pmatrix} = \begin{pmatrix} -\frac{1}{2F} T_0^n - \frac{h_l \Delta x}{k} T_{\infty l} \\ -\frac{1}{F} T_1^n \\ \vdots \\ -\frac{1}{F} T_{l-1}^n \\ -\frac{1}{2F} T_l^n - \frac{h_r \Delta x}{k} T_{\infty r} \end{pmatrix}$$

Δt can be chosen freely but should reflect the physical time scales of the problems, e.g., when boundary conditions are time dependent.