

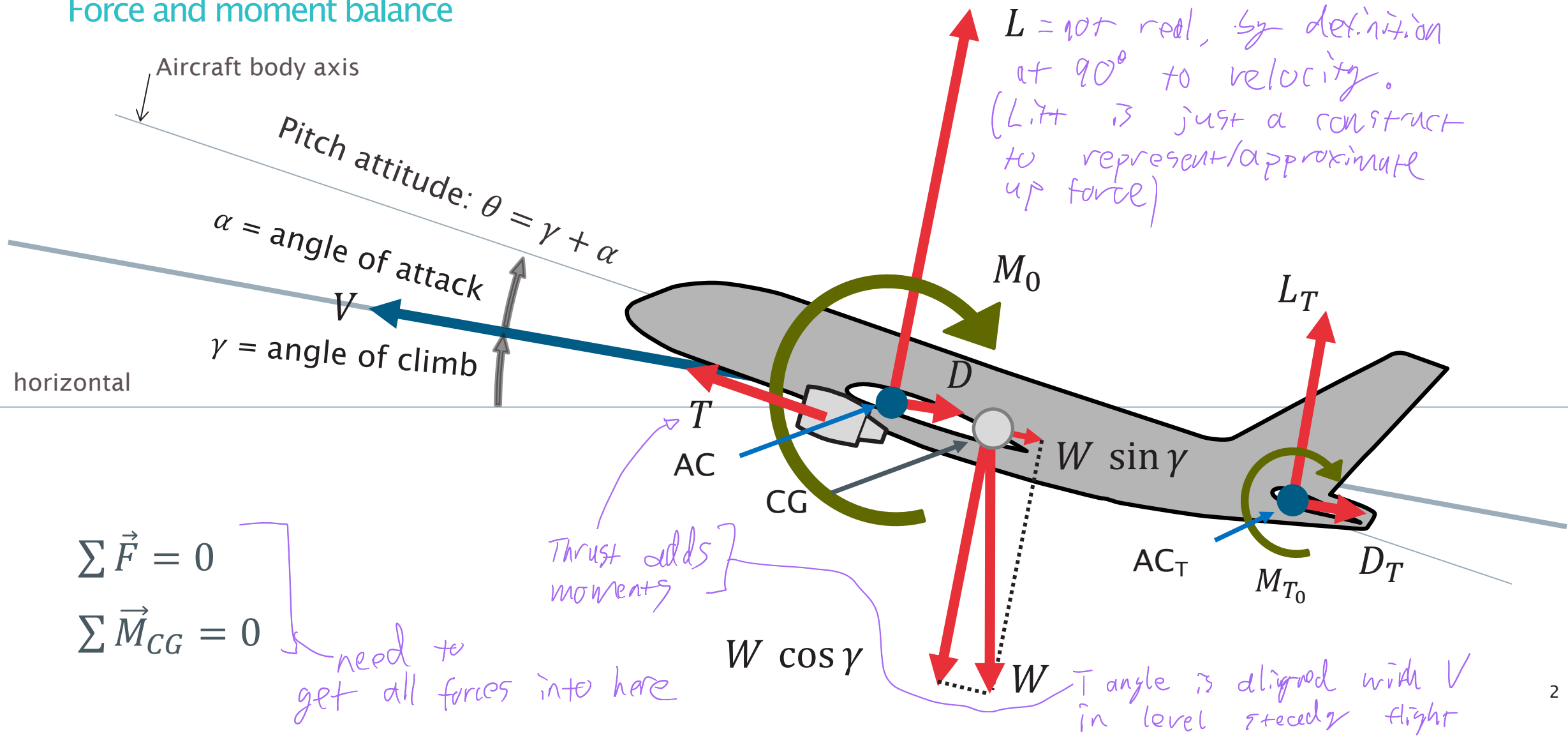
# SESA2025 Mechanics of Flight

## Equations of motion and tail plane equation

Lecture 1.1

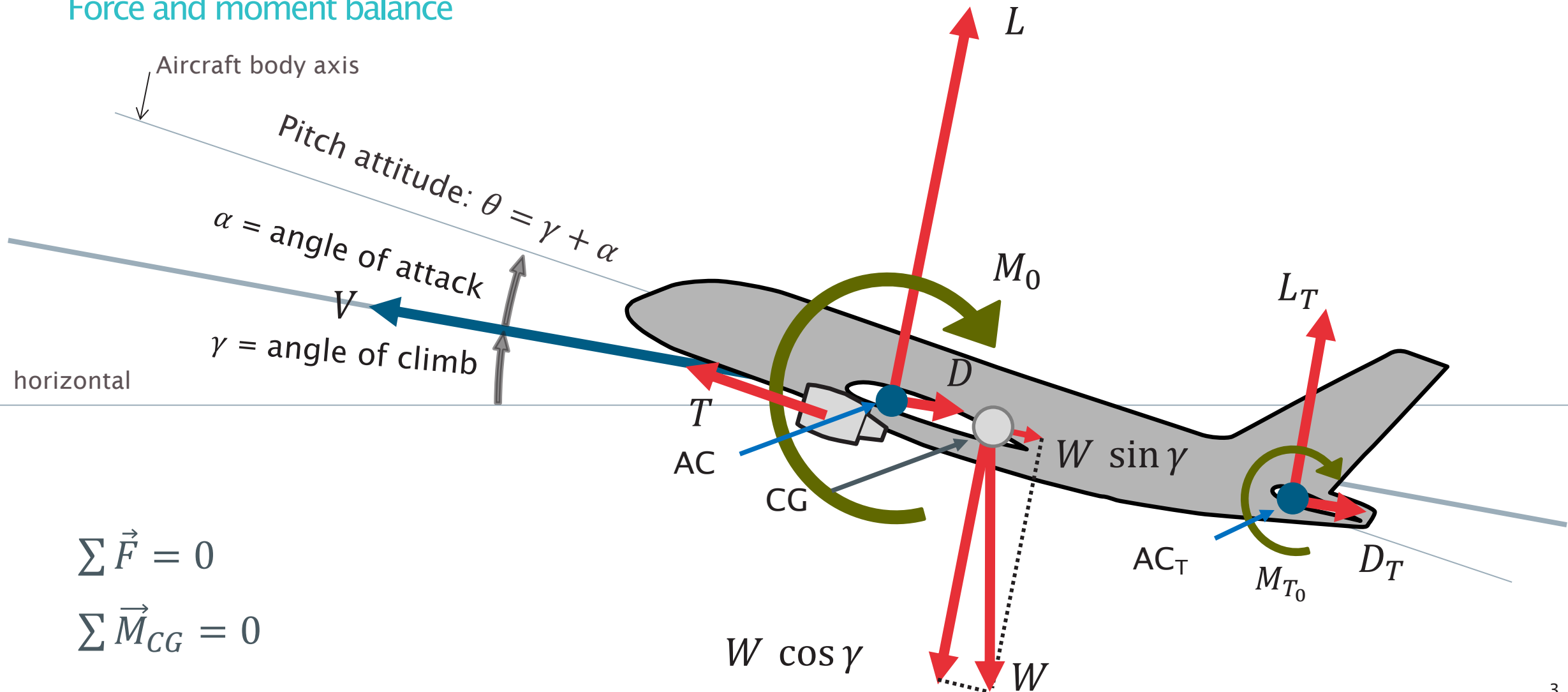
# Forces on an Aircraft (Steady, trimmed flight)

## Force and moment balance



# Forces on an Aircraft (Steady, trimmed flight)

## Force and moment balance



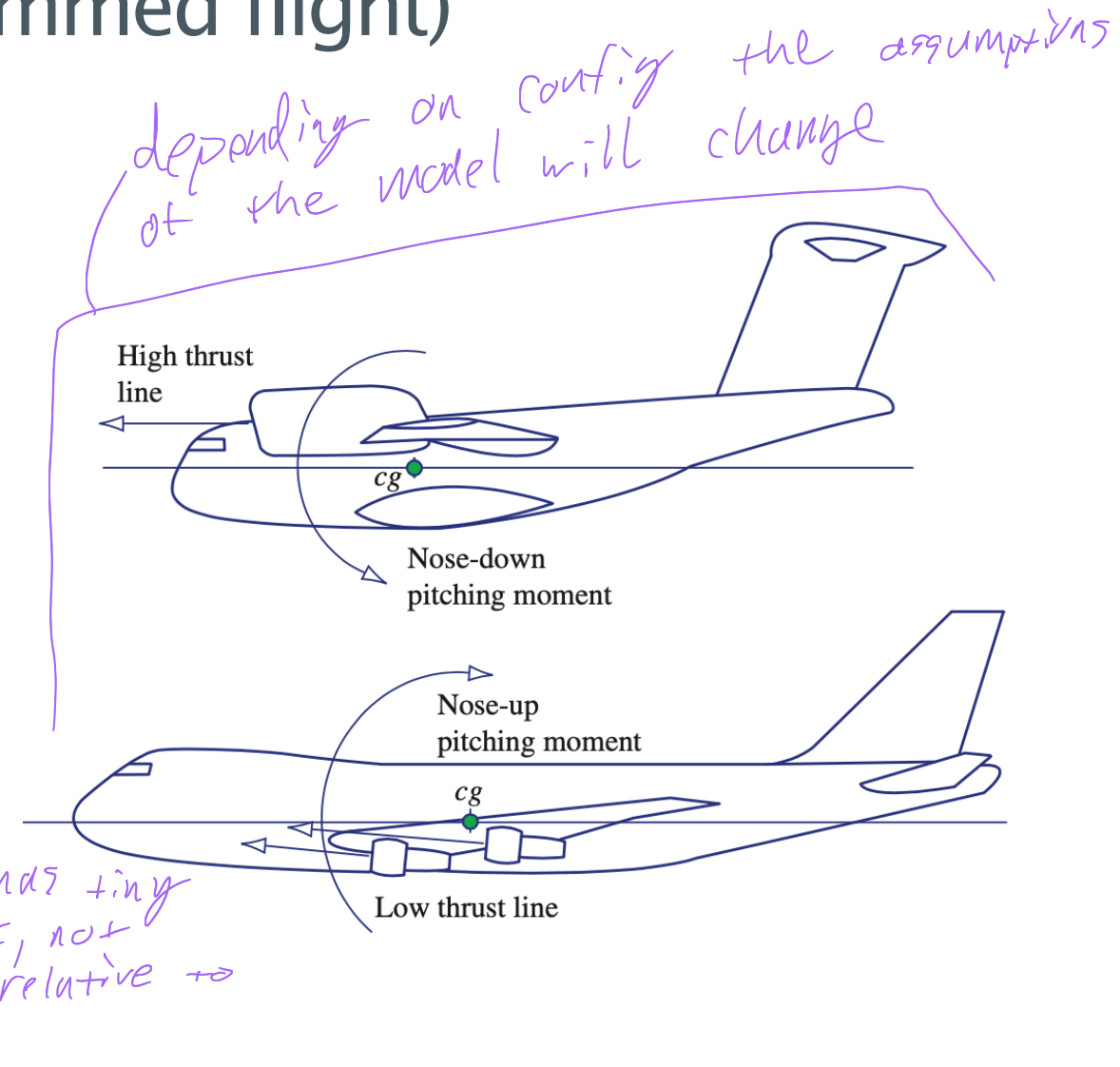
$$\sum \vec{F} = 0$$

$$\sum \vec{M}_{CG} = 0$$

# Forces on an Aircraft (Steady, trimmed flight)

## Simplifications and assumptions

- small angle of attack
  - $T, D, D_T, W \sin \gamma$  on the same axis
- balance along path
  - $T = D + D_T + W \sin \gamma$
- symmetrical (and small) tailplane
  - $M_{T_0} = 0$  } neglecting
- neglect moments by  $T, D, D_T$ 
  - see Cook sec 3.1.4



# Forces on an Aircraft (Steady, trimmed flight)

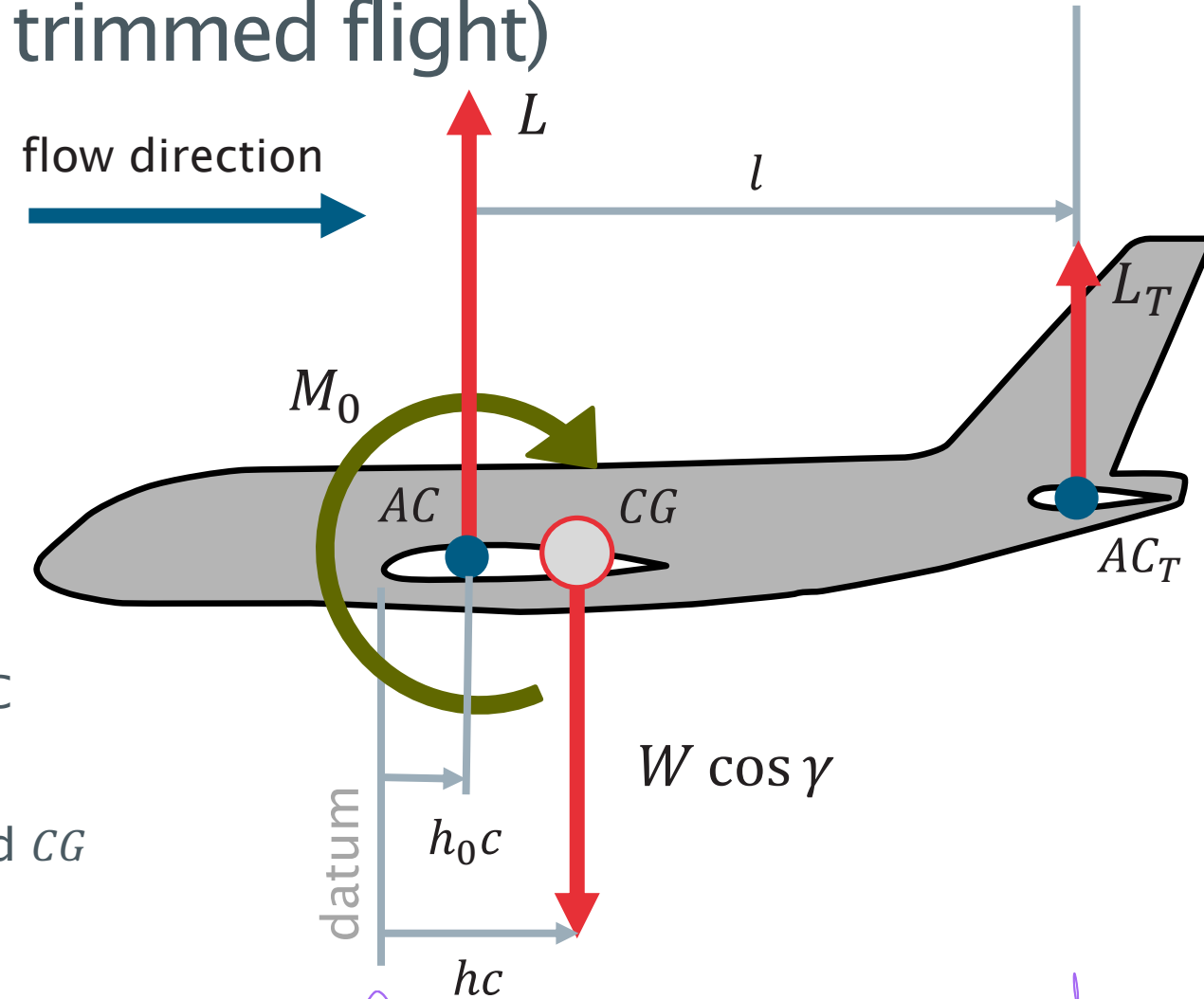
Final sketch

*simplified from prev to show assumptions*

Define positive directions

- $M_0$ : wing pitching moment about  $AC$  (+ve: nose up; constant with AoA)
- $l$ : distance from  $AC$  to  $AC_T$  (+ve: downstream)
- $h$ : distance from  $LE$  to  $CG$  divided by MAC (+ve: downstream)
- $h_0$ : distance from  $LE$  to  $AC$  divided by MAC (+ve: downstream)

Take force balance and moment balance around  $CG$



*somehow arbitrary datum used as reference for distance*

# Forces on an Aircraft (Steady, trimmed flight)

## Trim conditions

Aircraft in equilibrium  $\Rightarrow \sum \vec{F} = 0$ :

$$L + L_T - W \cos \gamma = 0$$

$$\left[ L^* \stackrel{\text{def}}{=} L + L_T \right] = W \cos \gamma$$

where  $L^*$  is the total aircraft lift

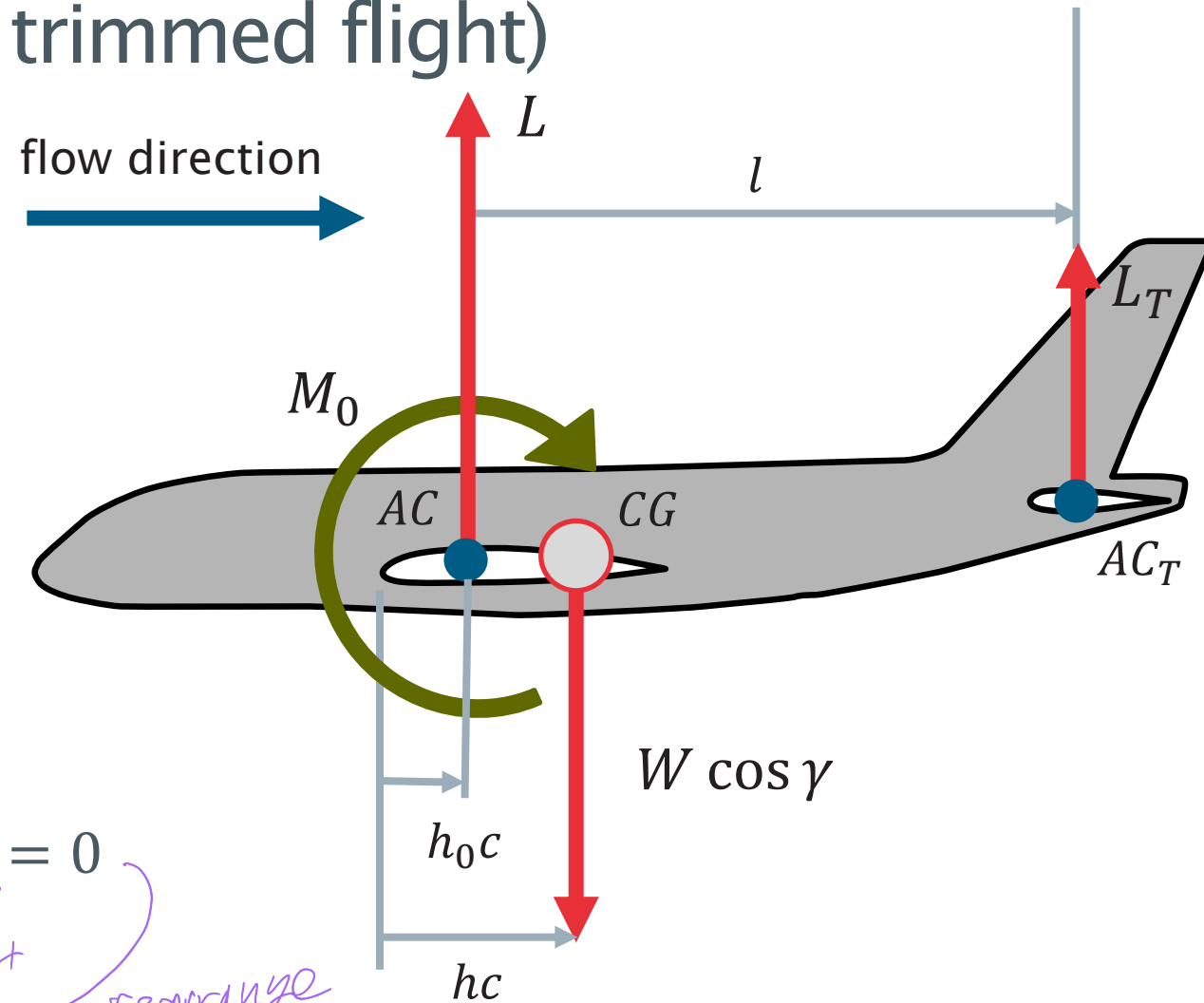
Moment balance about CG  $\Rightarrow \sum \vec{M} = 0$ :

$$M_0 + L(h - h_0)c - L_T(l - (h - h_0)c) = 0$$

Or

$$M_0 + (L + L_T)(h - h_0)c - L_T l = 0$$

$= L^*$



# Forces on an Aircraft (Steady, trimmed flight)

Nondimensional trim conditions *converting to coefficients*

Now rewrite in coefficient form using:

*note by using  $S_T$   $C_{LT}$  is a more intuitive number (by magnitude)*

$$C_{L^*} = \frac{L^*}{\frac{1}{2}\rho V^2 S}; \quad C_L = \frac{L}{\frac{1}{2}\rho V^2 S}; \quad C_W = \frac{W}{\frac{1}{2}\rho V^2 S};$$

$$C_{LT} = \frac{L_T}{\frac{1}{2}\rho V^2 S_T}; \quad C_{M_0} = \frac{M_0}{\frac{1}{2}\rho V^2 S c}$$

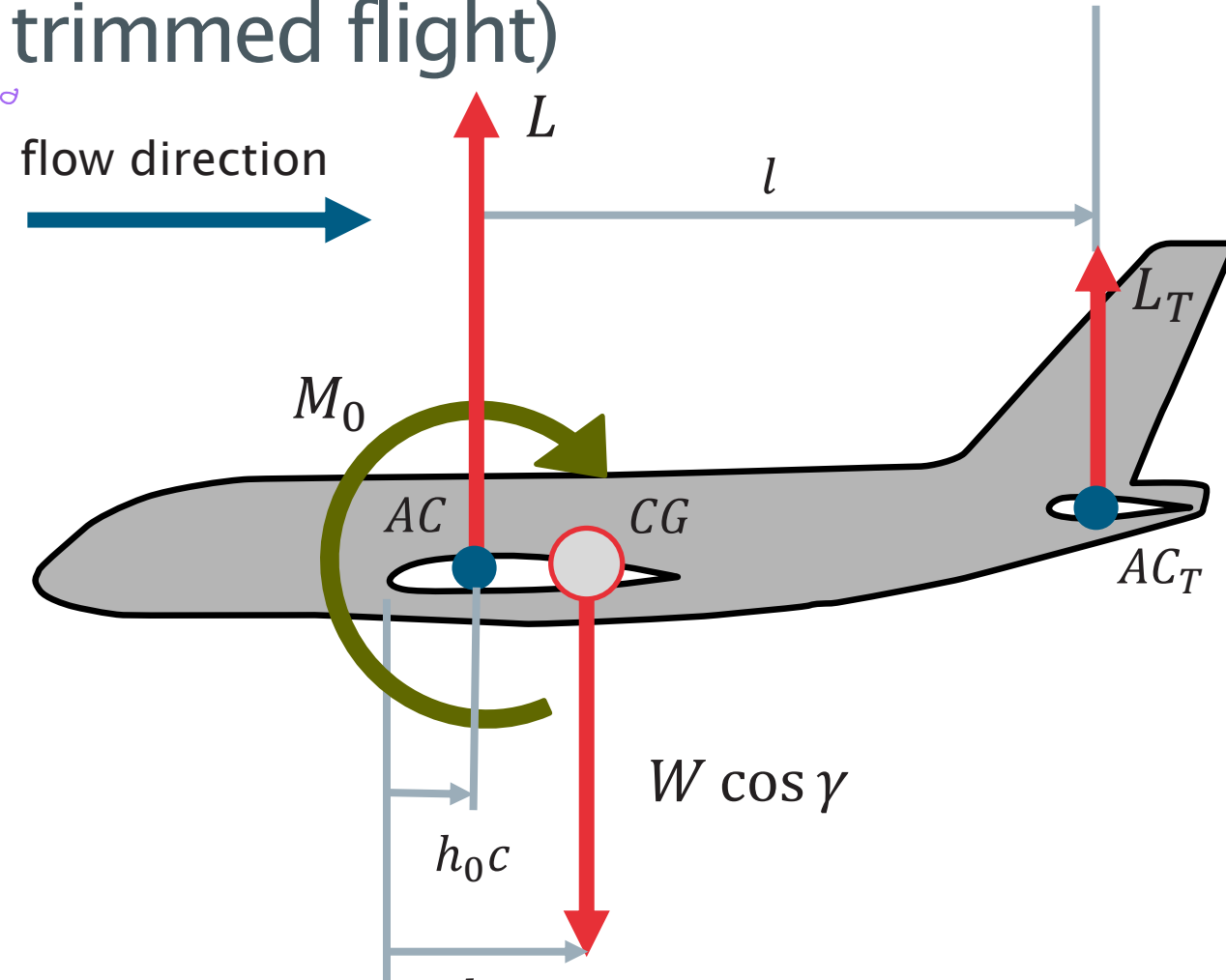
Resulting in:

$$C_{L^*} = C_L + C_{LT} \frac{S_T}{S} = C_W \cos \gamma$$

$$C_{M_0} + C_{L^*}(h - h_0) - C_{LT} K = 0$$

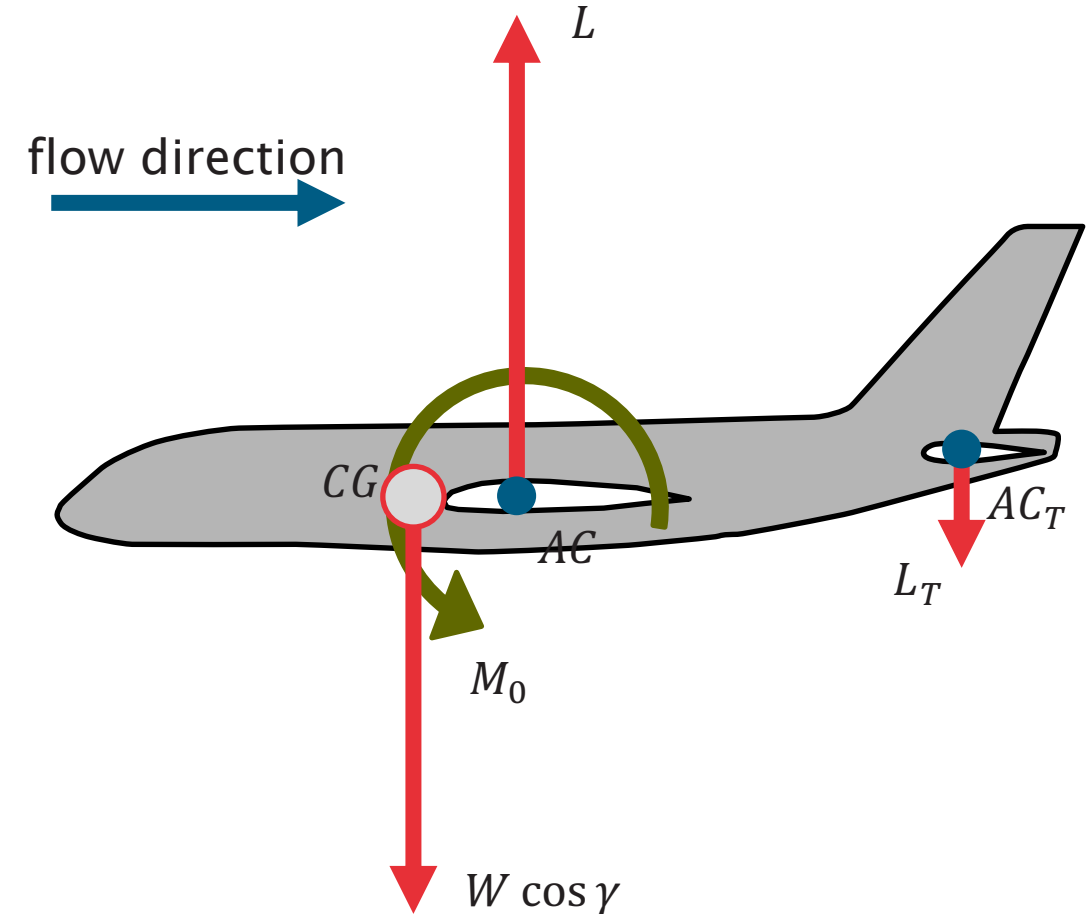
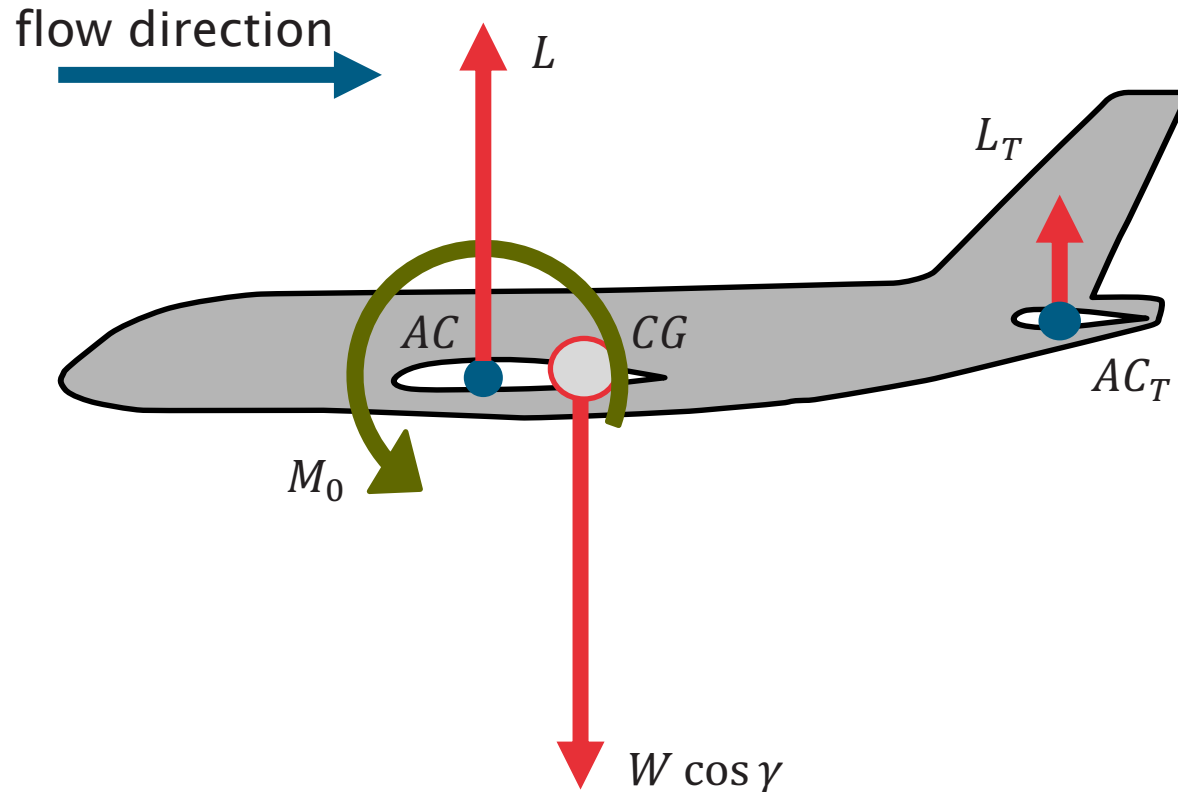
with the tail volume fraction

$$K \stackrel{\text{def}}{=} \frac{S_T l}{S c}; \quad \text{ratio of volumes with little physical meaning, just nice cleanup variable}$$



# Tailplane Lift

Positive or negative?



- Forward CG position benefits stability (but results in poorer handling quality at low speed)
- Tail plane design is affected: symmetric or negatively cambered airfoil sections



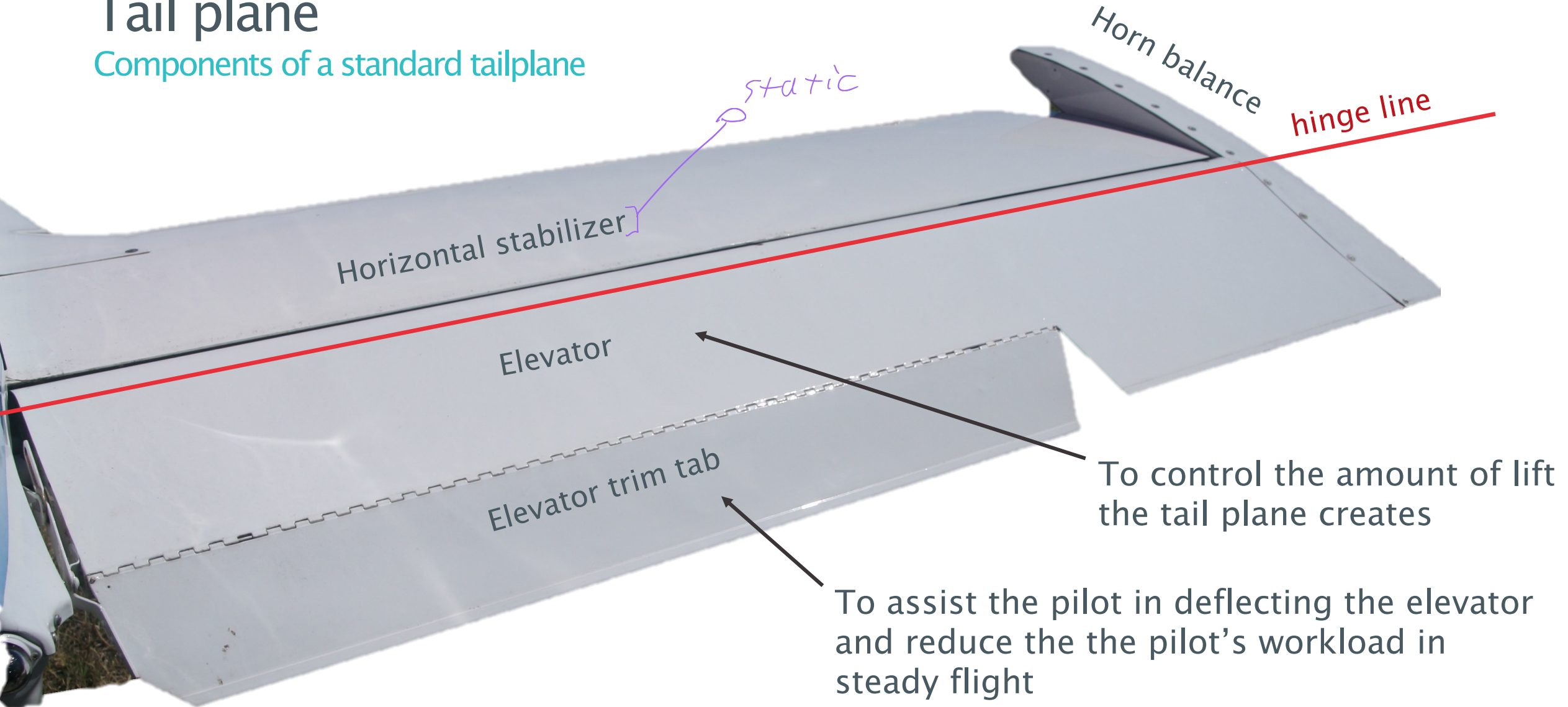
The Zenith STOL



The Zenith STOL

# Tail plane

## Components of a standard tailplane

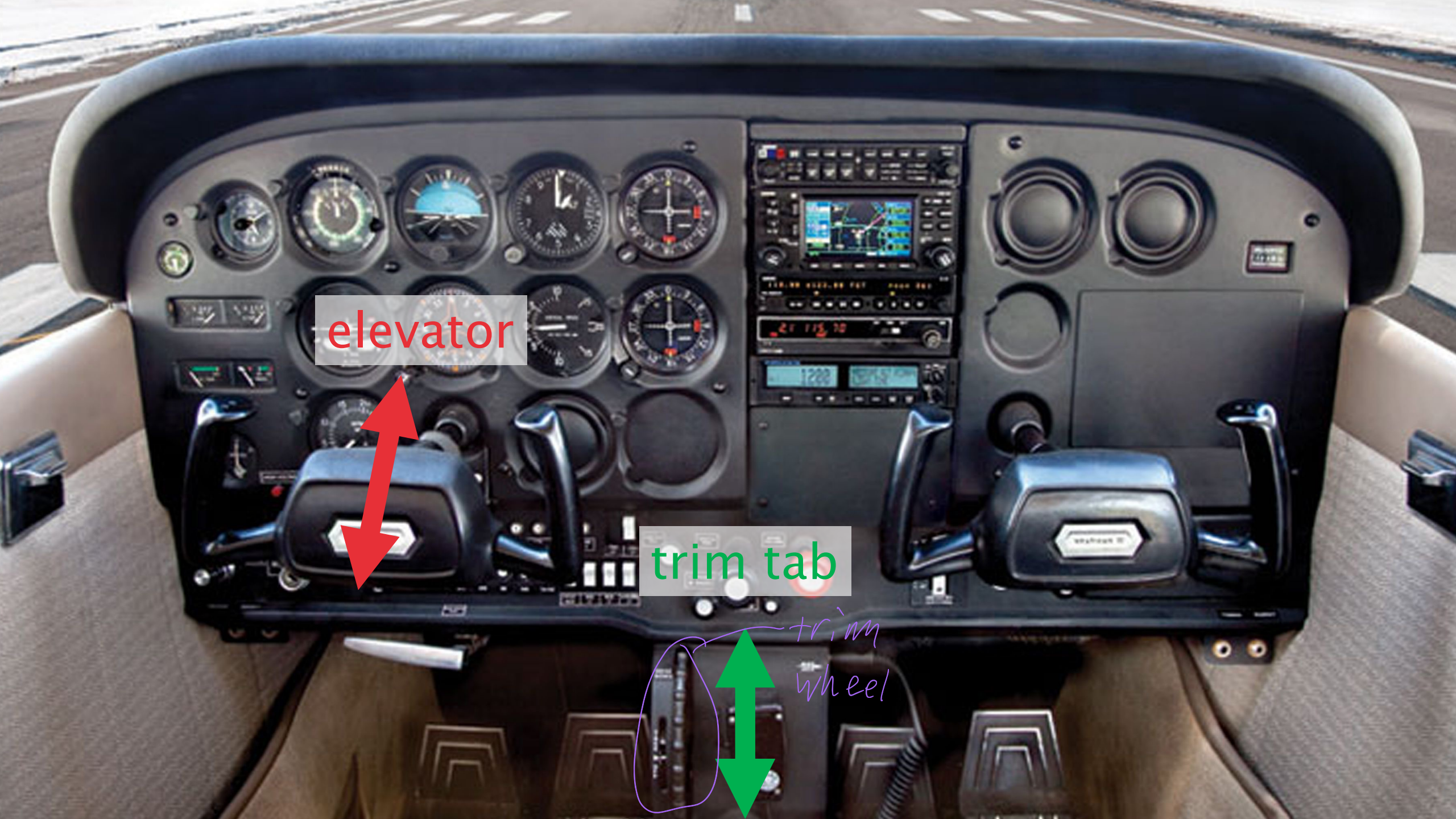




elevator

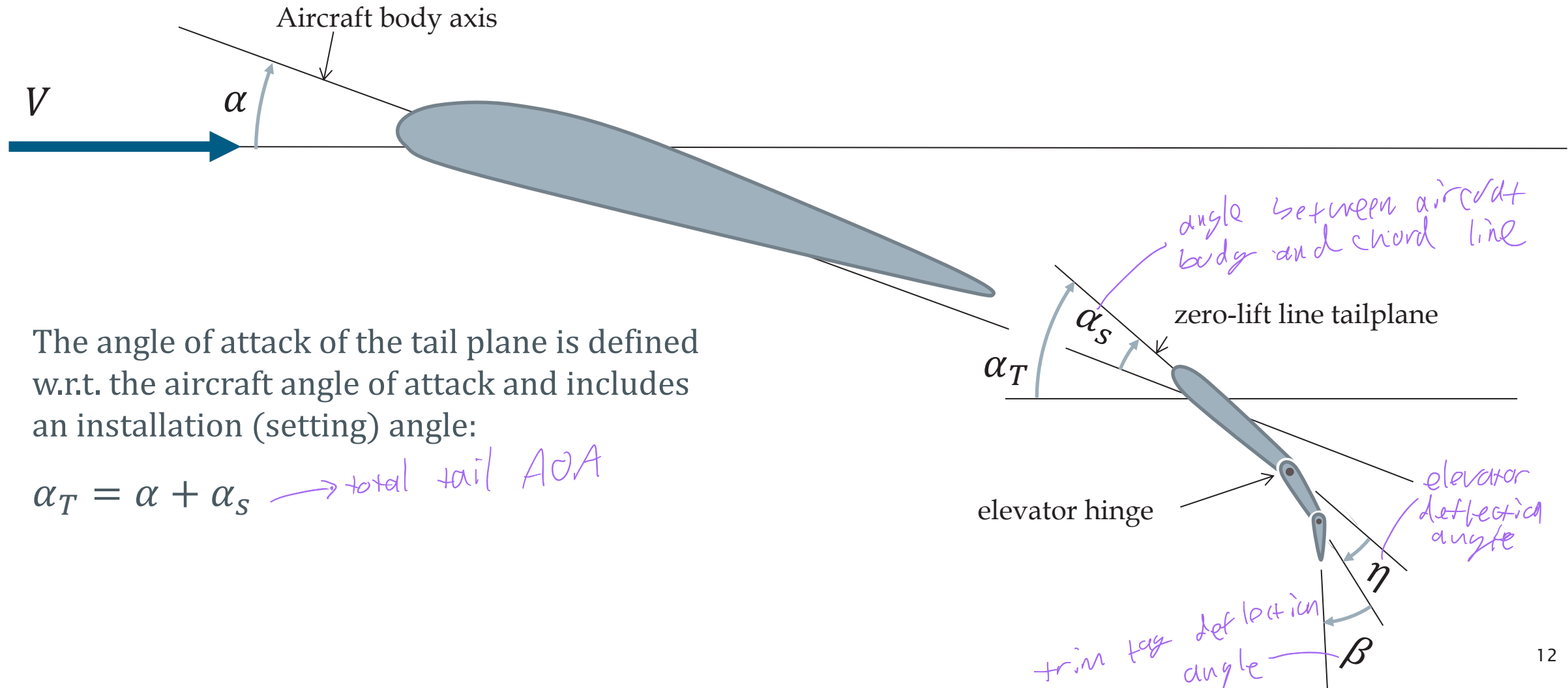
trim tab

trim wheel



# Tail plane models

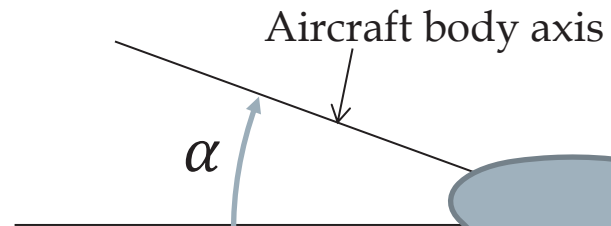
## General definitions



# Tail plane angle of attack

Influence of downwash

*cringing minus  $V_{\infty}$  is not suitable for air hitting tail*

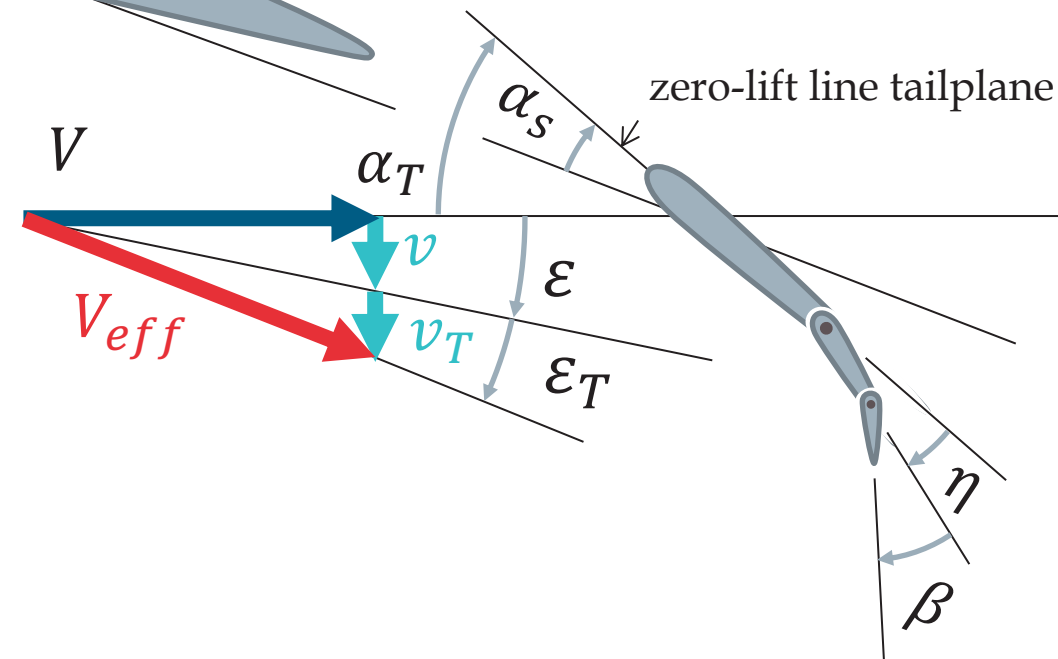


To obtain the effective angle of attack of the tail plane, we need :

- the downwash of the main wing
- the downwash of the tail itself

Resulting in:

$$\alpha_{T_{eff}} = \alpha_T - \underbrace{\varepsilon + \varepsilon_T}_{\text{downwash effect}}$$



# Tail plane angle of attack

## Influence of downwash II

Given:

$$\alpha_{T_{eff}} = \underbrace{\alpha + \alpha_s}_{\alpha_T = \alpha + \alpha_s} - \underbrace{\varepsilon - \varepsilon_T}$$

Expand the downwash terms

$$\alpha_{T_{eff}} = \alpha + \alpha_s - \left[ \varepsilon_\alpha (\alpha - \alpha_0) - \frac{C_{LT}}{\pi A_T e_T} \right]$$

tail setting angle

zero lift angle of attack

tail downwash



# Tail plane

## Lift equation

Tail plane lift depends on:

$\alpha_{T_{eff}}$ : tail plane angle of attack

$\eta$ : elevator angle

$\beta$ : elevator trim tab angle

A linear model is:

$$C_{L_T} = a_1 \alpha_{T_{eff}} + a_2 \eta + a_3 \beta$$

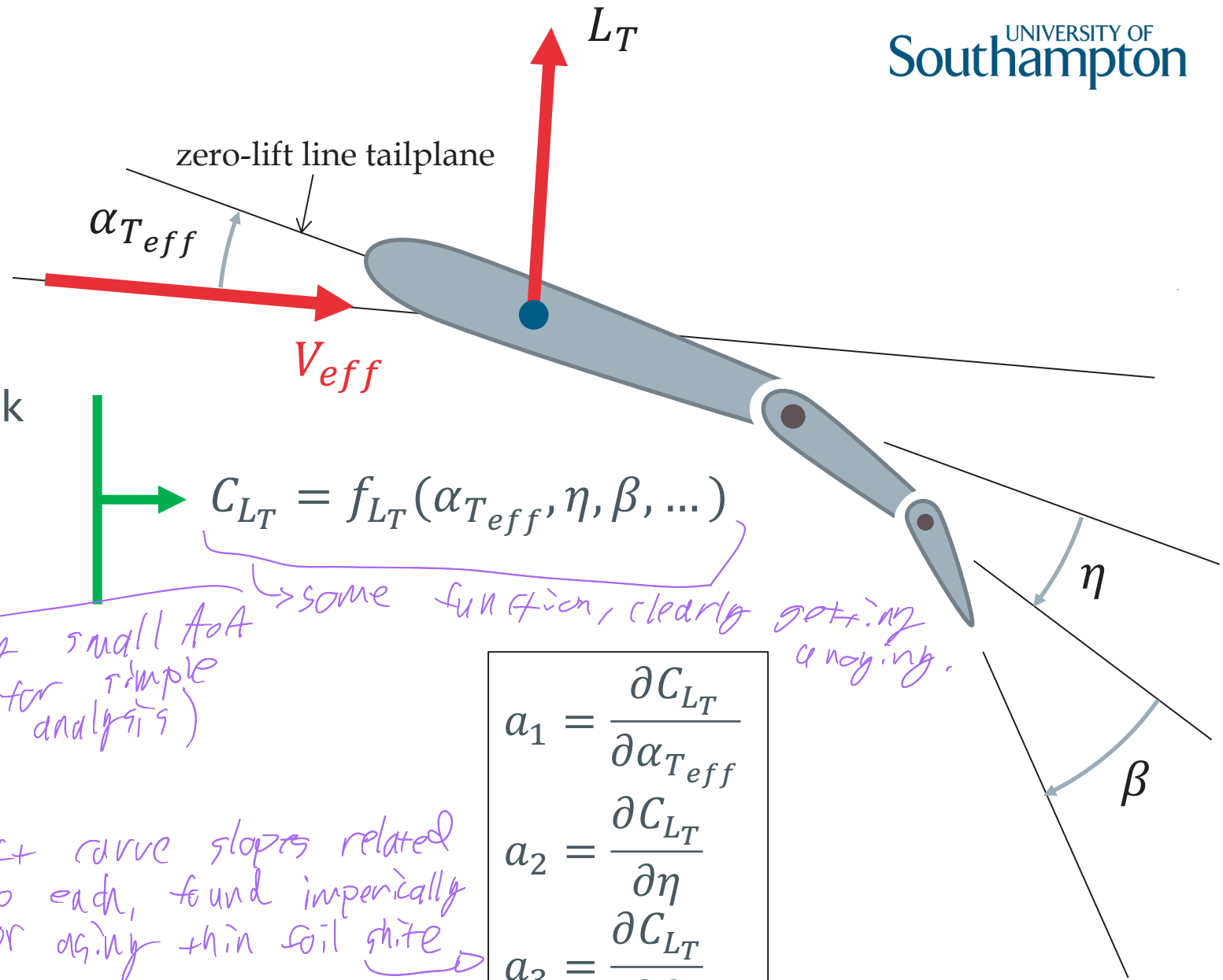
↑ includes downwash

lift curve slopes related to each, found empirically or using thin airfoil theory

$$C_{L_T} = f_{L_T}(\alpha_{T_{eff}}, \eta, \beta, \dots)$$

some function, clearly getting annoying.

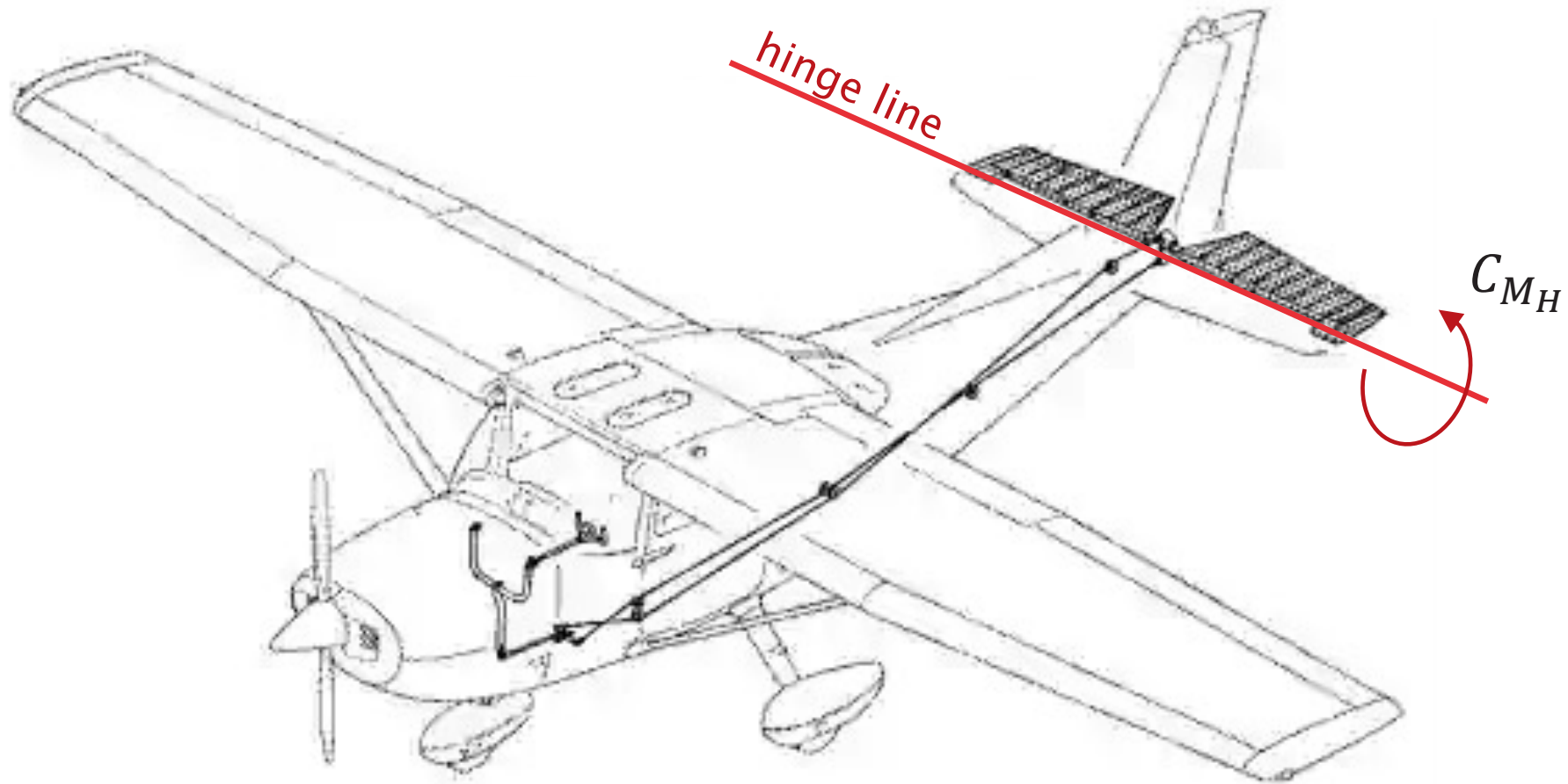
$$\begin{aligned} a_1 &= \frac{\partial C_{L_T}}{\partial \alpha_{T_{eff}}} \\ a_2 &= \frac{\partial C_{L_T}}{\partial \eta} \\ a_3 &= \frac{\partial C_{L_T}}{\partial \beta} \end{aligned}$$



What would you do to estimate these coefficients?

# Tail plane

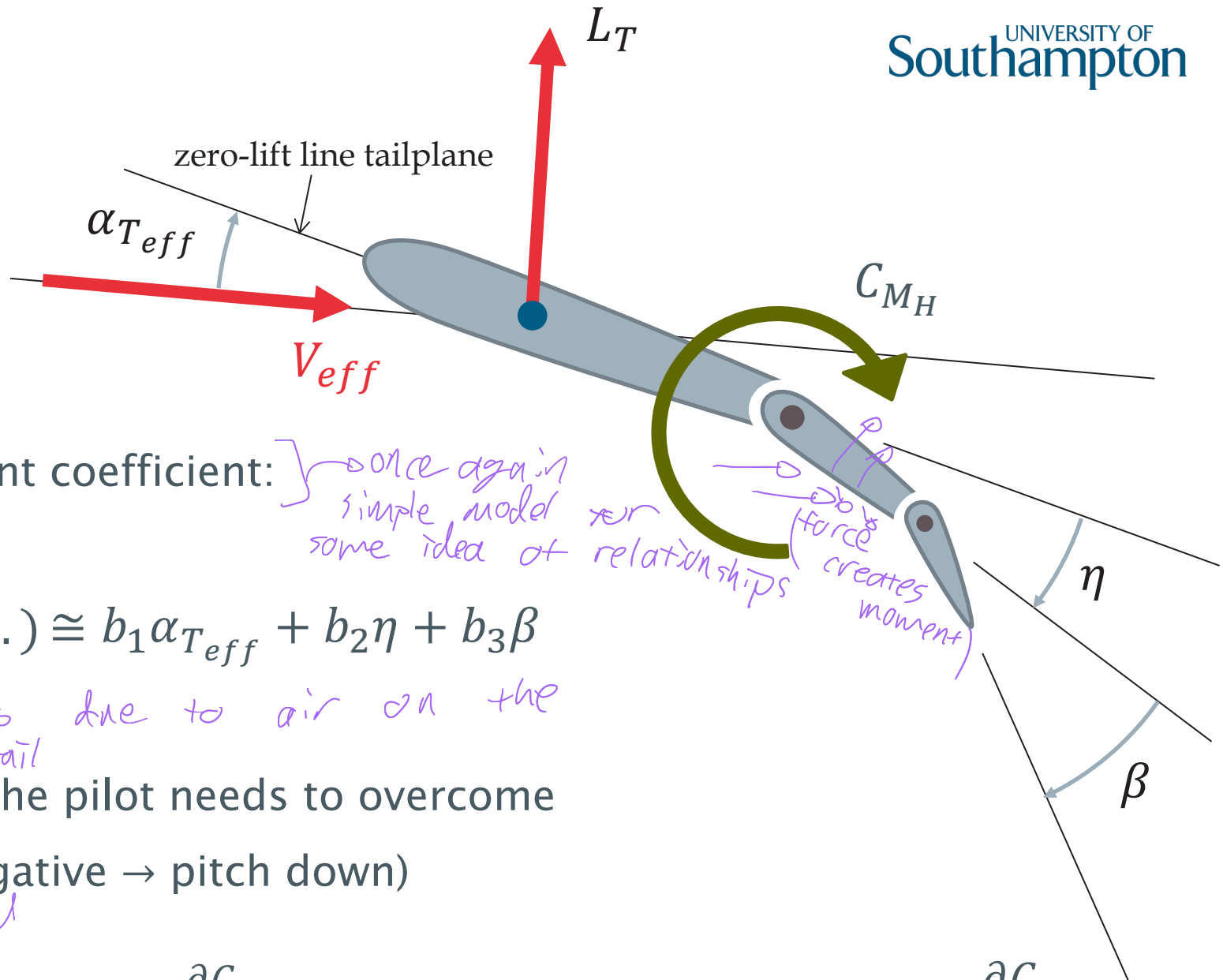
Aerodynamic forces produce a hinge moment





# Tail plane

## Hinge moment equation



Model for elevator hinge moment coefficient:

$$C_{MH} = f_{MH}(\alpha_{T_{eff}}, \eta, \beta, \dots) \cong b_1 \alpha_{T_{eff}} + b_2 \eta + b_3 \beta$$

moment forces due to air on the deflected tail

This is the hinge moment that the pilot needs to overcome

(positive  $\rightarrow$  pitch up, negative  $\rightarrow$  pitch down)

describes force needed to deflect tail

$$b_1 = \frac{\partial C_{MH}}{\partial \alpha_{T_{eff}}} \rightarrow \text{floating tendency}$$

$$b_2 = \frac{\partial C_{MH}}{\partial \eta} \rightarrow \text{restoring tendency}$$

$$b_3 = \frac{\partial C_{MH}}{\partial \beta}$$

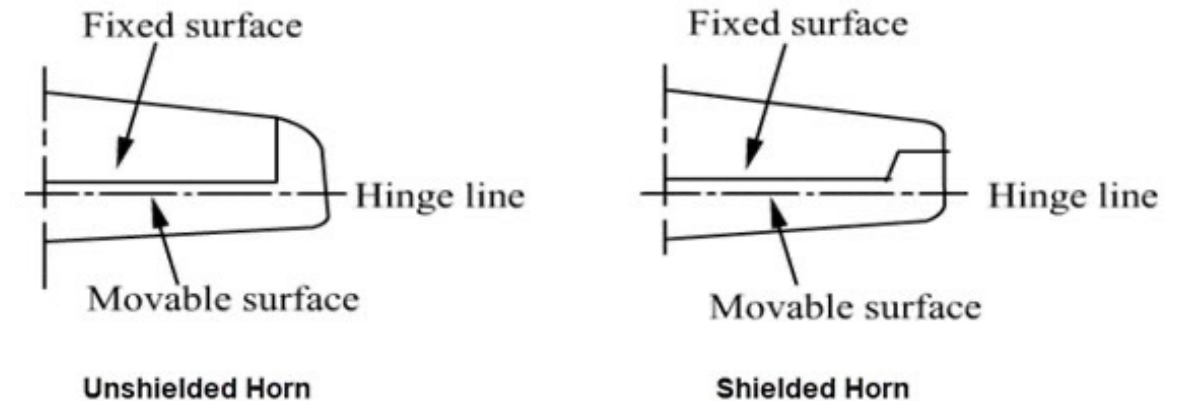
# Horn balance

Aerodynamic balancing: function and effect on modelling



The tail of the Spitfire, with unshielded horns elevator and rudder.

- Shielded/unshielded

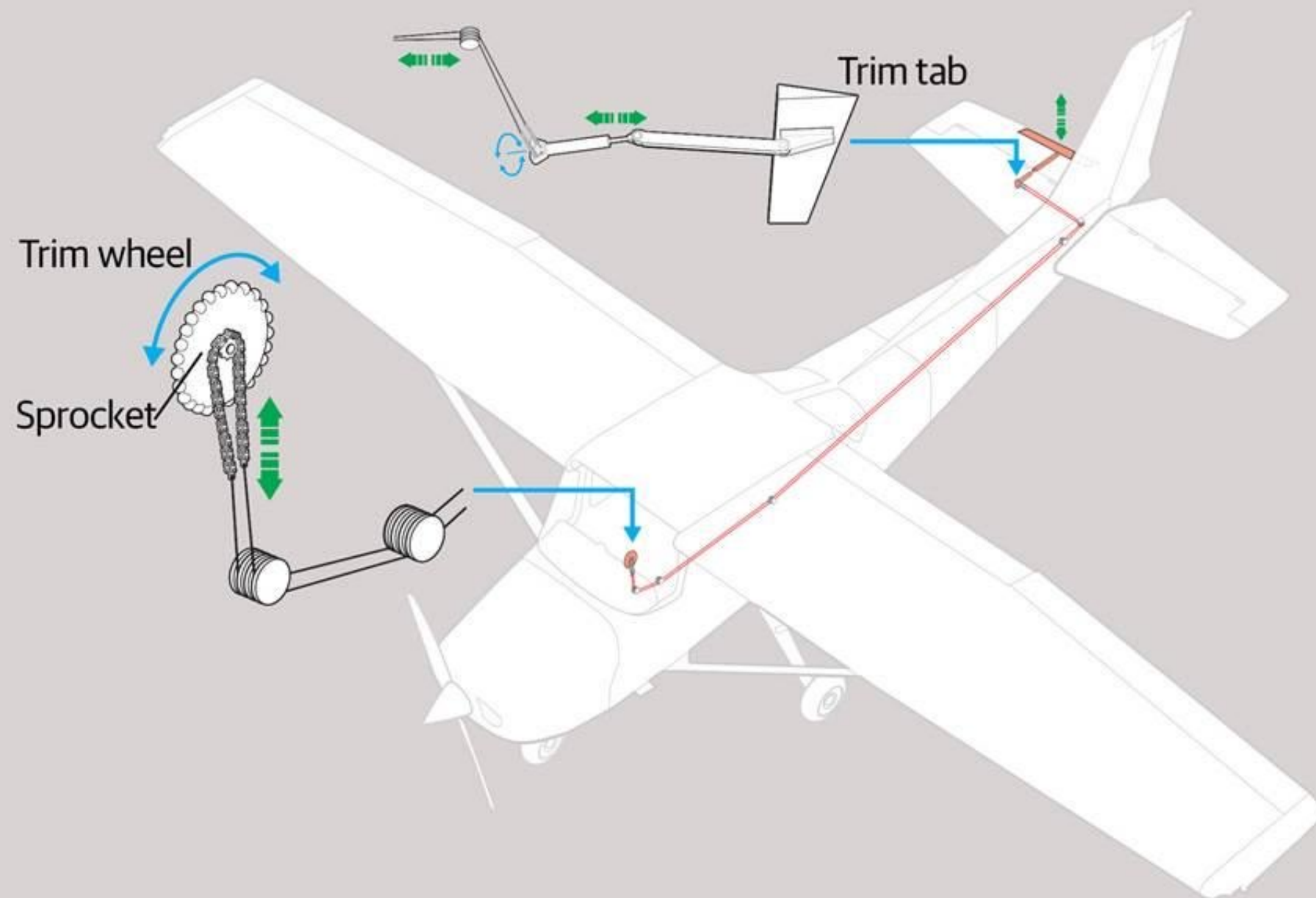


- Reduces floating/restoring tendency

$$C_{M_H} = b_1 \alpha_{T_{eff}} + b_2 \eta + b_3 \beta$$

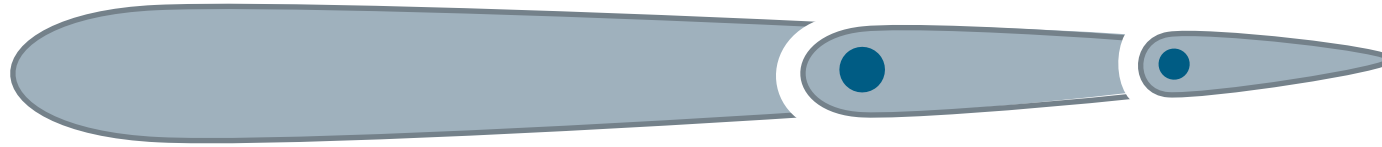
↑
↑

reduces moments acting on hinge so less force is needed to control it (bused)



# Tail plane

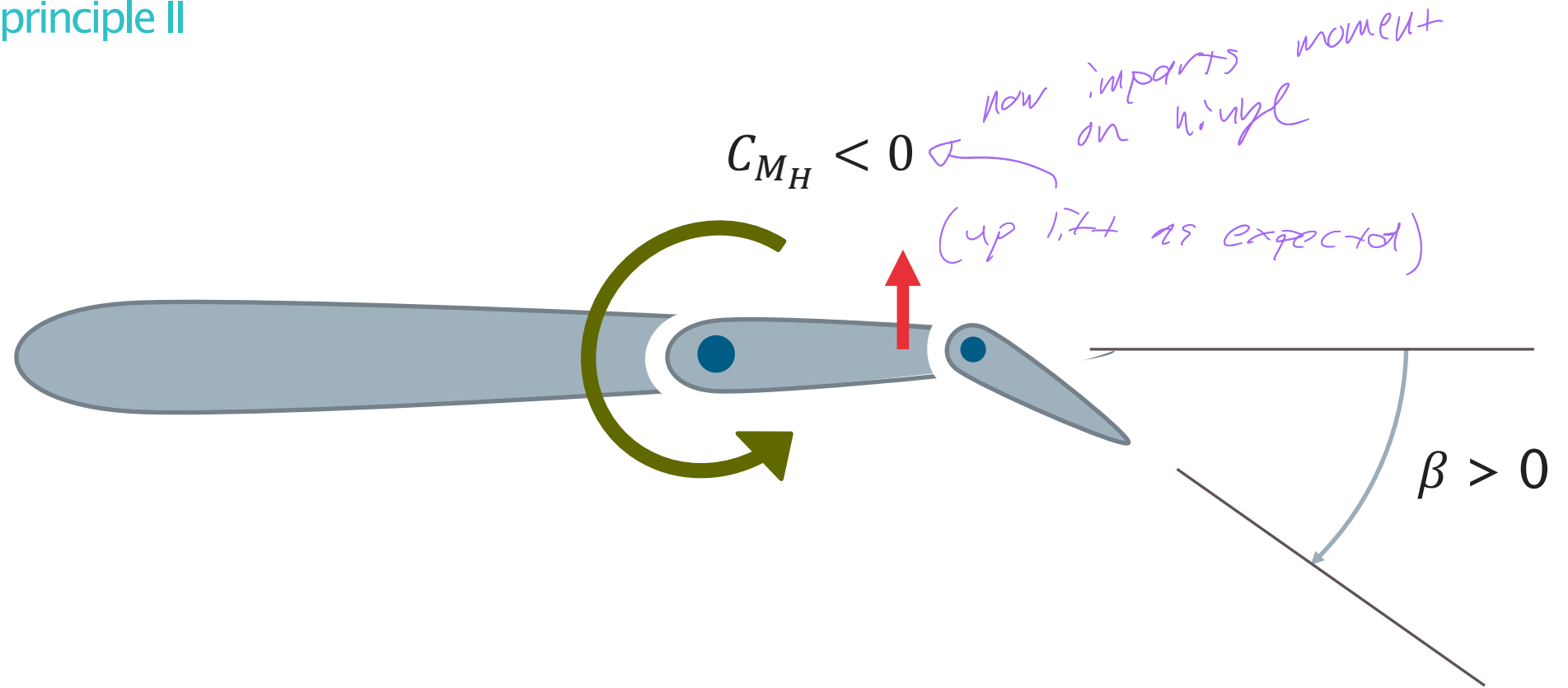
Trim tab working principle I



Assume we want to produce a negative tail lift, where should the elevator go?

# Tail plane

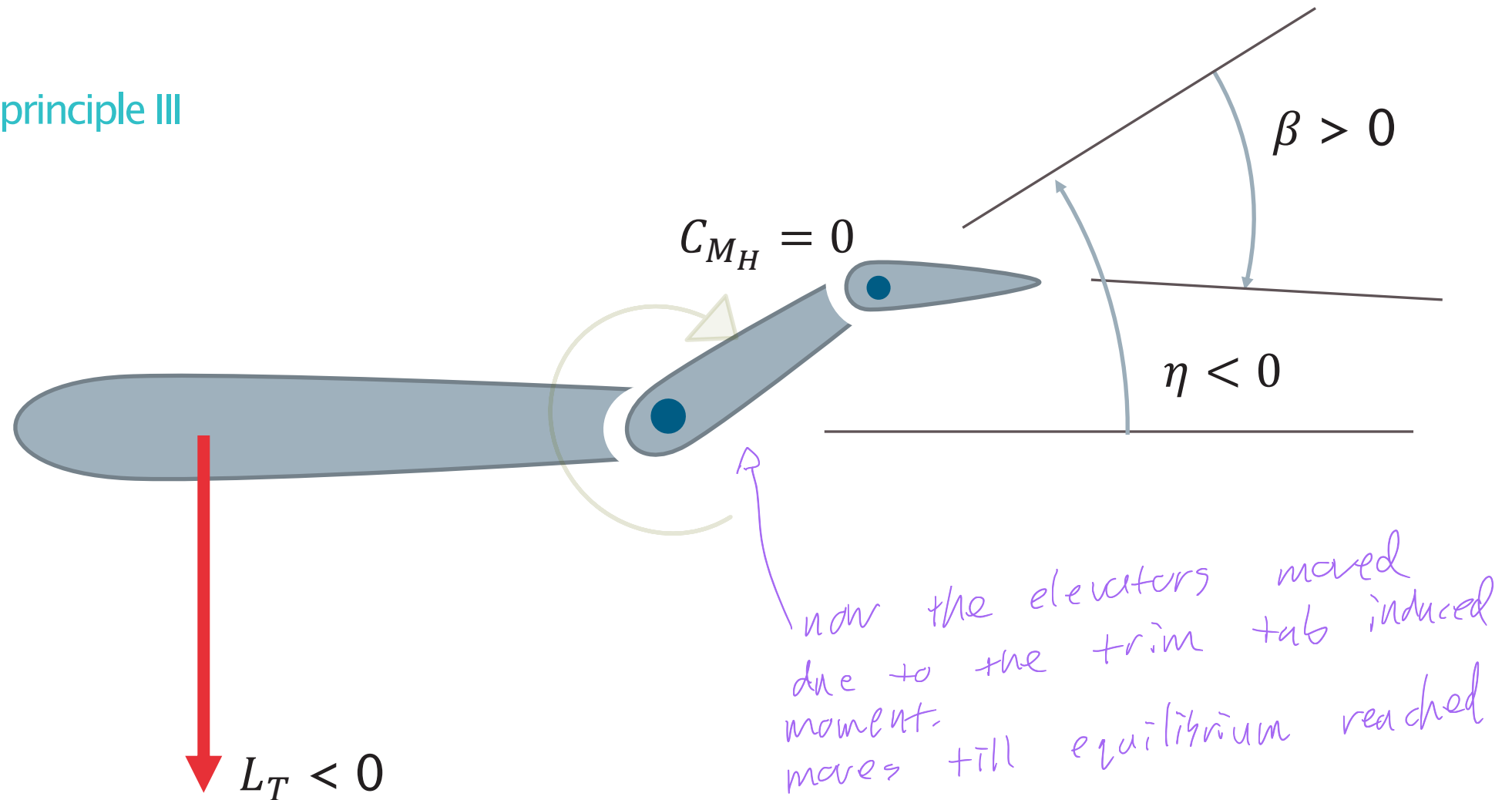
## Trim tab working principle II



This configuration produces a pitch down moment on the elevator

# Tail plane

## Trim tab working principle III



The stick is free to move, but the aircraft is trimmed.