

# Reguleringsteknik 1

J. Christian Andersen

Kursusuge 12

## Plan

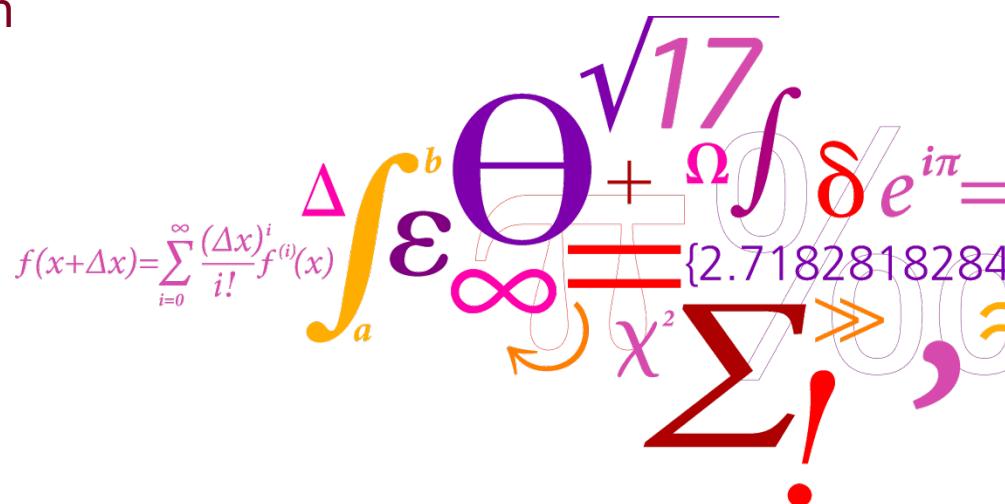
- Feed forward af input
- Feed forward af forstyrrelser
- Systemer med tidsforsinkelse

## Grupperegning

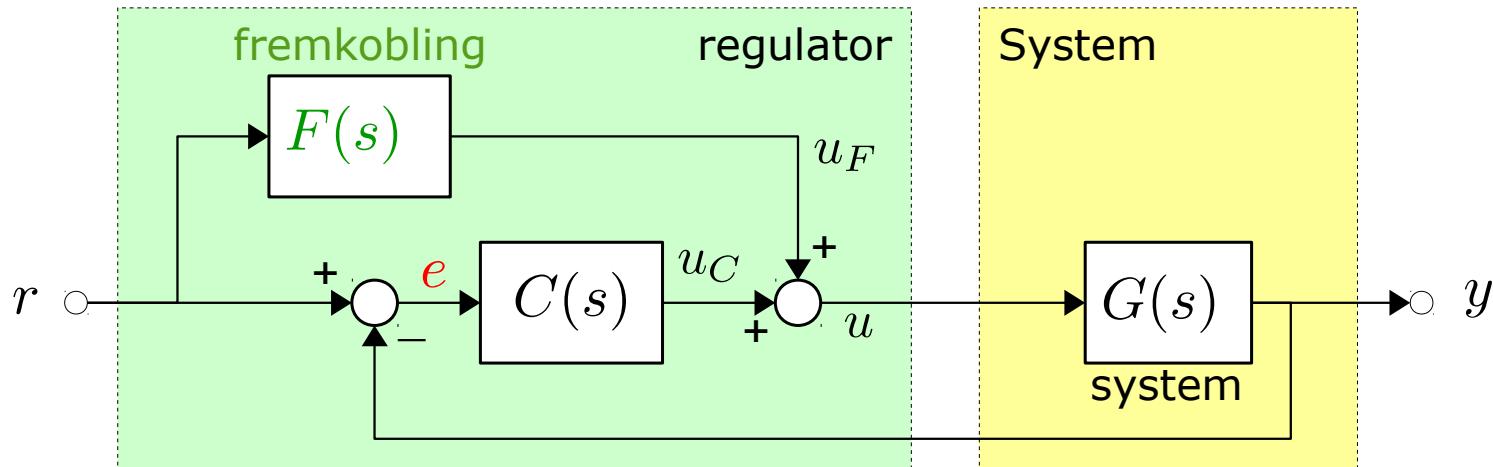
- Feed forward og delay design

## Øvelse

- REGBOT balance



# Fremkobling (Feed forward)



Fejlen  $e$  er nu en sum af 3 led

$$e = r - rF(s)G(s) - eC(s)G(s)$$

$$e + eC(s)G(s) = r(1 - F(s)G(s))$$

$$e = r \frac{1 - F(s)G(s)}{1 + C(s)G(s)}$$

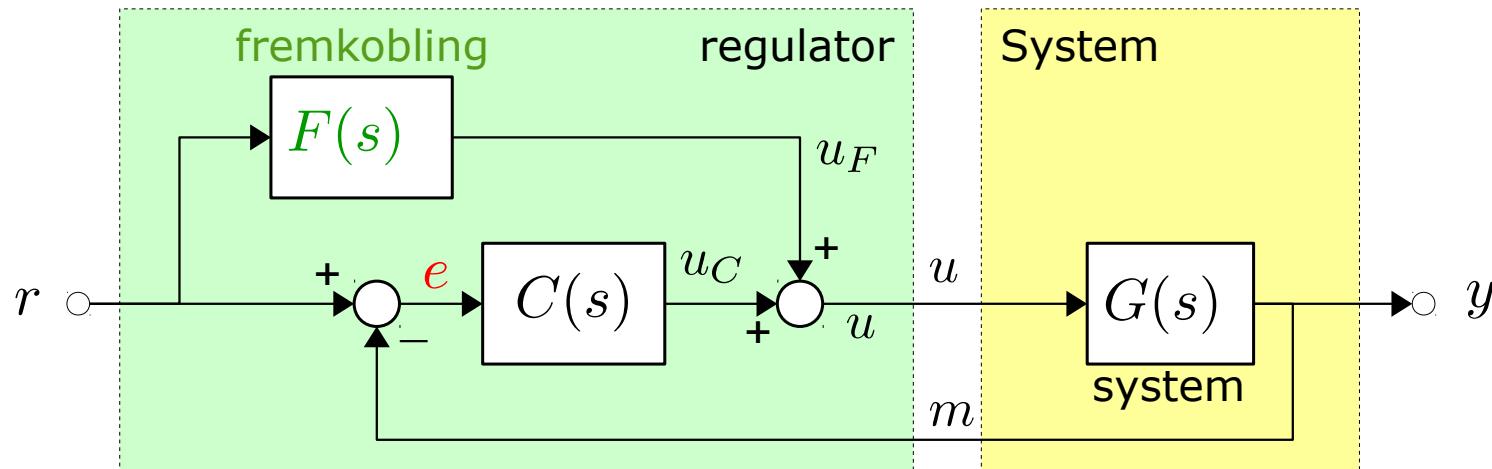
Kan  $F(s)$  reducere fejlen?

$$y = r \frac{C(s)G(s)}{1 + C(s)G(s)} + rF(s) \frac{G(s)}{1 + C(s)G(s)}$$

$$y = r \frac{F(s)G(s) + C(s)G(s)}{1 + C(s)G(s)}$$

$$\frac{y}{r} = \frac{F(s)G(s) + C(s)G(s)}{1 + C(s)G(s)}$$

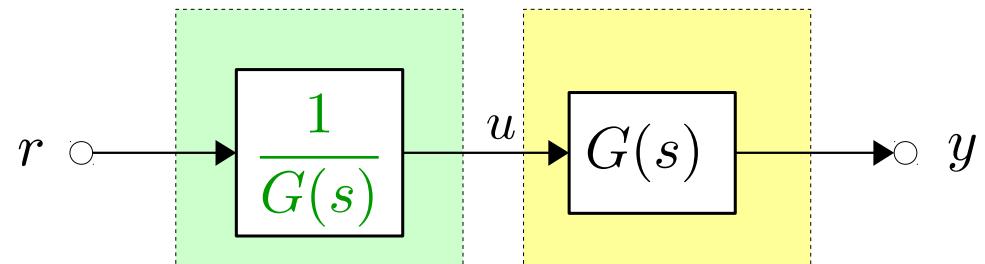
# Feed forward (fremkobling)



$$e = r \frac{1 - F(s)G(s)}{1 + C(s)G(s)}$$

Fejlen er 0, hvis:

$$F(s) = \frac{1}{G(s)}$$



$$\frac{y}{r} = 1 \quad (C(s) = 0)$$

Perfekt uden regulator!  
Hvor er ulempene?

# 4 Eksempel: et el-køretøj skal hastighedsstyres

Motorspænding

$$V_A(s)$$

12V motor  
6000 RPM

$$L = 0.05 \text{ H}$$

$$R = 2\Omega$$

$$K_\tau = 0.016 \text{ Nm/A}$$

$$K_m = 0.016 \text{ Vs}$$

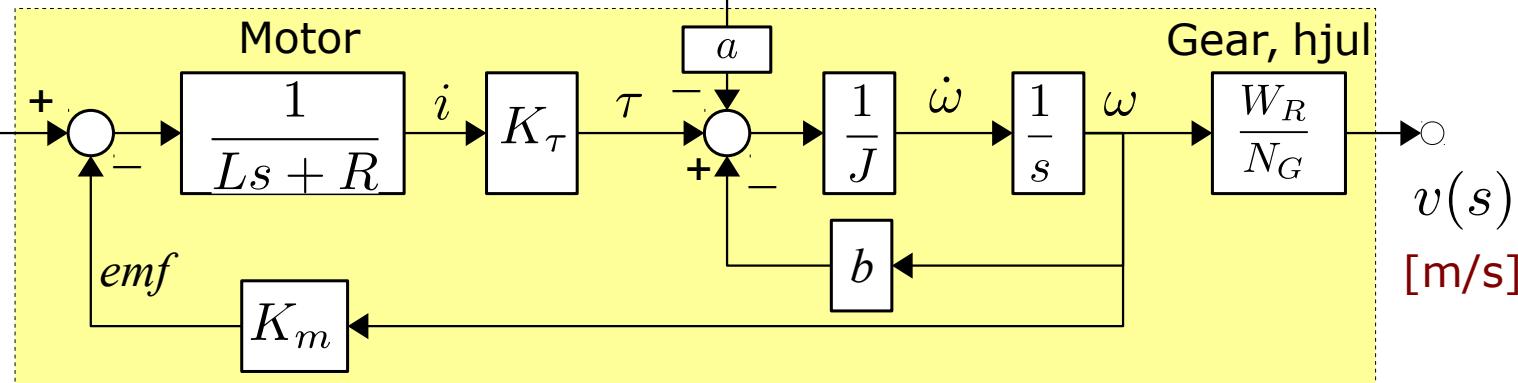
$$J = 20 \cdot 10^{-6} \text{ Nms}^2$$

$$b = 25 \cdot 10^{-6} \text{ Nms}$$

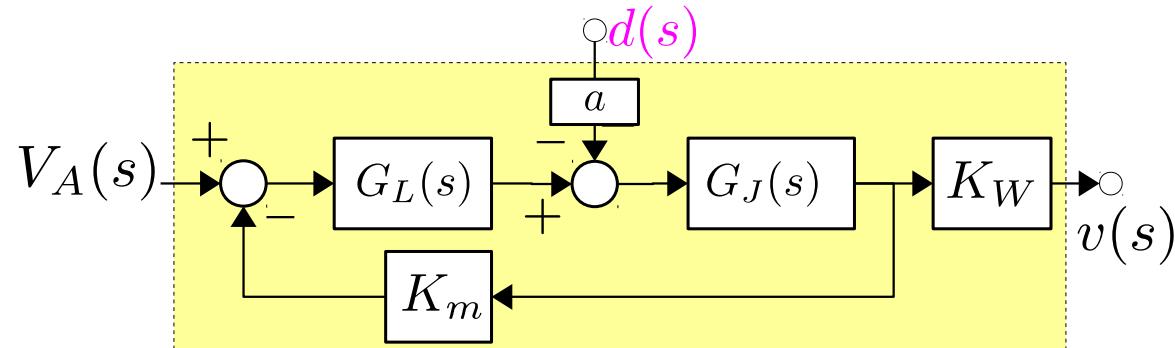
$$W_R = 0.045 \text{ m}$$

$$N_G = 10$$

$$a = \frac{W_r}{N_G} \text{ m}$$



Belastningskraft [N]  
(forstyrrelse)  
 $d(s)$

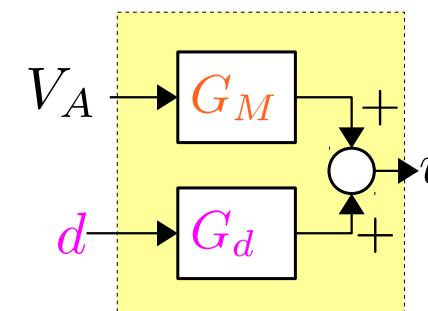


$$G_L(s) = \frac{0.016}{0.05s + 2}$$

$$G_J(s) = \frac{5 \cdot 10^4}{s + 1.25}$$

$$G_M(s) = \frac{72}{s^2 + 41.25s + 306}$$

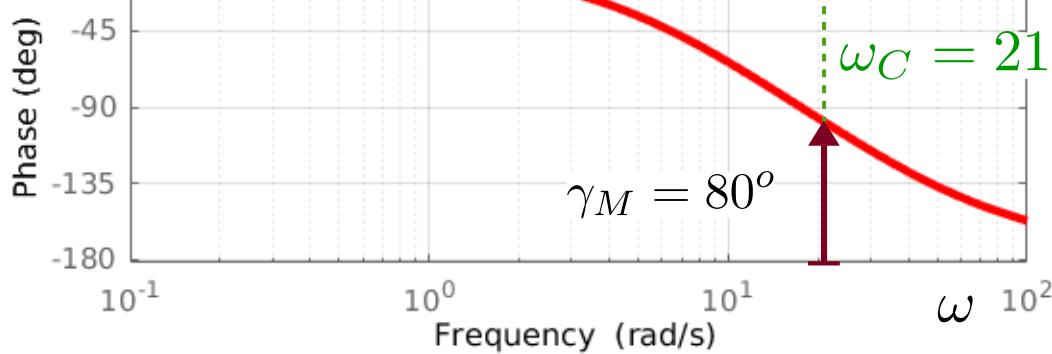
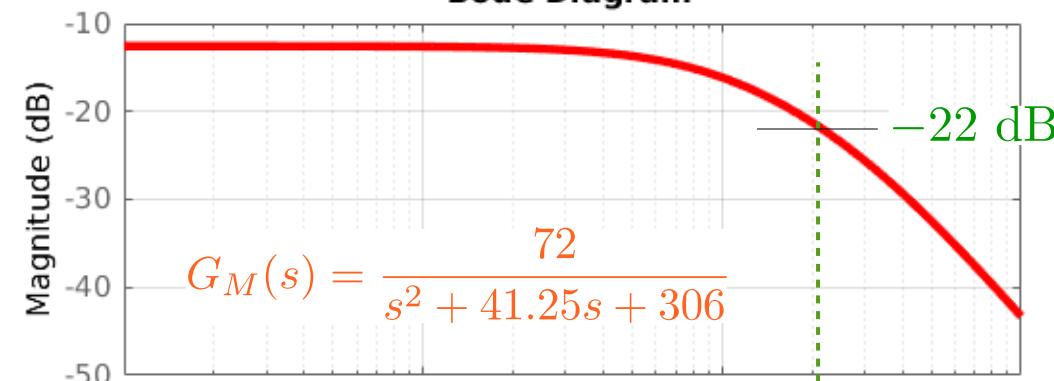
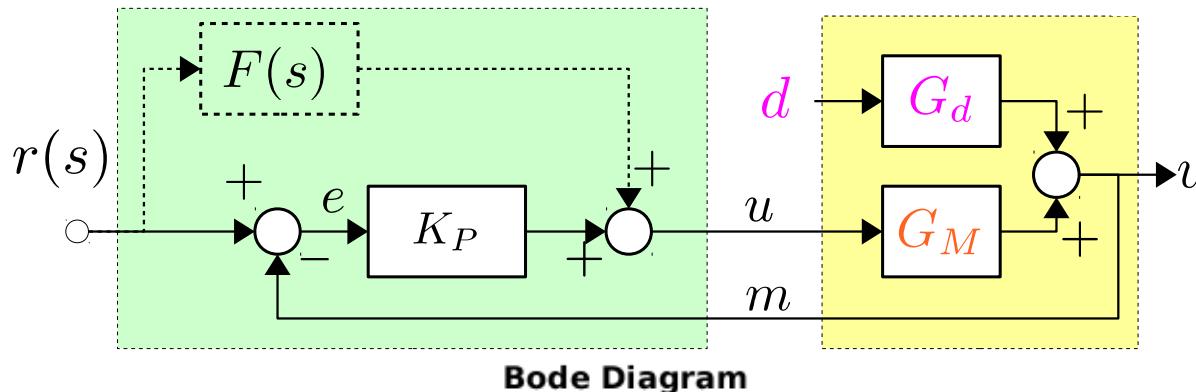
$$G_d(s) = \frac{1.01s + 40.5}{s^2 + 41.25s + 306}$$



$$G_M(s) = \frac{72}{s^2 + 41.25s + 306}$$

# Normal regulator design (P)

$$G_d(s) = \frac{1.01s + 40.5}{s^2 + 41.25s + 306}$$



$$K_P = 10^{\frac{22}{20}} = 12.5$$

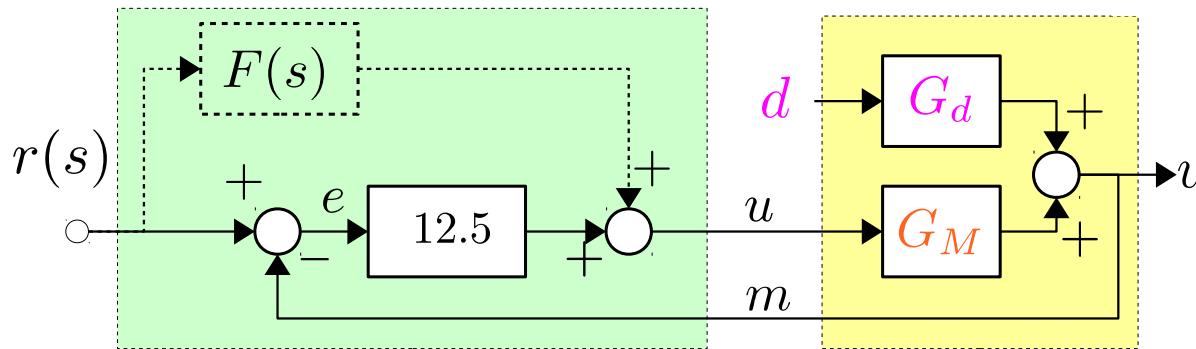
$$G_M(s) = \frac{72}{s^2 + 41.25s + 306}$$

# Normal regulator design (P)

$$G_d(s) = \frac{1.01s + 40.5}{s^2 + 41.25s + 306}$$

$$G_{\dot{a}} = \frac{12.5 \cdot 72}{s^2 + 41.25s + 306}$$

$$G_{cl} = \frac{G_{\dot{a}}}{1 + G_{\dot{a}}}$$



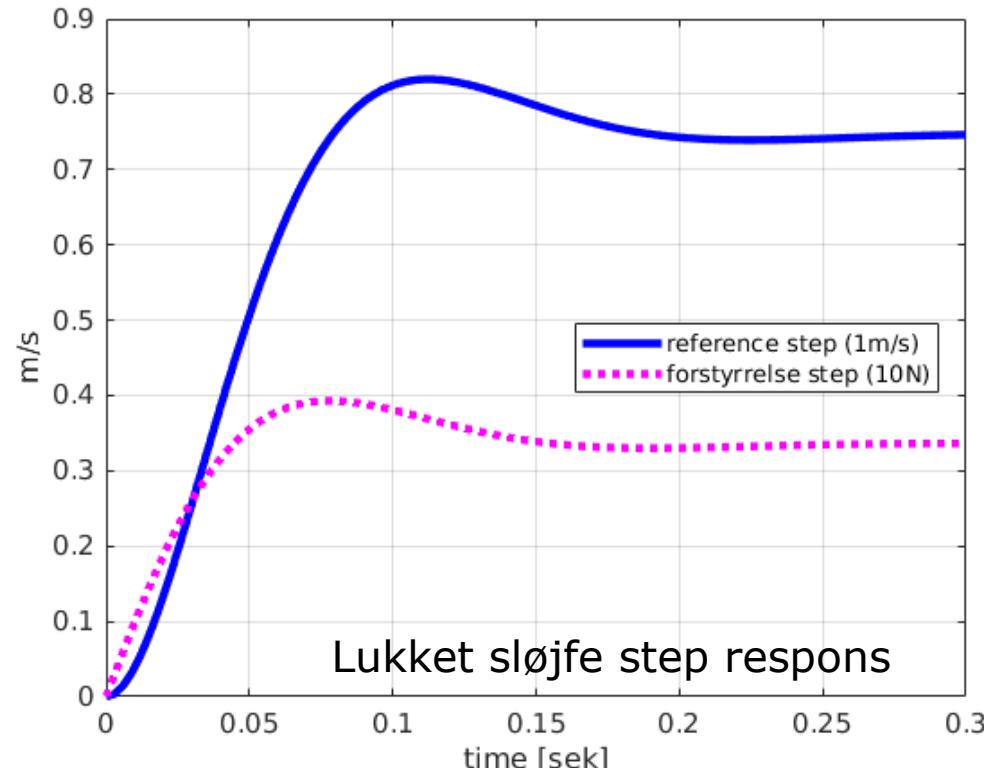
Enhedsstep stationær fejl:

$$e_{r,ss} = \lim_{s \rightarrow 0} s \frac{1}{s} \frac{1}{1 + G_{\dot{a}}}$$

$$e_{r,ss} = \frac{1}{1 + K_0}$$

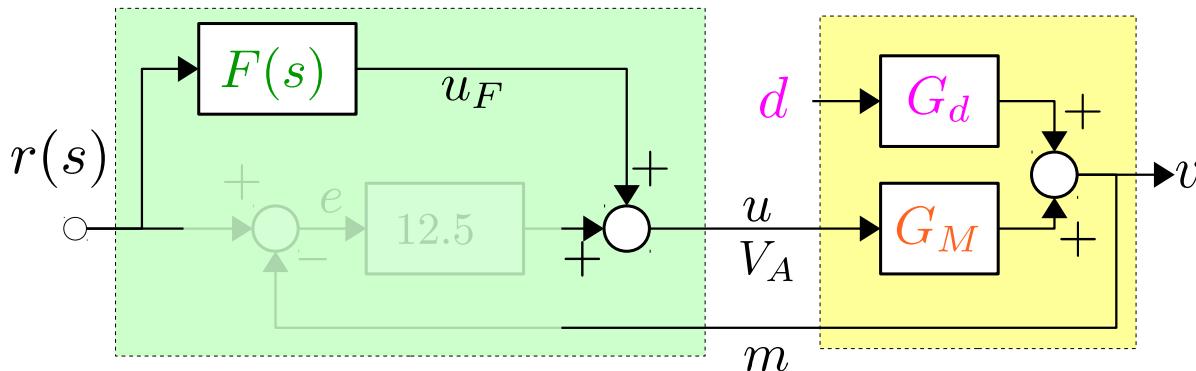
$$\text{Loop gain ved DC } K_0 = \lim_{s \rightarrow 0} G_{\dot{a}}$$

$$e_{r,ss} = \frac{1}{1 + 12.5 \frac{72}{306}} = 0.25 \quad (25\%)$$



$$G_M(s) = \frac{72}{s^2 + 41.25s + 306}$$

# Fremkobling



$$e = r \frac{1 - F(s)G_M(s)}{1 + C(s)G_M(s)}$$

Optimal fremkobling (uden regulator)

$$F(s) = \frac{1}{G_M(s)}$$

$$F(s) = \frac{u_F(s)}{r(s)} = \frac{s^2 + 41.25s + 306}{72}$$

Steady state

$$G_{M,ss}(s) = \frac{72}{306}$$

$$V_A = 10V \Rightarrow$$

$$v = 10 \frac{72}{306} = 2.35 \text{ m/s}$$

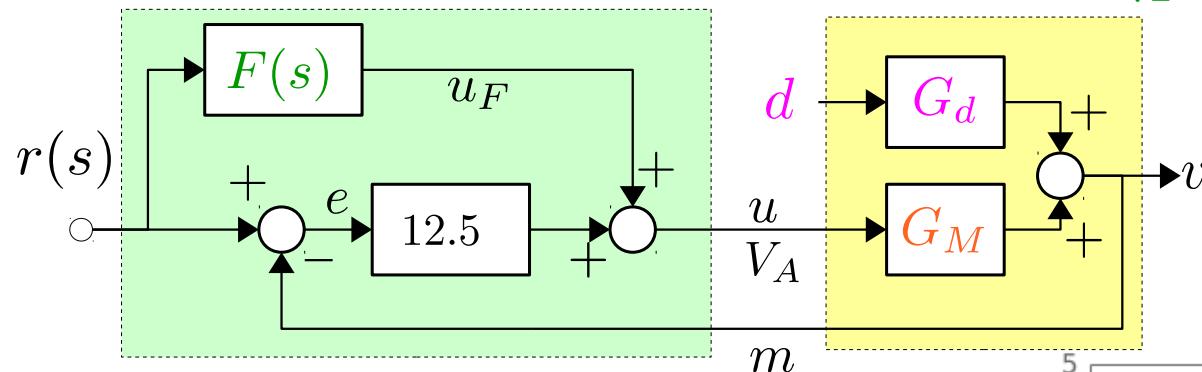
$F(s)$  i tidsdomænet

$$u_F(t) = \ddot{r}(t) \frac{1}{72} + \dot{r}(t) \frac{41.25}{72} + r(t) \frac{306}{72}$$

Måske er steady state del nok

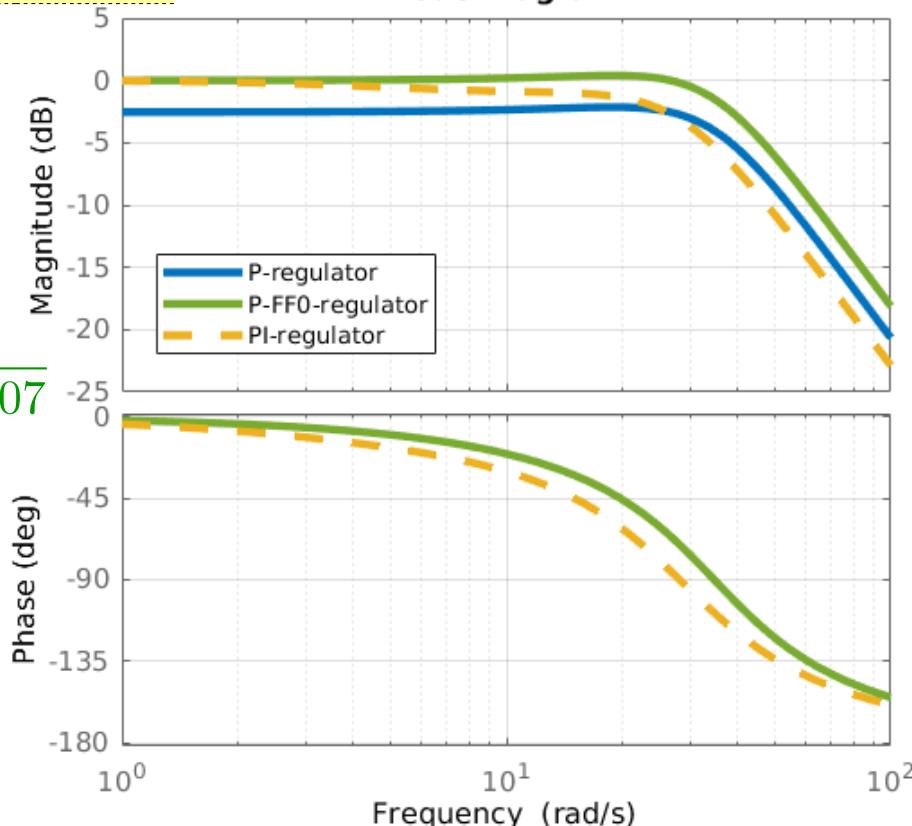
$$G_M(s) = \frac{72}{s^2 + 41.25s + 306}$$

# Fremkobling



$$F_0(s) = \frac{306}{72} = 4.25$$

Bode Diagram



Ny lukket sløjfe

$$G_{cl} = \frac{G_{\ddot{a}}}{1 + G_{\ddot{a}}} + \frac{F_0 G_M}{1 + G_{\ddot{a}}}$$

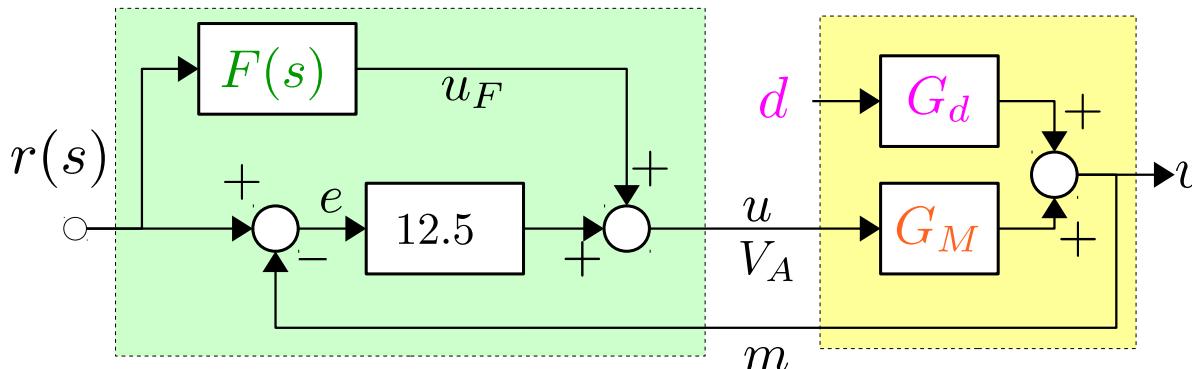
$$G_{cl} = \frac{901}{s^2 + 41.25s + 1207} + \frac{306}{s^2 + 41.25s + 1207}$$

$$G_{cl} = \frac{1207}{s^2 + 41.25s + 1207}$$

Steady state gain nu 1

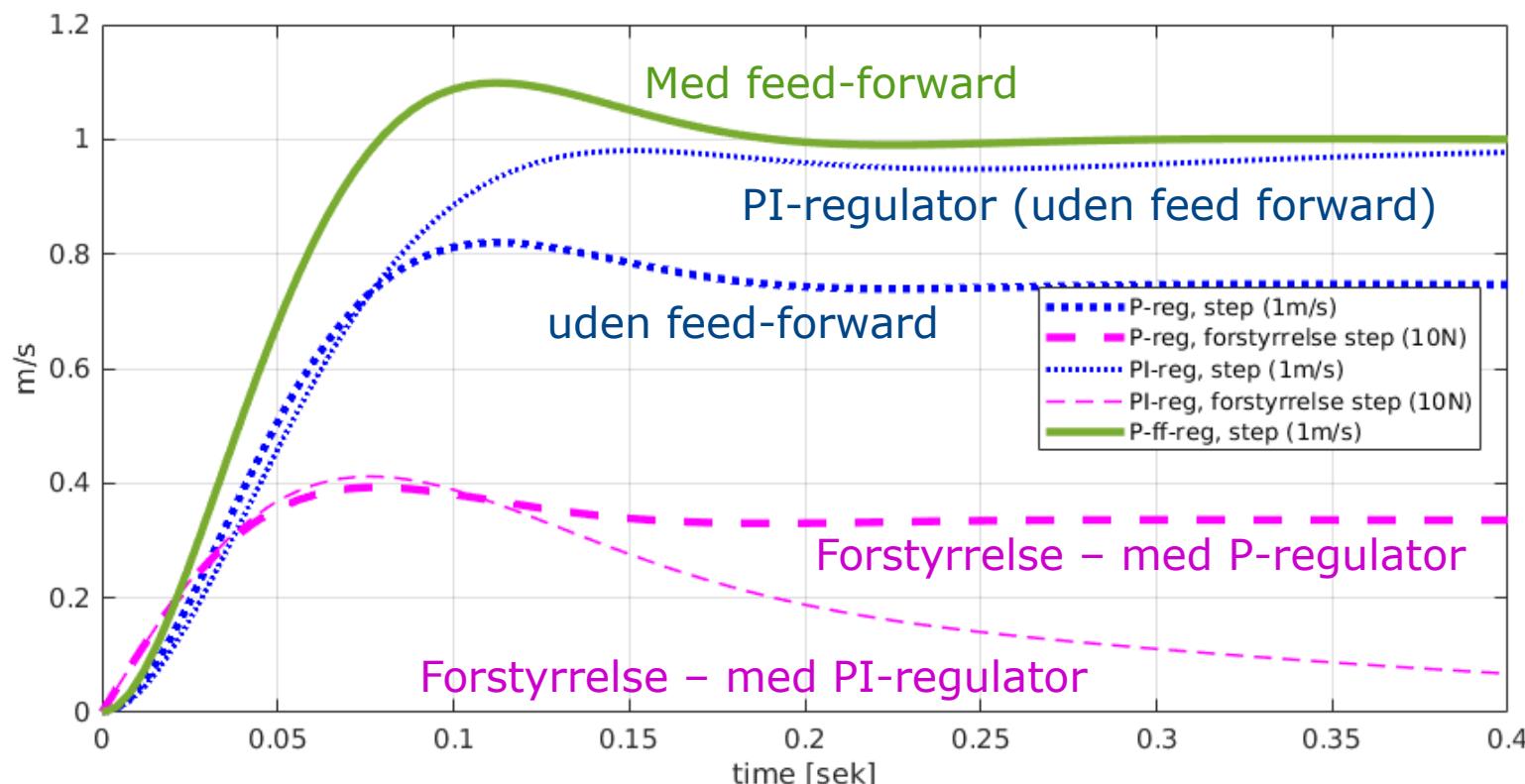
$$G_M(s) = \frac{72}{s^2 + 41.25s + 306}$$

# Fremkobling



$$G_{cl,p} = \frac{901}{s^2 + 41.25s + 1207}$$

$$G_{cl,ff} = \frac{1207}{s^2 + 41.25s + 1207}$$



# Kontrolspørgsmål Fremkobling (feed forward)

- 1) Giver feed forward stabilitetsproblemer?
- 2) Giver feed forward problemer med forstærkning af målestøj?
- 3) Giver feed forward problemer med integrator wind-up?
- 4) Hjælper feed forward med undertrykkelse af forstyrrelser?
- 5) Hvis systemet der skal reguleres indeholder en integrator,  
Vil det så stadig være en fordel med denne type feed forward?

# Kontrolspørgsmål

## Fremkobling (feed forward)

1) Giver feed forward stabilitetsproblemer?

Nej, feed forward påvirker ikke polplacering  
(indgår ikke i reguleringsløjfen)

2) Giver feed forward problemer med forstærkning af målestøj?

Nej

3) Giver feed forward problemer med integrator wind-up?

Feed forward kan fjerne statisk fejl uden at give wind-up problemer.

4) Hjælper feed forward med undertrykkelse af forstyrrelser?

Nej, desværre ikke.

5) Hvis systemet der skal reguleres indeholder en integrator,

Vil det så stadig være en fordel med denne type feed forward?

Nej, feed forward bruger kun steady state led af  $G_M(s)$

$$G_M(s) = \frac{b}{a_2 s^2 + a_1 s + 0} \Rightarrow \lim_{s \rightarrow 0} \frac{1}{G_M} = 0$$

# Feed forward af forstyrrelse

# Reguleringsteknik 1

J. Christian Andersen

Kursusuge 12

## Plan

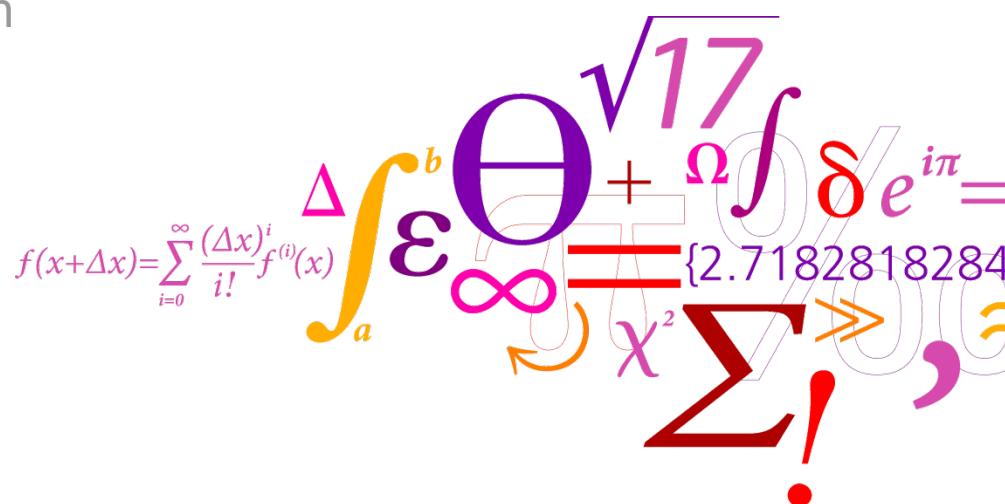
- Feed forward af input
- Feed forward af forstyrrelser
- Systemer med tidsforsinkelse

## Grupperegning

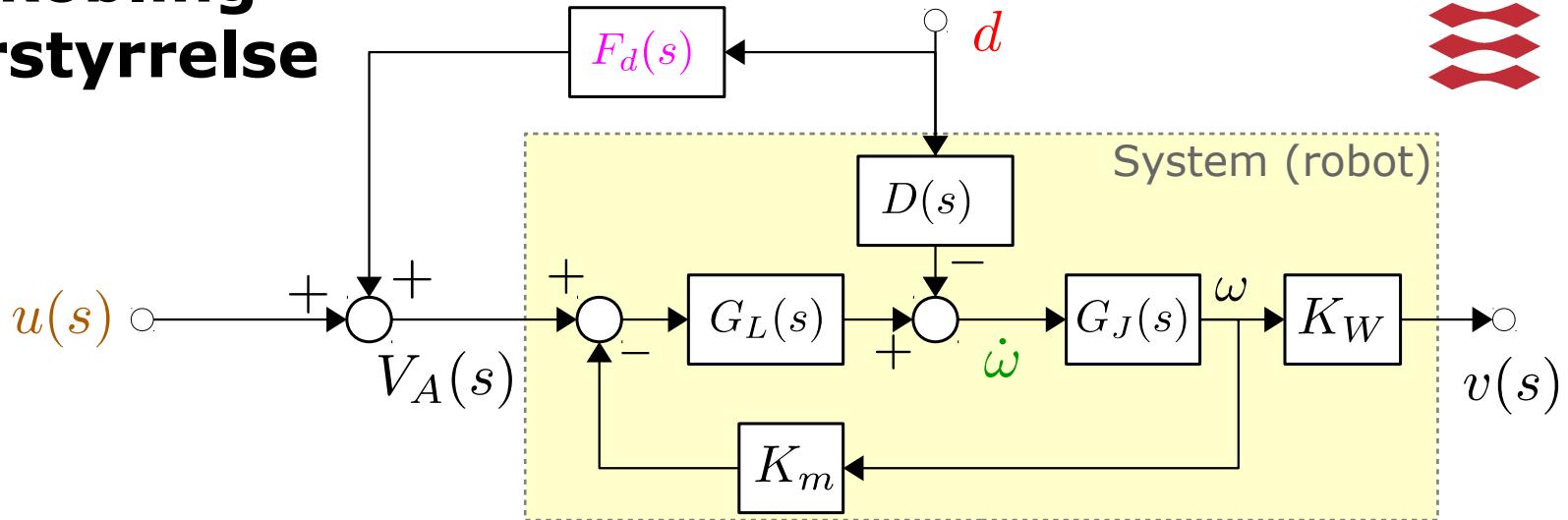
- Feed forward og delay design

## Øvelse 10+11+12

- REGBOT balance øvelse



# Fremkobling af forstyrrelse



$$\dot{\omega} = -dD - \dot{\omega}G_JK_mG_L + dF_dG_L + uG_L$$

$$\dot{\omega}(1 + G_JK_mG_L) = d(F_dG_L - D)$$

$$\dot{\omega} = d \frac{F_dG_L - D}{1 + G_JK_mG_L}$$

$$v = d \frac{F_dG_L - D}{1 + G_JK_mG_L} G_j K_W$$

$$F_d = \frac{D}{G_L} \Rightarrow \frac{v(s)}{d(s)} = 0$$

**Eksempel**

$$D(s) = 0.02 \quad G_L(s) = \frac{0.016}{0.05s + 2}$$

**0. orden fremkobling**

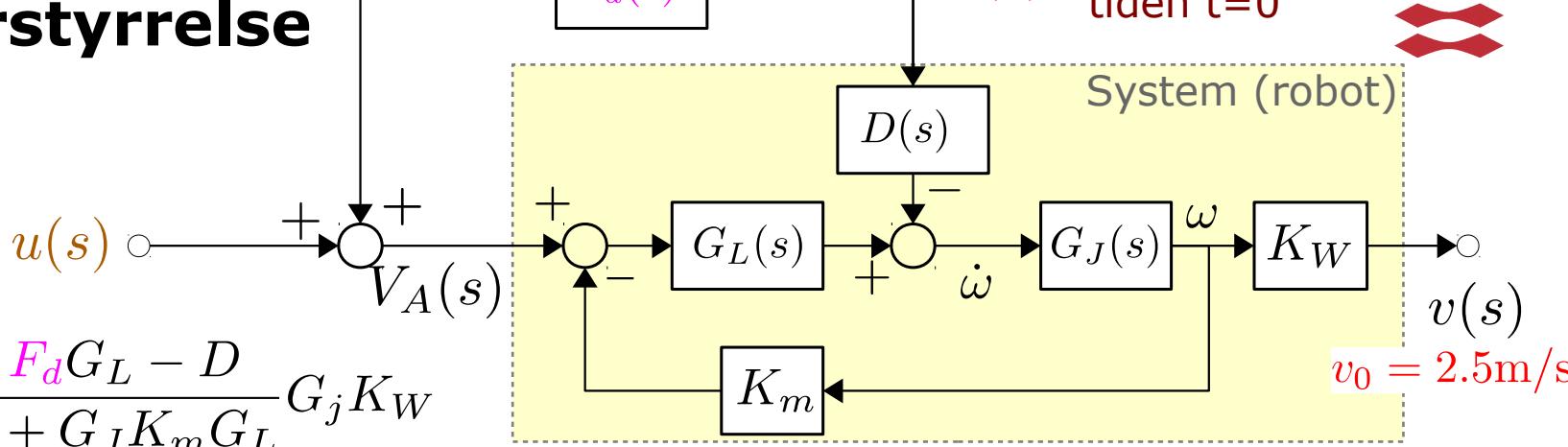
$$F_{d1}(s) = 0.02 \frac{2}{0.016} = 2.5$$

**1. orden (praktisk) fremkobling**

$$F_{d2}(s) = \frac{0.02 (0.05s + 2)}{0.016(0.00025s + 1)}$$

**Ekstra pol**

# Fremkobling af forstyrrelse



$$F_d = \frac{D}{G_L} \Rightarrow \frac{v(s)}{d(s)} = 0$$

Optimal fremkobling

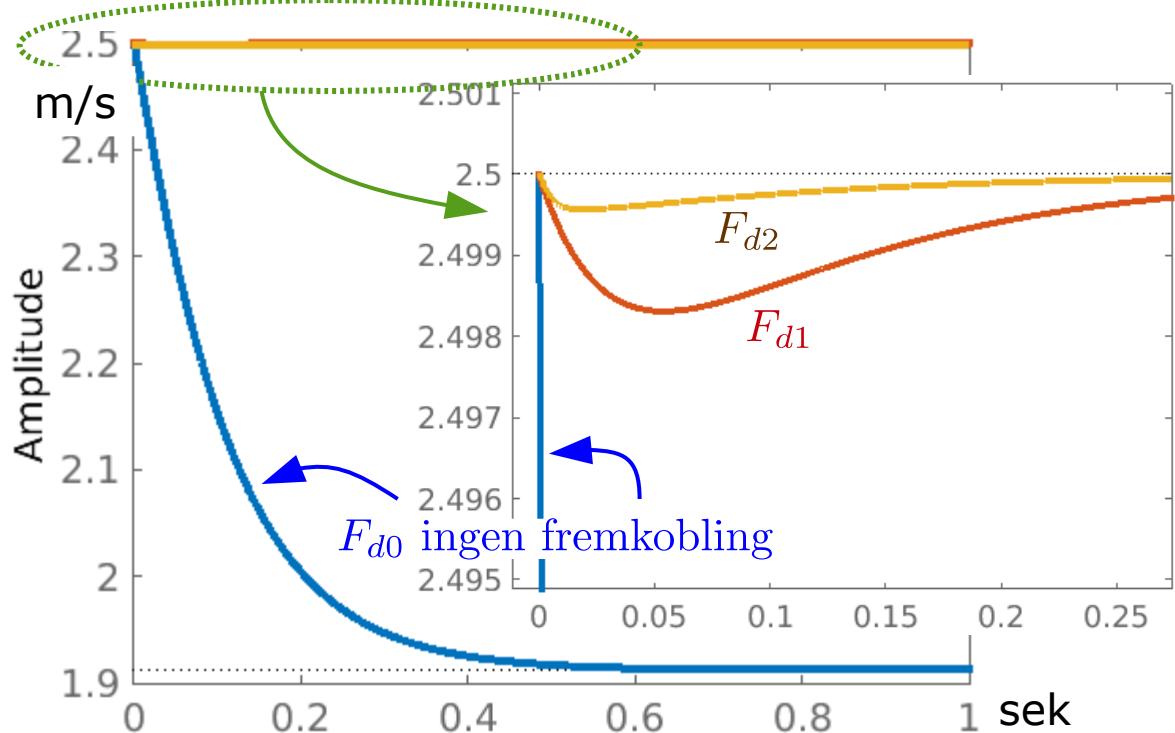
$$\frac{D}{G_L} = 0.02 \frac{0.05s + 2}{0.016}$$

0. orden fremkobling

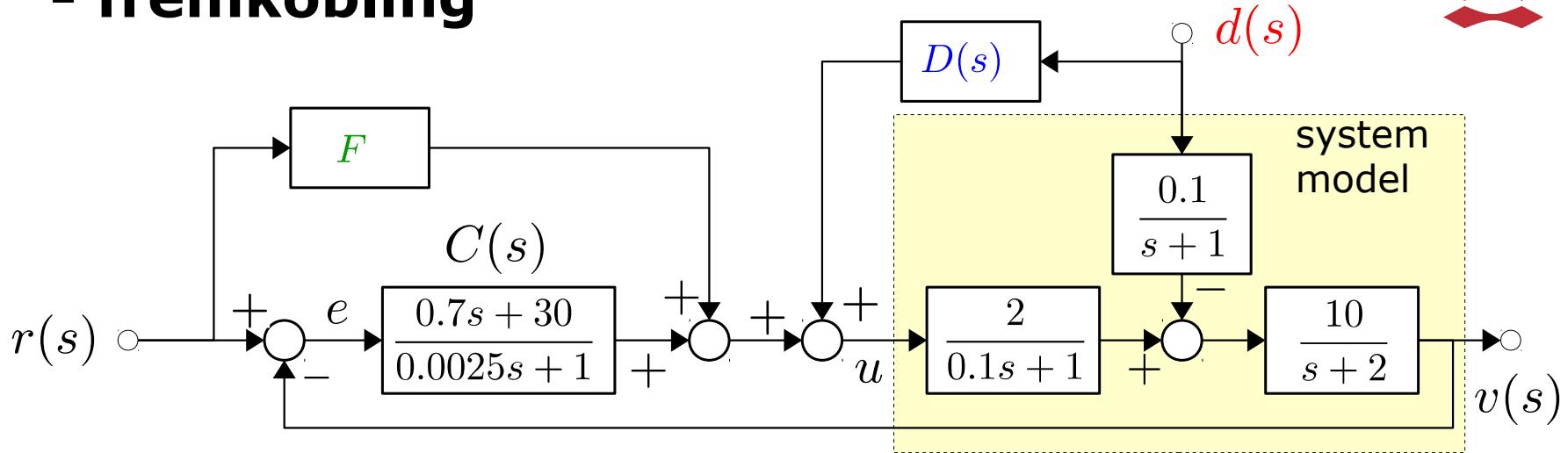
$$F_{d1}(s) = 0.02 \frac{2}{0.016} = 2.5$$

1. orden fremkobling

$$F_{d2}(s) = \frac{0.02 (0.05s + 2)}{0.016(0.005s + 1)}$$



# Kontrolspørgsmål 2 - fremkobling



## Opgaver

a) Hvilken gain  $F$  fjerner statis fejl for step på  $r(s)$  ?

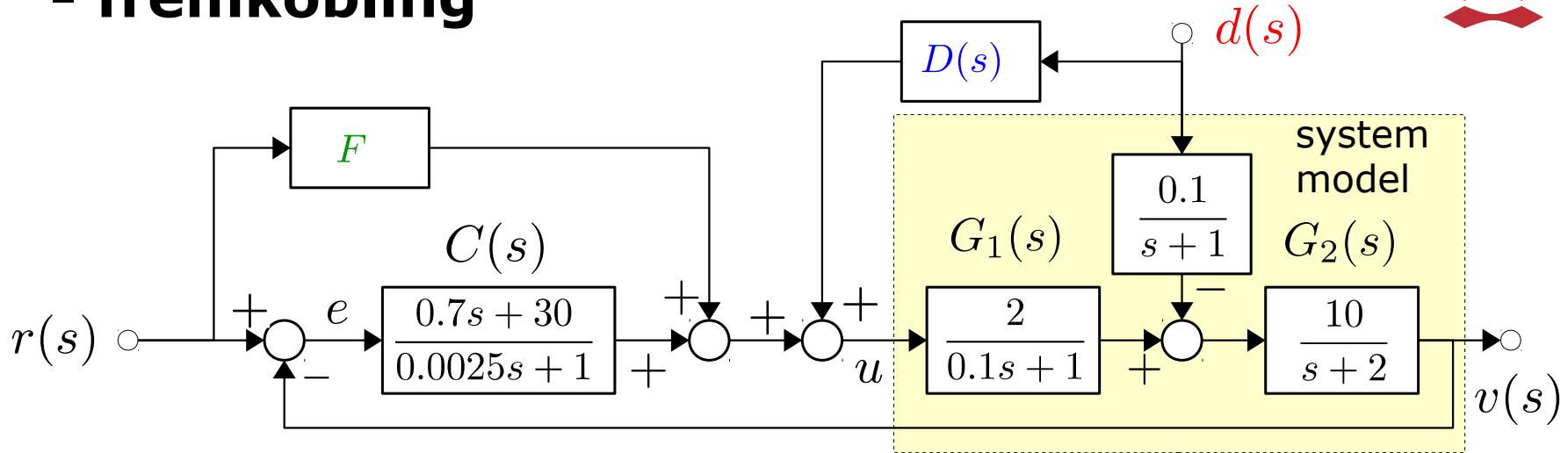
b) Hvad bliver overføringsfunktionen fra  $r(s)$  til  $v(s)$ ?

c) Hvis  $D(s)$  kun er en gain, hvilken værdi skal  $D$  så have?

d) Hvad er optimal fremkobling  $D(s)$  ?

e) Hvis der ikke er modelfejl, vil optimal  $D(s)$  så fjerne effekt af  $d(s)$  ?

# Kontrolspørgsmål 2 - fremkobling



## Opgaver

- a) Hvilken gain  $F$  fjerner statis fejl for step på  $r(s)$  ?

Fra  $u$  til  $v$  er statisk gain 10, derfor derfor må statis gain  $F=0.1$

- b) Hvad bliver overføringsfunktionen fra  $r(s)$  til  $v(s)$ ?

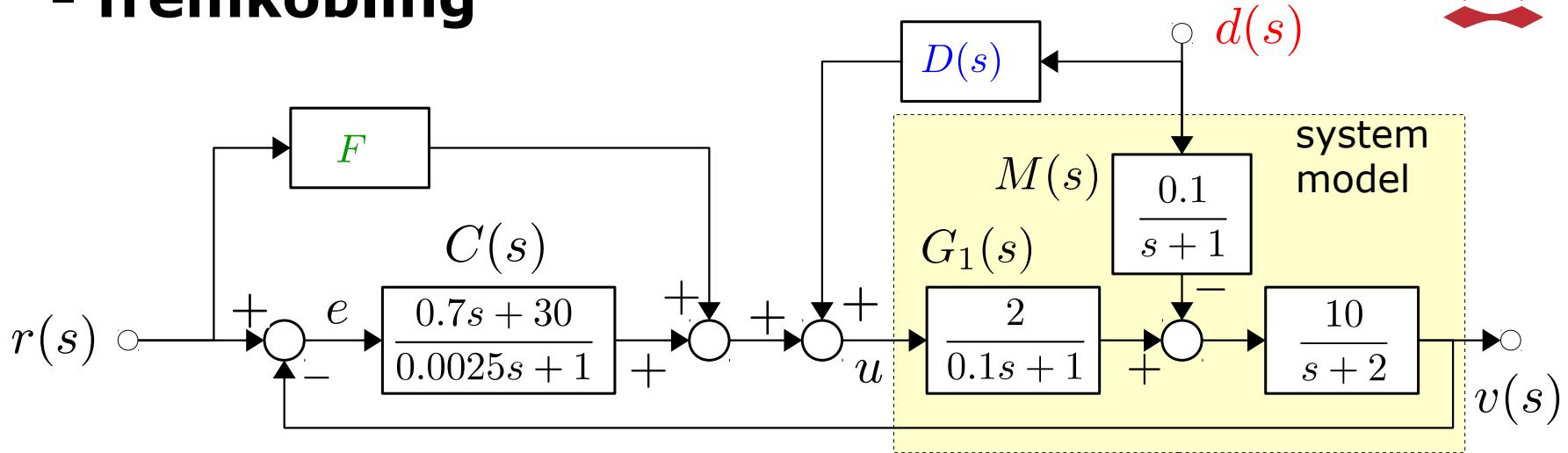
$$G_{cl} = \frac{v(s)}{r(s)}$$

$$G_{cl} = F \frac{G_1 G_2}{1 + G_a} + \frac{G_a}{1 + G_a}$$

$$G_{cl} = \frac{F G_1 G_2 + G_a}{1 + G_a}$$

$$G_{cl} = \frac{56020s + 2408000}{s^3 + 412s^2 + 60820s + 2408000}$$

# Kontrolspørgsmål 2 - fremkobling



- c) Hvis  $D(s)$  kun er en gain, hvilken værdi skal  $D$  så have?

$$D(s) = \frac{M}{G_1} = \frac{0.1(0.1s + 1)}{(s + 1)2}$$

$$D = \lim_{s \rightarrow 0} = \frac{0.1(0.1s + 1)}{(s + 1)2} = 0.05$$

- d) Hvad er optimal fremkobling  $D(s)$ ?

$$D(s) = \frac{M}{G_1} = \frac{0.1(0.1s + 1)}{(s + 1)2}$$

- e) Hvis der ikke er modelfejl, vil optimal  $D(s)$  så fjerne effekt af  $d(s)$ ?

Ja

# Systemer med tidsforsinkelse

# Reguleringsteknik 1

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## Plan

- Feed forward af input
- Feed forward af forstyrrelser
- **Systemer med tidsforsinkelse**

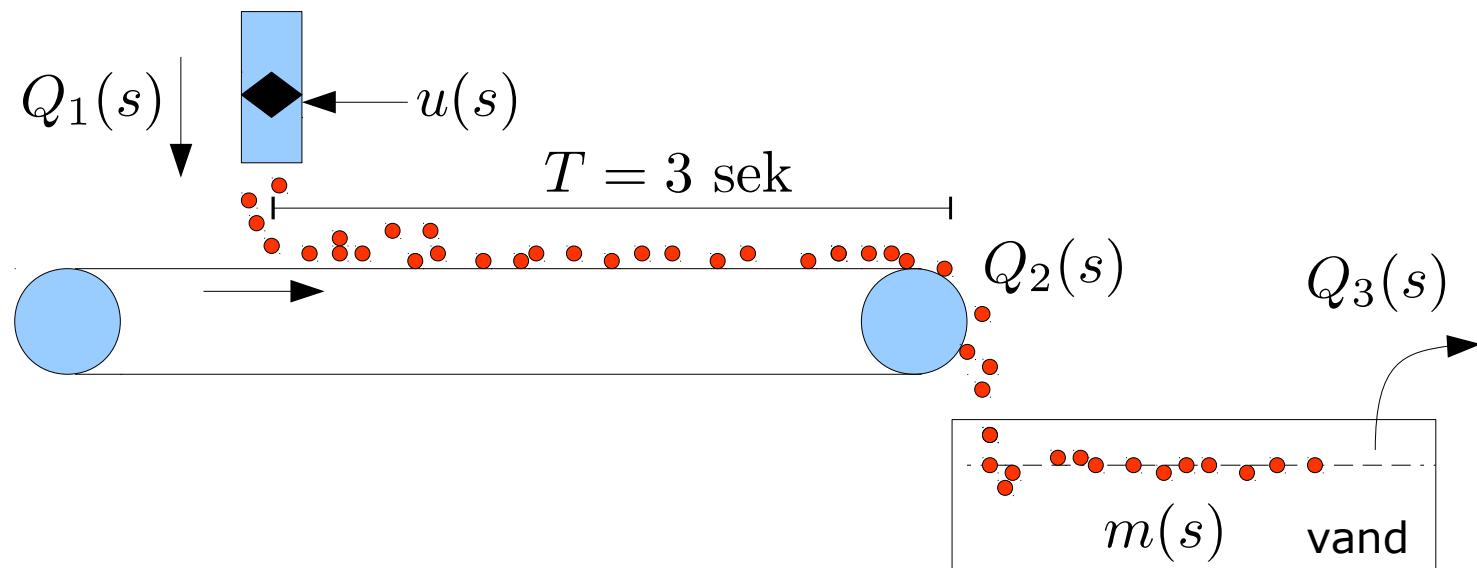
Grupperegning

- Feed forward og delay design

Øvelse 10+11+12

- REGBOT balance øvelse

# Forsinkelse i overføringsfunktioner eksempel

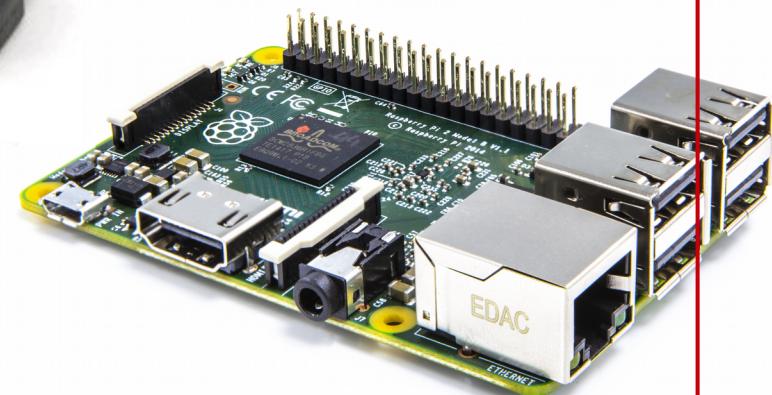


Forsinkelse på transportbånd  
Flow kan styres med  $u(s)$  og antal i bassin  $m(s)$  måles

# Forsinkelse Eksempel



Gør lysere



Måling:  
- for mørkt  
(stadic)

Under  
eksponering

For lyst



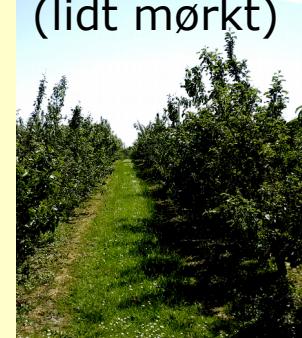
kamera  
buffer

OK

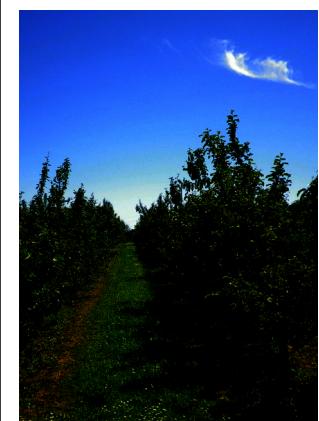


På vej

OK  
(lidt mørkt)

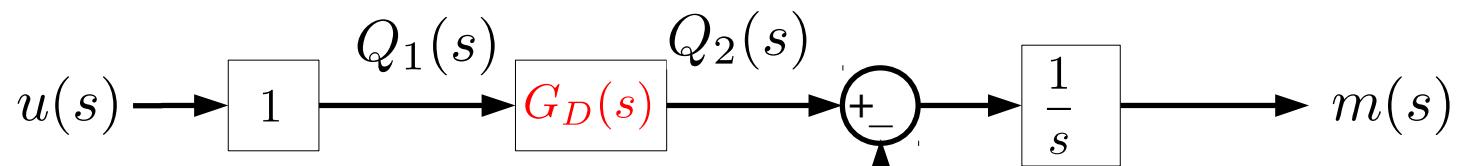
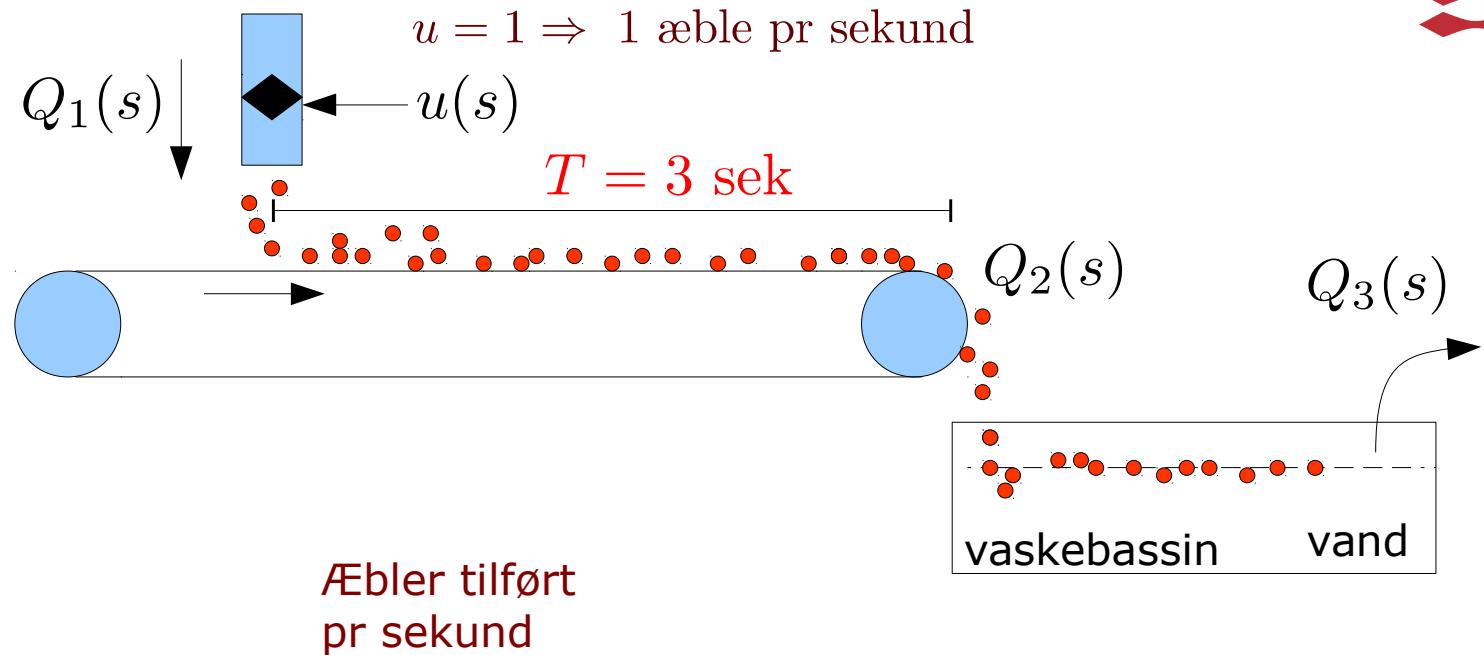


Driver  
Buffer (xN)



Billeder der endnu ikke er modtaget i software

# Transportbånd eksempel (æblekagefabrik)



$$G_D(s) = e^{-Ts}$$

$$G_D(s) = e^{-3s}$$

# Forsinkelse Padé tilnærmelse

$$G(s) = e^{-Ts}$$

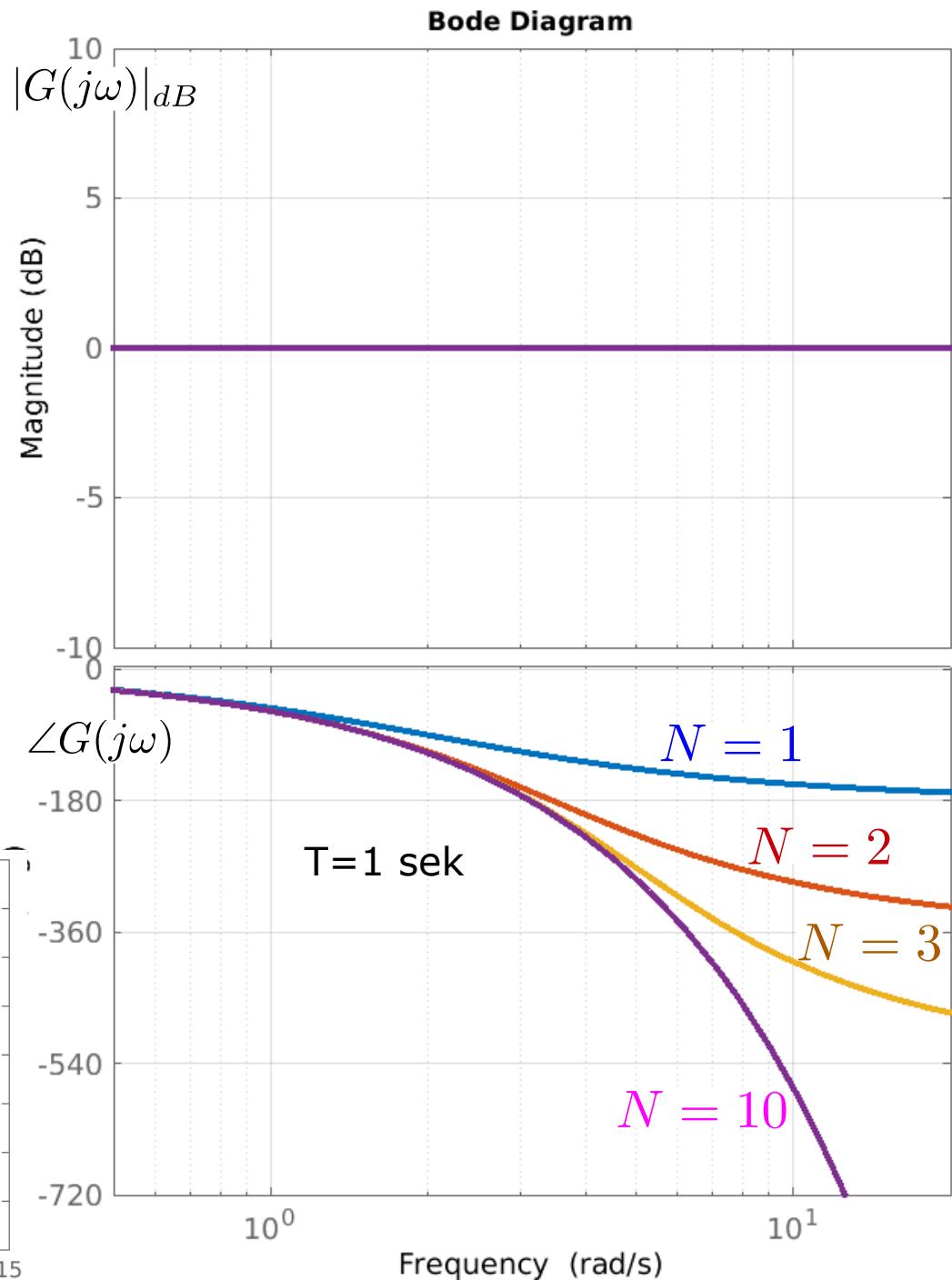
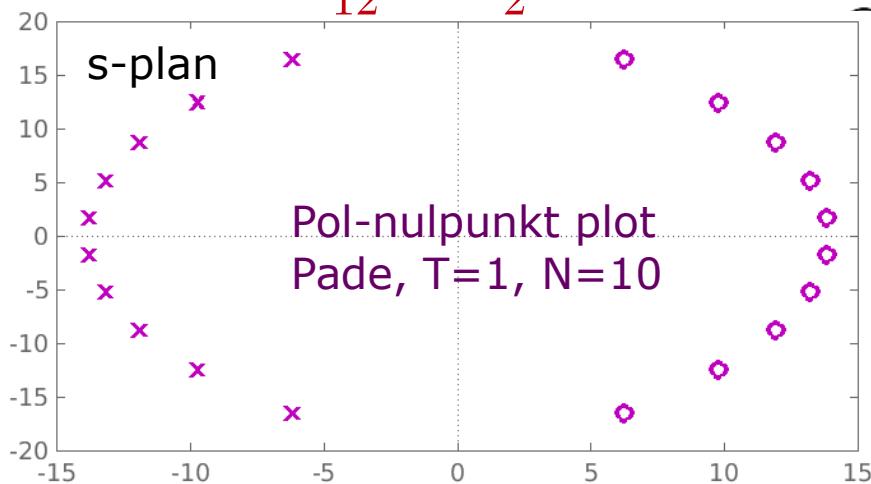
[num,den] = pade(T,N)

$$N = 1$$

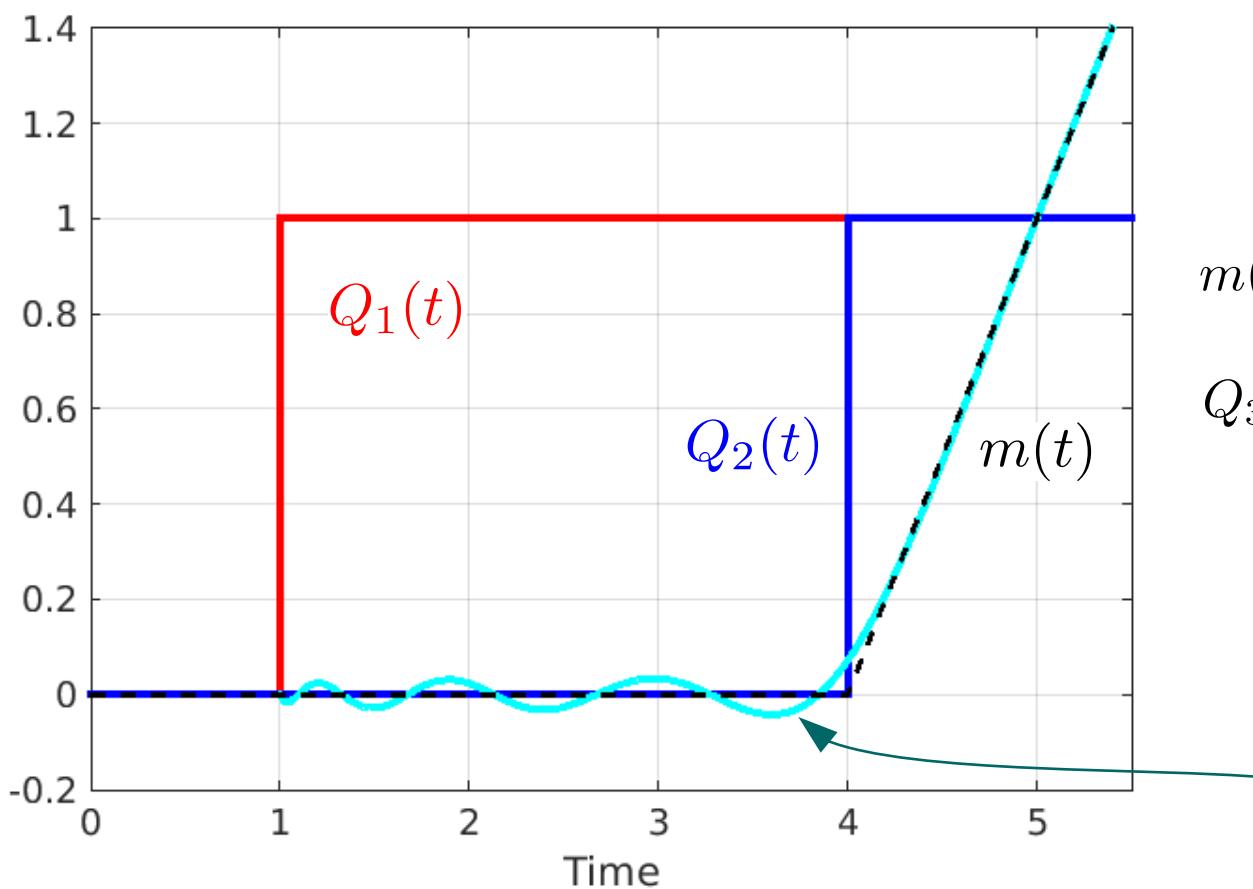
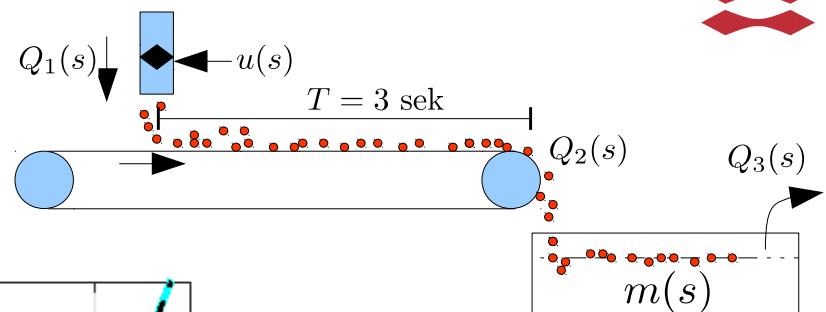
$$G_{p1}(s) = \frac{-\frac{T}{2}s + 1}{\frac{T}{2}s + 1}$$

$$N = 2$$

$$G_{p2}(s) = \frac{\frac{T^2}{12}s^2 - \frac{T}{2}s + 1}{\frac{T^2}{12}s^2 + \frac{T}{2}s + 1}$$



# Forsinkelse i overføringsfunktioner

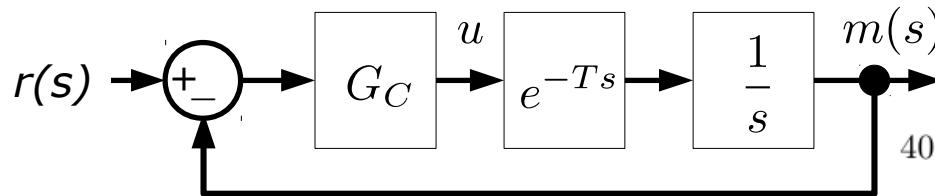


$$m(s) = u(s) \frac{e^{-3s}}{s} - Q_3(s) \frac{1}{s}$$

$$Q_3(t) = 0$$

$pade(T, N)$   
 $N = 7$  tilnærmelse

# Regulering af æblevask



$$G = \frac{m(s)}{u(s)} = \frac{e^{-3s}}{s}$$

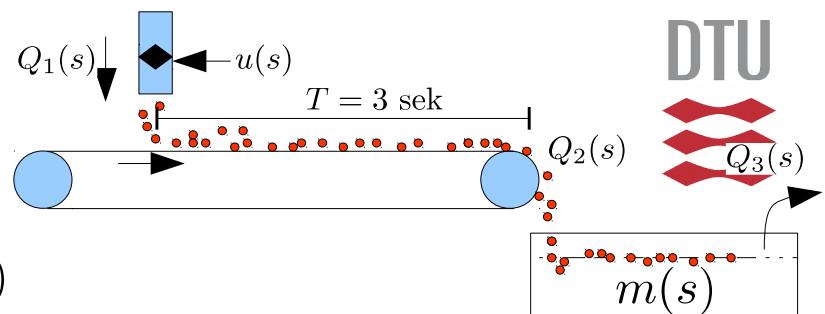
$$\gamma_M = 60^\circ$$

P-regulator

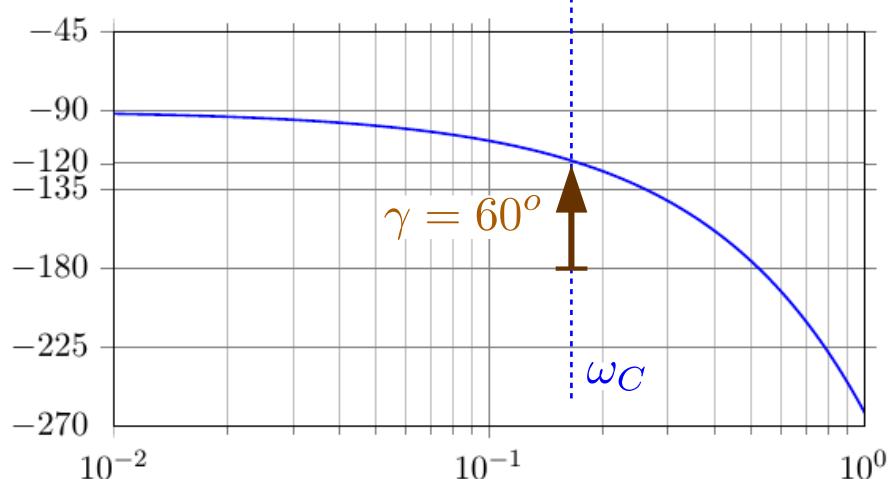
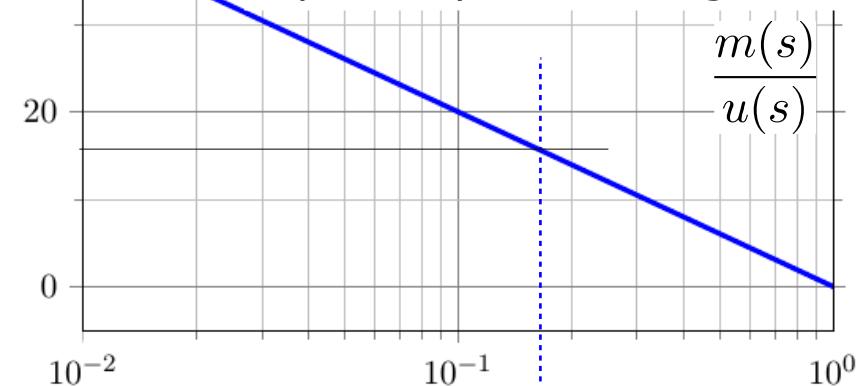
$$\omega_C = 0.17 \text{ rad/s}$$

$$|G(j\omega_C)|_{dB} = 15 \text{ dB}$$

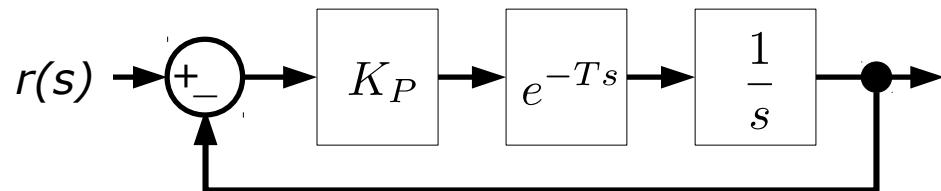
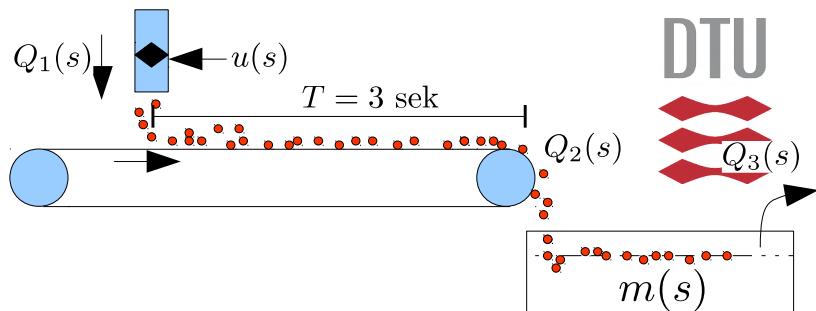
$$K_P = \frac{1}{5.7} = 0.175$$



Open loop - uden regulator

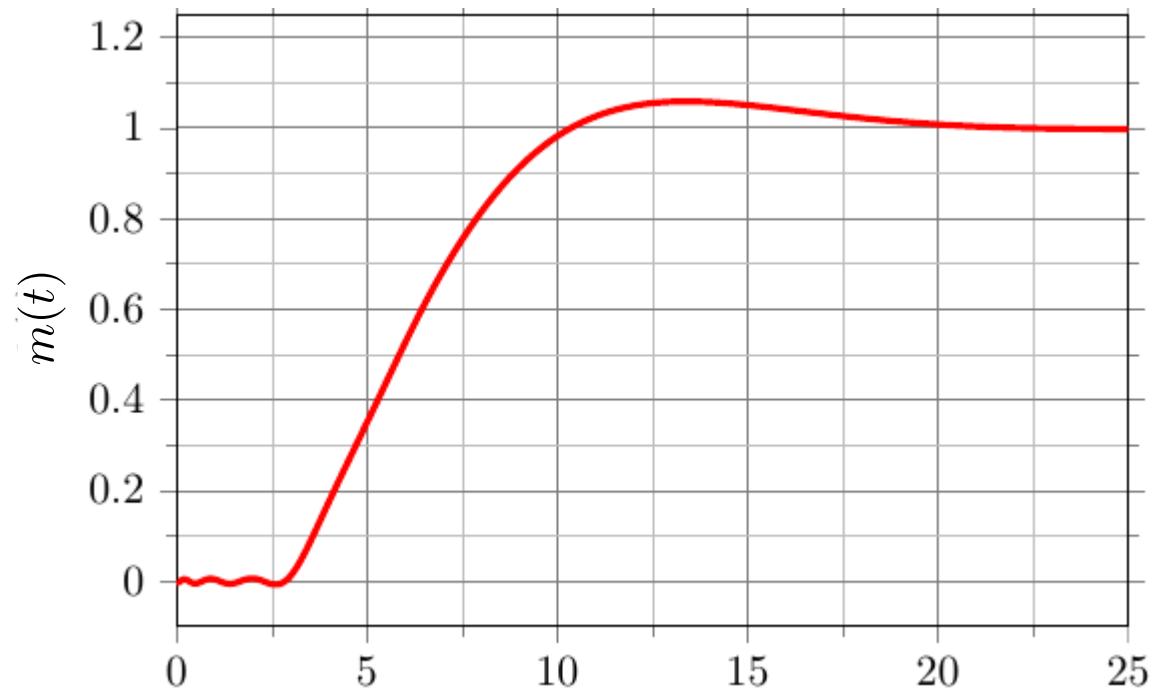


# Æblevask eksempel

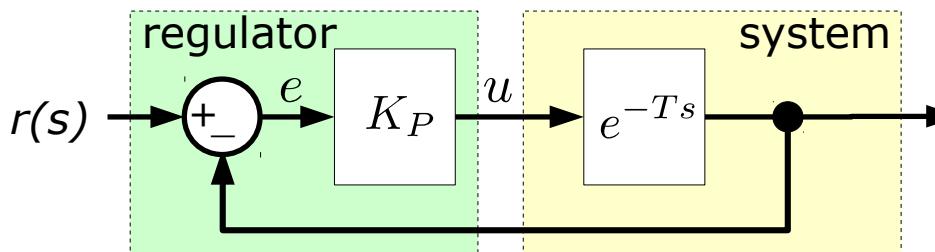


$$T = 3$$

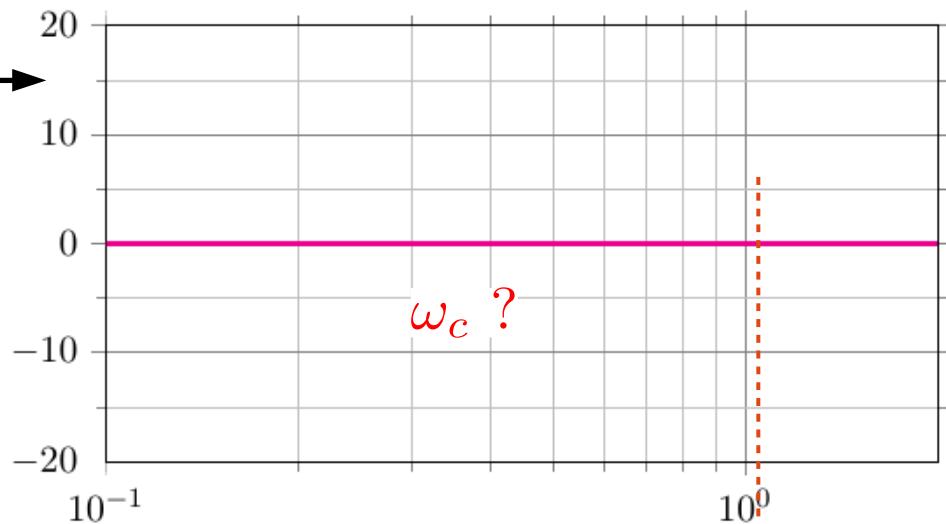
$$K_P = 0.175$$



# Regulering af kun delay



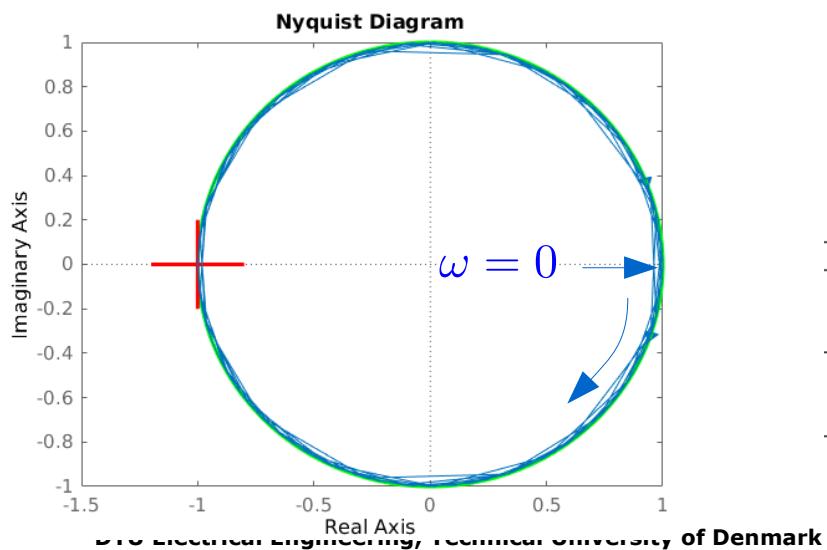
Bodeplot af system  
uden regulator ( $T=1$ )



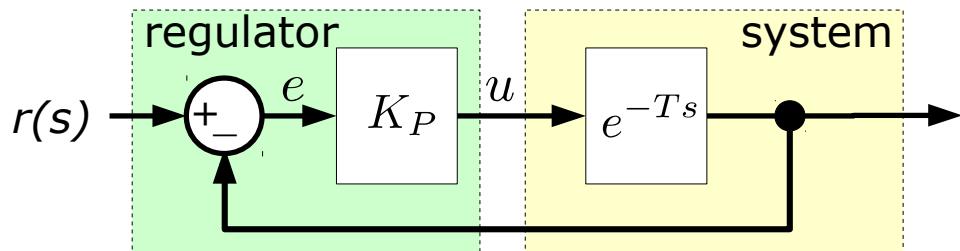
Hvilken  $K_P$  gør lukket sløjfe stabil?

$$K_P = ?$$

Fasemargin, gainmargin?



# Regulering af kun delay



Hvilken  $K_P$  gør lukket sløjfe stabil?

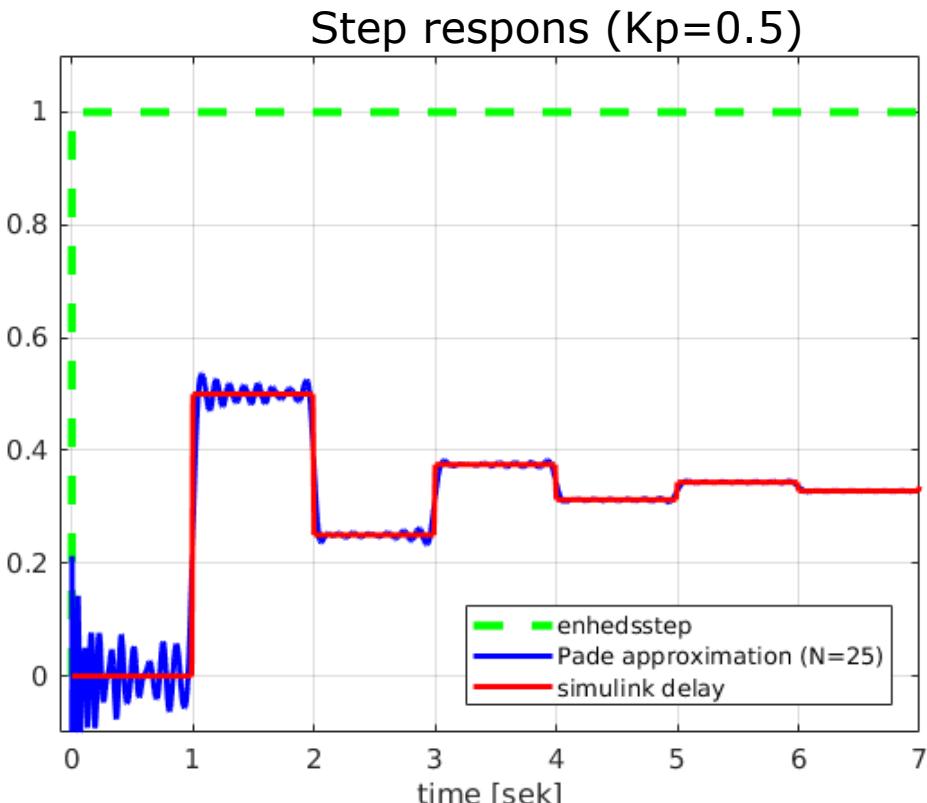
$$K_P = 0.5$$

Stationær fejl (enhedsstep på  $r(s)$ )

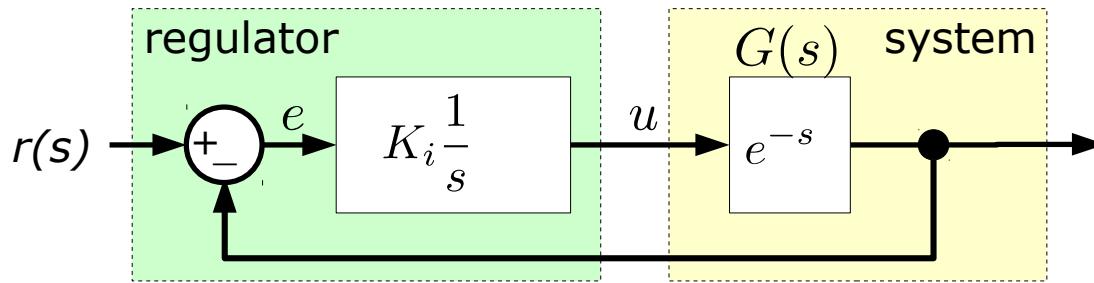
$$e_{r,ss} = \lim_{s \rightarrow 0} s \frac{1}{s} \frac{1}{1 + K_P e^{-Ts}}$$

$$e_{r,ss} = \frac{1}{1 + K_P}$$

$$e_{r,ss} = 0.67 \text{ (67\%)}$$



# Regulering af kun delay – I-regulator



I-regulator – PI kan bruges  
- system med I-led:

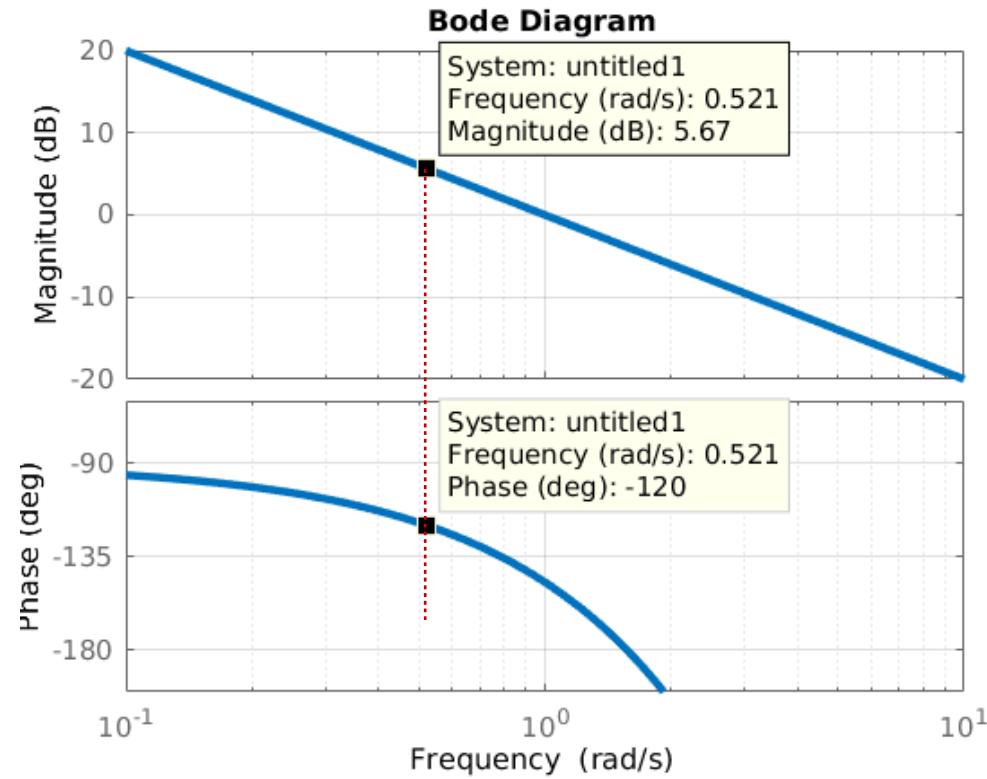
$$G_i = \frac{e^{-s}}{s}$$

$$\gamma_M = 60^\circ$$

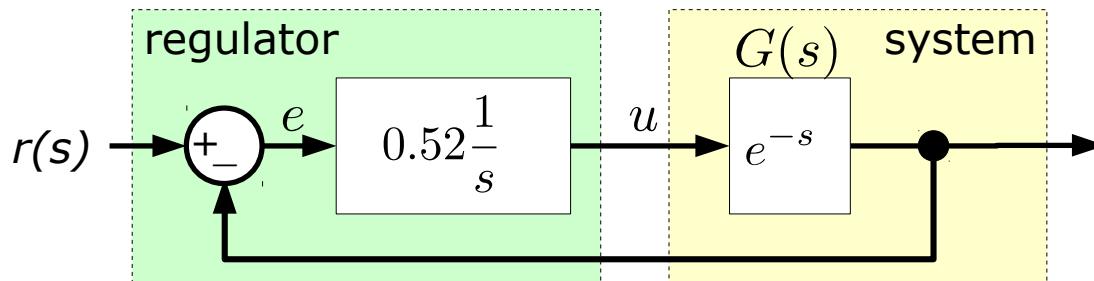
$$\angle G_i(\omega_c) = -180 + \gamma_M = -120^\circ$$

$$\omega_c = 0.521 \text{ rad/sek}$$

$$K_i = 10^{\frac{-5.67}{20}} = 0.52$$

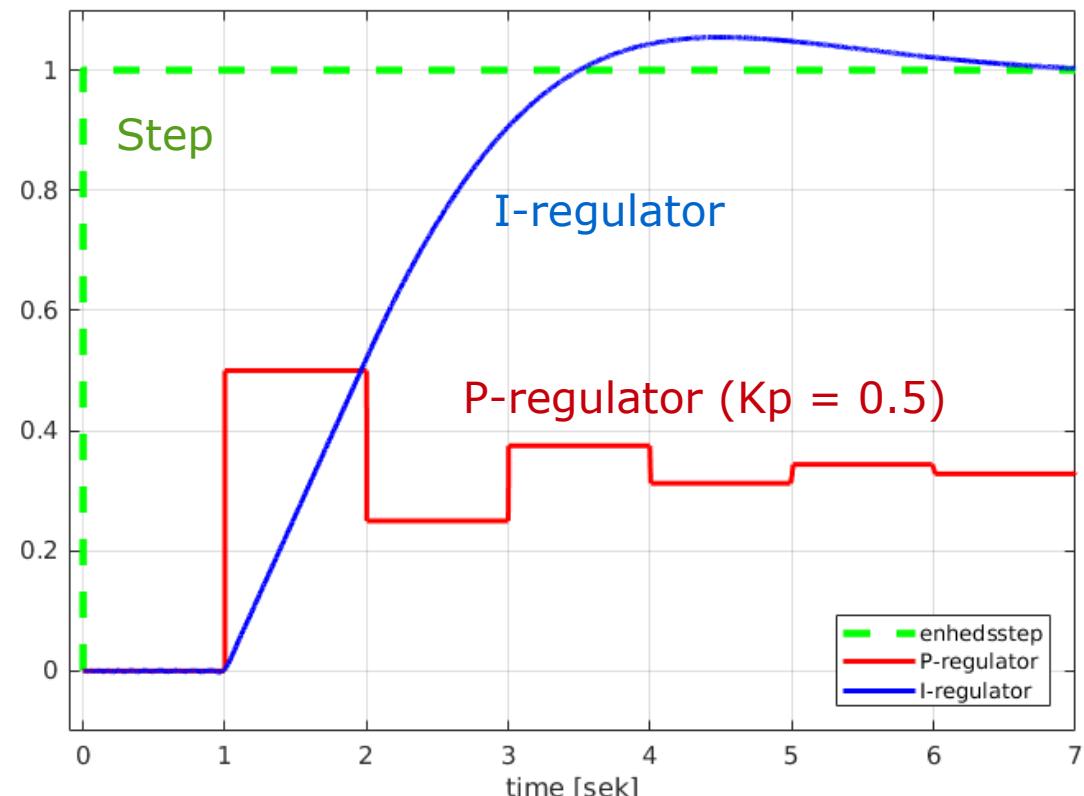


# Regulering af kun delay – I-regulator

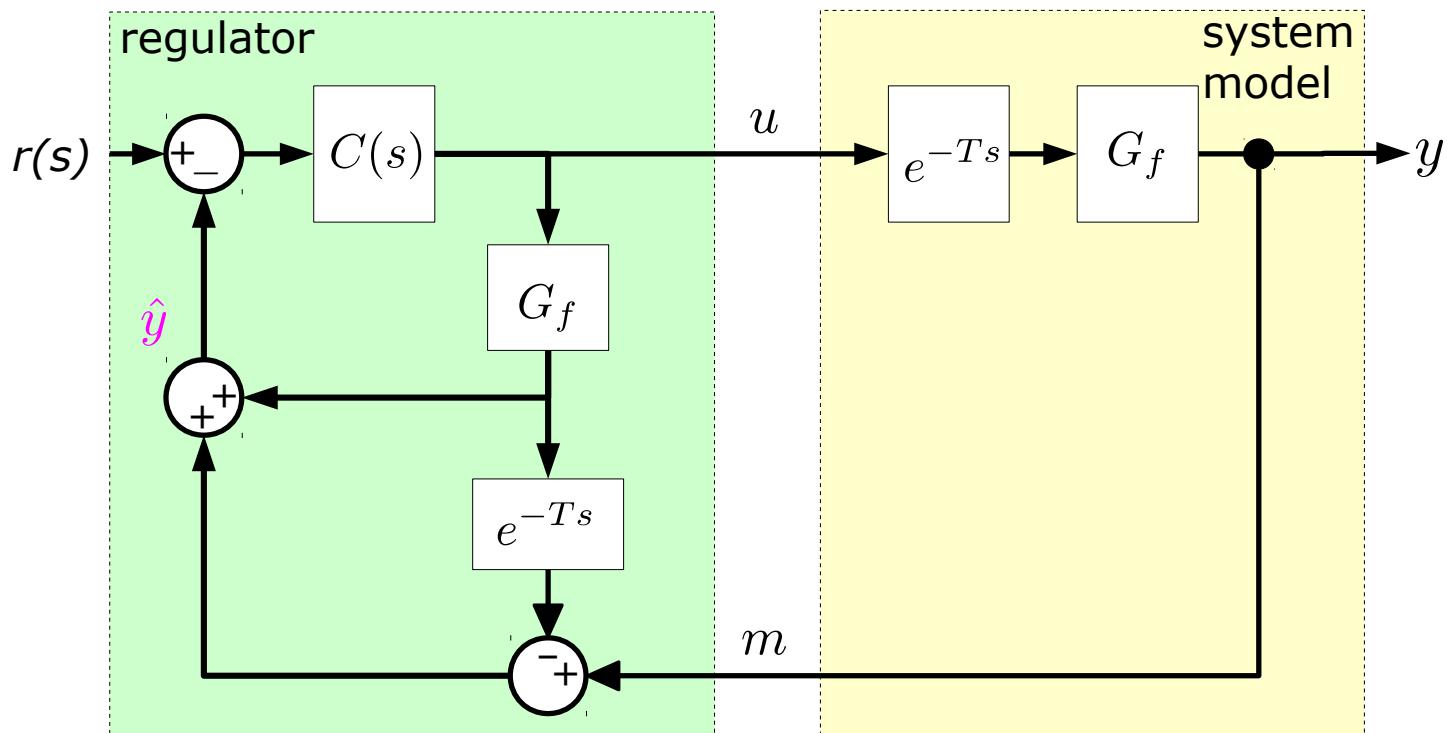


Delay: 1 sekund

Indsvingningstid  
ca. 6 sekunder



# Schmidt predictor - bedre metode



$$\hat{y} = u(e^{-Ts}G_f + G_f - G_f e^{-Ts})$$

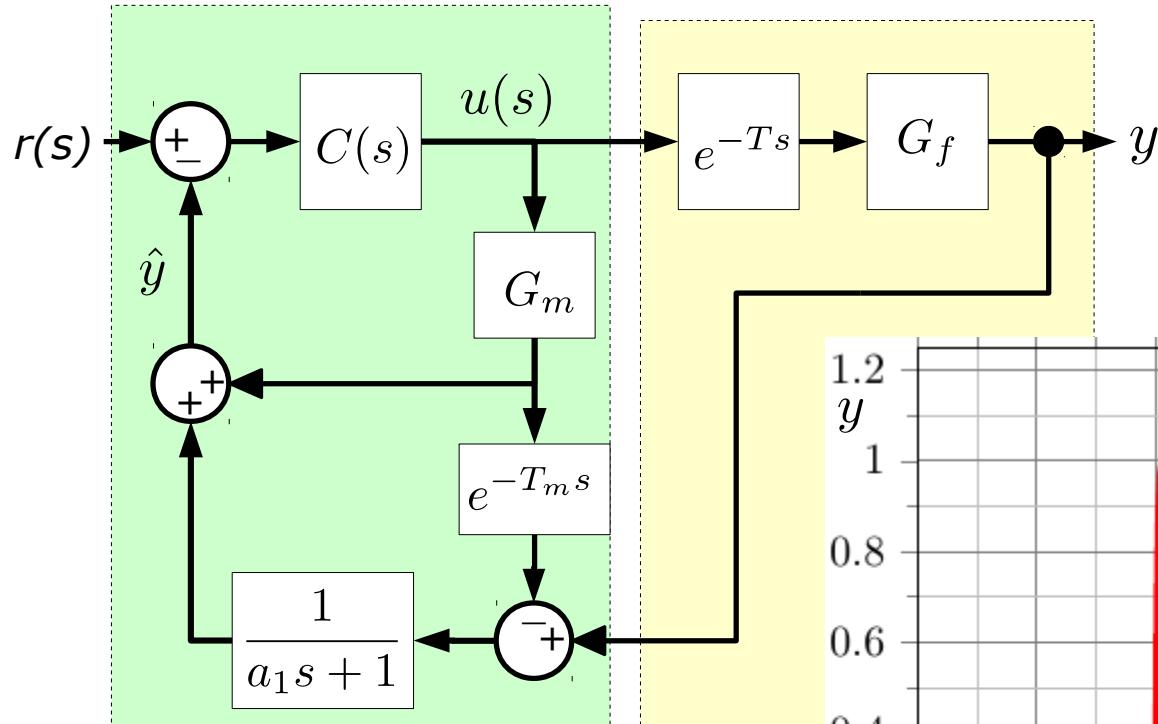
$$\hat{y} = uG_f$$

$G_C$  kan nu designes uden hensyn til forsinkelse!

Hvad hvis model er usikker?

# Schmidt predictor (stadig I-regulator)

- hvis usikkerhed i  $T$  eller  $G_f(s)$



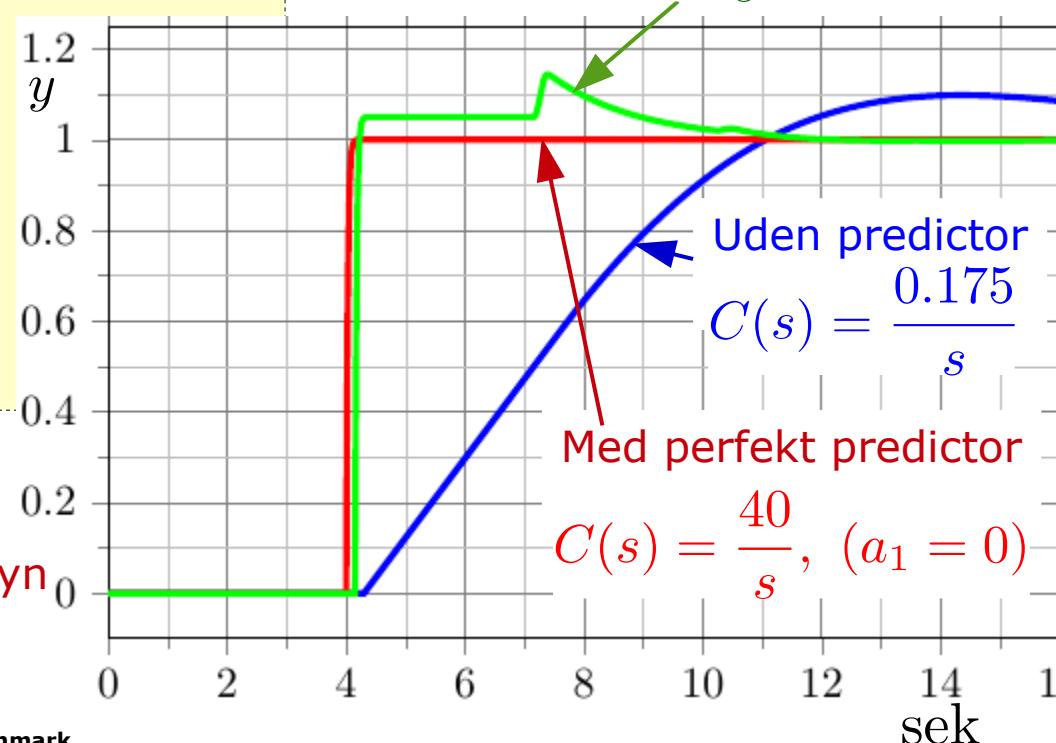
$$G_m = G_f = 1$$

$$T_m = T = 3 \text{ sek}$$

$$a_1 \approx \underbrace{|T - T_m|}_{\text{usikkerhed}} \cdot 10$$

$G_C$  kan designes  
næsten uden hensyn  
til forsinkelse

Med predictor og  
5% modelfejl  
 $T = 3.15, G = 1.05$   
 $C(s) = \frac{40}{s}, a_1 = 1.5$



# Kontrolspørgsmål

## Systemer med forsinkelse

### Spørgsmål

- a) En forsinkelse i Laplace  $e^{-Ts}$   
Hvordan skrives det i polynomium-form?
- b) Et system med kun forsinkelse,  
Hvad er ulempen ved en P-regulator?
- c) Et system med kun forsinkelse,  
Hvad er ulempen ved en I-regulator?

# Kontrolspørgsmål

## Systemer med forsinkelse

### Spørgsmål

- a) En forsinkelse i Laplace  $e^{-Ts}$   
Hvordan skrives det i polynomium-form?

Forsinkelsen omformuleres med Padé approksimation, der består af en serie poler og nulpunkter, og hvor nulpunkter har samme værdi som poler, men i højre halvplan

- b) Et system med kun forsinkelse,  
Hvad er ulempen ved en P-regulator?

Stor stationær fejl og lang indsvingningstid

- c) Et system med kun forsinkelse,  
Hvad er ulempen ved en I-regulator?

Lang indsvingningstid

# Nu og fremover

- Grupperegning – feed forward og delay
- Dagens øvelse: REGBOT Balance fortsat
- Husk kursusevaluering  
(bruges af underviser, studienævn, nye studerende, DTU, ministerium)
- Plan for resten af kurset (lektion og øvelse)
  - Kursusuge 13: Prøveeksamen, kursusevaluering  
(*REGBOT rapport*)
  - Skriftlig eksamen – 4 timer ca. 20 spørgsmål