

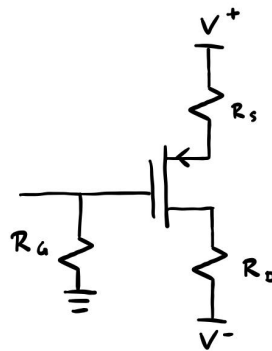
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 Experiment 4 Lab Report  
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## PMOS Common-Source Amplifier

### DC Operating Point Analysis

Using the PMOS common-source amplifier, a simplified model of which is seen in *Figure 1*, allows for characteristic calculations of the circuit and transistor to be completed. A PMOS transistor, such as the [CD4007](#) can be used.

### PMOS Common Source Amplifier



*Figure 1: Simplified PMOS common-source amplifier.*

The DC current going through  $R_g$  can be found to equal  $\sim 0A$ . This reveals that the transistor has an overdrive voltage of  $2.12V$ , seen in the following calculation:

$$\begin{aligned}
 V_{OV} &= V_{SG} - |V_{tp}| \\
 I_D &= \frac{1}{2} k_p' \frac{W}{L} (v_{SG} - |v_{tp}|)^2 \text{ such that} \\
 v_{SG} &= \sqrt{\frac{2I_D}{k_p' \frac{W}{L}}} + |v_{tp}| \\
 V_{OV} &= \sqrt{\frac{2I_D}{k_p' \frac{W}{L}}} + |v_{tp}| - |v_{tp}| = \sqrt{\frac{2I_D}{\mu_p \frac{\epsilon_{ox} W}{t_{ox} L}}} = 2.12V
 \end{aligned}$$

From there, we can calculate

$$\begin{aligned}
 g_m &= \frac{2I_D}{V_{OV}} = 943.4 \mu S \\
 V_{SG} &= V_{OV} + |V_{tp}| = 2.62V
 \end{aligned}$$

$$r_o = \frac{1}{\lambda I_d'} = 23.8k\Omega$$

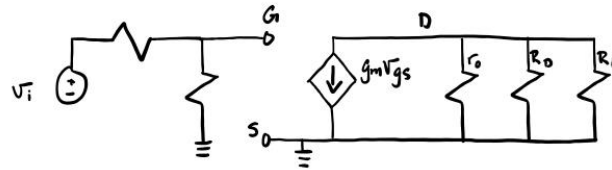
Finally, we can calculate  $R_S$ , which can be achieved by connecting resistors in any series or parallel combination to achieve  $R_S$ .

$$R_S = \frac{V_s - V_{ss}}{I_D} = 17.62k\Omega$$

### AC Analysis

The PMOS common-source amplifier can be modeled using a small-signal analysis seen in *Figure 2*. The resulting model has no  $R_S$ , as a result of a bypass capacitor. Additionally,  $V_+$  becomes part of the transconductance and acts to bias the circuit.

### PMOS Small Signal Model



*Figure 2: PMOS small-signal model.*

By inspection, we can see that  $v_i = v_{sig}$ , as  $v_{sig}$  is the small signal input voltage for the model. This means that  $\frac{v_i}{v_{sig}} \approx 1$ . Further, the voltage gain,  $A_v$ , can be derived from the following calculations:

$$\begin{aligned} v_o &= -g_m v_{gs} R_D \\ v_i &= v_{sig} = v_{gs} \\ A_v &= \frac{v_o}{v_i} = -g_m (R_D || R_L) \end{aligned}$$

This would mean that, for a small-signal voltage gain of at least  $A_v = -5 V/V$ , that

$(R_D || 10k\Omega) = \frac{A_v}{-g_m} = 5.3k\Omega$  such that  $R_D = 12.7k\Omega$ . While this value isn't a standard resistance, it can be achieved by connecting resistors in any series or parallel combination to achieve  $R_D$ . The DC voltage at the drain is equal to  $-2.3V$ . Since  $v_{DG} \geq |V_{tp}|$  the transistor is in saturation. Finally,  $r_o$  is equal to that found before:  $r_o = \frac{1}{\lambda I_d'} = 23.8k\Omega$ .

### Simulation

Simulating this circuit with capacitances of  $47\mu F$  and the resistance values found above provides the following outputs in *Figure 3*, *Figure 4*, and *Figure 5*. The DC values are seen in *Figure 6*.

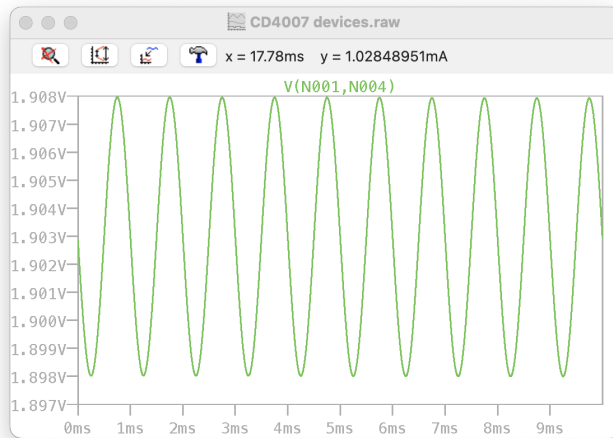


Figure 3:  $V_{SG}$ .

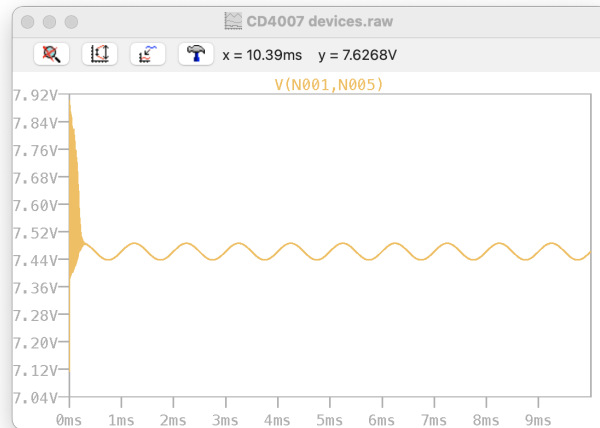


Figure 4:  $V_{SD}$ .

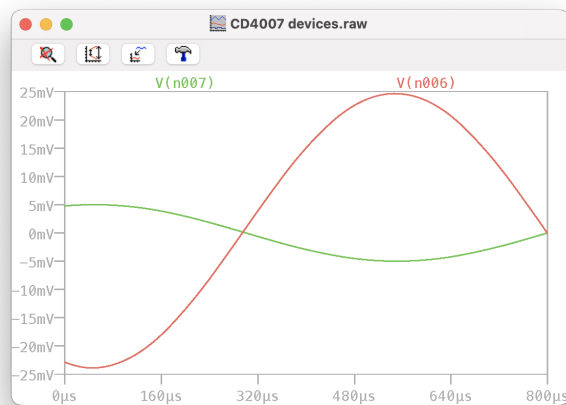


Figure 5:  $I_D$ .

$V_{SG}$	$\sim 1.90V$
$V_{SD}$	$\sim 7.48V$
$I_D$	$\sim 744\mu A$

*Figure 6: DC values of measurements.*

These values seem to be consistent with the calculations, when it is taken into account that, because of the more complex model of a real transistor, there are some small variations. Finally, in *Figure 7* we can see the input and output signals. The observed output is closer to  $-4.9 V/V$  rather than  $-5 V/V$ .



*Figure 7: Input vs output signals.*

## NMOS Common-Source Amplifier

### DC Operating Point Analysis

Using the NMOS common-source amplifier, a simplified model of which is seen in *Figure 8*, allows for characteristic calculations of the circuit and transistor to be completed. A NMOS transistor, such as the [CD4007](#) can be used.

## NMOS Common Source Amplifier

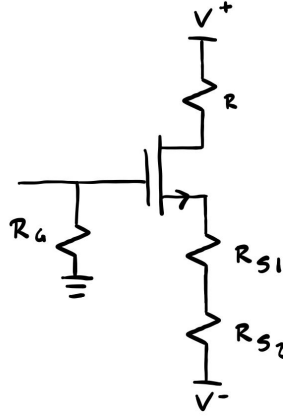


Figure 8: Simplified NMOS common-source amplifier.

The DC current going through  $R_g$  can be found to equal  $\sim 0A$ . This reveals that the transistor has an overdrive voltage of 2.88V, seen in the following calculation:

$$V_{OV} = V_{GS} - V_{tn}$$

$$I_D = \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_{tn})^2 \text{ such that}$$

$$v_{GS} = \sqrt{\frac{2I_D}{k_n' \frac{W}{L}}} + V_{tn}$$

$$V_{OV} = \sqrt{\frac{2I_D}{k_n' \frac{W}{L}}} + V_{tn} - V_{tn} = \sqrt{\frac{2I_D}{\mu_n \frac{\epsilon_{ox}}{t_{ox}} \frac{W}{L}}} = 2.88V$$

From there, we can calculate

$$g_m = \frac{2I_D}{V_{OV}} = 694.4\mu S$$

$$V_{GS} = V_{OV} + V_{tn} = 3.98V$$

$$r_o = \frac{1}{\lambda I_D} = 7.58k\Omega$$

Finally, we can calculate  $R_{S2}$ , which can be achieved by connecting resistors in any series or parallel combination to achieve  $R_S$ .

$$R_S = \frac{V_S - V_{SS}}{I_D} - 220\Omega = 10.98k\Omega$$

### AC Analysis

The NMOS common-source amplifier can be modeled using a small-signal analysis seen in *Figure 9*. The resulting model has no  $R_{S2}$ , as a result of a bypass capacitor. The model does, however, have a  $R_{S1}$  component. Additionally,  $V_-$  becomes part of the transconductance and acts to bias the circuit.

## NMOS Small Signal Model

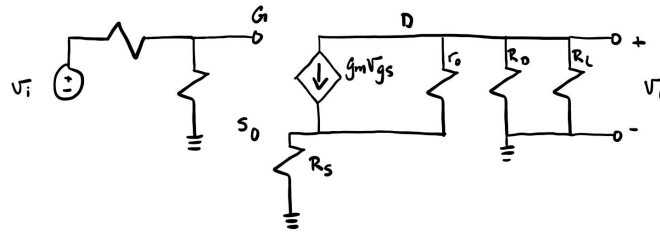


Figure 9: NMOS small-signal model.

By inspection, we can see that  $v_i = v_{sig}$ , as  $v_{sig}$  is the small signal input voltage for the model. This means that  $\frac{v_i}{v_{sig}} \approx 1$ . Further, the voltage gain,  $A_v$ , can be derived from the following calculations:

$$v_o = IR_D$$

$$I = \frac{g_m v_i}{1 + g_m R_s}$$

$$v_i = v_{sig} = v_{gs}$$

$$A_v = \frac{v_o}{v_i} = - \frac{(R_D || R_L)}{1/g_m + R_s}$$

This would mean that, for a small-signal voltage gain of at least  $A_v = -4 V/V$ , that

$(R_D || 10k\Omega) = A_v(-\frac{1}{g_m} + R_s) = 4.88k\Omega$  such that  $R_D = 9.55k\Omega$ . While this value isn't a standard resistance, it can be achieved by connecting resistors in any series or parallel combination to achieve  $R_D$ . The DC voltage at the drain is equal to  $V_D = 1mA(9.55k\Omega) - 15V = -5.45V$  meaning that since  $v_{GD} \leq V_{tn}$  that the transistor is in saturation.

### Simulation

Simulating this circuit with capacitances of  $47\mu F$  and the resistance values found above provides the following outputs in Figure 10, Figure 11, and Figure 12. The DC values are seen in Figure 13.

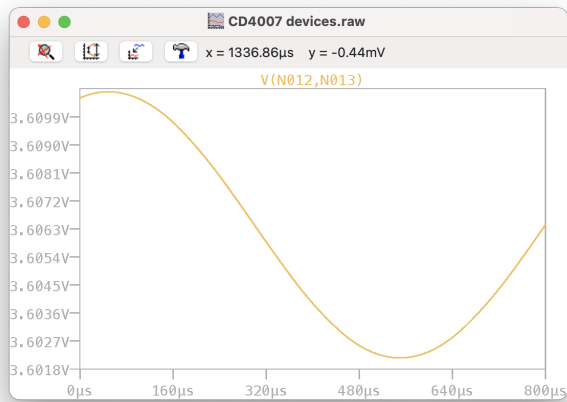


Figure 10:  $V_{GS}$

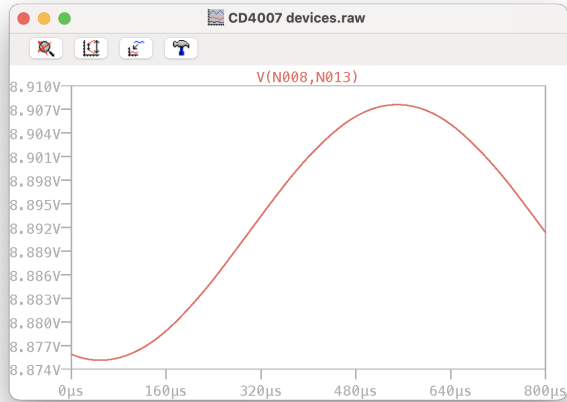


Figure 11:  $V_{DS}$

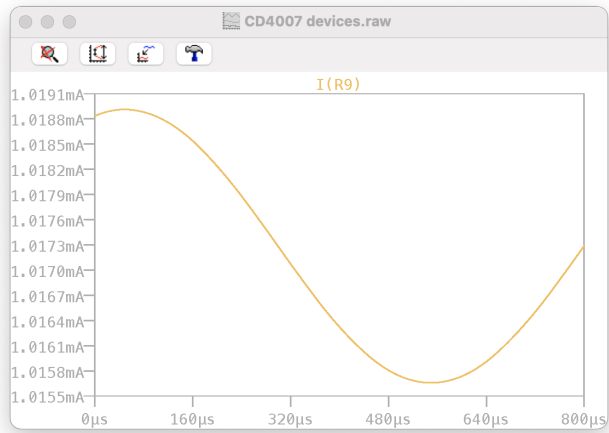
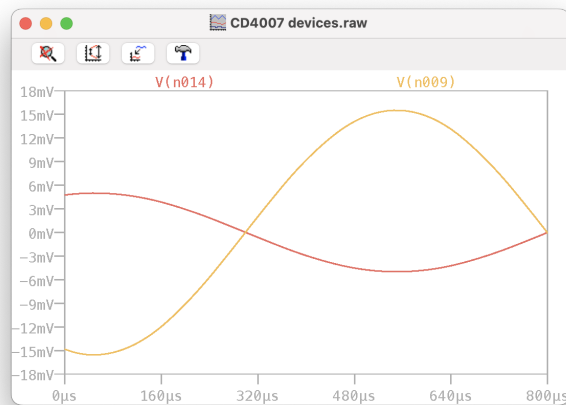


Figure 12:  $I_D$

$V_{GS}$	$\sim 3.60V$
$V_{DS}$	$\sim 8.89V$
$I_D$	$\sim 1.02mA$

*Figure 13: DC values of measurements.*

These values seem to be consistent with the calculations, when it is taken into account that, because of the more complex model of a real transistor, there are some small variations. Finally, in *Figure 14* we can see the input and output signals. The observed output is closer to  $-3.08 V/V$  rather than  $-4 V/V$ .



*Figure 14: Input vs. output signal.*

## NMOS Source Follower

### DC Operating Point Analysis

Using the PMOS common-source amplifier, a simplified model of which is seen in *Figure 15*, allows for characteristic calculations of the circuit and transistor to be completed. A NMOS transistor, such as the [CD4007](#) can be used.



## NMOS Source Follower

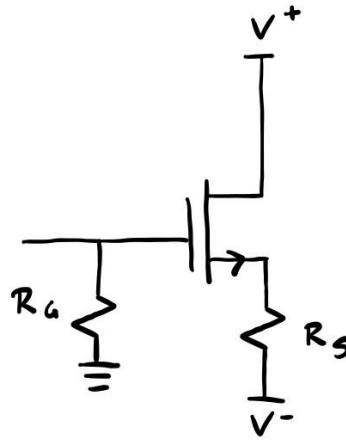


Figure 15: Simplified NMOS source follower.

The DC current going through  $R_g$  can be found to equal  $\sim 0A$ . As seen in the NMOS common-source amplifier, this transistor has an overdrive voltage of 2.88V.

$$V_{OV} = V_{GS} - V_{tn}$$

$$I_D = \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_{tn})^2 \text{ such that}$$

$$v_{GS} = \sqrt{\frac{2I_D}{k_n' \frac{W}{L}}} + V_{tn}$$

$$V_{OV} = \sqrt{\frac{2I_D}{k_n' \frac{W}{L}}} + V_{tn} - V_{tn} = \sqrt{\frac{2I_D}{\mu_n \frac{\epsilon_{ox}}{t_{ox}} \frac{W}{L}}} = 2.88V$$

With a required  $I_D$  of 1mA, this means that  $R_s = 2.88k\Omega$ .

### AC Analysis

## NMOS Small Signal Model

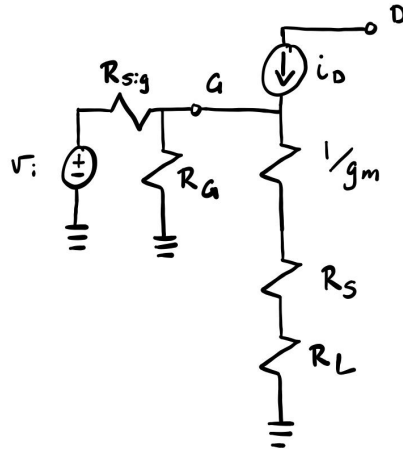


Figure 16: NMOS source follower small-signal model.

From this model, we can find that the ratio between the output and input signals can be simplified as follows:

$$v_i = v_{sig} \text{ such that } \frac{v_i}{v_{sig}} = 1$$

$$A_v = \frac{V_o}{V_i} = \frac{(R_L + R_S)}{(R_L + R_S) + 1/g_m}$$

$$g_m = \frac{2I_D}{V_{ov}} = 694.4 \mu S$$

$$A_v = \frac{(R_L + R_S)}{(R_L + R_S) + 1.44 k\Omega}$$

$$R_o = \frac{1}{g_m} = 1.44 k\Omega$$

From these equations, we can see that  $(R_L \parallel R_S)$  must be at least  $5.67 k\Omega$ , therefore,  $R_L = R_S = 11.34 k\Omega$ .

### Simulation

Simulating this circuit with capacitances of  $47 \mu F$  and the resistance values found above provides the following outputs in Figure 17, Figure 18, and Figure 19. The DC values are seen in Figure 20.

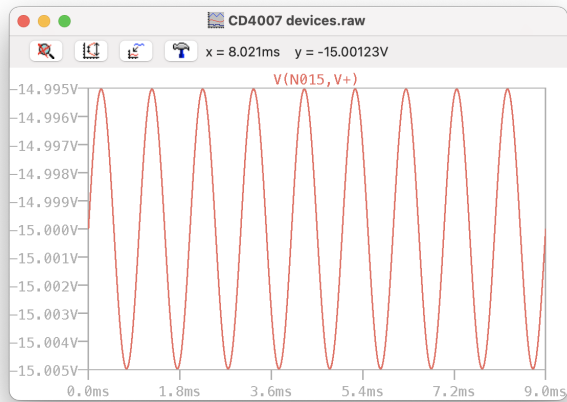


Figure 17:  $V_{GS}$

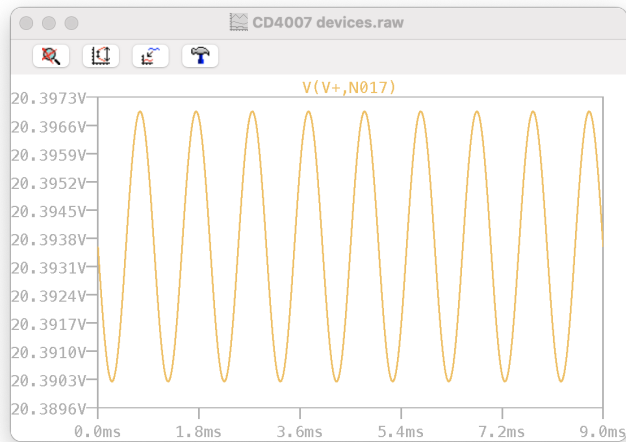


Figure 18:  $V_{DS}$



Figure 19:  $I_D$

$V_{GS}$	$\sim 15.0V$
$V_{DS}$	$\sim 20.39V$
$I_D$	$\sim 1.02mA$

*Figure 13: DC values of measurements.*

These values seem to be consistent with the calculations, when it is taken into account that, because of the more complex model of a real transistor, there are some small variations. Finally, in *Figure 14* we can see the input and output signals. The observed output is closer to  $-0.68 V/V$  rather than  $-0.8 V/V$ .



*Figure 20: Input vs. output signal.*