

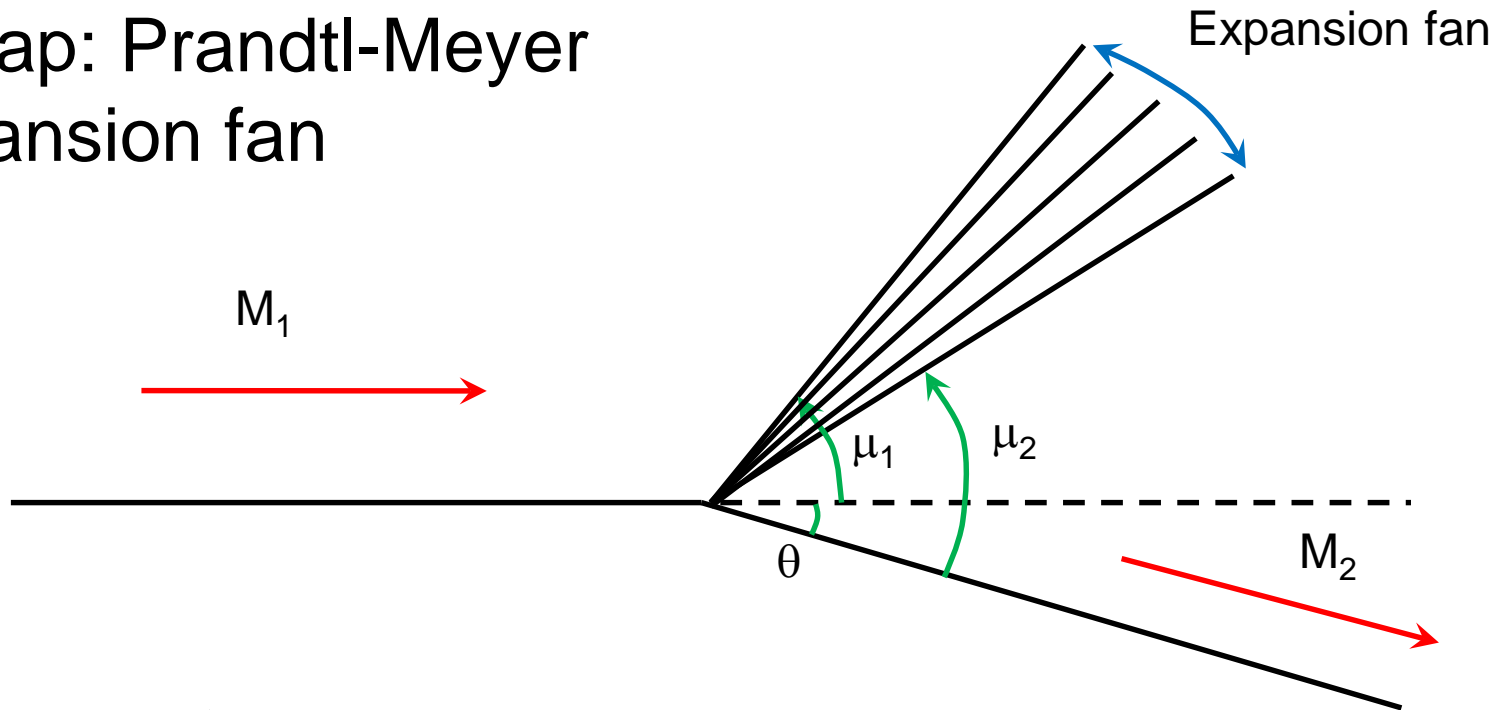
SESA3029

Aerothermodynamics

Lecture 2.5

Shock-expansion method

Recap: Prandtl-Meyer expansion fan

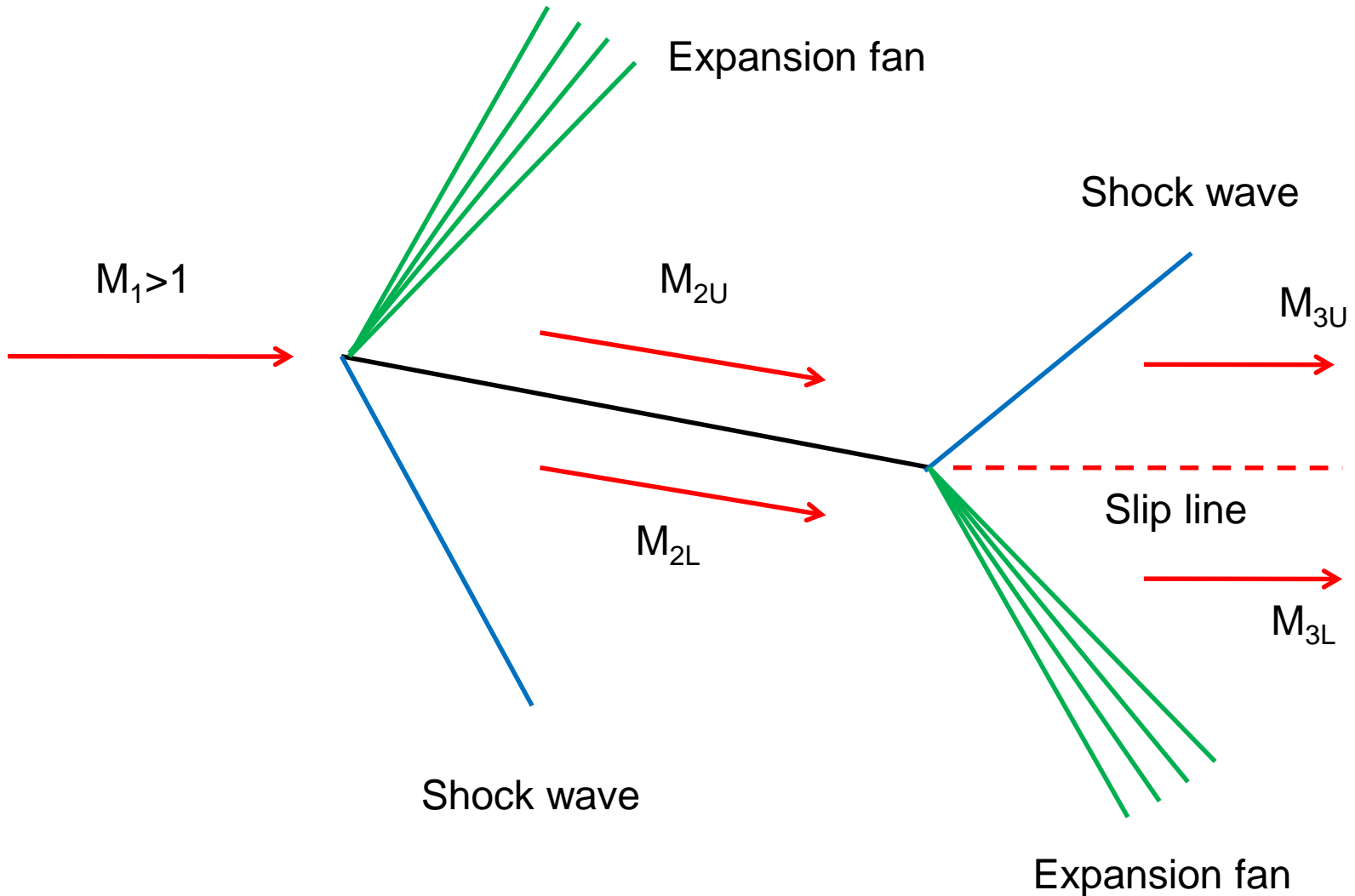


$$\sin \mu_1 = \frac{1}{M_1}$$

$$\sin \mu_2 = \frac{1}{M_2}$$

$$\theta = \nu(M_2) - \nu(M_1)$$

Flow past a flat plate at incidence



Example

- $M_1=2$, $p_1=30 \text{ kN/m}^2$, 1m chord plate at 10 degrees incidence
 - Find M_{2U} , M_{2L} , p_{2U} , p_{2L}
 - Find lift, drag and pitching moment
 - Find centre of pressure and aerodynamic centre
 - Convert to coefficient form

Expansion fan (1 to 2U)

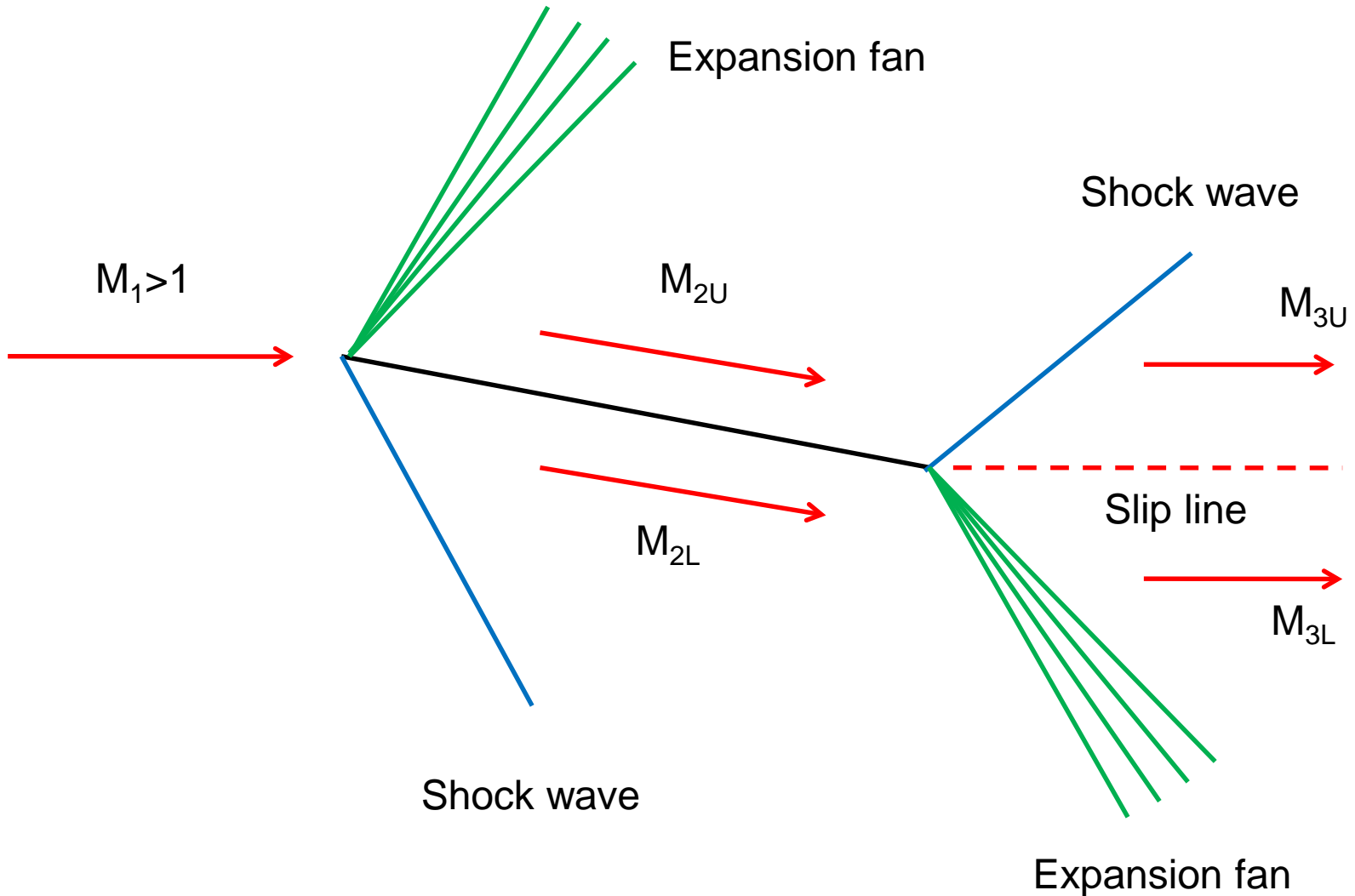
Isentropic-flow table ($\gamma = 1.4$):					
M	p / p_0	ρ / ρ_0	T / T_0	ν (deg.)	A / A^*
2.0000	0.1278	0.2300	0.5556	26.3798	1.6875

- Isentropic process,
 - $M_1=2$ IFT gives $\nu(M_1)=26.38$ deg., $p_1/p_0=0.1278$
 - P-M equation $\theta=\nu(M_2)-\nu(M_1)$
 - Hence $\nu(M_2)=36.38$ deg.

2.3800	0.0706	0.1505	0.4688	36.2607	2.3593
2.4000	0.0684	0.1472	0.4647	36.7465	2.4031

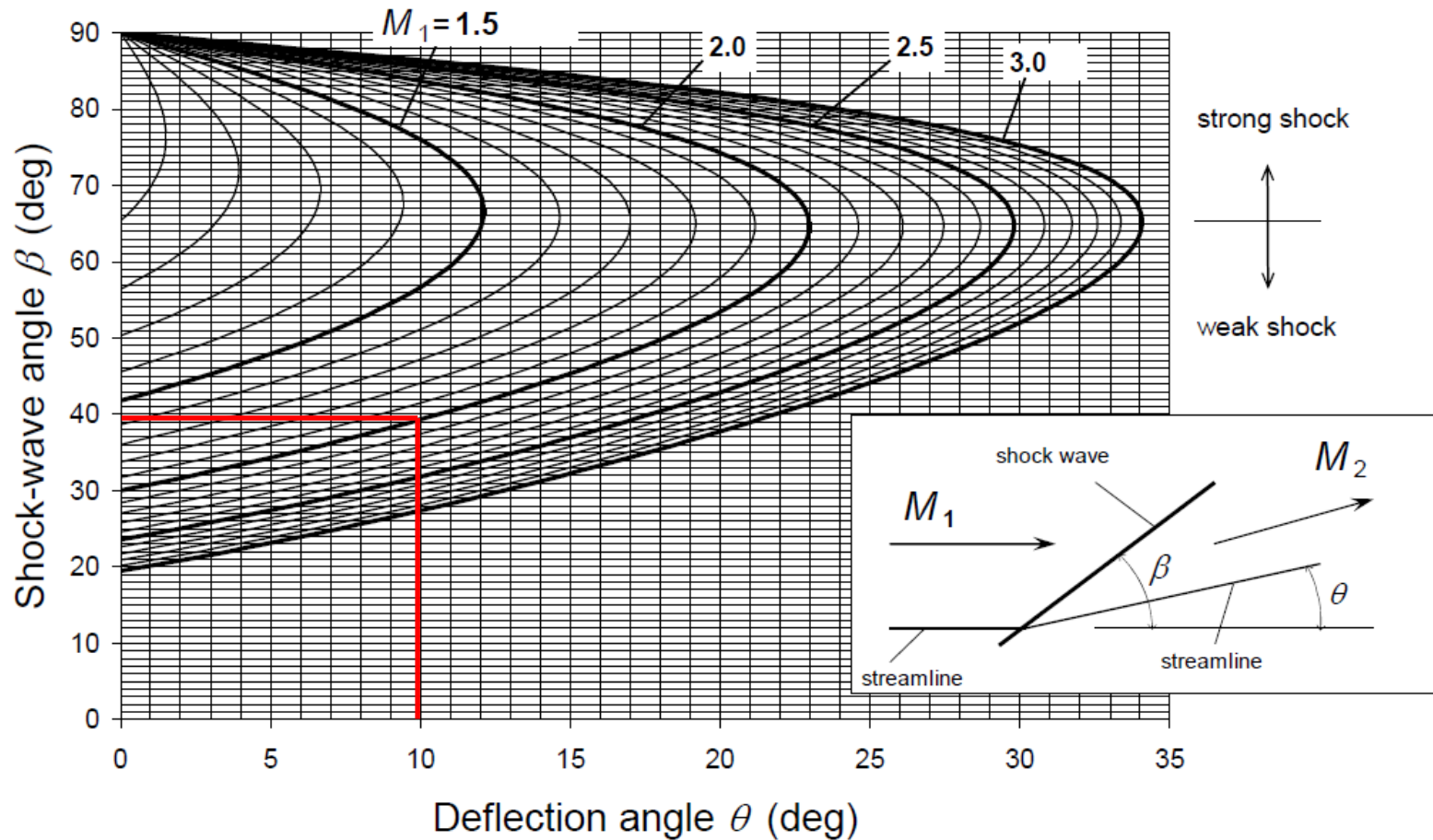
Interpolation from IFT: $M_{2U}=2.385$, $p_{2U}/p_0=0.0701$
 Hence $p_{2U}=16.5 \text{ kN/m}^2$

Flow past a flat plate at incidence



Oblique shock (1 to 2L)

Oblique-shock chart: $\gamma = 1.4$



Shock angle 39 deg.

Oblique shock calculation

$$M_{n1} = M_1 \sin \beta = 2 \cdot \sin(39) = 1.259$$

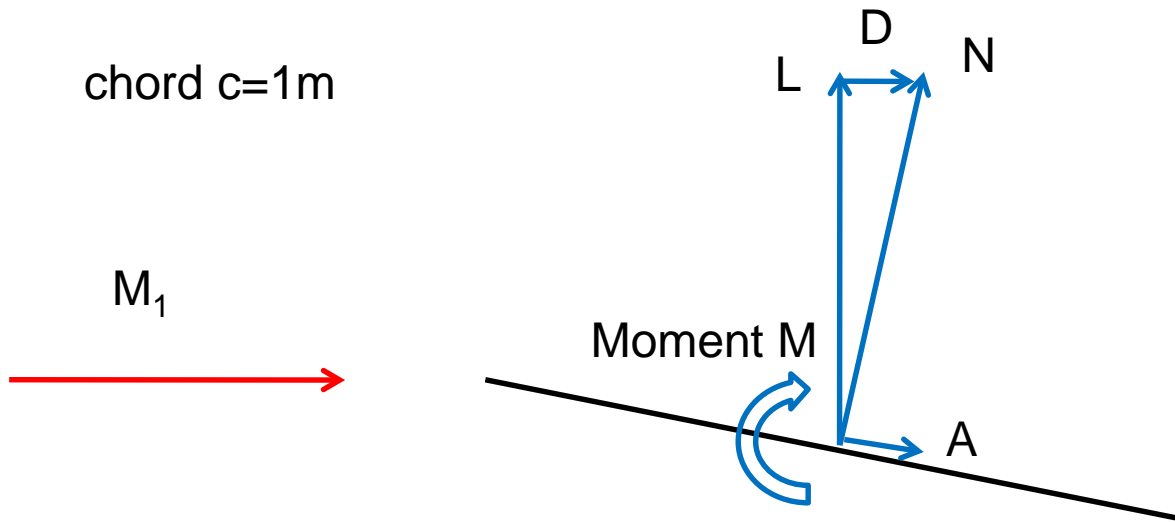
NST gives $p_{2L}/p_1 = 1.683$ (interpolation)

$$\text{Hence } p_{2L} = 50.5 \text{ kN/m}^2$$

For $M_{n1} = 1.259$ NST gives $M_{n2} = 0.8077$ (interpolation)

$$\text{Hence } M_{2L} = 0.8077 / \sin(39 - 10) = 1.67$$

Aerodynamic forces



$$L = N \cos \alpha - A \sin \alpha$$

$$D = A \cos \alpha + N \sin \alpha$$

Here $A=0$ (flat plate);

Pressure is constant along both upper and lower surfaces (centre of pressure is at the half chord)

$$N = (p_{2L} - p_{2U})c = (50.5 - 16.5) = 34.0 \text{ kN/m}$$

$$L = N \cos \alpha = 34 \cos 10 = 33.5 \text{ kN/m}$$

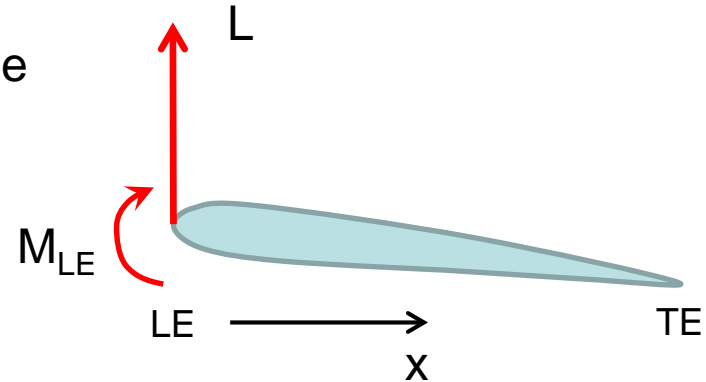
$$D = N \sin \alpha = 34 \sin 10 = 5.9 \text{ kN/m (Non zero!)}$$

$$M_{LE} = \int_0^c (p_{2U} - p_{2L}) x dx$$

$$= \left[-34 \frac{x^2}{2} \right]_0^1 = -17 \text{ kN}$$

Centre of pressure and aerodynamic centre

Forces and moments about leading edge

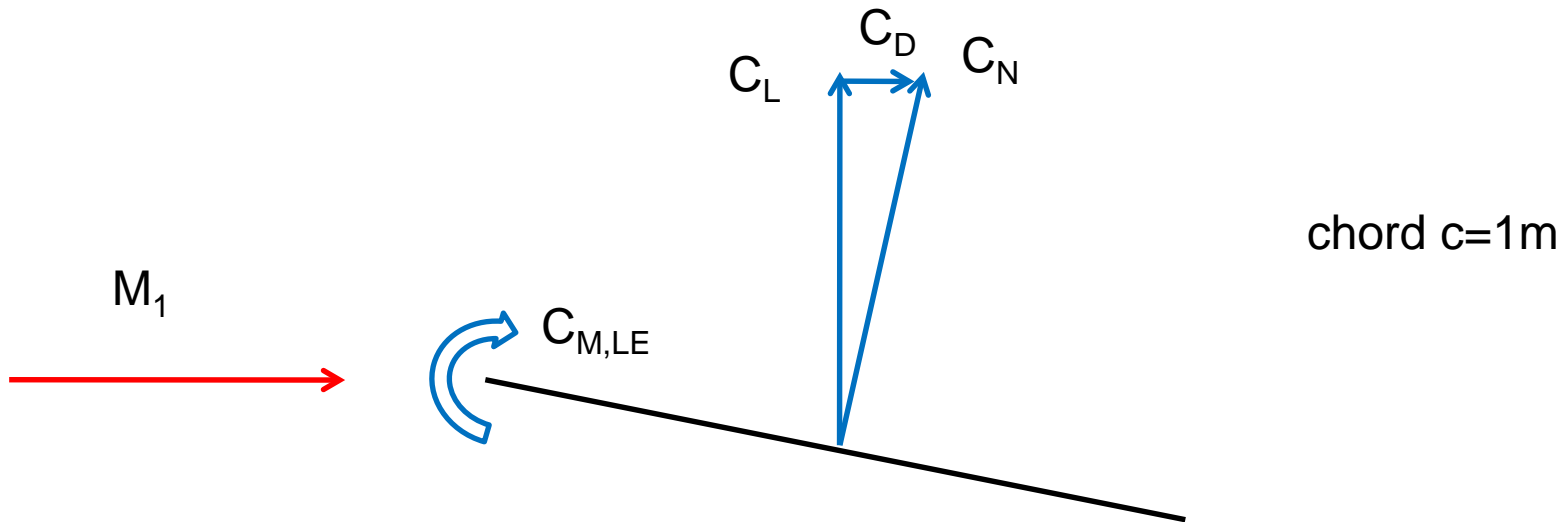


Moment coefficient about any point

$$C_{M,x} = C_{M,LE} + \bar{x}C_L \quad \Rightarrow \quad \bar{x}_{cp} = -\frac{C_{M,LE}}{C_L} \quad (\text{point where force acts with no moment})$$

$$\frac{dC_{M,x}}{dC_L} = \frac{dC_{M,LE}}{dC_L} + \bar{x} \quad \Rightarrow \quad \bar{x}_{ac} = -\frac{dC_{M,LE}}{dC_L} \quad (\text{point where } C_M \text{ is independent of } C_L)$$

Aerodynamic coefficients



$$C_L = \frac{L}{\frac{1}{2} \rho_1 V_1^2 c} = \frac{2L}{\gamma p_1 M_1^2 c} = \frac{2 \times 33,500}{1.4 \times 30,000 \times 2^2} = 0.40$$

$$C_D = \frac{D}{\frac{1}{2} \rho_1 V_1^2 c} = \frac{2D}{\gamma p_1 M_1^2 c} = \frac{2 \times 5,900}{1.4 \times 30,000 \times 2^2} = 0.070$$

$$C_{M,LE} = \frac{M_{LE}}{\frac{1}{2} \rho_1 V_1^2 c^2} = \frac{2M_{LE}}{\gamma p_1 M_1^2 c^2} = \frac{2 \times (-17,000)}{1.4 \times 30,000 \times 2^2 \times 1^2} = -0.20$$

$$\bar{x}_{CP} = \frac{-C_{M,LE}}{C_L} = \frac{0.2}{0.4} = 0.5$$

$$\bar{x}_{AC} = \frac{-dC_{M,LE}}{dC_L} = 0.5$$

(assuming linear variation of coefficients with incidence)

Key points

- In supersonic inviscid flow we have non-zero drag – this is called **wave drag**.
- Centre of pressure and aerodynamic centre are at the **half chord position** for a flat plate in supersonic flow
 - Compared to quarter chord location for incompressible flow
 - Movement of aerodynamic centre of a wing as we pass through Mach 1 has control implications