

# SESA3029 Aerothermodynamics

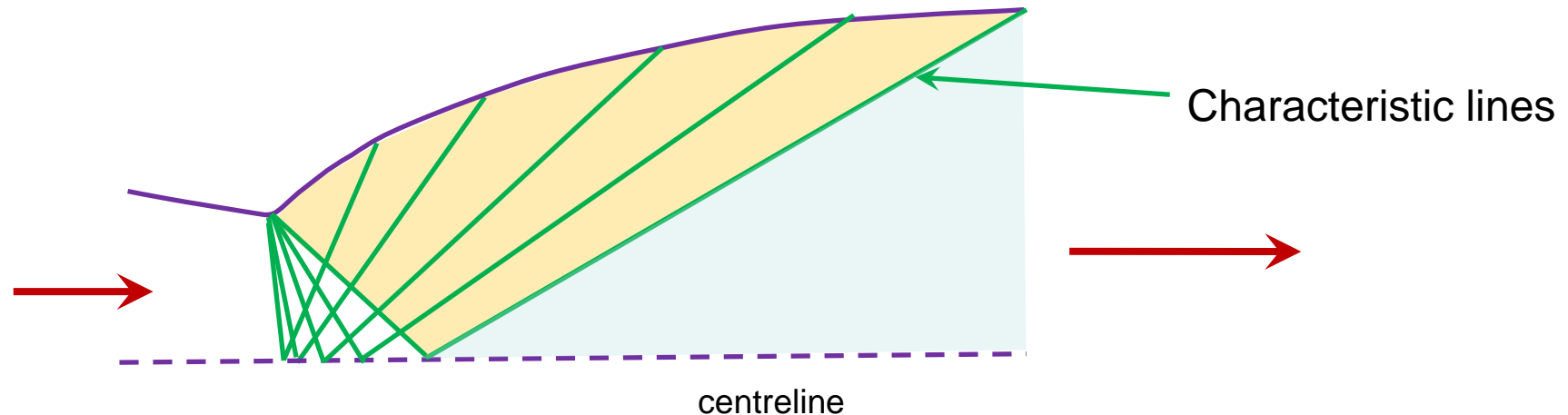
## Lecture 3.1

Method of characteristics:  
theory (part A)

# Objective

everywhere has same entropy  
(isentropic on every thing)

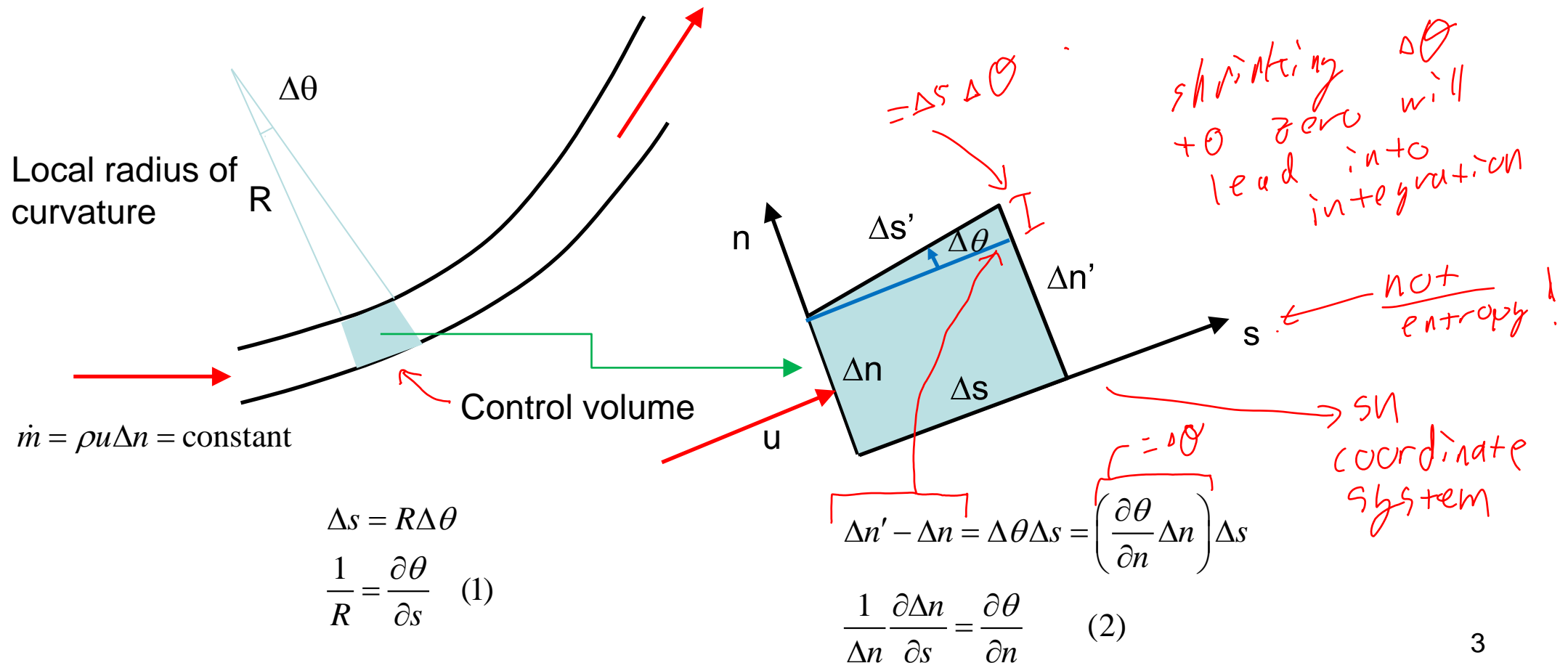
- Introduce the equations for steady flow with entropy constant everywhere (defined as 'homentropic' flow')
  - Enables a simpler derivation of the method of characteristics
  - Eventually we will have method for nozzle design



# Curved streamtube

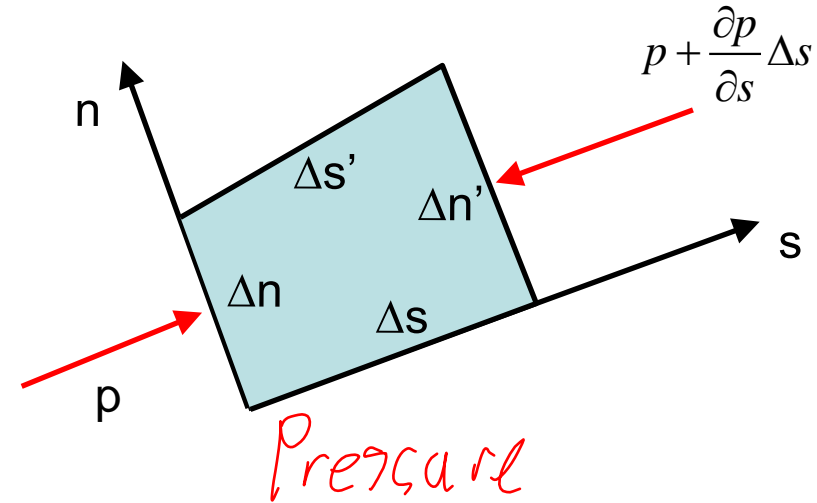
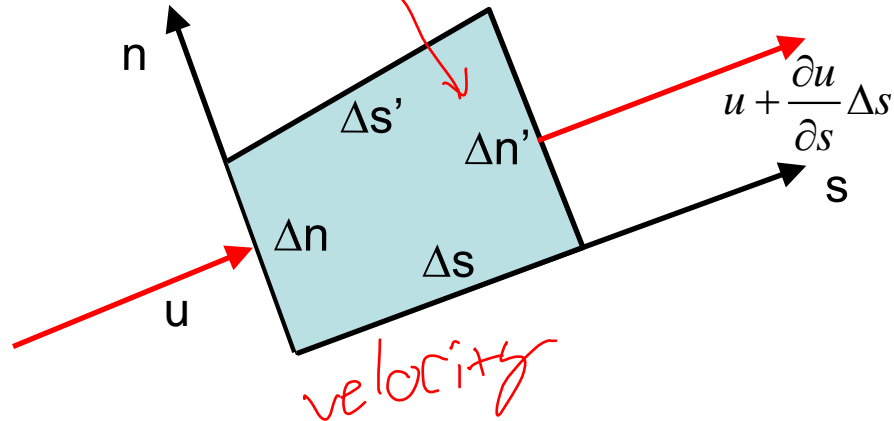
No flow across streamlines, therefore for steady flow  
mass flowrate in = mass flowrate out

similar to  
last year  
aerodynamics



can be diverging  
or  
converging  
(compressible)

# Euler s-equation



s-momentum out – s-momentum in = force applied in s direction

$$\dot{m} \left[ u + \frac{\partial u}{\partial s} \Delta s \right] - \dot{m} u = - \left( \frac{\partial p}{\partial s} \Delta s \right) \Delta n$$

(highest order  
term only on RHS)

$$\dot{m} = \rho u \Delta n$$

sub  
in

hence

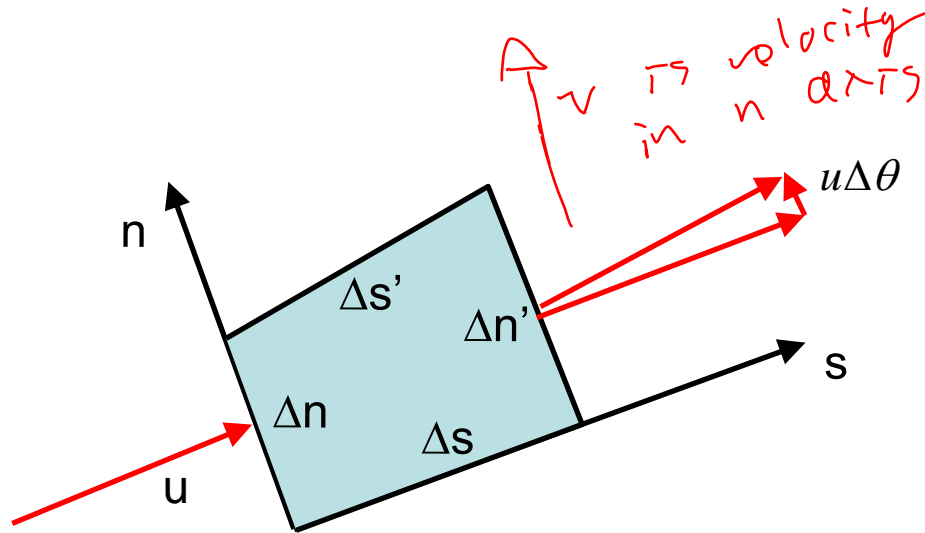
becomes

$$\rho u \frac{\partial u}{\partial s} = - \frac{\partial p}{\partial s}$$

euler  
equation

which integrates for Bernoulli's equation for constant density

# Vorticity $\omega$



Cartesian co-ordinate form

$$\omega = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$$

Here, if  $x, y$  are originally aligned with  $s, n$  we have  $dv = u d\theta$

conversion

$$\omega = u \frac{\partial \theta}{\partial s} - \frac{\partial u}{\partial n}$$

# Mass conservation

$$\dot{m} = \rho u \Delta n = \left( \rho + \frac{\partial \rho}{\partial s} \Delta s \right) \left( u + \frac{\partial u}{\partial s} \Delta s \right) \left( \Delta n + \frac{\partial \Delta n}{\partial s} \Delta s \right)$$

$$= \rho u \Delta n + \rho u \frac{\partial \Delta n}{\partial s} \Delta s + \rho \Delta n \frac{\partial u}{\partial s} \Delta s + u \Delta n \frac{\partial \rho}{\partial s} \Delta s$$

$$0 = \frac{1}{\Delta n} \frac{\partial \Delta n}{\partial s} + \frac{1}{u} \frac{\partial u}{\partial s} + \frac{1}{\rho} \frac{\partial \rho}{\partial s}$$

*Divide by  $\rho u \Delta n$  and rearrange*

Finally, using (2)

*↓  
prev  
equation*

$$\frac{\partial \theta}{\partial n} + \frac{1}{u} \frac{\partial u}{\partial s} + \frac{1}{\rho} \frac{\partial \rho}{\partial s} = 0$$

# Combine mass conservation and Euler-s equation

Euler s-  
equation

$$\rho u \frac{\partial u}{\partial s} = - \frac{\partial p}{\partial s}$$

Continuity

$$\frac{\partial \theta}{\partial n} + \frac{1}{u} \frac{\partial u}{\partial s} + \frac{1}{\rho} \frac{\partial \rho}{\partial s} = 0$$

Homentropic  
flow

$$\rho u \frac{\partial u}{\partial s} = - \left( \frac{\partial p}{\partial \rho} \right)_s \frac{\partial \rho}{\partial s}$$

$$\frac{\partial \rho}{\partial s} = - \rho \left( \frac{\partial \theta}{\partial n} + \frac{1}{u} \frac{\partial u}{\partial s} \right)$$

$$\rho u \frac{\partial u}{\partial s} = - a^2 \frac{\partial \rho}{\partial s}$$

substitute

$$u \frac{\partial u}{\partial s} = a^2 \left( \frac{\partial \theta}{\partial n} + \frac{1}{u} \frac{\partial u}{\partial s} \right)$$

Mach  
number

$$\left( \frac{u^2}{a^2} - 1 \right) \frac{1}{u} \frac{\partial u}{\partial s} = \frac{\partial \theta}{\partial n}$$

just re-arrange

constant  
entropy  
pressure-density  
gradient

# 2 equations in 2 unknowns

Recalling that

$$\tan \mu = \frac{1}{\sqrt{M^2 - 1}}$$

$$\text{and } \tan \mu dv = \frac{du}{u}$$

From Mach triangle

from Prandtl-Meyer  
(lecture 2.4, slide 4):

$$\frac{dV}{V} = \frac{d\theta_{PM}}{\sqrt{M^2 - 1}} = \tan \mu dv$$

$$(M^2 - 1) \frac{1}{u} \frac{\partial u}{\partial s} = \frac{\partial \theta}{\partial n}$$

becomes

$$\frac{1}{\tan \mu} \frac{\partial v}{\partial s} = \frac{\partial \theta}{\partial n}$$

We already have another  
equation relating  $u$  and  $\theta$   
from the definition of vorticity

$$\omega = u \frac{\partial \theta}{\partial s} - \frac{\partial u}{\partial n} = 0$$

(irrotational flow)

$$\text{hence } \frac{\partial v}{\partial s} - \tan \mu \frac{\partial \theta}{\partial n} = 0 \quad \text{and} \quad \frac{\partial \theta}{\partial s} - \tan \mu \frac{\partial v}{\partial n} = 0$$

Set of hyperbolic equations for  $u, v$

combine

expansion  
fan proof

Mach angle

doppler type stuff

$\mu$  is mach cone  
thingy



Mach  
triangle

NOTES!



# Homentropic flow in $(\theta, v)$ variables

*diagonalising equations?*

$$\frac{\partial v}{\partial s} - \tan \mu \frac{\partial \theta}{\partial n} = 0$$

$$\frac{\partial \theta}{\partial s} - \tan \mu \frac{\partial v}{\partial n} = 0$$

In matrix form:

$$\frac{\partial}{\partial s} \begin{pmatrix} v \\ \theta \end{pmatrix} + \begin{pmatrix} 0 & -\tan \mu \\ -\tan \mu & 0 \end{pmatrix} \frac{\partial}{\partial n} \begin{pmatrix} v \\ \theta \end{pmatrix} = 0$$

*Q is a  
single vector*

$$\frac{\partial \mathbf{Q}}{\partial s} + \mathbf{A} \frac{\partial \mathbf{Q}}{\partial n} = 0$$

The character of the solution will be determined by the properties of A

# Eigenvalues of **A**

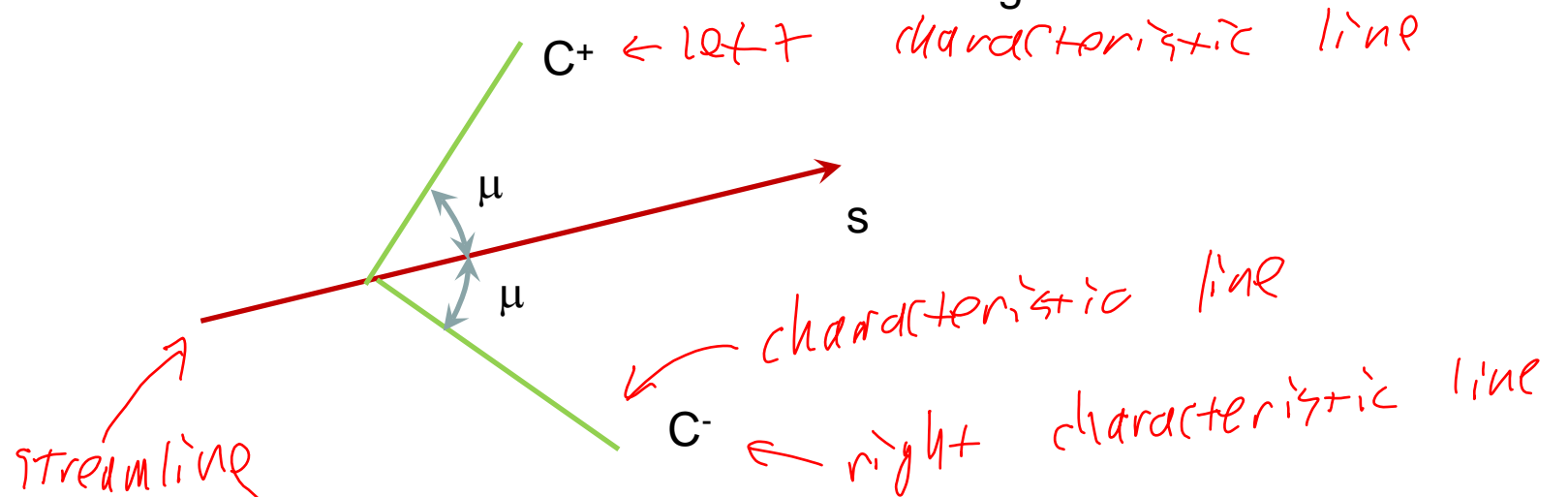
$$\det(\mathbf{A} - \mathbf{I}\lambda) = 0$$

solve determinant (easy)

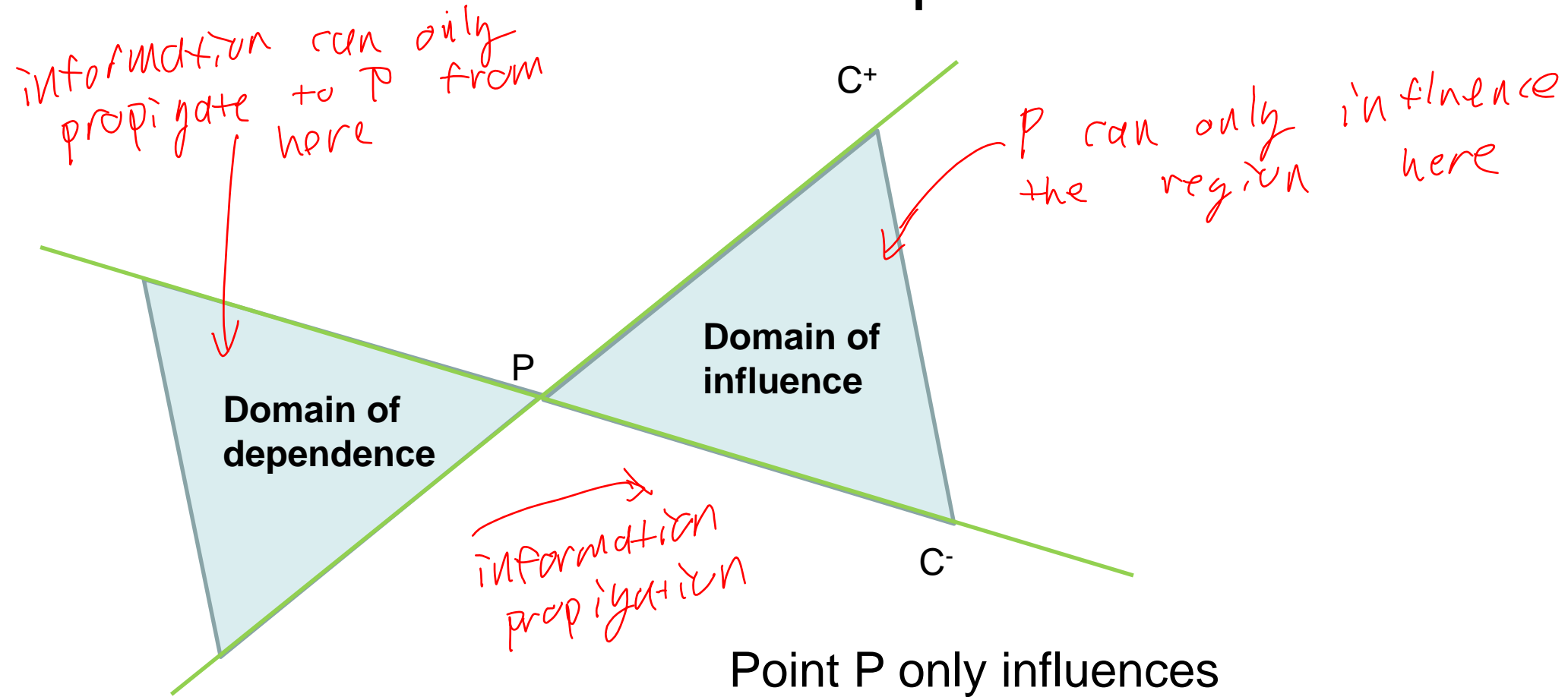
$$\begin{vmatrix} -\lambda & -\tan \mu \\ -\tan \mu & -\lambda \end{vmatrix} = 0$$

$$\lambda = \pm \tan \mu$$

i.e. the slopes of the Mach lines are the eigenvalues



# Domains of influence and dependence



Flow state at  $P$  only depends on events in the domain of dependence

Point  $P$  only influences events in the domain of influence

# Summary

- Homentropic irrotational steady supersonic flow has an underlying structure governed by its eigenvalues
- Characteristics are oriented at the Mach angle relative to the flow direction
- Next time: exploit this to form the Method of Characteristics (MoC)