

ASSIGNMENT - 1

1) We have,

$$B_{11} = -625 \text{ cm}^3/\text{mol}$$

$$B_{22} = -110 \text{ cm}^3/\text{mol}$$

$$B_{12} = B_{21} = -153 \text{ cm}^3/\text{mol}$$

$$P = 10 \text{ bar}$$

$$T = 313.2 \text{ K}$$

$$\text{mole fraction of butane} = \frac{(19 + 0.72)}{150} = \underline{\underline{0.61\%}}$$

$$\text{ie } y_1 = \underline{\underline{0.0061}}$$

$$y_2 = \underline{\underline{0.9939}}$$

By mixing rule, we have

$$\begin{aligned} B_{\text{mix}} &= y_1^2 B_{11} + y_1 y_2 B_{12} + y_2 y_1 B_{21} + y_2^2 B_{22} \\ &= y_1^2 B_{11} + 2y_1 y_2 B_{12} + y_2^2 B_{22} \\ &= (0.0061)^2 (-625) + 2(0.0061)(0.9939)(-153) \\ &\quad + (0.9939)^2 (-110) \\ &= \underline{\underline{-110.54 \text{ cm}^3/\text{mol}}} \end{aligned}$$

(This is very close to B_{22} because mole fraction of 1 is very low)

ie the mixture contains mostly CO_2

(a) To find molar volume of the mixture:

(At a moderate pressure like 10 bar, we can use pressure expansion of virial equation upto two terms)

$$Z = 1 + B'P$$

$$\text{But } B' = \frac{B}{RT}$$

$$\Rightarrow Z = 1 + \frac{BP}{RT}$$

$$\Rightarrow \frac{Pv}{RT} = 1 + \frac{B_{\text{mix}} P}{RT}$$

$$\Rightarrow v = B_{\text{mix}} + \frac{RT}{P} = -110.54 \frac{\text{cm}^3}{\text{mol}} + \frac{8.314 \times 313.2}{10 \times 10^5 \times 10^{-6}} \frac{\text{cm}^3}{\text{mol}}$$

$$\Rightarrow v = \underline{\underline{2493.40 \frac{\text{cm}^3}{\text{mol}}}} \rightarrow \text{molar volume of mixture}$$

(b) We can find k_{12} using the formula: (at 313.2 K)

$$|B_{12}| = \sqrt{B_{11} B_{22}} (1 - k_{12})$$

$$k_{12} = 1 - \frac{|B_{12}|}{\sqrt{B_{11} B_{22}}}$$

$$= 1 - \frac{153}{\sqrt{110 \times 625}}$$

$$\Rightarrow k_{12} = \underline{\underline{0.416481}} \rightarrow \text{binary interaction parameter}$$

$$2) \quad l = 2 \Rightarrow \text{alkane: } \underline{\underline{C_2H_6}} \quad M_w = 30 \text{ g/mol}$$

$$m = \underline{\underline{72 \text{ kg}}} \quad P = 10 + \frac{72}{19} = \underline{\underline{13.79 \text{ bar}}}$$

$$T = 273.15 + 2 \times 72 = 417.15^\circ \text{C} = \underline{\underline{690.3 \text{ K}}}$$

$$n = 72 \times 10^3 / 30 = \underline{\underline{2400 \text{ mol}}}$$

(a) Ideal gas model

$$Pv = RT$$

$$PV = nRT$$

$$V = \frac{nRT}{P} = \frac{2400 \times 8.314 \times 690.3}{13.79 \times 10^5} \text{ m}^3$$

$$V = \underline{\underline{9.988 \text{ m}^3}}$$

(b) Redlich-Kwong EOS

$$P = \frac{RT}{v-b} - \frac{a}{T^{1/2} v(v+b)} \rightarrow (1)$$

$$a = \frac{0.42748 R^2 T_c^{2.5}}{P_c} = 9.882 \left[\frac{\text{J m}^3 \text{K}^{1/2}}{\text{mol}^2} \right]$$

$$b = \frac{0.08664 R T_c}{P_c} = 4.513 \times 10^{-5} \left[\frac{\text{m}^3}{\text{mol}} \right]$$

$$\left[T_c = 305.4 \text{ K}, \quad P_c = 48.74 \text{ bar} \right]$$

Now, we can use

$P = 13.79 \times 10^5 \text{ Pa}$, $T = 690.3 \text{ K}$, a and b
to find v numerically

I used Newton-Raphson method (not including all the iterations here because of space constraint)

$$v = 0.004143 \text{ m}^3/\text{mol}$$

$$\Rightarrow V = v n = 0.004143 \times 2400 = \underline{\underline{9.9432 \text{ m}^3}}$$

(c) Peng-Robinson EOS

$$P = \frac{RT}{v-b} - \frac{a \alpha(T)}{v(v+b) + b(v-b)}$$

$$\text{where } \alpha = [1 + K(1 - \sqrt{T_n})]^2$$

$$T_n = \frac{T}{T_c} = \frac{690.3}{305.4} = \underline{\underline{2.2603}}$$

$$w \text{ of ethane} = 0.099$$

$$K = 0.37464 + 1.54226w + -0.26992w^2$$
$$= \underline{\underline{0.52468}}$$

$$\Rightarrow \underline{\underline{\alpha = 0.5415}}$$

~~Substituting~~

$$a = \frac{0.45724(RT_c)^2}{P_c} = 0.6048 \left[\frac{\text{J m}^3}{\text{mol}^2} \right]$$

$$b = \frac{0.07780 RT_c}{P_c} = 4.053 \times 10^{-5} \left[\frac{\text{m}^3}{\text{mol}} \right]$$

Now, we use the values of P, T, R, a, b and α in Peng-Robinson EOS to find v numerically

I used Newton-Raphson method

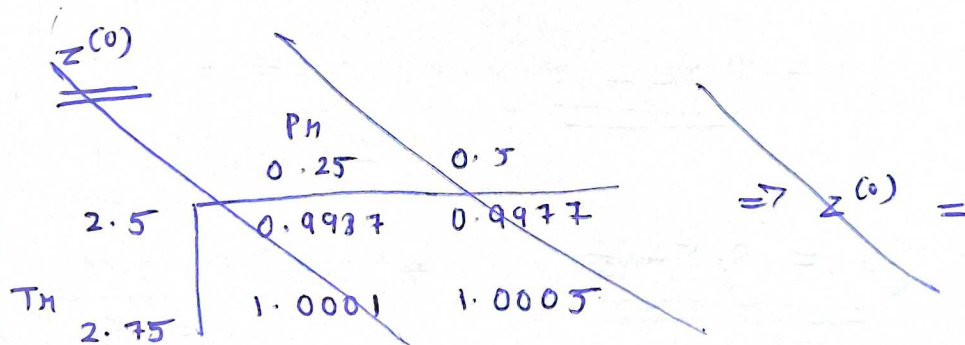
$$v = 0.004149 \frac{\text{m}^3}{\text{mol}}$$

$$\Rightarrow V = v \times n = 0.004149 \times 2400 = \underline{\underline{9.9576 \text{ m}^3}}$$

(d) Compressibility charts

$$T_h = \frac{T}{T_c} = \frac{690.3}{305.4} = 2.2603$$

$$P_h = \frac{P}{P_c} = \frac{13.79}{48.74} = 0.283$$



<u>$Z^{(0)}$</u>		P_h	
		0.25	0.5
T_h	2.25	0.9965	0.9935
	2.5	0.9987	0.9977

By double interpolation,

$$Z^{(0)} = \underline{\underline{0.9962}}$$

z⁽¹⁾

T _n	P _n	
	0.25	0.5
2.25	0.0181	0.0360
2.5	0.0168	0.0334

By double interpolation,

$$z^{(1)} = \underline{\underline{0.02}}$$

w = 0.099 for ethane

$$z = z^{(w)} + z^{(1)} \times w = \frac{P_v}{RT}$$

$$v = \frac{8.314 \times 690.3}{13.79 \times 10^5} [0.9962 + 0.02 \times 0.099]$$

$$v = 0.004154 \frac{\text{m}^3}{\text{mol}}$$

$$\Rightarrow V = v n = 0.004154 \times 2400 = \underline{\underline{9.97 \text{ m}^3}}$$

All methods - Tabulated

Value of V in m³

Ideal gas : 9.988

Redlich - Kwong : 9.9432

Peng - Robinson : 9.9576

Compressibility charts : 9.97

3)

Berthelot EOS

(a)

$$P = \frac{RT}{v-b} - \frac{a}{Tv^2}$$

At critical point, $P = P_c$, $T = T_c$, $v = v_c$

$$\Rightarrow P_c = \frac{RT_c}{v_c - b} - \frac{a}{T_c v_c^2}$$

$$\left(\frac{\partial P}{\partial v} \right)_{T_c} = \frac{-RT_c}{(v_c - b)^2} + \frac{2a}{T_c v_c^3} = 0 \rightarrow (1)$$

$$\left(\frac{\partial^2 P}{\partial v^2} \right)_{T_c} = \frac{2RT_c}{(v_c - b)^3} - \frac{6a}{T_c v_c^4} = 0 \rightarrow (2)$$

$$\left[\frac{\partial P}{\partial v} \text{ and } \frac{\partial^2 P}{\partial v^2} = 0 \text{ at critical point} \right]$$

~~$$(1) \times 2 + (2) \times$$~~

$$(eqn (1)) \times 2 + (eqn (2)) \times (v_c - b)$$

$$\Rightarrow \frac{4a}{T_c v_c^3} - \frac{6a(v_c - b)}{T_c v_c^4} = 0$$

$$\Rightarrow \boxed{v_c = 3b} \rightarrow (3)$$

Substituting $v_c = 3b$ in eqn (1)

$$\Rightarrow \boxed{a = \frac{9}{8} v_c R T_c^2} \rightarrow (4)$$

Substituting (3) and (4) in

$$P_c = \frac{RT_c}{v_c - b} - \frac{a}{T_c v_c^2}$$

$$\Rightarrow P_c = \frac{RT}{3b - b} - \frac{\frac{a}{8} v_c R T_c^2}{T_c v_c^2}$$

$$P_c = \frac{RT}{2b} - \frac{9RT_c^3}{8(3b)} = \frac{RT_c}{8P_c}$$

$$\Rightarrow \boxed{b = \frac{RT_c}{8P_c}}$$

$$a = \frac{9}{8} v_c R T_c^2 = \frac{9}{8} (3b) R T_c^2$$

$$= \frac{9}{8} \times \left(3 \times \frac{RT_c}{8P_c} \right) \times R T_c^2$$

$$\boxed{a = \frac{27 R^2 T_c^3}{64 P_c}}$$

(b) We have,

$$v_c = 3b \rightarrow (1)$$

$$a = \frac{27}{64} \frac{R^2 T_c^3}{P_c} \rightarrow (2)$$

$$b = \frac{RT_c}{8P_c} \rightarrow (3)$$

Substituting (1) in Boltzlot EOS

$$\Rightarrow P = \frac{RT}{v - \frac{v_c}{3}} - \frac{a}{Tv^2}$$

$$\Rightarrow P = \frac{\frac{RT}{v_c}}{\left(\frac{v}{v_c}\right) - \frac{1}{3}} - \frac{a}{Tv^2}$$

$$(v_h = \frac{v}{v_c})$$

$$\Rightarrow P = \frac{\frac{RT}{b}}{3v_h - 1} - \frac{a}{Tv^2}$$

Substituting (3)

$$\Rightarrow P = \frac{\frac{RT}{RT_c} \times 8P_c}{3v_h - 1} - \frac{a}{Tv^2}$$

$$\Rightarrow P = \frac{8P_c T_h}{3v_h - 1} - \frac{a}{Tv^2} \quad (T_h = \frac{T}{T_c})$$

Substituting (2)

$$\Rightarrow P = \frac{8P_c T_h}{3v_h - 1} - \frac{27 T_c^3 R^2}{64 P_c T v^2}$$

$$\text{From (3), } R^2 T_c^2 = 64 P_c^2 b^2$$

$$\Rightarrow P = \frac{8P_c T_h}{3v_h - 1} - \frac{27 P_c T_c b^2}{Tv^2}$$

Now substituting (1)

$$\Rightarrow P = \frac{8 P_c T_H}{3 v_H - 1} - \frac{3 P_c T_c v_c^2}{T v^2} \quad (P_H = \frac{P}{P_c})$$

$$\Rightarrow \boxed{P_H = \frac{8 T_H}{3 v_H - 1} - \frac{3}{T_H v_H^2}} \rightarrow \text{reduced form}$$

(c) From (2), we have

$$P = 13.79 \text{ bar}$$

$$T = 690.3 \text{ K}$$

$$a = \frac{27 R^2 T_c^3}{64 P_c} = \underline{\underline{602.347 \text{ Pa K}^{\frac{3}{2}} \frac{\text{m}^6}{\text{mol}}}}$$

$$b = \frac{R T_c}{8 P_c} = \underline{\underline{23.016 \times 10^{-5} \frac{\text{m}^3}{\text{mol}}}}$$

Substituting these values in Berthelot EOS:

$$P = \frac{RT}{v-b} - \frac{a}{T v^2}$$

We can solve v using numerical techniques.
 & using Newton-Raphson method

$$v = 0.004251 \text{ m}^3/\text{mol}$$

$$V = v \times n = 0.004251 \times 2400 = \underline{\underline{10.2 \text{ m}^3}}$$

4)

Vanderwaal's parameters

$$a = \frac{27}{64} \frac{R^2 T_c^2}{P_c} \left[\frac{\text{J m}^3}{\text{mol}^2} \right]$$

$$b = \frac{R T_c}{8 P_c} \left[\frac{\text{m}^3}{\text{mol}} \right]$$

I choose Benzene ($\text{mw} = 78 \text{ g/mol} \rightarrow \text{condition (1)}$).

oxygen and propane (oxygen $\rightarrow 0 \rightarrow \text{condition (2)}$)

Gas	P_c (bar)	T_c (K)	$a = \frac{27 R^2 T_c^2}{64 P_c}$ $\left(\frac{\text{J m}^3}{\text{mol}^2} \right)$	$b = \frac{R T_c}{8 P_c}$ $\left(\text{m}^3/\text{mol} \right)$
Benzene	48.94	562.1	1.88	1.19×10^{-4}
Oxygen	50.46	154.6	0.138	3.18×10^{-5}
Propane	42.44	370	0.94	9.06×10^{-5}

a : Benzene > Propane > Oxygen

b : Benzene > Propane > Oxygen

Physical significance

a \rightarrow affected by attractive interaction

b \rightarrow affected by size

a

All three of them are non-polar molecules. Therefore, only London dispersion forces are prevalent. Larger and heavier atoms and molecules exhibit stronger dispersion forces than smaller and lighter ones.

This is because in larger atom or molecule, the valence electrons are, on average, further from the nuclei than in a smaller atom or molecule.

They are less tightly held and can more easily form temporary dipoles, i.e. larger molecules have more polarizability. Benzene is largest and heaviest, while O_2 is the smallest.

\therefore a: Benzene > Propane > Oxygen

b

b is directly dependent on size of molecule

~~\therefore~~ Benzene is largest and O_2 is smallest.

\therefore b: Benzene > Propane > Oxygen

5: Considering mixture of O_2 and propane

For both O_2 and propane, the dipole moments are zero. ($a \rightarrow O_2$ $b \rightarrow C_3H_8$)

\therefore dipole-dipole and induction forces are zero

$$\mu_a = \mu_b = 0$$

\therefore Only force is dispersion

$$\begin{aligned} \Gamma_{aa} &= \Gamma_{aa}^{\text{dipole-dipole}} + \Gamma_{aa}^{\text{induction}} + \Gamma_{aa}^{\text{dispersion}} \\ &\quad \downarrow \qquad \qquad \downarrow \qquad \qquad \downarrow \\ &\quad \frac{-2}{3} \frac{\mu_a^2 \mu_a^2}{kT} \frac{1}{r^6} \qquad \frac{-\alpha_a \mu_a^2}{r^6} - \frac{\alpha_a \mu_a^2}{r^6} \qquad \frac{-3}{2} \frac{\alpha_a \alpha_a}{r^6} \frac{I_a I_a}{I_a + I_a} \\ &\quad \downarrow \qquad \qquad \qquad \downarrow \qquad \qquad \downarrow \\ &\quad 0 \qquad \qquad \qquad 0 \qquad \qquad \frac{-3}{4} \frac{\alpha_a^2 I_a}{r^6} \end{aligned}$$

$$\boxed{\Gamma_{aa} = -\frac{3}{4} \frac{\alpha_a^2 I_a}{r^6}}$$

$$\begin{aligned} \Gamma_{bb} &= \Gamma_{bb}^{\text{dipole-dipole}} + \Gamma_{bb}^{\text{induction}} + \Gamma_{bb}^{\text{dispersion}} \\ &\quad \downarrow \qquad \qquad \downarrow \qquad \qquad \downarrow \\ &\quad \frac{-2}{3} \frac{\mu_b^2 \mu_b^2}{kT} \frac{1}{r^6} \quad \frac{-\alpha_b \mu_b^2}{r^6} - \frac{\alpha_b \mu_b^2}{r^6} \qquad \frac{-3}{4} \frac{\alpha_b^2 I_b}{r^6} \\ &\quad \downarrow \qquad \qquad \qquad \downarrow \qquad \qquad \downarrow \\ &\quad 0 \qquad \qquad \qquad 0 \qquad \qquad \frac{-3}{4} \frac{\alpha_b^2 I_b}{r^6} \end{aligned}$$

$$\boxed{\Gamma_{bb} = -\frac{3}{4} \frac{\alpha_b^2 I_b}{r^6}}$$

$$\Gamma_{ab} = \underbrace{\Gamma_{a-b}}_{\text{dipole-dipole}} + \underbrace{\Gamma_{a-b}}_{\text{induction}} + \underbrace{\Gamma_{a-b}}_{\text{dispersion}}$$

$$\downarrow \qquad \qquad \downarrow \qquad \qquad \downarrow$$

$$\frac{-2}{3} \frac{\mu_a^2 \mu_b^2}{kT} \frac{1}{r^6} \qquad \frac{-\alpha_a \mu_b^2}{r^6} - \frac{\alpha_b \mu_a^2}{r^6} \qquad \frac{-3}{2} \frac{\alpha_a \alpha_b}{r^6} \frac{I_a I_b}{I_a + I_b}$$

$$\downarrow \qquad \qquad \downarrow$$

$$0 \qquad \qquad 0$$

$$\boxed{\Gamma_{ab} = \frac{-3}{2} \frac{\alpha_a \alpha_b}{r^6} \frac{I_a I_b}{I_a + I_b}}$$

Note: the terms became zero because $\mu_a = \mu_b = 0$
(dipole moment is zero for non-polar molecules)

Oxygen (a)

$$\alpha_a = 16 \times 10^{-25} \text{ cm}^3$$

$$I_a = 12.07 \text{ eV}$$

Propane (b)

$$\alpha_b = 62.9 \times 10^{-25} \text{ cm}^3$$

$$I_b = 10.94 \text{ eV}$$

Substituting the above values,

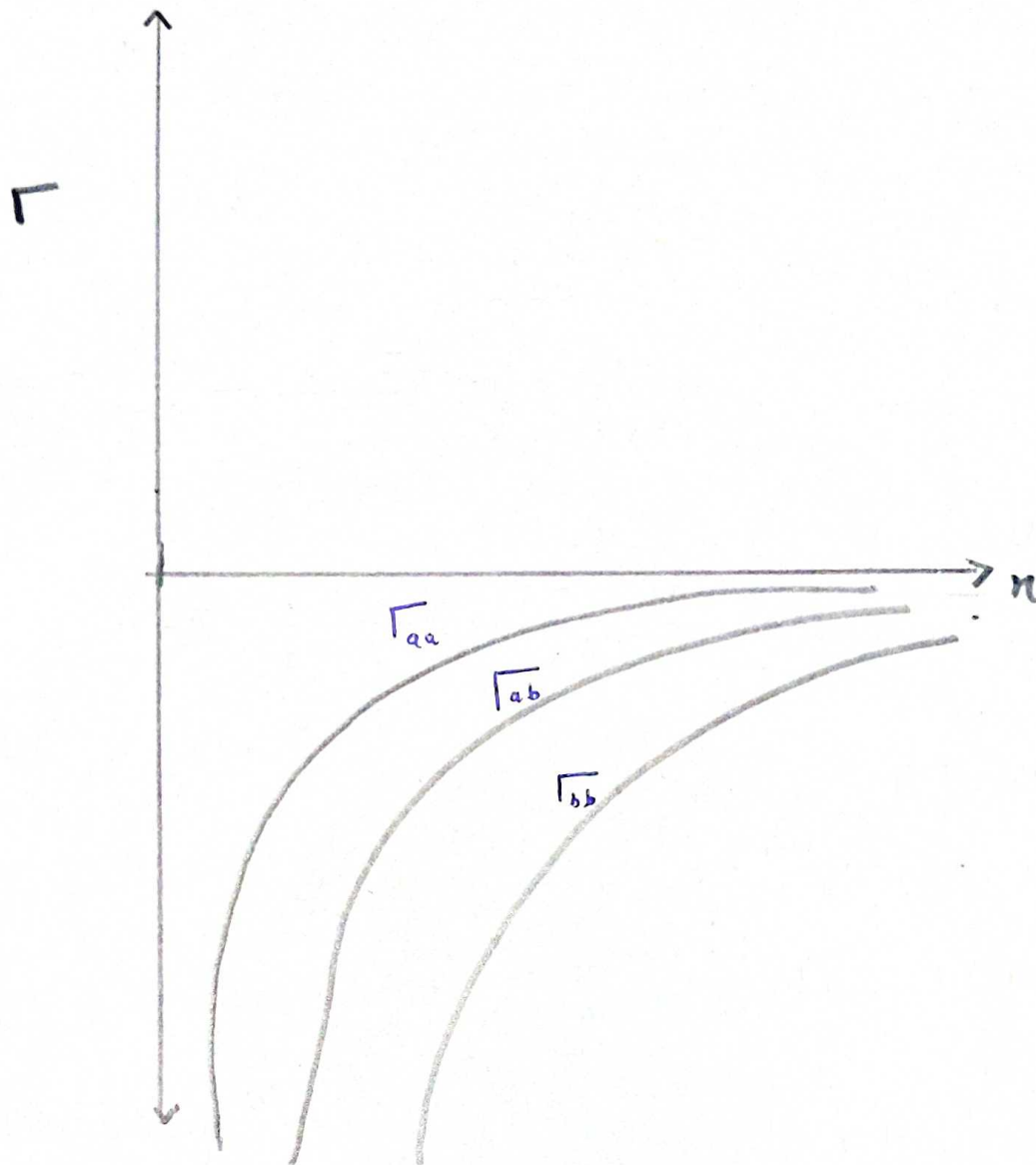
$$\Gamma_{aa} = \frac{-2.317 \times 10^{-47}}{r^6} \text{ (eV) (cm}^6\text{)}$$

$$\Gamma_{bb} = \frac{-32.462 \times 10^{-47}}{r^6} \text{ (eV) (cm}^6\text{)}$$

$$\Gamma_{ab} = \frac{-8.663 \times 10^{-47}}{r^6} \text{ (eV) (cm}^6\text{)}$$

} attractive
interactions

Qualitative plot of Γ_{aa} , Γ_{ab} , Γ_{bb}



Attractive interactions are maximum when $n \rightarrow 0$