

SESA3029

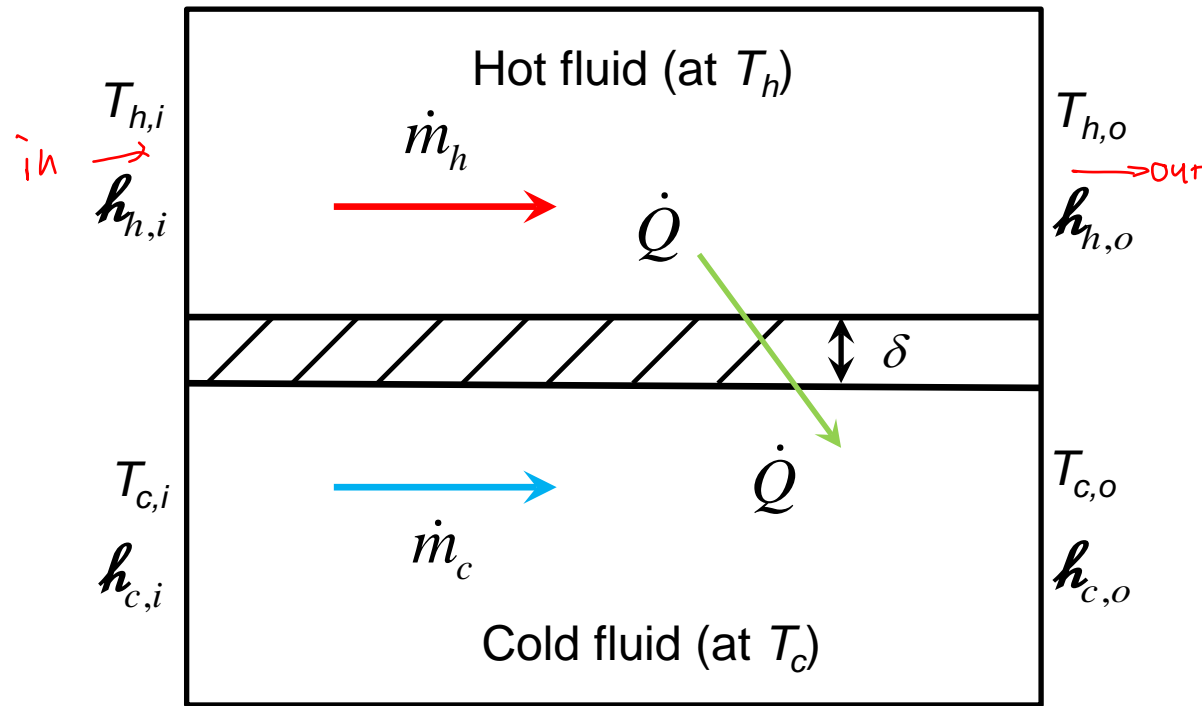
Aerothermodynamics

Lecture 5.8

Heat exchangers -

Log mean temperature difference method

Heat exchanger – General equations



h: hot
c: cold
i: inlet
o: outlet
 \dot{m} : mass flow
 h : enthalpy
 C_p : fluid heat capacity

Parallel-flow heat exchanger depicted but (1) and (2) are the same for the counter-flow heat exchanger!

Evaluation of heat transfer rate with inlet and outlet temperatures:

$$\dot{Q} = \dot{m}_h (h_{h,i} - h_{h,o}) = \dot{m}_h c_{p,h} (T_{h,i} - T_{h,o}) = C_h (T_{h,i} - T_{h,o}) \quad (1)$$

$$\dot{Q} = \dot{m}_c (h_{c,o} - h_{c,i}) = \dot{m}_c c_{p,c} (T_{c,o} - T_{c,i}) = C_c (T_{c,o} - T_{c,i}) \quad (2)$$

C_h and C_c are the **capacities**. *→ non-specific constant pressure heat capacity*

← obviously heat is conserved

Heat exchanger – General equations

On a unit area basis:

h_h and h_c are the heat transfer coefficients on **h**ot and **c**old side and k_w is the wall conductivity

In practice δ is usually taken as 0

series resistance?

$$\left[\frac{1}{h'} = \frac{1}{h_h} + \frac{\delta}{k_w} + \frac{1}{h_c} \right]$$

Since the temperature difference $\Delta T = T_h - T_c$ is spatially varying, a suitable **mean** temperature difference needs to be found to evaluate the heat transfer rate of the overall system as

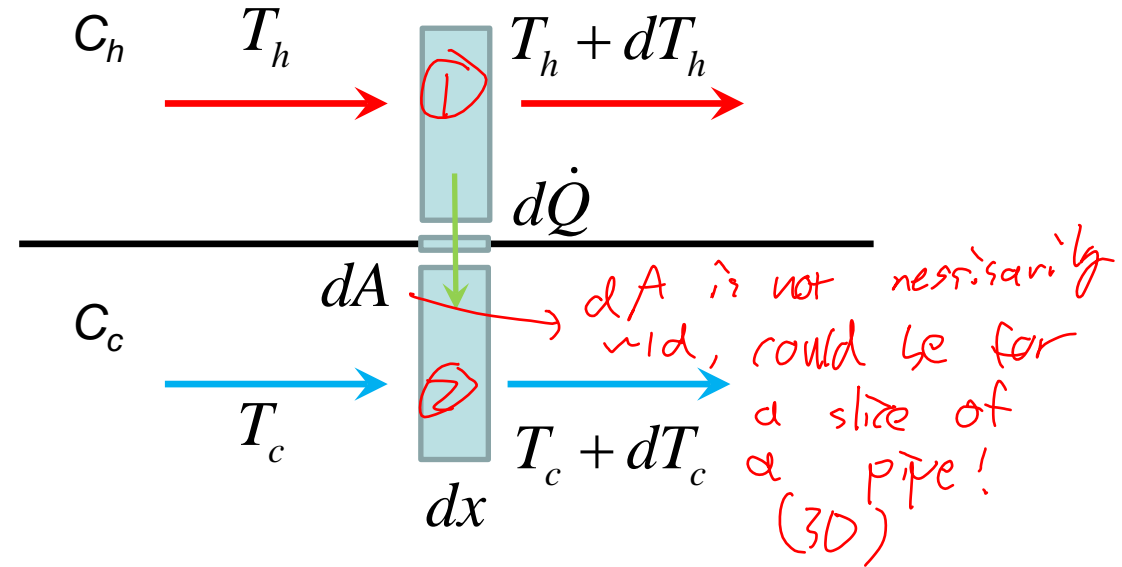
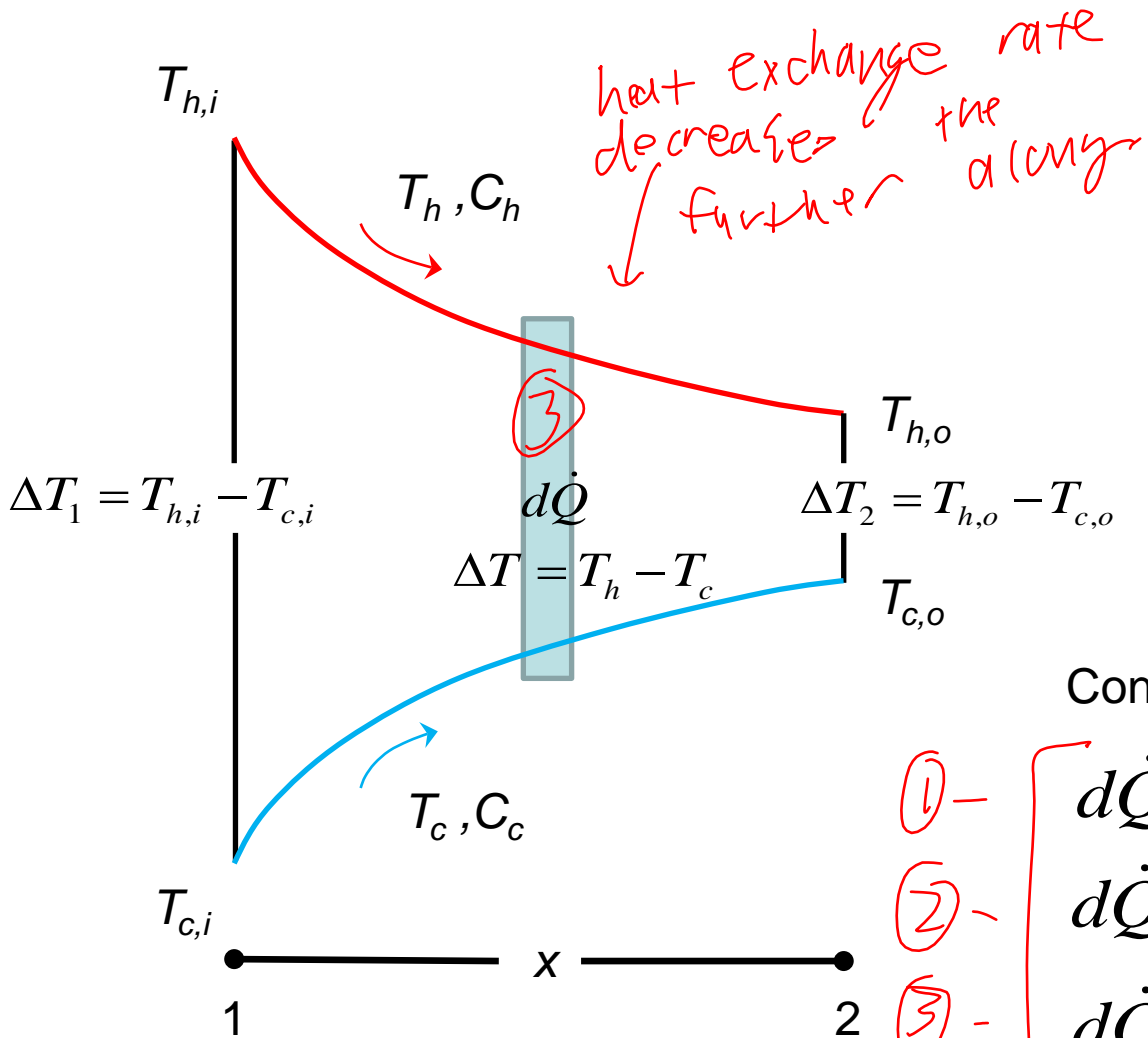
$$\dot{Q} = h' A \Delta T_m$$

This leads to the *log mean temperature difference* method.

Derivation follows Bergman et al., pages 713-715 / Incropera et al., pages 659-662 closely.

no separating solid boundary

Parallel-flow heat exchanger



Construct heat balance on elements dx dA :

① - $d\dot{Q} = -\dot{m}_h c_{p,h} dT_h = -C_h dT_h$ (3) heat loss side

② - $d\dot{Q} = \dot{m}_c c_{p,c} dT_c = C_c dT_c$ (4) heat absorbed side

③ - $d\dot{Q} = h' dA \Delta T$ (5) total temp diff ver

→ assume loss-less system

Starting from $d(\Delta T) = dT_h - dT_c$ and using (3) and (4) together with (5), we obtain

subbed in and rearranged →

$$d(\Delta T) = -h' dA \Delta T \left(\frac{1}{C_h} + \frac{1}{C_c} \right)$$

Now integrate from location 1 to 2, i.e.,

$$\int_1^2 \frac{d(\Delta T)}{\Delta T} = -h' \left(\frac{1}{C_h} + \frac{1}{C_c} \right) \int_1^2 dA$$

outlet (above 2) and *inlet* (below 1)

and use the general heat exchanger relations (1) and (2) to replace the capacities to obtain

$$\ln(\Delta T_2) - \ln(\Delta T_1) = -h'A \left(\frac{\cancel{Q} T_{h,i} - \cancel{Q} T_{h,o} + \cancel{Q} T_{c,o} - \cancel{Q} T_{c,i}}{\dot{Q}} \right) \quad (6)$$

Inserting $\Delta T_1, \Delta T_2$ for the parallel-flow heat exchanger gives

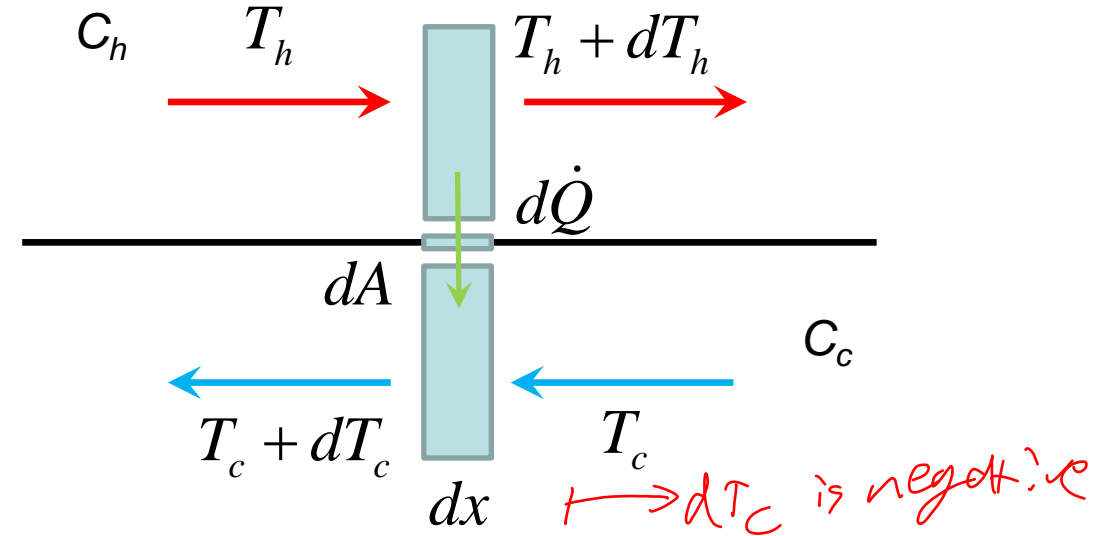
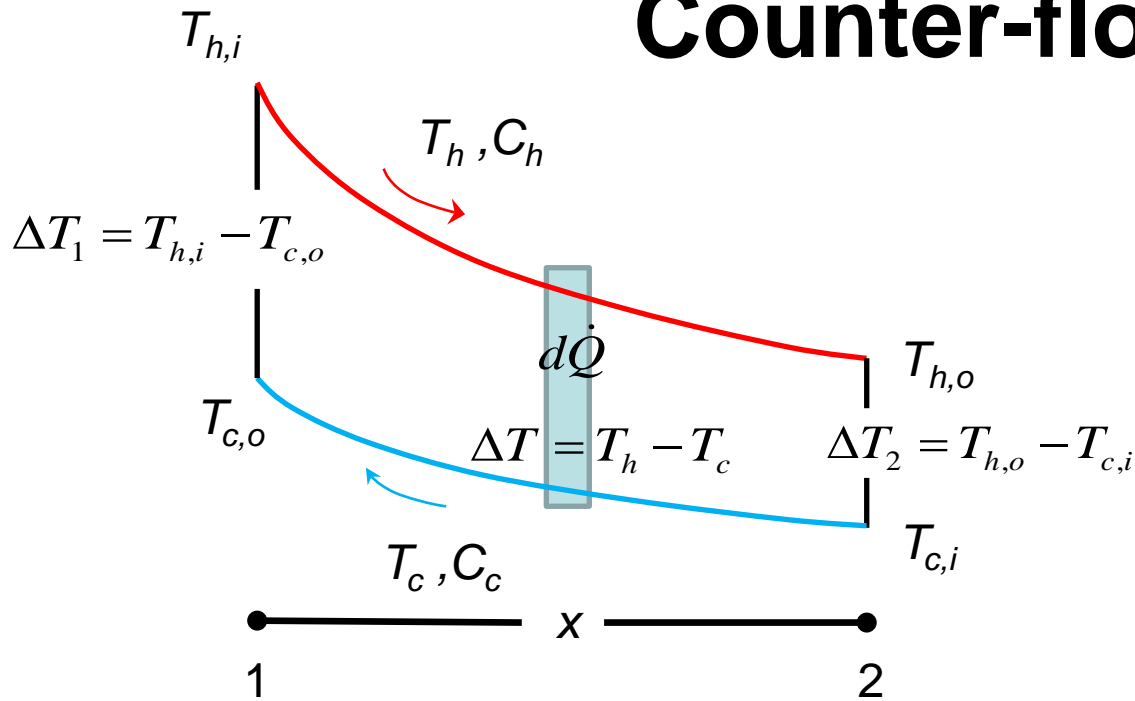
$$\ln \left(\frac{\Delta T_2}{\Delta T_1} \right) = -\frac{h'A}{\dot{Q}} (\Delta T_1 - \Delta T_2)$$

from which we readily deduce

$$\dot{Q} = h'A \Delta T_{lm} \quad \text{with} \quad \Delta T_{lm} = \frac{\Delta T_1 - \Delta T_2}{\ln(\Delta T_1 / \Delta T_2)}$$

logarithmically weighted temp difference (with arrow pointing to ΔT_{lm})

Counter-flow heat exchanger



Construct heat balance on elements dx dA : $d\dot{Q} = -\dot{m}_h c_{p,h} dT_h = -C_h dT_h$ (7)

$$d\dot{Q} = -\dot{m}_c c_{p,c} dT_c = -C_c dT_c$$
 (8)

Starting from $d(\Delta T) = dT_h - dT_c$ and using (7) and (8) together with (5), we obtain after integration from position 1 to 2

$$\ln(\Delta T_2) - \ln(\Delta T_1) = -\frac{h'A}{\dot{Q}} \left(\frac{T_{h,i} - T_{h,o}}{\dot{Q}} - \frac{T_{c,o} - T_{c,i}}{\dot{Q}} \right) \quad (9) \quad \text{i.e. } \dot{Q} = h'A \Delta T_{lm} \text{ with } \Delta T_{lm} \text{ as before.}$$

Remember differences in ΔT_1 and ΔT_2 !

Note that for this case the LMTD method is not applicable for $C_h = C_c$ and (5) needs to be integrated directly.

Example: Counter-flow heat exchanger

Cold flow: capacity rate $C_c=1500$ W/K, $h_c=275$ W/(m²K), $T_{c,i}=15^\circ\text{C}$

Hot flow: capacity rate $C_h=3000$ W/K, $h_h=400$ W/(m²K), $T_{h,i}=150^\circ\text{C}$

Find area A for which hot outlet temperature is $T_{h,o}=110^\circ\text{C}$.

1. Compute heat transfer rate from Eq. (1)

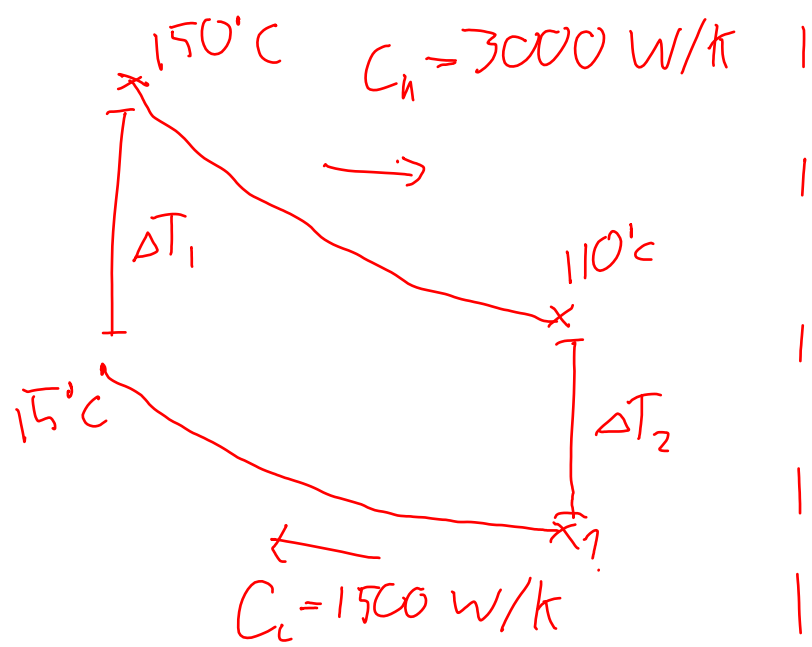
$$\dot{Q} = C_h (T_{h,i} - T_{h,o}) \rightarrow \dot{Q} = 3000 \text{ W/K} (150 - 110) \text{ K} = 120 \text{ kW}$$

2. Compute $T_{c,o}$ from Eq. (2)

$$\dot{Q} = C_c (T_{c,o} - T_{c,i}) \rightarrow T_{c,o} = T_{c,i} + \frac{\dot{Q}}{C_c} = 15^\circ\text{C} + \frac{120 \text{ kW}}{1500 \text{ W/K}} = 95^\circ\text{C}$$

3. Compute overall convective heat transfer rate (ignoring conduction)

$$\frac{1}{h'} = \frac{1}{h_c} + \frac{1}{h_h} = \frac{1}{275} + \frac{1}{400} \rightarrow h' = 162.963 \text{ W/(m}^2 \text{ K)}$$



$$\dot{Q} = C_h (T_{hi} - T_{ho}) = 120000 \text{ W}$$

$$\dot{Q} = C_c (T_{co} - T_{ci}) \rightarrow T_{co} = \frac{\dot{Q}}{C_c} + T_{ci} = T_{co} = 95^{\circ}\text{C}$$

Cold flow: capacity rate $C_c=1500 \text{ W/K}$, $h_c=275 \text{ W/(m}^2\text{K)}$, $T_{c,i}=15^\circ\text{C}$

Hot flow: capacity rate $C_h=3000 \text{ W/K}$, $h_h=400 \text{ W/(m}^2\text{K)}$, $T_{h,i}=150^\circ\text{C}$

4. Compute log mean temperature difference for counter-flow heat exchanger

$$\Delta T_1 = T_{h,i} - T_{c,o} = 150^\circ\text{C} - 95^\circ\text{C} = 55\text{K}$$

$$\Delta T_2 = T_{h,o} - T_{c,i} = 110^\circ\text{C} - 15^\circ\text{C} = 95\text{K}$$

$$\Delta T_{lm} = \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)} = \frac{95\text{K} - 55\text{K}}{\ln(95\text{K} / 55\text{K})} = 73.187\text{K}$$

5. Compute area from $\dot{Q} = h'A\Delta T_{lm}$

$$A = \frac{\dot{Q}}{h'\Delta T_{lm}} = \frac{120\text{kW}}{162.963\text{W/(m}^2\text{K)} \times 73.187\text{K}} = 10.06\text{m}^2$$

