

Vibroacoustic Quantification of a Coastal Seabed

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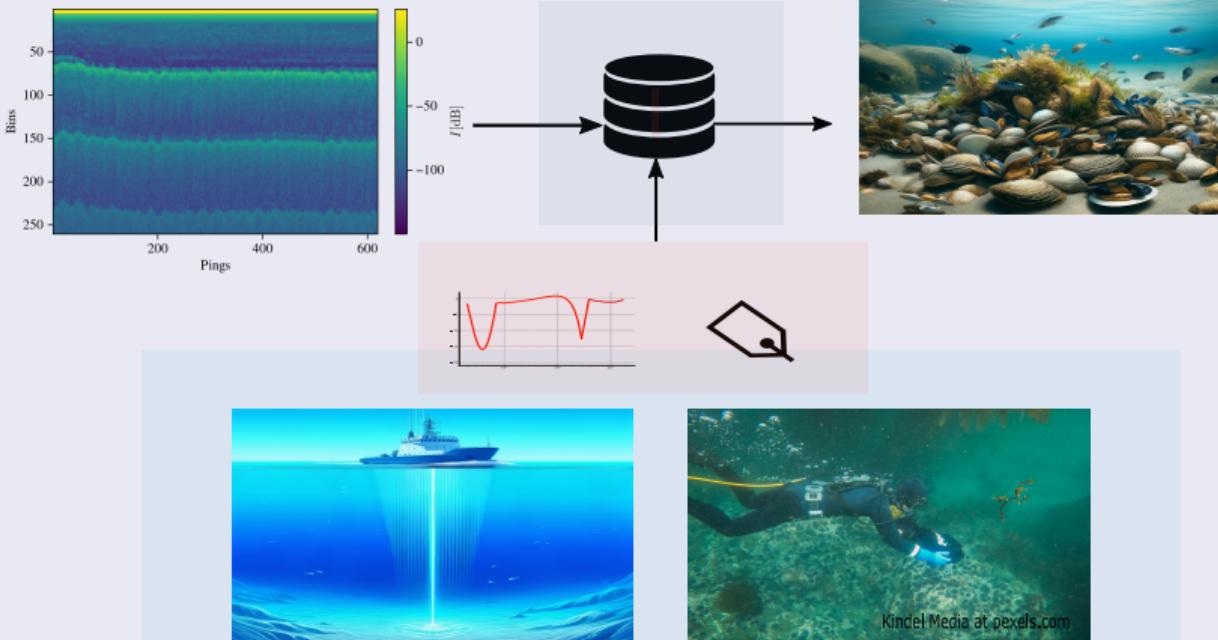
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Introduction

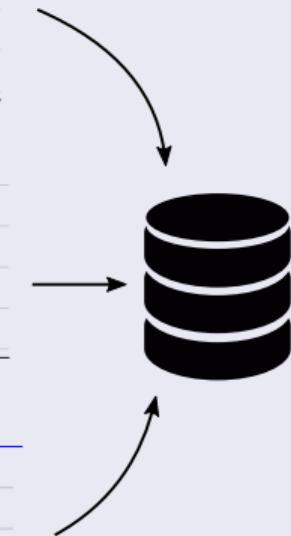
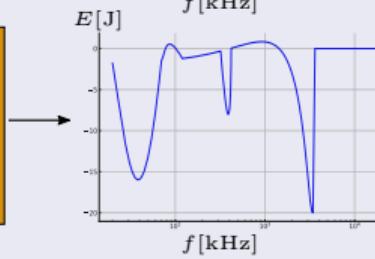
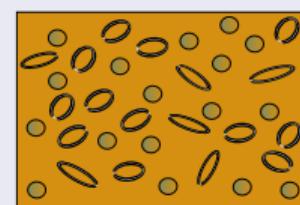
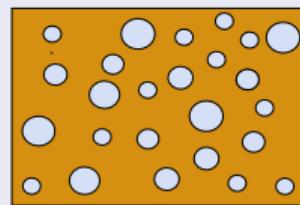
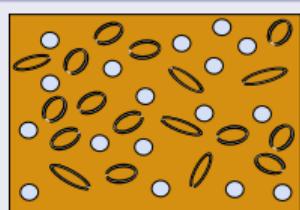
Interest in monitor the marine ecosystem



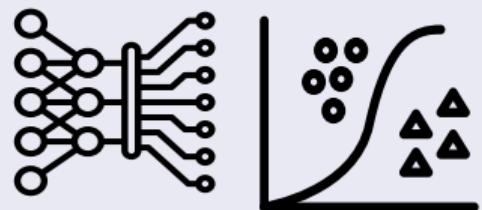
- A priori estimations.
- Database necessity.
- Traditional workflows.
- Highly time-consuming.

Objective

Can this database be generated virtually?

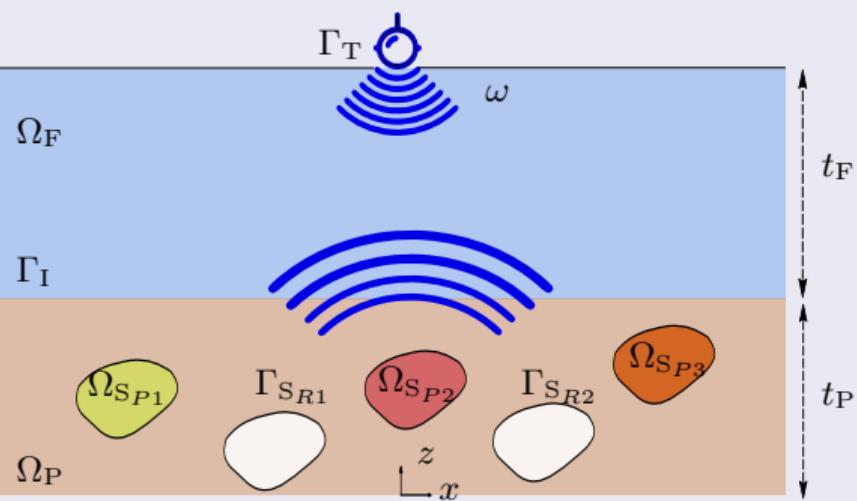


- Data base constructed
- Can we take advantage of this database and generate classifiers?
- Recognise new scenarios



Original problem

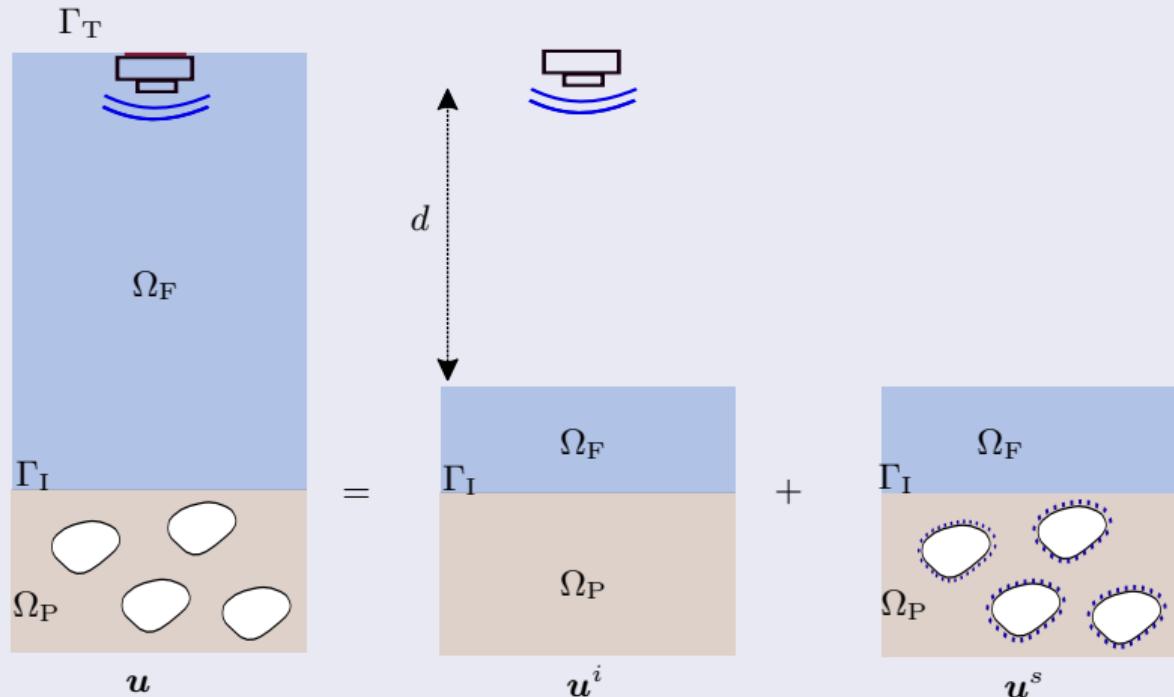
Statement of the problem: Total field



$$\left\{ \begin{array}{ll} -\omega^2 \rho_F \mathbf{u}_F - \nabla(K_F \operatorname{div} \mathbf{u}_F) = \mathbf{0} & \text{in } \Omega_F, \\ -\omega^2 \rho_P(\omega) \mathbf{u}_P - \nabla(K_P(\omega) \operatorname{div} \mathbf{u}_P) = \mathbf{0} & \text{in } \Omega_P, \\ -\omega^2 \rho_S(\omega) \mathbf{u}_S - \nabla(K_S(\omega) \operatorname{div} \mathbf{u}_S) = \mathbf{0} & \text{in } \Omega_{S_P}, \\ -\rho_F c_F^2 \operatorname{div} \mathbf{u}_F = \Pi_0 & \text{on } \Gamma_T, \\ \rho_F c_F^2 \operatorname{div} \mathbf{u}_F = K_P(\omega) \operatorname{div} \mathbf{u}_P & \text{on } \Gamma_I, \\ \mathbf{u}_F \cdot \mathbf{n} = \mathbf{u}_P \cdot \mathbf{n} & \text{on } \Gamma_I, \\ K_S(\omega) \operatorname{div} \mathbf{u}_F = K_P(\omega) \operatorname{div} \mathbf{u}_P & \text{on } \Gamma_{S_P}, \\ \mathbf{u}_P \cdot \mathbf{n} = \mathbf{u}_S \cdot \mathbf{n} & \text{on } \Gamma_{S_P}, \\ \mathbf{u}_P \cdot \mathbf{n} = 0 & \text{on } \Gamma_{S_R}, \\ \text{radiation conditions} & \text{at } |\mathbf{x}| \rightarrow \infty \end{array} \right.$$

Translation of the solution

Is necessary to simulate all the water column?



Incident field known for fluid and seabed domain

$$\mathbf{u} = \mathbf{u}^i + \mathbf{u}^s$$

Advantages

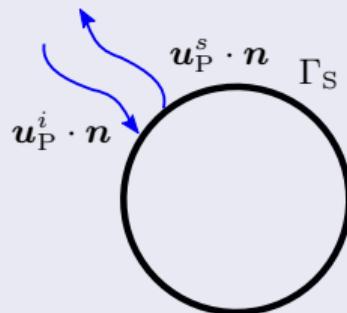
- Computation time ✓

Inconveniences

- Loss of physical domain ✗
- Analytical solution ✗

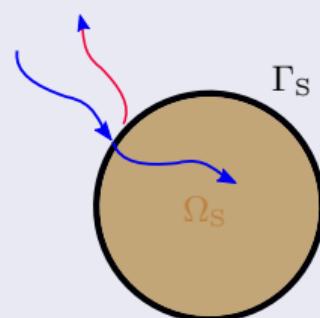
Translation of the solution

How the incident field chosen affect to the scattering objects?



Rigid \rightarrow Boundary condition to the porous domain:

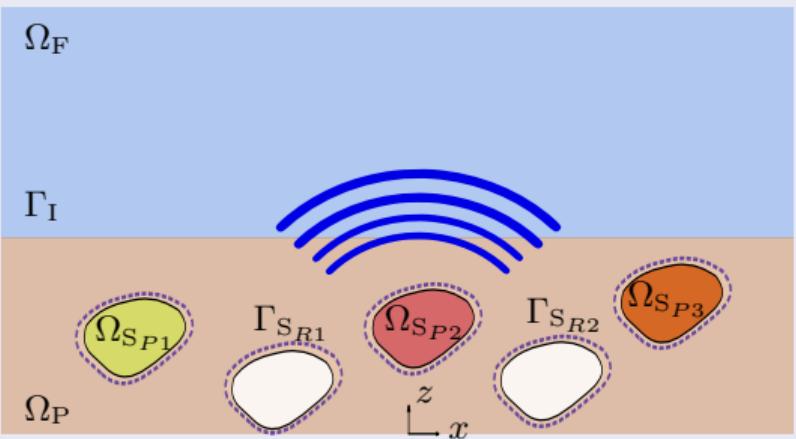
$$u_P^s \cdot n = -u_P^i \cdot n \quad \text{on } \Gamma_S.$$



Porous \rightarrow New medium, u_s^i is considered equal to u_P^i :

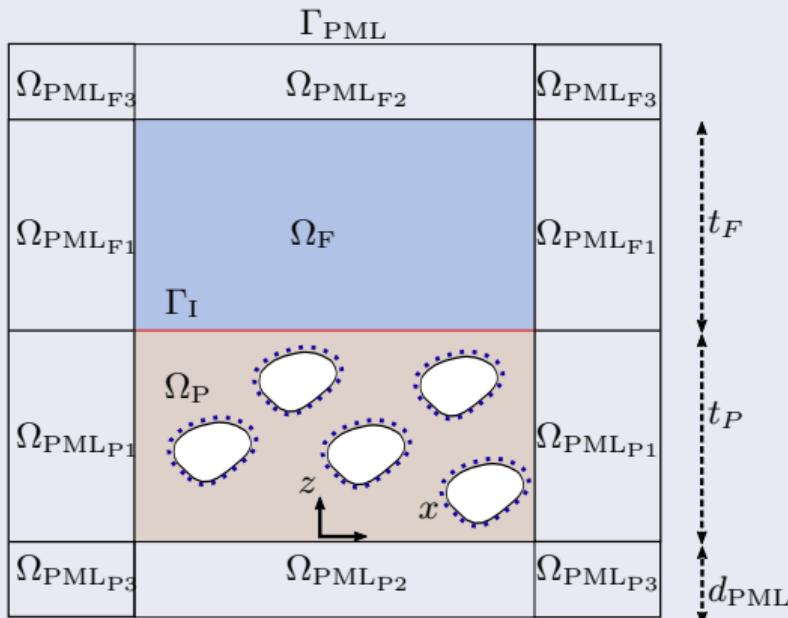
$$\begin{cases} -\rho_S \omega^2 \mathbf{u}_S^s - K_S(\omega) \nabla (\operatorname{div} \mathbf{u}_S^s) = (\rho_S \omega^2 - k_P^2 K_S(\omega)) \mathbf{u}_P^i & \text{in } \Omega_S, \\ \mathbf{u}_S^s \cdot \mathbf{n} = \mathbf{u}_P^s \cdot \mathbf{n} & \text{on } \Gamma_S, \\ K_P(\omega) \operatorname{div} \mathbf{u}_P^s - K_S(\omega) \operatorname{div} \mathbf{u}_S^s = (1 - K_S(\omega)/K_P(\omega)) \Pi_P^i & \text{on } \Gamma_S. \end{cases}$$

Statement of the problem: Scattering field



$$\left\{ \begin{array}{ll} -\omega^2 \rho_F \mathbf{u}_F^s - \nabla(K_F \operatorname{div} \mathbf{u}_F^s) = \mathbf{0} & \text{in } \Omega_F, \\ -\omega^2 \rho_P(\omega) \mathbf{u}_P^s - \nabla(K_P(\omega) \operatorname{div} \mathbf{u}_P^s) = \mathbf{0} & \text{in } \Omega_P, \\ -\omega^2 \rho_S(\omega) \mathbf{u}_S^s - \nabla(K_S(\omega) \operatorname{div} \mathbf{u}_S^s) = \mathbf{f} & \text{in } \Omega_{S_P}, \\ \rho_F c_F^2 \operatorname{div} \mathbf{u}_F^s = K_P(\omega) \operatorname{div} \mathbf{u}_P^s & \text{on } \Gamma_I, \\ \mathbf{u}_F^s \cdot \mathbf{n} = \mathbf{u}_P^s \cdot \mathbf{n} & \text{on } \Gamma_I, \\ K_S(\omega) \operatorname{div} \mathbf{u}_F^s = K_P(\omega) \operatorname{div} \mathbf{u}_P^s + g & \text{on } \Gamma_{S_P}, \\ \mathbf{u}_P^s \cdot \mathbf{n} = \mathbf{u}_S^s \cdot \mathbf{n} & \text{on } \Gamma_{S_P}, \\ \mathbf{u}_P^s \cdot \mathbf{n} = -\mathbf{u}_P^i \cdot \mathbf{n} & \text{on } \Gamma_{S_R}, \\ \text{radiation conditions} & \text{at } \|x\| \rightarrow \infty \end{array} \right.$$

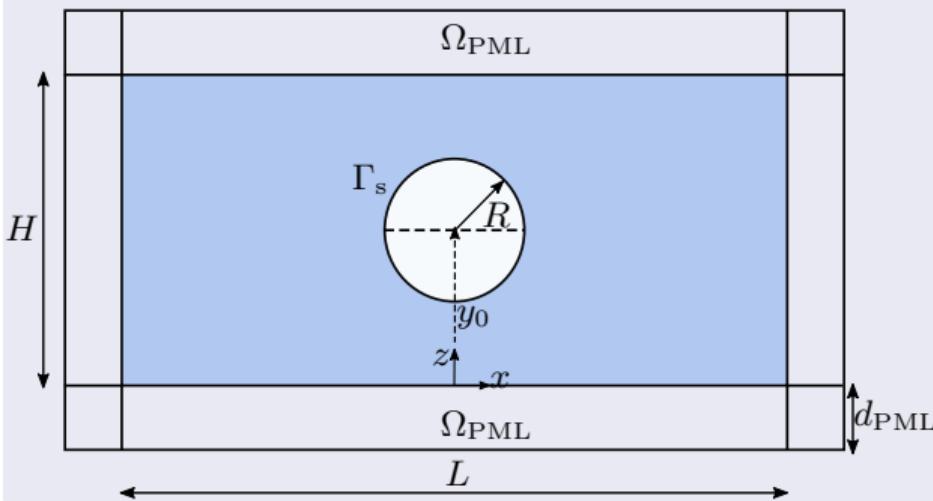
Perfectly Matched Layers



- New PML formulation has been developed
 - Conventional formulation:
$$-\rho(\omega)\omega^2 J\mathbf{u} - \operatorname{div}\left(K(\omega)\left(JH^{-T}(H^{-1} : \nabla\mathbf{u})\right)\right) = \mathbf{0}$$
 - Novel formulation:
- $$-\rho(\omega)\omega^2 J^{-1} H^T H \mathbf{U} - \nabla\left(K(\omega)J^{-1} \operatorname{div} \mathbf{U}\right) = \mathbf{0}$$
- where $\mathbf{U} = JH^{-1}\mathbf{u}$, H := PML absorbing 2×2 tensor and $J = \det H$
- Continuity in normal displacements inside PML
 - PML quadratic absorbing profile

PML verification: Conventional vs Novel PML formulation

Benchmark solved:



Analytical solution in terms of Hankel functions:

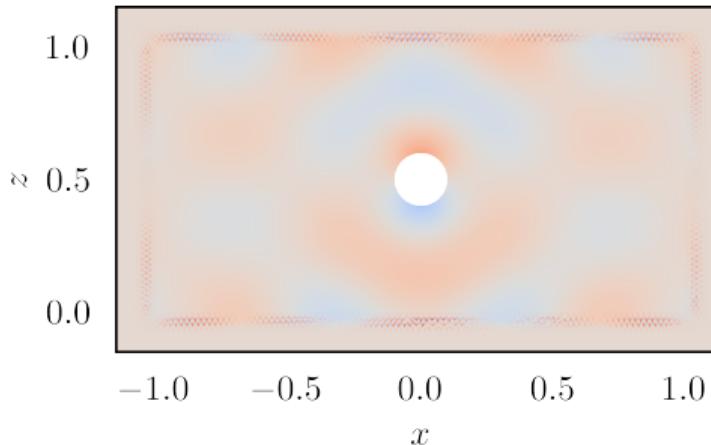
$$\Pi(x, y) = \Pi_0 \frac{H_0^{(1)} \left(k \sqrt{(x - x_0)^2 + (z - z_0)^2} \right)}{H_0^{(1)}(kR)}$$

Objectives to check:

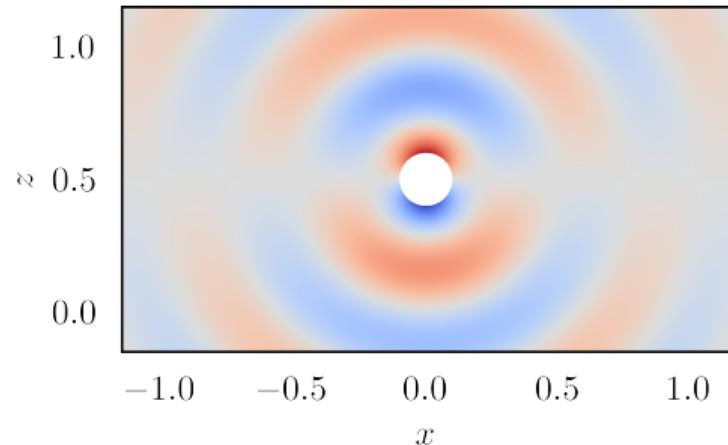
- Numerical instabilities
- New formulation ensures continuity

Benchmark results

$$-\rho\omega^2 J\mathbf{u} - \operatorname{div} \left(K(\omega) \left(JH^{-T} (H^{-1} : \nabla \mathbf{u}) \right) \right) = \mathbf{0} \quad \text{in } \Omega$$



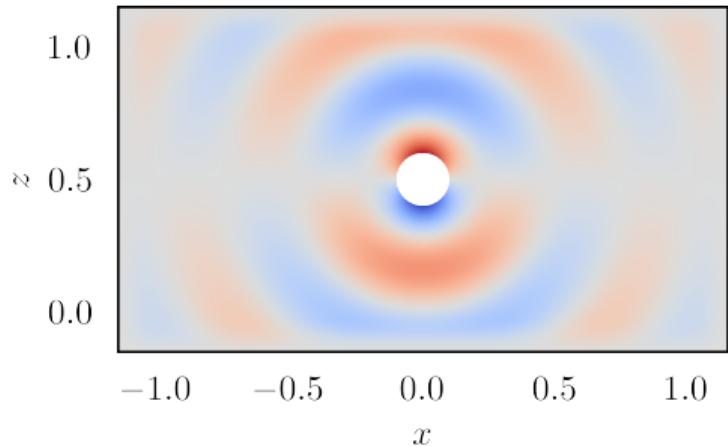
$\operatorname{Re}(u_z)$
-3.6e-07 3.1e-07
Conventional PML formulation



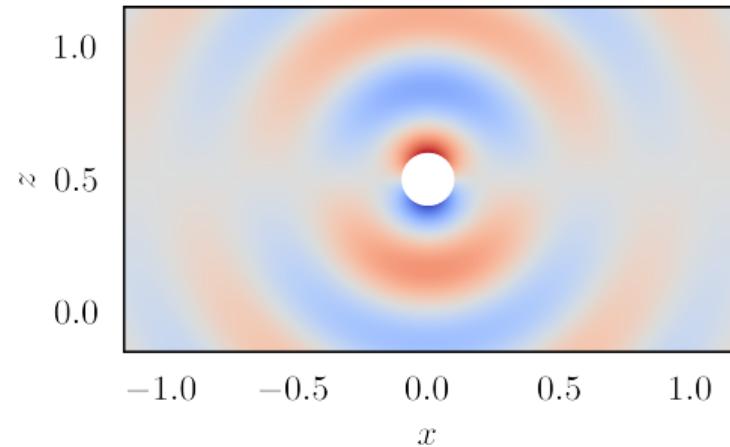
$\operatorname{Re}(u_{ex_z})$
-3.5e-07 3.5e-07
Analytical solution

Benchmark results

$$-\rho\omega^2 J^{-1} H^T H \mathbf{U} - \nabla (K(\omega) J^{-1} \operatorname{div} \mathbf{U}) = \mathbf{0} \quad \text{in } \Omega$$



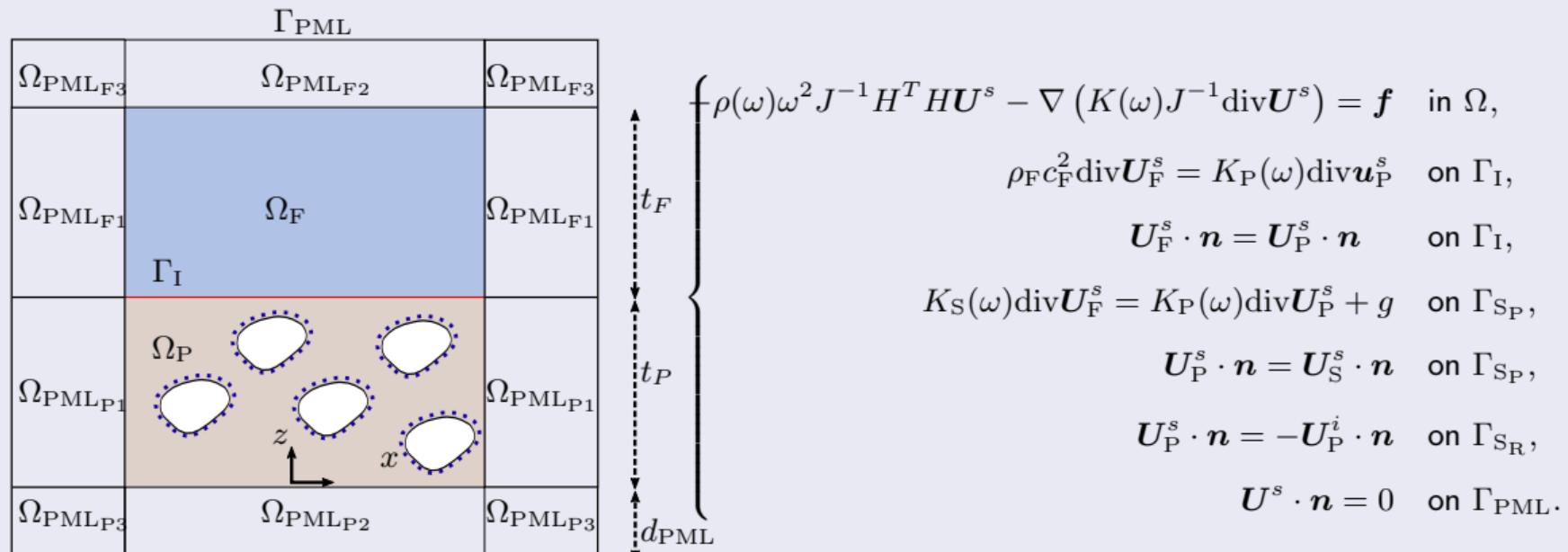
$\operatorname{Re}(u_z)$
Novel PML formulation



$\operatorname{Re}(u_{ex_z})$
Analytical solution

Translated and bounded problem

Model with PML



Remark 1: $\Omega = \Omega_F \cup \Omega_P \cup \Omega_S \cup \Omega_{\text{PML}}$

Remark 2: In $\Omega_F \cup \Omega_P \cup \Omega_S$, $H = I$ and $J = 1$ so $-\omega^2 \rho(\omega) \mathbf{U}^s - \nabla(K(\omega) \operatorname{div} \mathbf{U}^s) = \mathbf{0}$

Variational formulation

What about the trial and test functions?

Trial space:

$$\mathbf{U}^s \in V = \left\{ \mathbf{w} \in [L^2(\Omega)]^2 : \operatorname{div} \mathbf{w} \in L^2(\Omega), \mathbf{w} \cdot \mathbf{n} = 0 \text{ on } \Gamma_{\text{PML}} \right\} \subset H(\operatorname{div}, \Omega).$$

Test space:

$$\mathbf{v} \in V_0 = \{ \mathbf{w} \in H(\operatorname{div}, \Omega) : \mathbf{w} \cdot \mathbf{n} = 0 \text{ on } \Gamma_{\text{PML}} \text{ and } \mathbf{w} \cdot \mathbf{n} = 0 \text{ on } \Gamma_{S_R} \}.$$

For a given fixed angular frequency $\omega > 0$, and an incident field in the seabed domain \mathbf{u}_P^i , find $\mathbf{U}^s \in V$ such that $\mathbf{U}^s \cdot \mathbf{n} = \mathbf{u}_P^i \cdot \mathbf{n}$ on Γ_{S_R} and

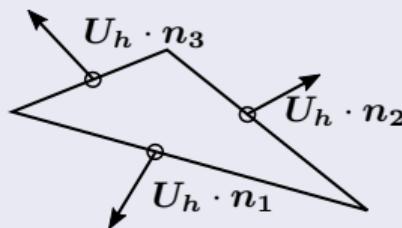
$$\underbrace{-\omega^2 \int_{\Omega} \rho(\omega) J^{-1}(H\mathbf{U}^s) \cdot (H\mathbf{v}) \, d\Omega + \int_{\Omega} K(\omega) J^{-1} \operatorname{div} \mathbf{U}^s \operatorname{div} \mathbf{v} \, d\Omega}_{\substack{\text{mass term} \\ \text{stiffness term}}} =$$
$$\underbrace{\int_{\Omega} \mathbf{f} \cdot \mathbf{v} \, d\Omega}_{\substack{\text{volumetric source term}}} - \underbrace{\int_{\Gamma_{S_P}} g(\mathbf{v} \cdot \mathbf{n}) \, d\Gamma_{S_P}}_{\substack{\text{boundary source term}}} , \quad \forall \mathbf{v} \in V_0.$$

Discretisation

What about the finite elements used to discretize the problem?

First-order Raviart-Thomas finite elements for all the domains

$$V_h = \left\{ \boldsymbol{w}_h \in V : \boldsymbol{w}_h|_T = \boldsymbol{a}_T + \boldsymbol{b}_T(x, z)^T, \boldsymbol{a}_T \in \mathbb{C}^2, \boldsymbol{b}_T \in \mathbb{C}, T \subset \Omega, T \in \mathcal{T}_h \right\}$$



$$(-\omega^2 \mathcal{M} + \mathcal{K}) \vec{w}_h = \vec{f} + \vec{g}$$

$$[\mathcal{M}]_{ij} = \int_{\Omega} \rho(\omega) F J^{-1} (H \boldsymbol{\varphi}_i) \cdot (H \boldsymbol{\varphi}_j) \, d\Omega$$

$$[\boldsymbol{f}]_i = \int_{\Omega} \boldsymbol{f} \cdot \boldsymbol{\varphi}_i \, d\Omega$$

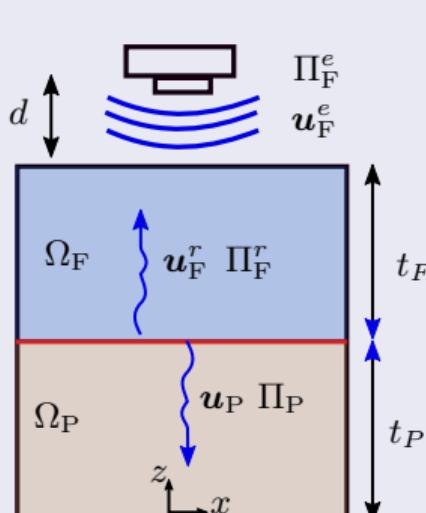
$$[\mathcal{K}]_{ij} = \int_{\Omega} K(\omega) J^{-1} \operatorname{div} \boldsymbol{\varphi}_i \operatorname{div} \boldsymbol{\varphi}_j \, d\Omega$$

$$[\boldsymbol{g}]_i = \int_{\Omega} g (\boldsymbol{v} \cdot \boldsymbol{\varphi}_i) \, d\Gamma_{S_P}$$

Calculation of the incident field

How is the incident field computed?

Fourier Mode Decomposition of the emitted field on the interface:



$$\Pi_F^e(x, t_P) = \sum_{j=-N/2}^{N/2} \pi_{0j} e^{-ik_j x}, \quad \mathbf{u}_F^e(x, t_P) = \sum_{j=-N/2}^{N/2} \mathbf{u}_{0j} e^{-ik_j x}$$

$$\Pi_F^r(x, z) = \sum_j \Pi_F^r j e^{i\sqrt{k_F^2 - k_j^2}z} e^{-ik_j x}, \quad \Pi_P(x, z) = \sum_j \Pi_P^r j e^{-i\sqrt{k_P^2 - k_j^2}z} e^{-ik_j x}$$

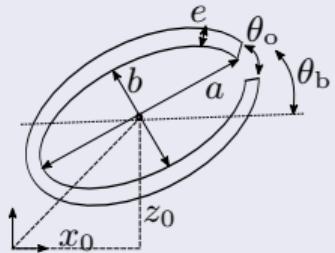
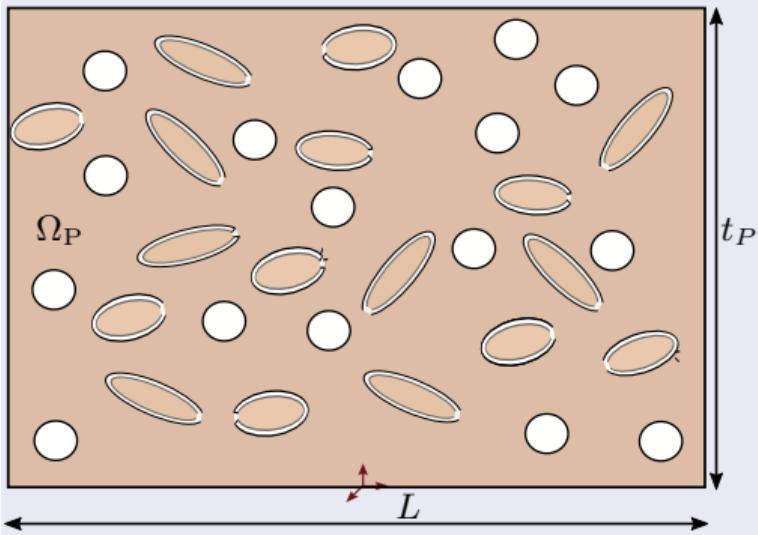
$$\left\{ \begin{array}{l} \Delta \Pi_F^r - k_F^2 \Pi_F^r = 0 \quad \text{in } \Omega_F, \\ \Delta \Pi_P^r - k_P^2 \Pi_P^r = 0 \quad \text{in } \Omega_P, \\ \Pi_F^r + \Pi_F^r i = \Pi_P^r \quad \text{on } \Gamma_I, \\ \frac{1}{\rho_F \omega^2} \frac{\partial \Pi_F^r}{\partial \mathbf{n}} + \frac{1}{\rho_F \omega^2} \frac{\partial \Pi_F^e}{\partial \mathbf{n}} = \frac{1}{\rho_P \omega^2} \frac{\partial \Pi_P^r}{\partial \mathbf{n}} \quad \text{on } \Gamma_I. \end{array} \right.$$

Remark: $\mathbf{u}^i = \frac{1}{\rho \omega^2} \nabla \Pi$

Obstacles inside porous domain

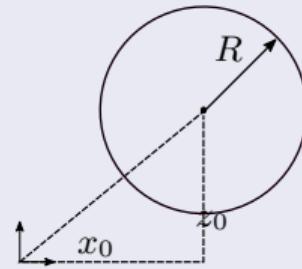
How are the scattering objects generated?

In Ω_P a combination of the following objects could be generated:



Ellipses:

- $a \sim \mathcal{N}(a_0, \sigma_a^2)$
- $b \sim \mathcal{N}(b_0, \sigma_b^2)$
- $\theta_o \sim \mathcal{N}(\theta_0, \sigma_{\theta_0}^2)$
- $\theta_b \sim \mathcal{N}(\theta_b, \sigma_{\theta_b}^2)$
- $e \sim \mathcal{N}(e_0, \sigma_e^2)$
- $x_c \sim \mathcal{U}(-L/2, L/2)$
- $y_c \sim \mathcal{U}(0, t_P)$

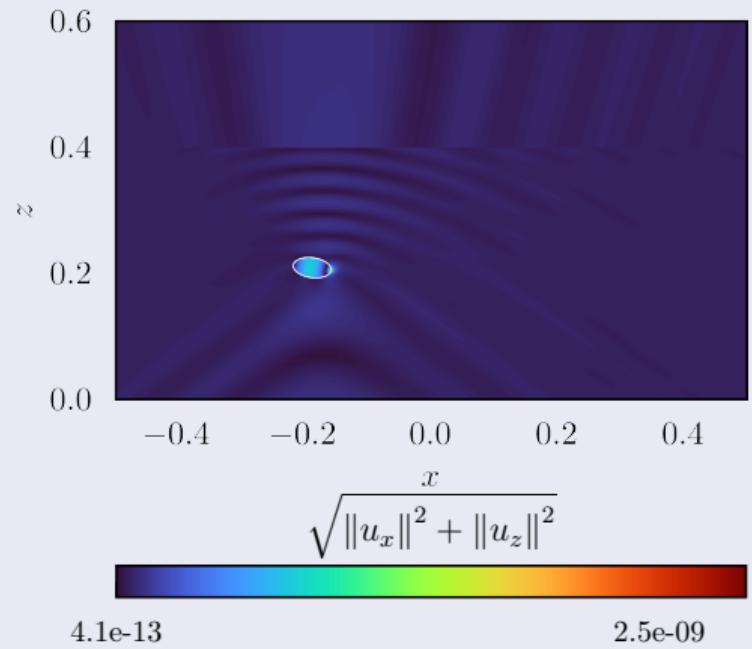
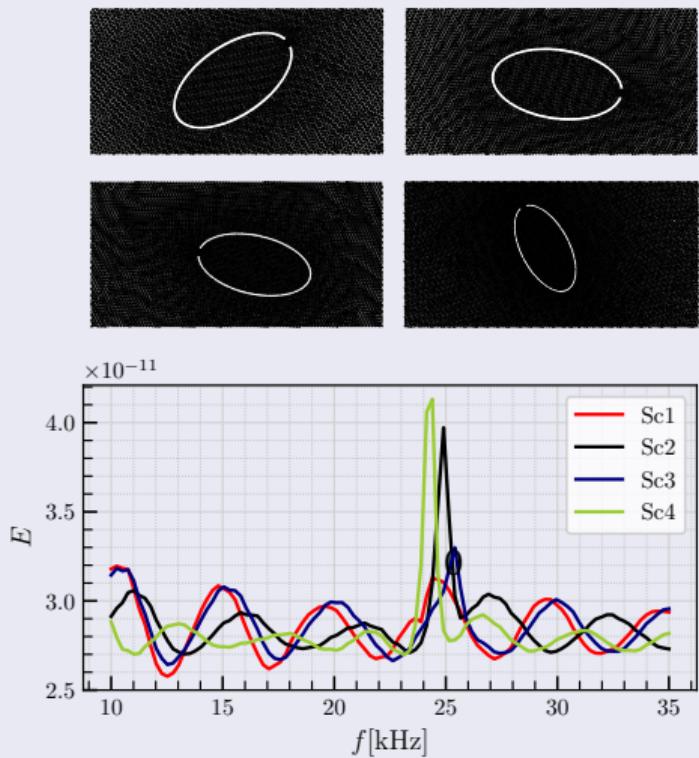


Circles:

- $R \sim \mathcal{N}(R_0, \sigma_r^2)$
- $x_c \sim \mathcal{U}(-L/2, L/2)$
- $y_c \sim \mathcal{U}(0, t_P)$

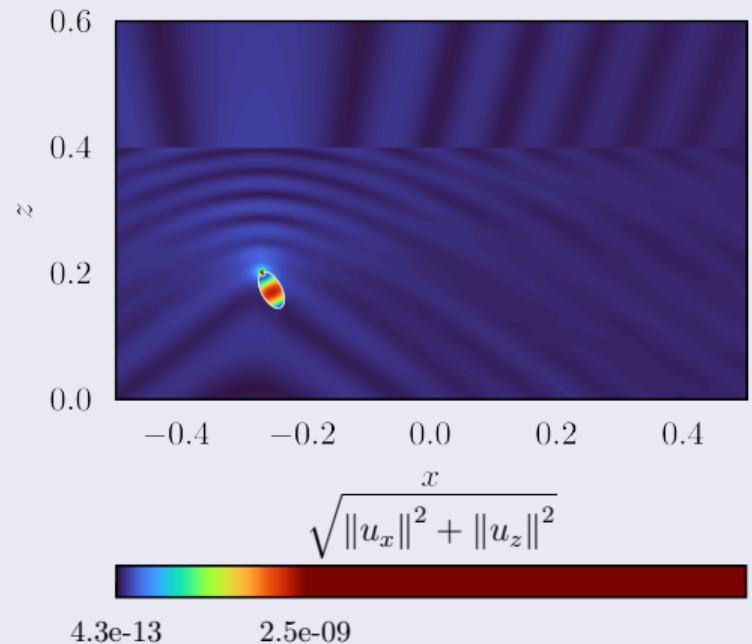
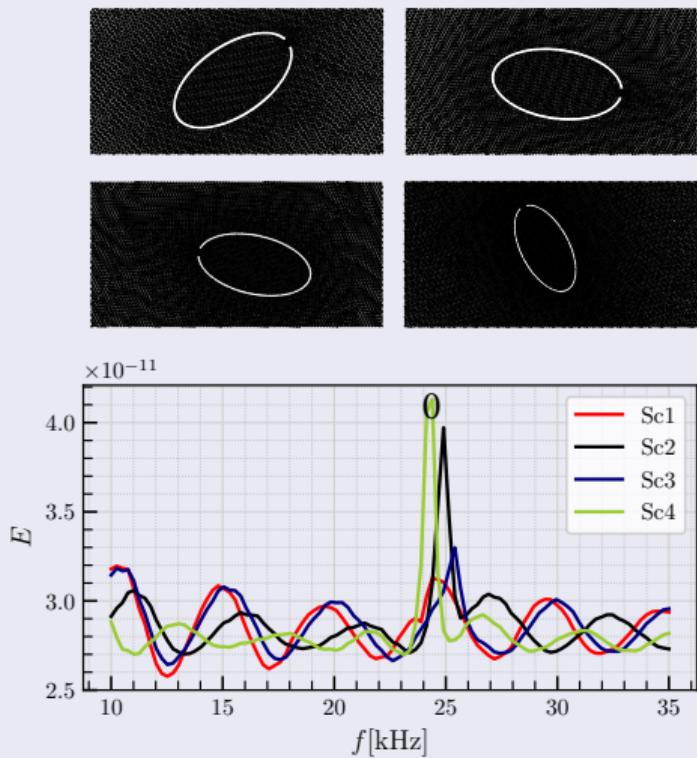
Scenarios of study

Case of study 1: One open rigid ellipse



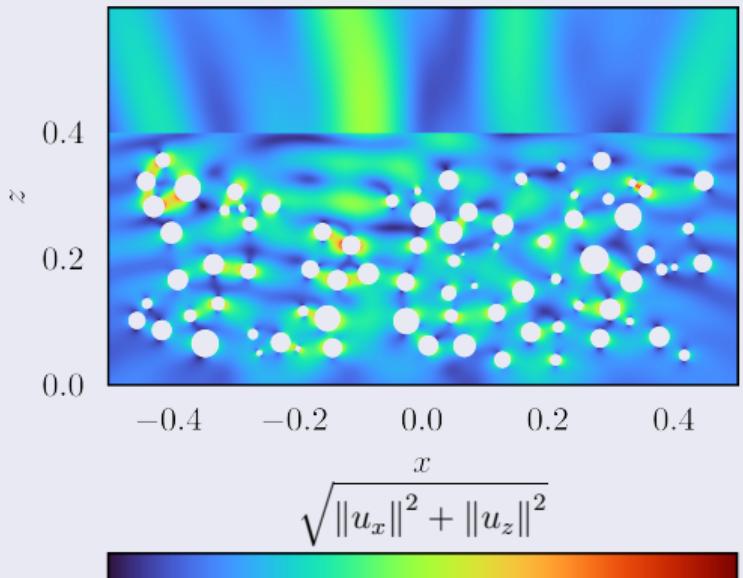
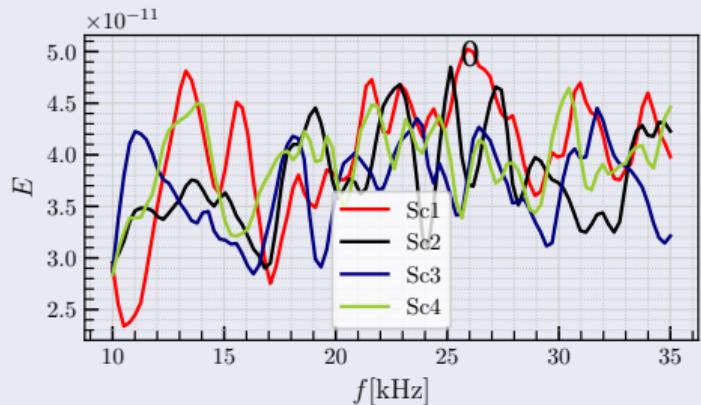
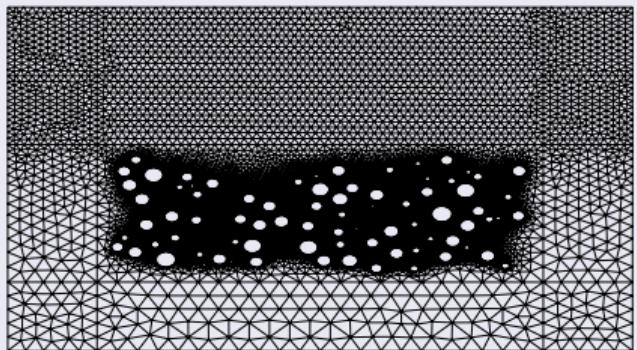
Scenarios of study

Case of study 1: One open rigid ellipse



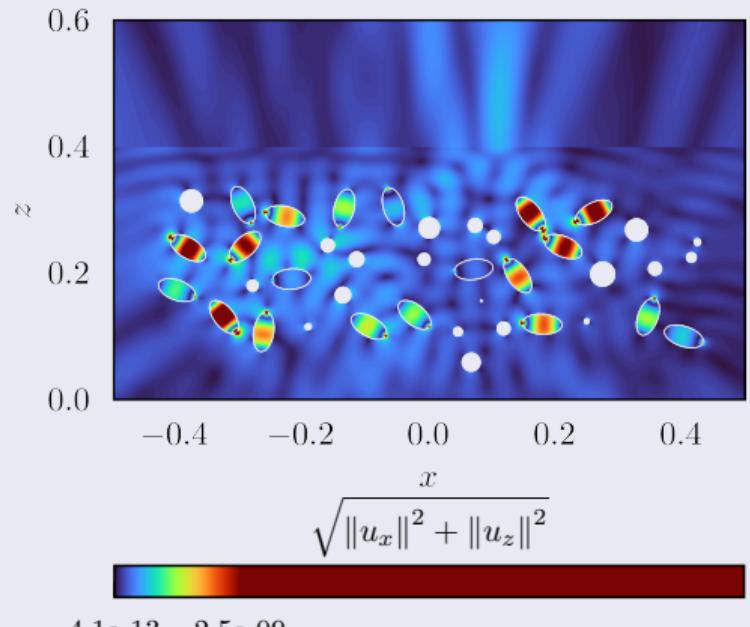
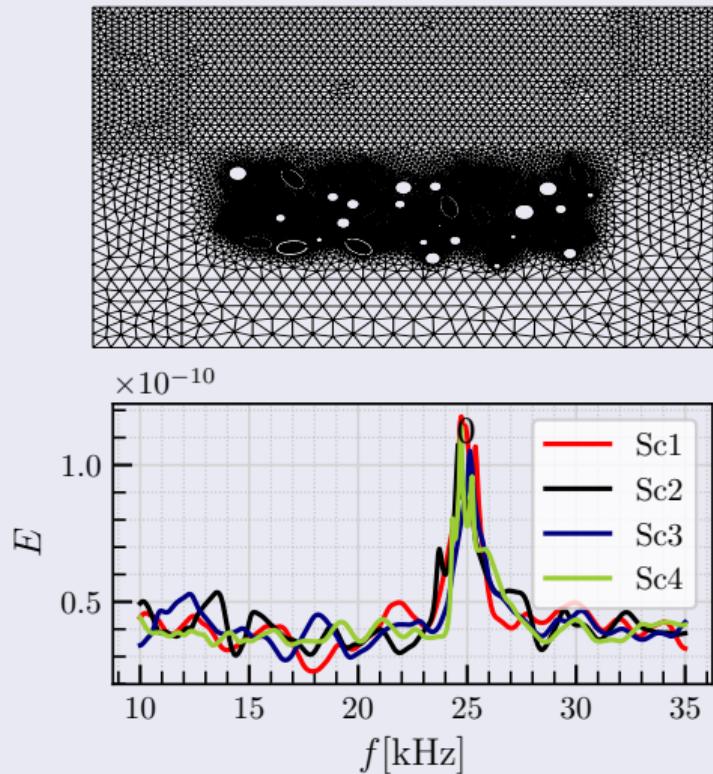
Scenarios of study

Case of study 2: Eighty rigid circles



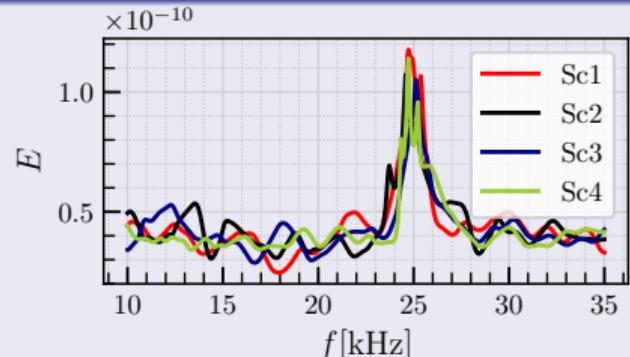
Scenarios of study

Case of study 3: Mixture of rigid circles and open rigid ellipses

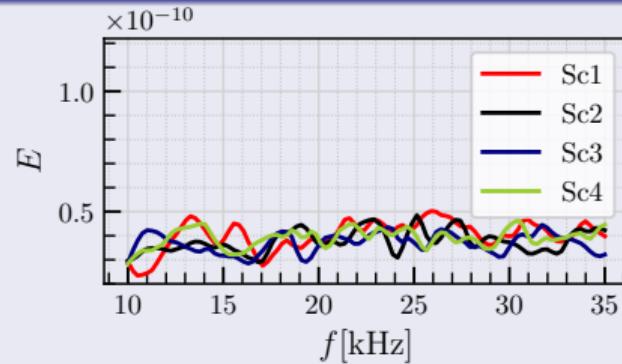


Scenarios of study

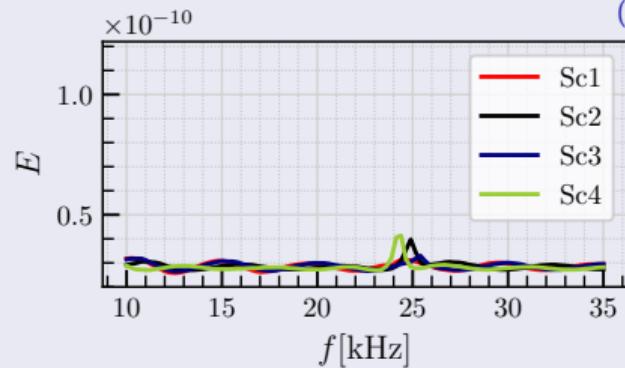
Comparison results of the three cases of study



(a) Mixture.



(b) Eighty rigid circles.



(c) Single open rigid ellipse.

Conclusions and future work

Conclusions

- A tool for generating scenarios was constructed.
- Frequency response functions that allow identification of different obstacles were obtained.

Future work

- Uncertainty quantification for a variety of scenarios.
- Mathematical modelling of the seabed using the Biot-Stoll model.

The results presented in this work have been presented at the 9th European Congress on Computational Methods in Applied Sciences and Engineering (ECCOMAS 2024) held 05-06-2024 in Lisbon, Portugal, under the title: *Numerical Quantification of the Biological Presence Buried in Granular Sediments in Coastal Environments*.

