

Matthew Ning Honer Physics I THERMO DYNAMICS THERMAL Expansion $\Delta L = L \alpha \Delta T$, $\Delta V = V \beta \Delta T$ Heat $Q = C(T_f - T_i) = mc(T_f - T_i)$

Heat of Fusion/Vaporization $Q = Lm$ 1st Law of Thermodynamics $W = \int p dV \Rightarrow \Delta E_{int} = Q - W$, $Q > 0$ Heat enter the system. $W > 0$. System does work. Adiabatic process $Q = 0$, $\Delta E_{int} = -W$ Constant Volume $W = 0$, $\Delta E_{int} = Q$ Cyclic $\Delta E_{int} = 0$, $Q = W$ Free Expansion $Q = W$, $\Delta E_{int} = 0$ PV Graph, $\Delta p \Delta V = \text{Work}$, $M = m N_A$ Ideal Gas $PV = nRT = NkT$, $R = 8.31 \frac{J}{mol \cdot K}$ Isothermal (constant-T) process $W = nRT \ln(V_f/V_i)$ RMS speed $v_{rms} = \sqrt{\frac{3RT}{M}}$, $p = \frac{nMv_{rms}^2}{3V}$ Molar Specific Heat @ constant V $C_V = \frac{Q}{n\Delta T} = \frac{\Delta E_{int}}{n\Delta T}$ For ideal monatomic gas $C_V = \frac{3}{2}R$ Molar Specific Heat @ constant P $C_P = C_V + R$

Translational KE $K_{avg} = \frac{3}{2} \frac{R}{N_A} T$ (is ind. of molar mass) Internal Energy of Ideal Gas $E_{int} = \frac{3}{2} nRT = nC_V T$ For any process, $\Delta E_{int} = nC_V \Delta T$. Degrees of Freedom. $E_{int} = (\frac{f}{2}) nRT$, $C_V = (\frac{f}{2})R$ $f = 3, 5, 6$ (mono, dia, poly) In adiabatic process, $pV^\gamma = \text{constant}$ where $\gamma = C_P/C_V$. For free expansion, $pV = \text{constant}$ and T is constant. 2nd Law of Thermodynamics, $S = \text{Entropy}$ $\Delta S = S_f - S_i = \int_i^f \frac{dQ}{T}$. In isothermal process ($\Delta T = 0$) $\Delta S = \frac{Q}{T}$. If ΔT is small, then $\Delta S \approx \frac{Q}{T_{avg}}$. $\int \frac{dT}{T} = \ln(\frac{T_f}{T_i})$

SHM Spring $x = x_m \cos(\omega t + \phi)$, $v = -\omega x_m \sin(\omega t + \phi)$, $a = -\omega^2 x_m \cos(\omega t + \phi)$, $\omega = \sqrt{\frac{k}{m}}$, $T = 2\pi \sqrt{\frac{m}{k}}$. Hooke's Law $F = -kx$, $k = \omega^2 m$ Energy in Spring $U(t) = \frac{1}{2} kx^2 = \frac{1}{2} kx_m^2 \cos^2(\omega t + \phi)$, $U + K = E = \frac{1}{2} kx_m^2$ Angular SHM, use torque $\tau = -k\theta \Rightarrow T = 2\pi \sqrt{\frac{I}{k}}$ Simple pendulum $T = 2\pi \sqrt{\frac{I}{mgl}}$ Physical pendulum $T = 2\pi \sqrt{\frac{I}{mgh}}$ Torque in pendulum: $\tau = -L(F_g \sin \theta) = I\alpha$ 2 springs in series $k_{eff} = (\frac{1}{k_1} + \frac{1}{k_2})^{-1}$ 2 springs in parallel $k_{eff} = k_1 + k_2$ In spring with torque, convert find C in term of k . For approximation $\Delta x \sim L\theta$.

GRAVITATION Force $F = G \frac{m_1 m_2}{r^2}$ Uniform Shell Theorem $F = \frac{Gmm}{R^2}$ Work $W = \int F dr = \int \frac{Gmm}{R^2} r dr = \frac{Gmm}{2R}$ PE $U = -\frac{Gmm}{r}$ Kepler's Law of Period $T^2 = (\frac{4\pi^2}{GM}) r^3$ For elliptical orbit $T^2 = (\frac{4\pi^2}{GM}) a^3$ 2nd Law is conservation of angular momentum $\frac{dA}{dt} = \frac{L}{2m} \Rightarrow L = mrv$ Energy in orbit $U = -\frac{Gmm}{r}$, $K = \frac{Gmm}{2r}$, $E = -\frac{Gmm}{2r}$, Elliptical orbit $E = -\frac{Gmm}{2a}$

Equilibrium Force $\vec{F}_{net} = 0$, Torque $\vec{\tau}_{net} = 0$. In static equilibrium $\vec{p} = 0$ Rotation Pure rotation + pure translation = $\vec{v}_{top} = 2\vec{v}_{com}$, \vec{v}_{com} , $\vec{v}_{bottom} = 0$ Rolling down a ramp (wheel) $a_{com,x} = -\frac{g \sin(\theta)}{1 + I_{com}/MR^2}$ using $KE = \frac{1}{2} I_{com} \omega^2 + \frac{1}{2} m v_{com}^2$ Torque applied: Friction $ma_{com} = f_s$, $\tau - f_s R = I_{com} \alpha$, this has no sliding. With sliding $ma_{com} = \mu_k mg$, $\tau - \mu_k mg R = I_{com} \alpha$. Force applied to center, w/ friction $ma_{com} = F - f_s \Rightarrow m\alpha R = F - f_s \Rightarrow \frac{FMR^2}{I_P} = F - f_s$

Angular Momentum $L = r \times p = m(r \times \vec{v})$ Torque/Angular momentum $\vec{\tau} = \frac{d\vec{L}}{dt}$

Fluids Density $\rho = \frac{m}{V}$ Pressure $p = \frac{F}{A}$ Pressure vs. Depth $p = p_0 + \rho g h$ Pascal's Principle $\Delta p = \frac{F_1}{A_1} = \frac{F_2}{A_2}$

$W = F_b d_o = F_c d_i$ Archimedes' Principle $F_{\text{buoyant}} = m_{\text{fluid}} g$ where m_{fluid} Apparent Weight $W_{\text{app}} = W - F_b$

Flow Rate $R_v = Av = \frac{V}{t} = \frac{m^3}{s}$ Mass Flow Rate $R_m = \rho R_v$ Bernoulli's Equation $p + \frac{1}{2} \rho v^2 + \rho g y = \text{constant}$ KE density = $\frac{KE}{\text{Volume}}$

WAVES I $y(x,t) = y_m \sin(kx - \omega t)$, $k = \frac{2\pi}{\lambda}$, $\omega = 2\pi f$, $v = \lambda f$ Traveling Wave $y(x,t) = y_m \sin(kx + \omega t)$ move backward

Graph Snapshot $2x - 4t$ $8x - 16t$ Transverse Speed (Max) $\frac{dy}{dt}$ Velocity & Tension $v = \sqrt{\frac{T}{\mu}}$ T is tension, μ is linear density $\frac{\text{kg}}{\text{m}}$

Speed of wave is ind. of frequency. Interference of waves traveling in same direction on same string

$$y'(x,t) = [2y_m \cos(\frac{1}{2}\phi)] \sin(kx - \omega t + \frac{1}{2}\phi)$$

Standing Wave $y(x,t) = 2y_m \sin(kx) \cos(\omega t)$ Harmonics $f = \frac{v}{\lambda} = n \frac{v}{2L}$ Tension affect frequency, not λ .

WAVES II velocity of sound (longitudinal) $v = \sqrt{\frac{\beta}{\rho}}$, $\beta = \text{bulk modulus} = -\frac{\Delta p}{\Delta V/V} = "PE"$ Displacement $s = s_m \cos(kx - \omega t)$ Pressure

Change $\Delta p = \Delta p_m \sin(kx - \omega t)$ where $\Delta p_m = (\rho v \omega) s_m$ Intensity $I = \frac{P}{A} = \frac{P}{4\pi r^2}$ $\frac{I_2}{I_1} = \left[\frac{d_2}{d_1}\right]^2$ Intensity is $\text{Watt}/\text{meter}^2 = p v$

P is power, p is pressure. $I = \frac{1}{2} \rho v \omega^2 s_m^2$ Sound Level $\beta = (10 \text{ dB}) \log\left(\frac{I}{I_0}\right)$ Speed of oscillating element $v_s = \frac{\partial s}{\partial t} = -\omega s_m \sin(kx - \omega t)$

Pipe open at both end $f = \frac{v}{\lambda} = \frac{nv}{2L}$ for $n=1,2,3,\dots$ Pipe open at one end $f = \frac{v}{\lambda} = \frac{nv}{4L}$ for $n=1,3,5$ (one node, one antinode at ends)

$f_{\text{beak}} = f_1 - f_2$ Doppler Effect $f' = f \left(\frac{v \pm v_o}{v \pm v_s} \right)$ Wind Speed $f' = f \left(\frac{v \pm v_{\text{wind}} \pm v_o}{v \pm v_{\text{wind}} \pm v_s} \right)$

COULOMB'S LAW Electrostatic Force $\vec{F} = k \frac{q_1 q_2}{r^2} \hat{r}$, $\vec{F} = k \frac{q_1 q_2}{1/r^3} \hat{r}$ because $\hat{r} = \frac{\vec{r}}{r}$ $F = \frac{k q_1 q_2}{r^2}$

ELECTRIC FIELD $\vec{E} = \frac{\vec{F}}{q_0}$ $E = k \frac{|q|}{r^2}$ Electric Field due to dipole $E = 2k \frac{p}{z^3}$ where z is distance betw. P & midpt. of dipole. Electric Field due to Line $dq = \lambda ds$ where $\lambda = \frac{Q}{L}$ then $dE = \frac{k dq}{r^2}$, $dq = \sigma dA$, $dE = \frac{k dq z}{(z^2 + r^2)^{3/2}}$

ELECTRIC FIELD DUE TO CHARGED RING $E = \frac{qz}{4\pi\epsilon_0 (z^2 + R^2)^{3/2}}$ ELECTRIC FIELD CHARGED DISK $E = \frac{\sigma}{2\epsilon_0} \left(1 - \frac{z}{\sqrt{z^2 + R^2}}\right)$

KINEMATIC EQs $d = d_i + v_i t + \frac{1}{2} a t^2$ $v_f^2 = v_i^2 + 2ad$ $v_f = v_i + at$ $d = \frac{v_i + v_f}{2} t$ (all assume constant a)

TRIG IDs $\sin(u \pm v) = \sin(u) \cos(v) \pm \cos(u) \sin(v)$ $\cos(u \pm v) = \cos(u) \cos(v) \mp \sin(u) \sin(v)$

$\cos(2u) = \cos^2 u - \sin^2 u$ $\sin(2u) = 2 \sin(u) \cos(u)$

WAVES III wave equation $\frac{\partial^2 y}{\partial x^2} = \frac{1}{v^2} \frac{\partial^2 y}{\partial t^2}$ v is wave speed. This is one-dimensional. Wavelength $\lambda = \frac{c}{f}$ (only EM waves not other waves) Phase velocity $v_p = \frac{\lambda}{T} = \frac{\omega}{k}$ ω is angular frequency. k is wave number. Group velocity $v_g = \frac{\partial \omega}{\partial k}$

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Electric Field $\vec{E} = k \frac{q_1 q_2}{r^2} = \frac{k q_1 q_2}{|r|^3}$ because $\hat{r} = \frac{\vec{r}}{r}$ and $k = \frac{1}{4\pi\epsilon_0}$ Electric Field $\vec{E} = \frac{\vec{F}}{q_0}$ Charge Distribution
 $\vec{E}(x,y,z) = k \int \frac{\rho(x',y',z') \vec{r}}{r^2} dx' dy' dz'$ Electric Field due to Dipole $E = 2k \frac{p}{z^2}$ where z is distance betw. P & midpt. of dipole.
 Electric Field due to Line $dq = \lambda ds$ then $dE = \frac{k dq}{r^2}$ Electric Field due to Area $dq = \sigma dA$ Gauss's Law Flux $d\Phi = \vec{E} \cdot d\vec{A}$ Net Flux

$\Phi = \oint \vec{E} \cdot d\vec{A} = \frac{q}{\epsilon_0} = \frac{1}{\epsilon_0} \int \rho dv$ Flux is scalar. $E = \frac{q}{A\epsilon_0}$ Charged Isolated Conductor, internal electric field is 0. Electric field due to nonconducting sheet $E = \frac{\sigma}{2\epsilon_0}$ Electric field for spherical shell ($r \geq R$) $E = k \frac{q}{r^2}$ Electric field for uniform shell sphere $E = \left(\frac{k q}{r^2} \right) \left(\frac{R^3}{r^3} \right)$

Electric Potential Potential difference $\phi_{21} = - \int_{r_1}^{r_2} \vec{E} \cdot d\vec{s}$ (line integral) Volt $1V = \frac{1J}{1C}$ Work $\Delta K = -q\Delta V + W_{app}$ Potential difference
 $\vec{E} = -\nabla\phi$ Because potential is scalar, orientation doesn't matter. $V = k \sum \frac{q_i}{r_i}$ Potential due to charge distribution $V = k \int \frac{dq}{r}$ Gauss's Theorem
 in diff. form $\oint \vec{E} \cdot d\vec{A} = \int_V \text{div } \vec{E} \cdot dv$ and $\text{div } \vec{E} = \frac{\rho}{\epsilon_0}$, $\nabla \cdot \vec{E} = -\nabla^2 \phi$ Uniqueness Theorem for Poisson's Equation $\nabla^2 \phi(\vec{r}) = -4\pi \rho(\vec{r})$

Vector Calc. Review Divergence $\text{div } \vec{F} = \lim_{V_i \rightarrow 0} \frac{1}{V_i} \int_{S_i} \vec{F} \cdot d\vec{A}_i$ Curl $\text{curl } \vec{F} = \lim_{A_i \rightarrow 0} \frac{\oint_{C_i} \vec{F} \cdot d\vec{s}}{A_i}$ Gauss's Theorem $\int_V \text{div } \vec{F} \cdot dv = \oint_S \vec{F} \cdot d\vec{A}$

Stokes' Theorem $\int_C \vec{F} \cdot d\vec{s} = \int_S \text{curl } \vec{F} \cdot d\vec{A}$ Capacitance capacitance $q = CV$ Parallel plate $C = \frac{\epsilon_0 A}{s}$ Sphere $C = 4\pi\epsilon_0 r$ Shell
 $C = 4\pi\epsilon_0 \frac{ab}{b-a}$ Potential from \vec{E} $\Delta V = - \int_i^f \vec{E} \cdot d\vec{s}$ Parallel $C_{eq} = \sum C_i$ Series $C_{eq}^{-1} = (\sum C_i^{-1})$ Energy $U = \frac{q^2}{2C} = \frac{1}{2} CV^2$, $V = Ed$

Current current $i = \frac{dq}{dt}$, $I = nq\vec{a} \cdot \vec{u}$ \vec{a} is accel, \vec{u} is velocity. current density $\vec{J} = \sum n_k q_k \vec{u}_k$ charge conservation $\text{div } \vec{J} = 0 = -\frac{\partial \rho}{\partial t}$ $I = JA$
 conductivity $\vec{J} = \sigma \vec{E}$ resistivity $\vec{E} = \rho \vec{J}$ resistance of wire $R = \rho \frac{L}{A}$ resistance $V = IR$ Ohm's Law $\rho = \frac{m}{e^2 n \tau}$ Power $P = IV = \frac{V^2}{R} = I^2 R$

Circuit electromotive force $\mathcal{E} = \frac{dW}{dq}$ RC circuits $q = CE(1 - e^{-t/RC})$ charging. Current $i = \left(\frac{E}{R} \right) e^{-t/RC}$ Magnetic Fields Electric Field in

current-carrying wire $E = \frac{\lambda}{\epsilon_0}$ Lorentz Force $\vec{F} = q\vec{E} + q\vec{v} \times \vec{B}$ Magnetic Force $|\vec{F}| = |q|vB \sin \phi$, $\vec{F} = I \vec{L} \times \vec{B}$ Magnetic Force on Wire
 $\vec{F} = -\hat{y} \frac{Iqv}{2\pi\epsilon_0 rc^2}$ Magnetic Field of Wire $\vec{B} = \hat{z} \frac{I}{2\pi\epsilon_0 rc^2} = \hat{z} \frac{\mu_0 I}{2\pi r}$ Force $d\vec{F} = I d\vec{L} \times \vec{B}$ Line integral of closed path that does not enclose the wire is 0 $\oint_C \vec{B} \cdot d\vec{s} = \mu_0 \times (\text{current enclosed by path})$, $\oint_C \vec{B} \cdot d\vec{s} = \mu_0 \iint_S \vec{J} \cdot d\vec{s} = \mu_0 I_{\text{enclosed}}$, $\nabla \times \vec{B} = \mu_0 \vec{J}$

Ampère's Law. Helmholtz Theorem $\nabla \times \vec{B} = \mu_0 \vec{J}$, $\nabla \cdot \vec{B} = 0$, $\nabla \times \vec{E} = 0$, $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$ Circulating Charged

Particle $|q|vB = \frac{mv^2}{r}$ where $r = \frac{mv}{|q|B}$, $f = \frac{v}{2\pi r} = \frac{|q|B}{2\pi m}$ Torque on loop $\tau = NiAB \sin \theta$ Magnetic Dipole Moment $\vec{\tau} = \vec{\mu} \times \vec{B}$

where $\mu = NiA$ Energy of Magnetic Dipole Moment $U(\theta) = -\vec{\mu} \cdot \vec{B}$ Assume that \vec{B} vanishes at infinity, $\nabla \times \vec{B} = \mu_0 \vec{J}$ and $\nabla \cdot \vec{B} = 0$ uniquely determines \vec{B} if \vec{J} is given. Scalar potential $\phi(x,y,z) = k \int \frac{\rho(x',y',z')}{r} dv'$ and $\vec{E} = -\nabla\phi$. Vector potential

$\vec{B} = \nabla \times \vec{A}$, $(\nabla \cdot (\nabla \times \vec{A})) = 0$ Magnetic field of wire in cylindrical coordinates $\vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\phi}$ Vector Potential $\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{J} dv'}{r}$

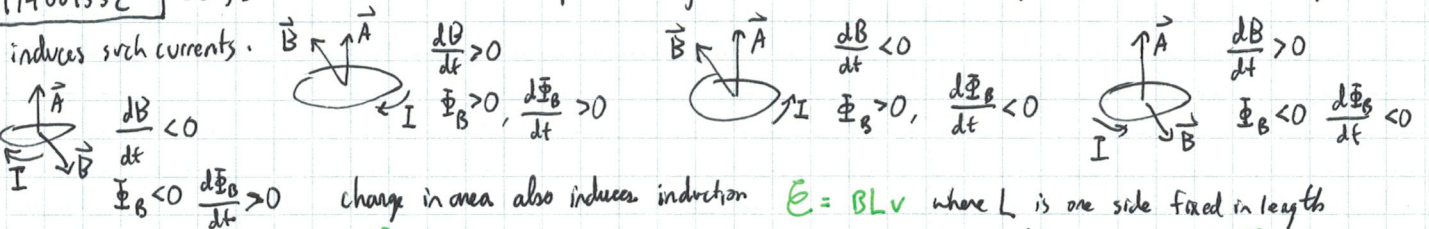
(when $\nabla \cdot \vec{A} = 0$). Vector potential of wire $\vec{A} = \frac{\mu_0 I}{4\pi} \int \frac{d\vec{L}}{r}$ Biot-Savart Law $d\vec{B} = \frac{\mu_0 I}{4\pi} \frac{d\vec{L} \times \vec{r}}{r^2} = \frac{\mu_0 I}{4\pi} \frac{d\vec{L} \times \vec{r}}{r^3}$ Magnetic Field at

Center of Arc $B = \frac{\mu_0 i \phi}{4\pi R}$ where ϕ is in rad. Magnetic field inside wire $B = \left(\frac{\mu_0 i}{2\pi R^2} \right) r$ Magnetic Field inside ideal solenoid

$B = \mu_0 i n$ Inside solenoid, $B = \frac{\mu_0 i N}{2\pi r}$ Net current inside solenoid $i_{enc} = i(nh)$ where n is $\frac{\# \text{ turns}}{\text{total length}}$

Induction & Inductance Magnetic Flux $\Phi_B = \int \vec{B} \cdot d\vec{A}$. If magnetic flux changes, current is produced $\mathcal{E} = -\frac{d\Phi_B}{dt}$

Lenz's Law: The induced current produces magnetic fields which tend to oppose the change in magnetic flux that induces such currents.



Faraday's Law $\oint \vec{E} \cdot d\vec{s} = -\frac{d\Phi_B}{dt}$ A changing magnetic field induces an electric field. Inside $E(2\pi r) = (\pi r^2) \frac{dB}{dt}$, Outside $E(2\pi r) = \pi r^2 \frac{dB}{dt}$
 $L = \frac{N\Phi_B}{i}$ inductance defined. Inductance per unit length $\frac{L}{l} = \mu_0 n^2 A$ Energy $U_B = \frac{1}{2} Li^2$ Current & Length $qV = ix$ where x is length. Self-Induction $V = -L \frac{di}{dt}$

Maxwell's Equations; Magnetism of Matter

Gauss' Law for Magnetic Fields

$\Phi_B = \oint \vec{B} \cdot d\vec{A} = 0$ Gauss' Law for Electric Fields $\Phi_E = \oint \vec{E} \cdot d\vec{A} = \frac{q_{enc}}{\epsilon_0}$ Induced Magnetic Fields $\oint \vec{B} \cdot d\vec{s} = \mu_0 \epsilon_0 \frac{d\Phi_E}{dt}$

Ampere-Maxwell Law $\oint \vec{B} \cdot d\vec{s} = \mu_0 \epsilon_0 \frac{d\Phi_E}{dt} + \mu_0 i_{enc}$ Displacement Current $i_d = \epsilon_0 \frac{d\Phi_E}{dt}$ Faraday's Law $\oint \vec{E} \cdot d\vec{s} = -\frac{d\Phi_B}{dt}$

$$\oint \vec{E} \cdot d\vec{A} = \frac{q_{enc}}{\epsilon_0} \quad \oint \vec{E} \cdot d\vec{s} = -\frac{d\Phi_B}{dt} \quad \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad \nabla \cdot \vec{B} = 0$$

$$\oint \vec{B} \cdot d\vec{A} = 0 \quad \oint \vec{B} \cdot d\vec{s} = \mu_0 \epsilon_0 \frac{d\Phi_E}{dt} + \mu_0 i_{enc} \quad \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \nabla \times \vec{B} = \mu_0 \vec{j} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

Electromagnetic Waves $E = E_m \sin(kx - \omega t)$ $B = B_m \sin(kx - \omega t)$ $c = \frac{E}{B} = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$ $B = \text{straight hand}$, $E = \text{curled hand}$

Poynting Vector $\vec{S} = \frac{1}{\mu_0} \vec{E} \times \vec{B}$ Intensity (time-avg rate per unit area at which energy is transported is \vec{S}_{avg})

$I = \frac{1}{\epsilon_0 \mu_0} E_{rms}^2$, $E_{rms} = \frac{1}{\sqrt{2}} E_m$ Point-source of EM waves $I = \frac{P}{4\pi r^2}$ Speed of Light $c = f\lambda$ Frequency Wavelength Width

$\left| \Delta \frac{s}{\lambda} \right| \approx \frac{c\Delta\lambda}{\lambda^2}$ Radiation Pressure $F = \frac{IA}{c}$ If radiation is totally reflected back along its original path $F = \frac{2IA}{c}$

Pressure $P_r = \frac{I}{c}$ Polarization. If original light is unpolarized $I = \frac{1}{2} I_0$. If original light is polarized $I = I_0 \cos^2 \theta$

Reflection & Refraction $n_2 \sin \theta_2 = n_1 \sin \theta_1$ Total Internal Reflection $\theta_c = \sin^{-1}(\frac{n_2}{n_1})$ critical angle. Polarization by Reflection

$\theta_B = \tan^{-1}(\frac{n_2}{n_1})$ Brewster angle Images Image $i = -p$ p is object distance from mirror. Spherical Mirror $\frac{1}{p} + \frac{1}{q} = \frac{1}{f} = \frac{2}{r}$

Magnitude $m = -\frac{i}{p}$ Concave $\odot \left(\begin{smallmatrix} + \\ f \end{smallmatrix} \right)$ Convex $\odot \left(\begin{smallmatrix} - \\ f \end{smallmatrix} \right)$ Refracting Surface $\frac{n_1}{p} + \frac{n_2}{q} = \frac{n_2 - n_1}{r}$

Then $\frac{1}{p} + \frac{1}{q} = \frac{1}{f} = (n-1) \left(\frac{1}{r_1} - \frac{1}{r_2} \right)$ real focus $\left(\begin{smallmatrix} + \\ f \end{smallmatrix} \right)$ virtual focus $\left(\begin{smallmatrix} - \\ f \end{smallmatrix} \right)$ if $(\frac{1}{r_1} - \frac{1}{r_2}) > 0$, will converge. Else diverge

Interference Image is real if $0 > f$, virtual if $0 < f$ (for converging lens) Diverging lens always yields virtual image (same side as object)

Interference & wavelength $\lambda_n = \frac{\lambda}{n}$ Index of refraction $n = \frac{c}{v}$ $\lambda_n = \lambda \frac{v}{c} = \frac{\lambda}{n}$

Young's Interference $d \sin(\theta) = m\lambda$ $(0, 1, 2)$ for maxima $d \sin(\theta) = (m + \frac{1}{2})\lambda$ $(0, 1, 2)$ for minima, d is slit sep. Intensity

$I = 4I_0 \cos^2(\frac{\phi}{2})$, $\phi = \frac{2\pi d}{\lambda} \sin(\theta)$ Interference in Thin Film $2L = m \frac{\lambda}{n_2}$ (minima), $2L = (m + \frac{1}{2}) \frac{\lambda}{n_2}$ maxima

Diffraction Single-slit $a \sin(\theta) = m\lambda$ (for $m=1, 2, 3, \dots$ min) Intensity $I(\theta) = I_m \left(\frac{\sin \alpha}{\alpha} \right)^2$, $\alpha = \frac{\pi a}{\lambda} \sin(\theta)$ Circular aperture

$\sin \theta = 1.22 \frac{\lambda}{d}$ d is diameter, Double slit diffraction $I(\theta) = I_m (\cos^2 \beta) \left(\frac{\sin \alpha}{\alpha} \right)^2$, $\alpha = \frac{\pi a}{\lambda} \sin(\theta)$, $\beta = \left(\frac{\pi d}{\lambda} \right) \sin(\theta)$

Grating $d \sin \theta = m\lambda$ ($m=0, 1, \dots$ max), $\Delta \theta_{hw} = \frac{\lambda}{Nd \cos \theta}$ half width Dispersion $D = \frac{\Delta \theta}{\Delta \lambda}$ Resolving power $R = \frac{\lambda_{avg}}{\Delta \lambda} = Nm$

Grating used for line spectrum, depends on wavelength.