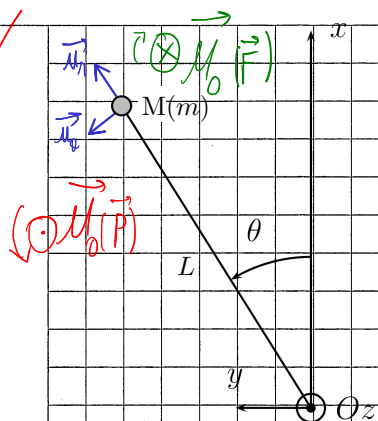


1/



1)

Systeme = {masse} Reperee par  $M(m)$

Repere: cylindrique  $(O, \vec{u}_r, \vec{u}_\theta, \vec{u}_z)$

Reperage:  $\vec{OM} = L \vec{u}_r$

$$\vec{v} = L \dot{\theta} \vec{u}_\theta$$

$$\vec{a} = L \ddot{\theta} \vec{u}_\theta - L \dot{\theta}^2 \vec{u}_r$$

BDF:  $\vec{P} = -mg \vec{u}_z = -mg(\cos \theta \vec{u}_r + \sin \theta \vec{u}_\theta)$   
 $\vec{F}$  inconnue

BdM:  $\mathcal{M}_O(\vec{P}) = \vec{OM} \wedge \vec{P} = +mgL \vec{u}_r \wedge (\cos \theta \vec{u}_r + \sin \theta \vec{u}_\theta) = +mgL \sin \theta \vec{u}_z$   
 $\mathcal{M}_O(\vec{F}) = -C \vec{u}_z$

et  $\mathcal{L}_O(M) = \vec{OM} \wedge m \vec{v} = mL \vec{u}_r \wedge L \dot{\theta} \vec{u}_\theta = mL^2 \dot{\theta} \vec{u}_z$

D'a sur l'axe  $(O, \vec{u}_z)$ :

$$\mathcal{M}_z(\vec{P}) = +mgL \sin \theta$$

$$\mathcal{M}_z(\vec{F}) = -C \theta$$

$$\mathcal{L}_z(M) = mL^2 \dot{\theta}$$

Ainsi avec le TMC,

$$\frac{d}{dt} \mathcal{L}_z(M) = \mathcal{M}_z(\vec{P}) + \mathcal{M}_z(\vec{F})$$

$$\Leftrightarrow mL^2 \ddot{\theta} = mgL \sin \theta - C \theta$$

$$\Leftrightarrow \ddot{\theta} + \frac{C}{mL^2} \theta - \frac{g}{L} \sin \theta = 0$$

2)

Au lieu de  $\theta_0 = 0$ ,  $\sin \theta \sim \theta$

$$\text{D'a } \ddot{\theta} + \left( \frac{C}{mL^2} - \frac{g}{L} \right) \theta = 0$$

stable si  $\rightarrow 0$  (a)

$$\Leftrightarrow C > mgL$$

Car eq. caract:  $\lambda^2 + \omega_0^2 = 0 \Rightarrow A \cos + B \sin$

3)

$$\vec{F} = -\frac{C}{L} \theta \vec{u}_r$$

$$\text{Sx } (\vec{F}) = -L \theta \vec{u}_r$$

$$d\vec{u}_r = \sin \theta \vec{u}_\theta + \cos \theta \vec{u}_z$$

$$\ddot{\theta} - \left( \frac{g}{L} - \frac{C}{mL^2} \right) \theta = 0$$

$$\text{ssi } \omega_0^2 > 0$$

$$\Delta \vec{D} = \vec{C} \cdot \vec{\theta} \cdot \vec{L} \cdot d\vec{\theta} = + d\vec{E}_{pot}$$

$$\Delta \vec{D} = \boxed{\frac{dE_{pot}}{d\theta} = C\theta} \Rightarrow E_{pot} = \frac{C\theta^2}{2} + K$$

Or,  $E_{pp} = mgL \cos \theta$  donc

$$E_{pot} = mgL \cos \theta + \frac{C\theta^2}{2} + K$$

$$\frac{dE_{pot}}{d\theta} = -mgL \sin \theta + C\theta = 0$$

$$\frac{d^2 E_{pot}}{d\theta^2} = -mgL \cos \theta + C \Rightarrow 0$$

soit pour  $\theta_0 = 0$ ,  $\left. \frac{d^2 E_{pot}}{d\theta^2} \right|_{\theta=0} > 0 \Leftrightarrow C > mgL$ ! Pareil! ✓

4)  $\omega = \sqrt{\frac{C - mgL}{mL^2}} \Rightarrow \frac{2\pi}{T} = \dots \Rightarrow T = 2\pi \sqrt{\frac{mL^2}{C - mgL}}$

5)  $g_0 = \frac{C}{mL} \Rightarrow T = 2\pi \sqrt{\frac{mL \times L}{mL(g_0 - g)}}$

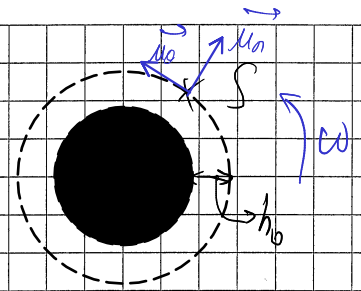
$$\Leftrightarrow T = 2\pi \sqrt{\frac{L}{g_0 - g}}$$

:  $g_0 \approx g \Rightarrow$  varia<sup>n</sup> de  $g$  se traduisent par fortes varia<sup>n</sup> de  $T$ , mesurables

Remarque:  $g_0 < g \Rightarrow$  ~~pas~~, plus d'oscill<sup>n</sup>.

II/1)

- Systeme: } satellite
- Reférentiel: géocentrique
- Repere: polaire,  $(\vec{r}, \vec{u}_r, \vec{u}_\theta)$
- Reperage:



$$\begin{aligned} \vec{OM} &= (R + h_0) \vec{u}_r = R \vec{u}_r \\ \vec{v} &= \dot{R} \vec{u}_r + R \dot{\theta} \vec{u}_\theta \Rightarrow v = |\dot{R} \vec{u}_r| \\ \vec{a} &= \ddot{R} \vec{u}_r - R \dot{\theta}^2 \vec{u}_r \\ \text{BDF: } \vec{F}_g &= -G \frac{m_1 m_2}{R^2} \vec{u}_r \Rightarrow E_p = -G \frac{m_1 m_2}{R} = -G \frac{m_1 m_2}{R + h_0} \\ \text{AFD: } m \vec{a} &= \vec{F}_g \\ \Rightarrow \begin{cases} -m \ddot{R} &= -G \frac{m_1 m_2}{R^2} \\ \ddot{\theta} &= 0 \end{cases} \Rightarrow \begin{cases} \dot{\theta} = \omega \\ \dot{\theta} = \omega \end{cases} \end{aligned}$$

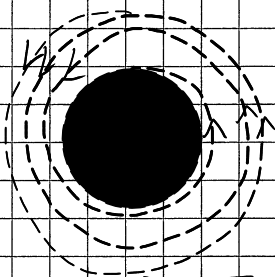
$$\text{Ainsi, } v = \sqrt{\frac{G m_1 m_2}{R}} \Rightarrow v = \sqrt{\frac{G m_1 m_2}{R + h_0}}$$

$$\begin{aligned} \text{Or, } E_m &= E_c + E_p \Rightarrow E_m = \frac{1}{2} m v^2 - G \frac{m_1 m_2}{R + h_0} \\ \Rightarrow E_m &= \frac{G m_1 m_2}{R + h_0} \left( \frac{1}{2} - 1 \right) \\ \Rightarrow E_m &= -\frac{1}{2} G \frac{m_1 m_2}{R + h_0} \end{aligned}$$

2) a-  $\vec{F}_{\text{g}}$  est très résistant, car  $\vec{F} = -\alpha \vec{v}$  donc  $P(\vec{F}) = -\alpha v^2 < 0$   
Ainsi, par le TPA,  
$$\frac{dE_m}{dt} = \sum P(\vec{F}_{nc}) = P(\vec{F}_g) < 0$$

et l'énergie mécanique décroît.

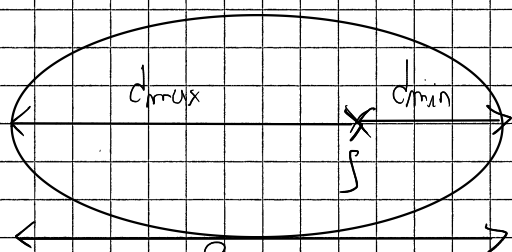
b- Il diminue forcément, puisque  $E_m = -\frac{k}{R + h(t)} \downarrow$  quand  $h \downarrow$   
(attention,  $E_m < 0$ , donc  $|E_m| \uparrow$  quand  $h \downarrow$  mais  $E_m \downarrow$ )



C-  $\sigma = \sqrt{\frac{G M m}{R + h}}$ , donc  $\sigma \nearrow$  qd.  $h \downarrow$

Peu intuitif a priori car  $g$  n'est pas constant, mais si  $\vec{F}_g$  est presque négligeable c'est logique (3<sup>ème</sup> loi de Kepler)

$T_H = 76 \text{ ans}$ ,  $d_{\min} = 0,59 \text{ UA}$



$d_{\max} = 2a - d_{\min}$

Or,  $\frac{T_H^2}{a_H^3} = \frac{4\pi^2}{G m_S}$

$\Rightarrow a_H = \sqrt[3]{\frac{G m_S T_H^2}{4\pi^2}}$

$G = 6,67 \cdot 10^{-11} \text{ SI}$

$m_S = 2,0 \cdot 10^{30} \text{ kg}$

$T_H = 76 \text{ ans}$

$= 76 \times 365,25 \times 24 \times 3600 \text{ s}$

$= 2,41 \cdot 10^{10} \text{ s}$

Ainsi,  $a_H = 2,69 \cdot 10^{12} \text{ m}$

$d_H = 17,9 \text{ UA}$

$\frac{T_H^2}{a_H^3} = \frac{T_T^2}{a_T^3} \Rightarrow a_H = \sqrt[3]{\frac{T_H^2 a_T^3}{T_T^2}}$

$T_H = 76 \text{ y.}$   
 $a_T = 1 \text{ UA}$   
 $T_T = 1 \text{ y.}$

$\Rightarrow \frac{a_H}{1 \text{ UA}} = \left( \frac{T_H}{1 \text{ y.}} \right)^{2/3} = 17,9 \text{ UA} \checkmark$

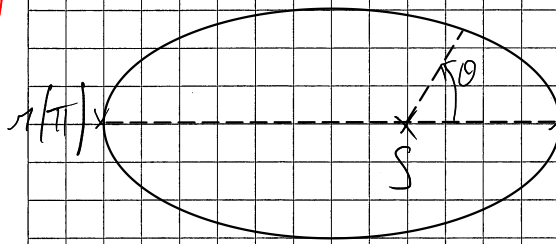
Ainsi,  $d_{\max} = 2a - d_{\min}$  avec  $a = 17,9 \text{ UA}$

A.N.:  $d_{\max} = 35,3 \text{ UA}$

$d_{\min} = 0,59 \text{ UA}$



3)



$$\left\{ \begin{aligned} d_{\min} &= r(0) = \frac{P}{1-e} \\ d_{\max} &= r(\pi) = \frac{P}{1+e} \end{aligned} \right.$$

$$\Leftrightarrow \left\{ \begin{aligned} 1-e &= \frac{P}{d_{\min}} \quad (1) \\ 1+e &= \frac{P}{d_{\max}} \quad (2) \end{aligned} \right.$$

Ainsi,

$$(1) + (2) \Rightarrow 1-e + 1+e = P \left( \frac{1}{d_{\min}} + \frac{1}{d_{\max}} \right)$$

$$\Leftrightarrow 2 = P \left( \frac{d_{\max} + d_{\min}}{d_{\min} d_{\max}} \right)$$

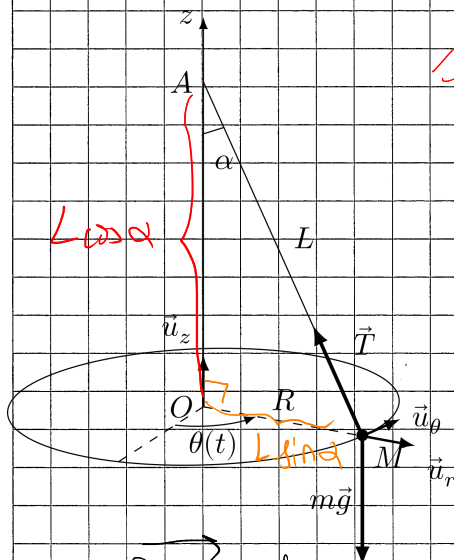
$$\Leftrightarrow P = 2 \frac{d_{\min} d_{\max}}{d_{\min} + d_{\max}}$$

$$(2) - (1) \Rightarrow 1+e - (1-e) = P \left( \frac{1}{d_{\max}} - \frac{1}{d_{\min}} \right)$$

$$\Leftrightarrow 2e = \frac{d_{\min} - d_{\max}}{d_{\min} d_{\max}} \left( \frac{d_{\min} d_{\max}}{d_{\min} + d_{\max}} \right)$$

$$\Leftrightarrow e = \frac{d_{\min} - d_{\max}}{d_{\min} + d_{\max}}$$

IV



1) Système = {masse} M(m)

□ Ressort, glissement

□ Repère cylindrique  $(O, \vec{u}_r, \vec{u}_\theta, \vec{u}_z)$ 

□ Repère Rige :

$$\begin{aligned} \vec{OM} &= R \vec{u}_r = L \sin \alpha \vec{u}_r \\ \vec{v} &= L \sin(\alpha) \dot{\theta} \vec{u}_\theta = L \omega \sin \alpha \vec{u}_\theta \\ \vec{a} &= -L \omega^2 \sin \alpha \vec{u}_r \end{aligned}$$

□  $\vec{L}_A(M) = \vec{AM} \wedge \vec{p}(M) = (\vec{AO} + \vec{OM}) \wedge m \vec{v}$

$$\Leftrightarrow \vec{L}_A(M) = [-L \cos \alpha \vec{u}_z \wedge L \sin \alpha \vec{u}_\theta] \wedge (m L \omega \sin \alpha \vec{u}_\theta)$$

$$\Rightarrow \vec{L}_A(M) = -mL^2 \omega \sin \alpha \cos \alpha (-\vec{u}_\alpha) + mL^2 \omega \sin \alpha \vec{u}_\alpha$$

$$\Rightarrow \vec{L}_A(M) = mL^2 \omega (\sin^2 \alpha \vec{u}_\alpha + \sin \alpha \cos \alpha \vec{u}_\alpha)$$

2)

BdF:  $\begin{cases} \vec{P} = m\vec{g} = -mg \vec{u}_y \\ \vec{T} = -T \vec{u}_\alpha \end{cases}$

BdM:  $\begin{cases} \vec{M}_A(\vec{P}) = \vec{AM} \wedge \vec{P} = L(\sin \alpha \vec{u}_\alpha - \cos \alpha \vec{u}_y) \wedge (-mg \vec{u}_y) \\ \vec{M}_A(\vec{T}) = \vec{AM} \wedge \vec{T} = \vec{0} \end{cases}$

Du  $\vec{M}_A(\vec{P}) = +mgL \sin \alpha \vec{u}_\alpha$

TMC:  $\frac{d\vec{L}_A(M)}{dt} = \sum \vec{M}_A(\vec{P}) = \vec{M}_A(\vec{P})$

$$\Rightarrow mL^2 \omega (\sin^2 \alpha \frac{d\vec{u}_\alpha}{dt} + \sin \alpha \cos \alpha \frac{d\vec{u}_\alpha}{dt}) = mgL \sin \alpha \vec{u}_\alpha$$

Par projec. sur  $\vec{u}_\alpha$ :

$$\Rightarrow mL^2 \omega \sin^2 \alpha \cos \alpha = mgL \sin \alpha$$

$$\Rightarrow \cos \alpha = \frac{g}{L\omega^2}$$

3)

IFD:  $\frac{d\vec{P}}{dt} = \sum \vec{P}_{\text{ext}}$

$$\Rightarrow -mL\omega \sin \alpha \vec{u}_\alpha = -mg \vec{u}_y + T(\cos \alpha \vec{u}_\alpha - \sin \alpha \vec{u}_\alpha)$$

$$\Rightarrow \begin{cases} +mL\omega \sin \alpha = +T \sin \alpha \\ 0 = -mg + T \cos \alpha \end{cases} \Rightarrow \begin{cases} T = mL\omega^2 \\ T = \frac{mg}{\cos \alpha} \end{cases} \Rightarrow \cos \alpha = \frac{g}{L\omega^2}$$

V/1)

$$v_2 = r_2 \dot{\theta}_2$$

$$\begin{cases} + m r_2 \dot{\theta}_2^2 = + \frac{\gamma m M}{r_2^2} \\ + m r_2 \ddot{\theta}_2 = 0 \end{cases}$$

$$\Leftrightarrow \begin{cases} \dot{\theta}_2 = \sqrt{\frac{\gamma M}{r_2^3}} \\ \theta_2 = c t_0 \end{cases}$$

$$v_2 = \sqrt{\frac{\gamma M}{r_2}} = 7300 \text{ m.s}^{-1}$$

2)

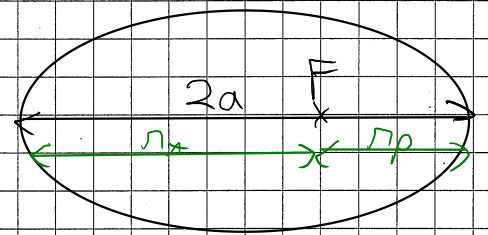
$$E_m = \frac{1}{2} m v^2 - \frac{\gamma M m}{r_A} = \frac{1}{2} \frac{m \gamma M}{r_A} - \frac{\gamma M m}{r_A}$$

$$\Leftrightarrow E_{m,1} = - \frac{\gamma m M}{2 r_1}$$

$$E_{m,2} = - \frac{\gamma m M}{2 r_2}$$

Orbite elliptique:  $2a = r_p + r_A = r_1 + r_2$

$$\text{et } E_{m,p} = - \frac{\gamma m M}{r_1 + r_2}$$



3)

Charge<sup>+</sup> de vitesse instantanée

$\Leftrightarrow$  posi<sup>o</sup> fixe

$\Leftrightarrow E_p = c_k$

$$\text{Donc } \Delta_{1,2} E_m = E_{m,2} - E_{m,1} = \frac{1}{2} m (v_2^2 - v_1^2)$$

$$\Leftrightarrow - \gamma M m \left( \frac{1}{r_1 + r_2} - \frac{1}{2 r_2} \right) = \frac{1}{2} m v_2^2 - \frac{1}{2} m v_1^2$$

$$\Leftrightarrow \frac{1}{2} m v_2^2 = - \gamma m M \left( \frac{2 r_2 - r_1 - r_2}{2 r_2 (r_1 + r_2)} \right) + \frac{\gamma m M}{2 r_1}$$

$$\Leftrightarrow \frac{1}{2} m v_2^2 = \frac{\gamma m M}{2 r_2 (r_1 + r_2)} (r_1 + r_2 - (r_1 - r_2))$$

Soit 
$$v_{e1} = \sqrt{\frac{2G M m_2}{r_2(r_1+m_1)}} = 1520 \text{ m.s}^{-1}$$

Ainsi,  $\Delta v_p = \dots = 2220 \text{ m.s}^{-1}$

TEM:  $\Delta_{ee} E_m = \Delta_{ee} W = W_p$

$\Leftrightarrow W_p = \frac{G m M (m_2 - m_1)}{2 r_2 (r_1 + m_1)} = 1,7 \cdot 10^{10} \text{ J} = 17 \text{ GJ}$

4) En P et A,  $\vec{OM} \perp \vec{v}$ ; soit  $\vec{v} \parallel \vec{u}$  ( $\dot{r} = 0$ )

$$\vec{L}_O(P) = \vec{OP} \wedge m \vec{v} = r_1 \vec{u} \wedge m v_{e1} \vec{u} = m r_1 v_{e1} \vec{e}_3$$

et  $\vec{L}_O(A) = \dots = m r_2 v_{e2} \vec{e}_3$

Or,  $\frac{d\vec{L}_O}{dt} = \vec{0}$ , soit  $m r_1 v_{e1} \vec{e}_3 = m r_2 v_{e2} \vec{e}_3$

$\Leftrightarrow r_1 v_{e1} = r_2 v_{e2}$

$\Leftrightarrow v_{e2} = v_{e1} \frac{r_1}{r_2} = \sqrt{\frac{2G M m_1 r_1}{r_2 (r_1 + m_1)}}$

A.N.  $v_{e2} = 1690 \text{ m.s}^{-1}$

5)  $v_2 = \sqrt{\frac{G M}{r_2}}$ ,  $\Delta v_1 = \frac{G M}{r_2} - \sqrt{\frac{2G M m_1 r_1}{r_2 (r_1 + m_1)}} = 1390 \text{ m.s}^{-1}$

$\Delta = 3080 \text{ m.s}^{-1}$

$$W_A = E_{m2} - E_{m1} = -\frac{G m M}{2 r_2} + \frac{G m M}{r_1 + m_1} = \frac{G m M (r_2 - m_1)}{2 r_2 (r_1 + m_1)}$$

A.N.:  $W_A = 3,0 \text{ GJ}$

$\hookrightarrow$  on a q. n P, donc  $W \downarrow$  de P à A ✓