### Reguleringsteknik 1

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#### Kursusuge 6

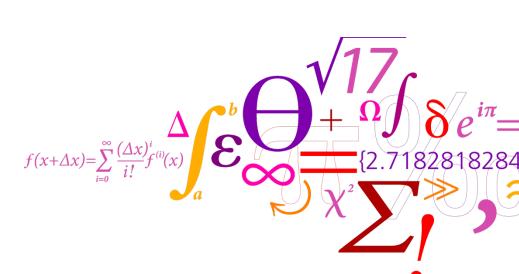
#### Plan

- Stabilitetsmargin
  - Begreber (igen)
  - Nyquist plot
- PID design ud fra frekvensanalyse
  - P- regulator
  - PI regulator
  - P-Lead regulator
- Grupperegningsopgaver
  - PI-Lead
  - Multiple choice

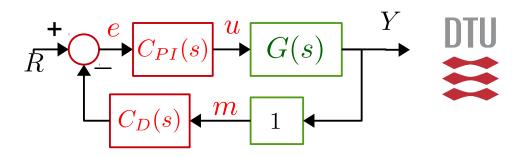
DTU Electrical Engineering

Department of Electrical Engineering





## **Grupperegning Lektion 6**



1. Design en PI-Lead regulator til et system G1

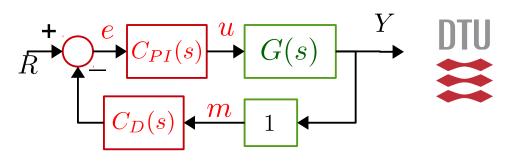
$$G_1 = \frac{9000}{(100s+1)(s^2+60s+900)}$$

a) Design en PI-Lead regulator, når der vælges:

$$N_i = 2, \ \alpha = 0.1 \text{ og } \gamma_M = 70^o$$

2. Multible choice opgaver på campusnet

### **Grupperegning**



- 1. Design en PI-Lead regulator til et system  $G_1 = \frac{3000}{(100s+1)(s^2+60s+900)}$
- a) Design en PI-Lead regulator, når der vælges:  $N_i=2,~\alpha=0.1~{
  m og}~\gamma_M=70^o$  Udregn fasedrejning for G1, hvor krydsfrekvensen skal ligge.

$$\varphi_i = -\arctan\frac{1}{N_i} = -26.6^o$$
  $\varphi_m = \arcsin\frac{1-\alpha}{1+\alpha} = 55^o$ 

$$\angle G_1(\omega=\omega_c)=-180+\gamma_M-\varphi_i-\varphi_m=-138^o \text{im}=\text{14.5 dB (at 49.9 rad/s), Pm}=\text{70 deg (at 13.5 rad/s)}$$

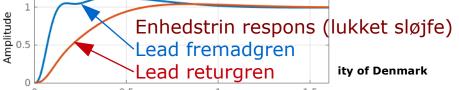
$$\omega_c = 13.4 \text{ rad/sek}$$

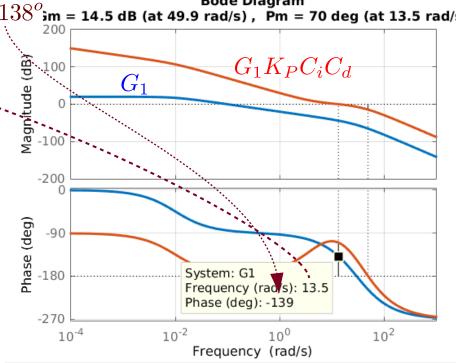
$$C_i = \frac{\tau_i s + 1}{\tau_i s}$$
  $C_d = \frac{\tau_d s + 1}{\alpha \tau_d s + 1}$ 

Find gain ved  $\,\omega_c\,$  for åben sløjfe uden  $\it Kp\,$ 

$$|G_{\mathring{a}}(\omega_c)| = |G_1 C_i C_d|_{s=j\omega_c}$$

$$|G_{\mathring{a}}(\omega_c)|_{dB} = -33.2dB \Rightarrow K_P = 45.8$$

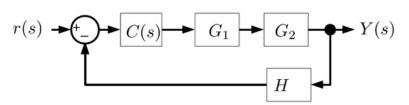




# Multiple choice – lektion 6

#### Lektion 06 supplerende opgaver

Et system kan beskrives som



Hvor G1 og G2 beskriver systemets dynamik og H beskriver målesystemets dynamik. Der skal designes regulatorer C(s), med det formål at Y(s) følger referencen r(s).

#### Spørgsmål 1

Et system er modelleret med en integrator således:

$$G_1 = \frac{2.2}{0.4s + 1}$$

$$G_2 = \frac{1}{s}$$

$$H = \frac{1}{0.02s + 1}$$

Design en P-Lead regulator til dette system med:

$$\gamma_M = 60^{\circ}$$
 $\alpha = 0.1$ 
 $\angle (G_1 G_2 H) = -180 + \gamma_M - \varphi_d = -175^{\circ}$ 

Hvad bliver indsvingningstiden (ca.) for et enhedstrin på referenceinput, hvis Lead-leddet placeres henholdsvis i fremadgrenen og i tilbagegrenen?

### **Bode Diagram** Gm = 18.1 dB (at 37.5 rad/s), Pm = 60 deg (at 9.08 rad/s)10 nitude (dB) $\frac{\tau_d s + 1}{0.1\tau_d s + 1}$ $G_{Kp} = G_1 G_2 H$ -50 $\tau_d = \frac{1}{\omega_c \sqrt{\alpha}} = 0.35$ $\omega_c = 9 \text{ rad/sek}$ -225 $10^{0}$ 101 $10^{2}$ Frequency (rad/s) 0.47sek $G_{cl} = \frac{K_P C_d G_1 G_2}{1 + G_{\circ}}$ 1.34sek $G_{cl} = \frac{K_P G_1 G_2}{1 + G_{\mathring{a}}}$ Fremad Retur (stepinfo)

Time (seconds)



## Multiple choice - lektion 6

#### Spørgsmål 2

En model af et andet system er beskrevet med:

$$G_1 = \frac{120}{0.01s + 1}$$

$$G_2 = \frac{1}{0.0025s^2 + 0.04s + 1}$$

$$H = \frac{1}{0.001s + 1}$$

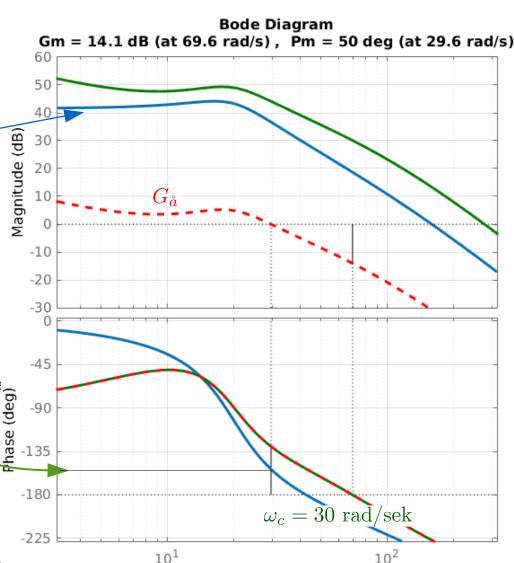
Design en PI-Lead regulator til dette system med

$$\gamma_M = 50^o 
N_i = 3 
\alpha = 0.2$$

Hvad bliver åben sløjfe krydsfrekvensen (ca.) for systeme

$$\angle(G_a G_{2H}) = -180 + \gamma_M - \varphi_i - \varphi_d = -153^{\circ}$$

$$\omega_c = 30 \text{ rad/sek}$$



Frequency (rad/s)



## Multiple choice - lektion 6

#### Spørgsmål 3

I en model med 2 integratorer (det kunne positionsstyring af være en

$$G_1 = \frac{2}{0.05s + 1}$$

$$G_2 = \frac{1}{s^2}$$

$$H = \frac{1}{0.002s + 1}$$

Design en P-Lead regulator med:

$$\gamma_M = 40^o$$
  
 $\alpha = 0.1$ 

$$\angle G(\omega_c) = -194^o$$

### **Bode Diagram** Gm = 14.4 dB (at 15.7 rad/s), Pm = 40 deg (at 5.1 rad/s)Magnitude (dB) -60 -135 Phase (deg) -225 $\omega_c = 5.1 \text{ rad/sek}$ 10<sup>1</sup>

Step Response

1.5

Time (seconds)

2.5

Oversving: 120%

$$T_d = 0.028$$

$$\tau_d = 0.62 \text{sek}$$
  $K_P = 4.25$ 

Oversving: 70%

Oversving: 40%

Stepinfo(lukket-sløjfe)

RiseTime: 0.1983 SettlingTime: 1.2011

SettlingMin: 0.9345 SettlingMax: 1.3932

Overshoot: 39.3218

Undershoot: 0

Peak: 1.3932 PeakTime: 0.5595 1.2 1 1 0.6 0.4 0.2

0.5

Oversving: 10%
Oversving: 0%